ELEMENTS

OF

PLANE AND SPHERICAL

TRIGONOMETRY,

WITH

ITS APPLICATIONS TO THE PRINCIPLES

OF

NAVIGATION AND NAUTICAL ASTRONOMY;

WITH THE

LOGARITHMIC AND TRIGONOMETRICAL TABLES.

BY J. R. YOUNG,

AUTHOR OF "THE ELEMENTS OF ANALYTICAL GEOMETRY," "ELEMENTS OF THE DIFFERENTIAL AND INTEGRAL CALCULUS," &c.

TO WHICH ARE ADDED

SOME ORIGINAL RESEARCHES IN

SPHERICAL GEOMETRY;

BY T. S. DAVIES, F.R.S.E., F.R.A.S., &c.

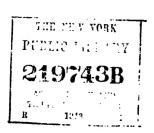
REVISED AND CORRECTED BY

J. D. WILLIAMS,

AUTHOR OF "KEY TO HUTTON'S MATHEMATICS," &c.

A NEW EDITION.

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TO

THE AMERICAN EDITION.

The extensive circulation and rapid sale which attended the republication, in this country, of Mr. Young's Treatise on Algebra, revised and corrected by Mr. Ward, the Elements of Geometry, by M. Floy, Jr., Analytical Geometry, by the Editor of the present Treatise, and also the Elements of the Differential and Integral Calculus, by Michael O'Shannessy, all of New-York,—together with the increasing demand for all his other Treatises upon the elements of abstract science, have induced me to attempt, by the publication of the present work, to place, as it were, the key-stone of the arch of Elementary Mathematics.

No further merit is claimed, in this edition, than that of a careful correction of all the errors occurring in the original and republished typography; as also of having altered the first part of the valuable Trigonometrical Tables connected with the work, so as to correspond with the improved plan, which was not adopted by the author, as will be seen by his preface, until after some few sheets were stereotyped, and consequently past all recall.

A consideration of the rapidly advancing state of analytical science amongst us, must be soul-reviving to every lover of his country:—And that her sons may continue daily to increase in a scientific knowledge of the mysterious principles hidden so long in the vast book of nature, is the fervent aspiration of one of Science's most humble votaries.

JOHN D. WILLIAMS.

NEW-YORK, 1833.

PREFACE.

It is the design of this treatise to establish the theory of Plane and Spherical Trigonometry analytically, and to present that theory, together with some of its most interesting and valuable applications, in a form

fitted for elementary instruction.

Of late years several analytical works on Trigonometry have been pubtished in this country; but, as they are confined almost entirely to the theory of the subject, it may be questioned whether, to many young students, they prove much else than so many collections of mere algebraical exercises. Yet a book upon so practical a subject as Trigonometry, ought undoubtedly to be something more than this, and ought not to be considered as complete when the various calculations which the science involves, and which its name implies, are wholly omitted.

The symbolical expression of a practical rule, in algebraic language, will often, to the young student, but indistinctly point out the numerical operation. Those much occupied in mathematical instruction, know full well that a learner may readily yield his assent to every stop of an algebraic process, be fully satisfied as to the truth of the result to which it leads, may even clearly see a valuable truth involved in it, and may yet be very far from perceiving how to turn it to account in any case of actual calculation. Indeed, algebraical formulas, transform them as we will, cannot always be made to indicate the best mode of arithmetical arrangement; and yet much, as regards facility of operation, depends upon this arrangement in many parts of practical mathematics, but especially in Trigonometry.

In the present volume, therefore, both the theory and the practice of the science have been introduced, every particular formula being illustrated by examples of the numerical calculation, arranged in the proper form. This plan of combining practice with theory, in works like the present, was always adopted by the earlier English writers, and it is to be regretted that recent authors have, in their admiration of foreign methods, departed so widely, in this respect, from the example of their predecessors, dwelling so much as they do upon the symbols, and so little upon the things signified. In addition to the practical illustration of formulas, a distinct part of the

In addition to the practical illustration of formulas, a distinct part of the work is devoted to the principles of Navigation and Nautical Astronomy, in which will be found a very short and convenient method of clearing the Lunar Distance, for the purpose of ascertaining the Longitude at Sea. This method is probably new, although, as the analytical expression for it occurs during the investigation of the well-known formula of Borda, it is equally

probable that it has been noticed before.

The supplement appended to the treatise is from the pen of my valued and accomplished friend, T. S. Davies, Esq. Fellow of the Royal Society of Edinburgh, and of the Royal Astronomical Society of London. It will be found to contain several new and interesting researches, which cannot fail to prove acceptable both to the inquiring student and to the more advanced analyst.

J. R. YOUNG.

January 1, 1833.

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PART I.

ELEMENTS OF PLANE TRIGONOMETRY.

CHAPTER I.

EXPLANATION OF THE TRIGONOMETRICAL LINES.

(Article 1.) Plane Trigonometry is that branch of pure mathematics of which the primary object is to determine the several parts of a

plane triangle from having certain other dependent parts given.

By the parts of a plane triangle we mean these six things, viz. the three sides and the three angles, and if any three of these six be given, provided only that a side be among them, the other three may always be determined either by geometrical construction, as shown in the Elements of Geometry, or by numerical computation, as will be seen hereafter.

From the foregoing definition it appears that quantities of two kinds, perfectly distinct from each other and admitting of no comparison, are

concerned in Trigonometry, viz. straight lines and angles.

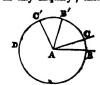
By means of certain happy contrivances, however, the whole business of trigonometry, and, indeed, the general theory of angular magnitude is conducted by help of linear quantities only; the angles themselves not entering into the computations, but certain straight lines dependent upon them and serving as indexes to them.

(2.) Before we explain the nature of these trigonometrical lines, it will

oe necessary first to show how angular magnitude is measured.

In order to this we must remark that when straight lines are submitted to calculation, all those which are concerned in the same inquiry must be measured in reference to one common standard of measure, called the linear unit; the choice of which unit is, however, arbitrary. Thus if we estimate any one of the lines concerned in any inquiry in feet, all must be estimated in feet, and the linear unit adopted will be a foot, which is represented by the numeral unit 1. Also if one of the lines is measured in yards all must be measured in yards, the linear unit being then a yard, which, as before, is represented in the calculation by the numeral unit 1. As far as the accurate representation of the lines are concerned, it is obviously a matter of indifference what length be assumed for the linear unit far the linear unit. sumed for the linear unit, for the length of any line will always be expressed numerically by that number which denotes the units it contains, but, for the purpose of facilitating computation, some scales of measure are often preferable to others.

(3.) Let now BAC be any angle concerned in any inquiry; then having chosen the linear unit AB, describe the circumference BCD about the centre A. The arc BC may be taken for the measure or representative of the angular magnitude CAB: for let there be any other angle B' AC' about the same centre A; then we know, by Geometry, that the angle BAC is to the angle BAC as the intercepted arc BC to the intercepted arc



B'C', (Geometry, p. 103); hence, as the intercepted arcs always vary as

the angles, the former may, obviously, be taken to represent the latter.

It is usual to consider the circumference of every circle to consist of 360 equal parts, called degrees of that circle; an arc consisting of any number of these, 24 for instance, is called an arc of 24 degrees, and represented for brevity thus, 24°; moreover each degree is supposed to consist of 60 equal parts, called minutes, and each minute of 60 equal parts called seconds. To express any number of minutes, we mark one accent over the number, and to express seconds we mark two; thus, 24° 16' 26", is 24 degrees 16 minutes 26 seconds. What we say of circular arcs applies equally to the angles which they measure, so that we call that an angle of 20° whose sides include an arc of 20° or the eighteenth part of a whole circumference.

Let us now speak of the trigonometrical lines before adverted to, and which are introduced for the purpose of reducing the entire theory of angular magnitude to the investigation of linear quantities only; we must, first, however, mention one or two further particulars respecting

the arcs to which these lines refer.

(4.) The arc CD which must be added to BC to make up a quadrant, or 90° is called the complement of the arc BC; and every arc will have a complement, even those which are themselves greater than 90°, provided we consider the arcs measured in the direction BCD, &c. as positive, and those measured in the opposite direction as negative; thus the complement CD of the arc BC commences at C where BC terminates, and may be considered as generated by the motion of C, the extremity of the radius AC, in the direction CD; but the complement ClD of the arc BC1, commencing in like manner at the extremity C1 of the proposed arc, must be generated by the motion of C₁ in the opposite direction, and the angular magnitude BAC₁, will here be diminished by

the motion of AC1, in generating the complement; the complement of BAC1, or of the arc BC1, is, therefore, with propriety considered as negative. Calling the arc BC, or BC₁, ω , the complement will be 90° — ω ; thus the complement of 24° 16' 4" is 65° 43' 56', and the complement of 120° 36' 10' is -30° 36 10°.



The arc CB1, which must be added to BC to make up a semicircle, or 180°, is called the *supplement* of the arc BC. If the arc is greater than 180°, as the arc BC2, its supplement C_2 B_1 measured in the reverse direction is negative. The expression for the supplement of any arc or angle ω is, therefore, $180^\circ - \omega$; thus the supplement of 110° 30° 20″ is 69° 29′ 40″, and the supplement of 200° 25′ is -

In the same manner as the complementary and supplementary arcs are considered as positive or negative, according to the direction in which they are measured, so are the arcs themselves positive or negative; thus, still taking B for the commencement of the arcs, as BC is positive BCs will be negative. In the doctrine of triangles we consider only positive angles or arcs, and the magnitudes of these are comprised between $\omega=0$ and $\omega=180^\circ$; but in the general theory of angular quantity, we consider both positive and negative angles, according as they are situated above or below the fixed line AB from which they are measured, as the angles CAB, C₃AB; moreover, an angle may consist of any number of degrees whatever, thus if the revolving line AC set out from the fixed line AB and make n revolutions, and a part the angular magnitude generated is measured by n times 360°, plus the degrees in the additional part.

Of the Sine.

(5.) The sine of an arc or of the angle which it measures, is the perpendicular, from one extremity of the arc, upon the diameter passing through the other extremity: thus CS is the sine of the arc BC; C₁ S₁ is the sine of the arc BC₁; C₂ S₂ is the sine of the arc BC2; C3 S3 the sine of the arc BC2, &c. If the proposed arc were a quadrant, or 90° the sine DA would be equal to the radius, and, therefore, its numerical value would be 1; the same would be the case if the arc consisted of



three quadrants, or 270°, or indeed of any odd number of quadrants; for all other arcs the numerical value of the sine will be a proper frac-tion or decimal. These, it must be observed, are the trigonometrical values of the sines, which are estimated according to the scale AB = 1; but it should be remarked that when we know the value of the sine of an arc agreeably to this scale, its value agreeably to any other scale is at once obtained by proportion; thus let R be any value assumed for the radius, and let us write the sine corresponding in capitals, MNE; then 1: sine :: R: Sine = $R \times \sin e$, so that the sine of an arc, corresponding to any assumed radius, is found by multiplying its trigonometrical sine by that radius; and, on the contrary, the sine according to any value of the radius being known, the trigonometrical sine is found by dividing it by that radius; the number, in fact, which expresses the trigonometrical sine being the ratio of the geometrical line stelf to the radius, whatever this may be. What we have said of the sine will be easily seen to apply to the other trigonometrical lines. As with the arcs so with the sines; those which lie in opposite directions take opposite signs, those above the fixed line B1 B being regarded as positive, and those below as negative; so that the sines in the first and second quadrants are positive, those in the third and fourth negative, while in the fifth and sixth they are again positive, and so on.

Every arc or angle has the same sine as its supplement; thus if B₁ C₁ is equal to BC it is obvious that BC₁ will be the supplement of BC, and the sine CS of the latter must be equal to the sine C1 S1 of the former.

Of the Cosine.

(6.) The cosine of an arc or angle is the sine of its complement: thus the cosine of the arc BC is the line Cs, which is, obviously, the sine of the arc DC, the complement

of BC. As the several sines are arranged on opposite sides of the diameter B1 B, so the cosines are arranged on opposite sides of the diameter DD₁; those on the right of DD₁ being regarded as positive, and those opposite as negative; hence in the first quadrant, the cosines are positive, in the second negative, in the third negative, in the



fourth positive, and so on; the cosine of an arc is equal to the cosine

of its supplement, but has a different sign.

When the arc is 0 the sine is 0, but the cosine BA is 1; when the arc is 90, the sine DA is 1, but the cosine is 0; when the arc is 180° the sine is 0, but the cosine is B₁ A = -1; when the arc is 270° the sine D₁ A is -1, but the cosine is 0; and when the arc is 360° the sine is 0, and the cosine 1, as at first, and so on.

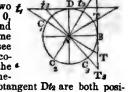
It is plain that the cosine of an arc is always equal to that part of the radius which is intercepted between the sine of that arc and the centre.

Thus referring to the figure in (5) AS is equal to the cosine of BC, and AS₂ to the cosine of BC₁C₂, or of BC₂C₂.

Of the Tangent, Cotangent, Secant, and Cosecant.

(7.) The tangent of an arc, and, therefore, of the angle which it measures, is a line drawn from one extremity of the arc, touching it at that extremity, and terminating in the diameter produced, drawn through the other extremity: thus BT is the tangent of the arc BC.

The cotangent is the tangent of the complement: thus Dt is the cotangent of the arc BC. It is easy to trace the changes which these two t, lines undergo as the arc BC increases from 0, for which value the tangent is obviously 0, and the cotangent infinite. Observing the same rules here as for the sine and cosine, we see that in the first quadrant the tangent and cotangent are both positive, in the second the tangent BT and cotangent Dt are both ne-



gative; in the third the tangent BT₂ and cotangent Dt₂ are both positive; and in the fourth the tangent BT₃ and cotangent Dt₃ are both negative, and so on; but as we shall soon see, the signs of the tangent and cotangent may always be at once inferred from those of the sine and cosine.

The secant of an arc is that portion of the prolonged diameter limiting the tangent, which is included between the centre and tangent; and the essecant is the secant of the complement. Thus in the last

figure AT is the secant of the arc BC, and At the cosecant.

In the four trigonometrical lines, sine, cosine, tangent and cotangent, we have seen that each is posited in one or other of two directly opposite directions, and that, therefore, one or other of the opposite signs + and —, prefixed to the numerical value of any such line, served to point out the proper direction for any particular value of the arc or angle. But as the secant and cosecant continually vary in direction, as well as in magnitude with the arc or angle, the geometrical position of either of these lines does not so clearly indicate to us the sign with which it should be represented. The proper sign, however, is always readily ascertained from knowing the signs of the sine and cosine, for upon these two lines all the others depend, as we shall shortly show.

(8.) Besides the six trigonometrical lines now defined there are three others, sometimes, although but seldom, employed; these are the versed sine or sagitta, the coversed sine, and the suversed sine. The versed sine of an arc BC (see fig. to art. 5) is the line BS between the commencement of the arc and the sine; it is always equal to the radius minus, the cosine, and, therefore, is always positive. The coversed sine is the versed sine of the complement, so that the coversed sine of BC is Ds (see fig. to art. 6;) also the suversed sine is the versed sine of the supplement. As the versed sine of any arc must be positive, it follows that the coversed sine and suversed sine must always be positive.

(9.) The following is the way in which the trigonometrical lines, connected with any arc or angle ω, are expressed in computation;

The sine	of ω	is expressed	thus,	sin.	ω
cosine			. (cos.	ω
tangent	of w		, 1	tan.	ω
cotangent	of w		. (cot.	•
secant	of ω			sec.	ω
cosecant	of w			COS.	ω

versed sine of ω vers. & coversed sine of w covers. w suversed sine of w suvers. w

From knowing the numerical value of any one of these lines, those of all the others may be obtained; thus, let the sine be given, then since the radius sine and cosine always form a right-angle triangle, of which the hypotenuse is the radius = 1, (see the fig. in art. 5,) we have

cos. $\omega = \sqrt{1 - \sin^2 \omega}$. Again, since the triangle formed by the radius, sine, and cosine, is always similar to that formed by the secant, tangent, and radius, and to that formed by the cosecant, radius, and cotan-gent, as the student will at once see by sketching these lines for any arc, it follows, from the proportionality of the sides of similar triangles, that

$$\tan \omega = \frac{\sin \omega}{\cos \omega}, \quad \cot \omega = \frac{\cos \omega}{\sin \omega} = \frac{1}{\tan \omega}$$

$$\sec \omega = \frac{1}{\cos \omega}, \csc \omega = \frac{1}{\sin \omega} = \frac{1}{1 + \cot \omega}$$

and, from these expressions, we at once see that the signs of the several lines, as well as their numerical values, are deducible from those of the Sine and cosine.

Now the numerical expression for sin. ω , for all values of ω , from $\omega = 0$ to $\omega = 90^{\circ}$, (between which limits every possible value is comprised) are actually computed by methods to be hereafter explained, and thence the values of the other trigonometrical lines are deduced. These values are then arranged as in table in, at the end, and form a table of natural sines, cosines, &c. By help of such a table we may readily find the values of the same lines, computed to any other radius R; for as observed at (5) we shall merely have to multiply the tabular value by R. Writing; therefore, for distinction sake, the words sin., cos., &c. in capitals, when the value of the radius is other than unity, the foregoing equations are the same as $\frac{\text{TAN.}\,\omega}{R} = \frac{\text{SIN.}\,\omega}{\text{COS.}\,\omega}$, $\frac{\text{COT.}\,\omega}{R} = \frac{R}{\text{TAN.}\,\omega}$

equations are the same as
$$\frac{\text{TAN.}\,\omega}{R} = \frac{\text{SIN.}\,\omega}{\text{COS.}\,\omega}$$
, $\frac{\text{COT.}\,\omega}{R} = \frac{R}{\text{TAN.}\,\omega}$, $\frac{\text{SEC.}\,\omega}{R} = \frac{R}{\text{COS.}\,\omega}$, $\frac{\text{COSEC.}\,\omega}{R} = \frac{R}{\text{SIN.}\,\omega}$; and thus by substituting in any trigonometrical formula $\frac{\text{SIN.}\,\omega}{R}$, $\frac{\text{COS.}\,\omega}{R}$

&c. for sin. ω , cos. ω , &c. the formula will become generalized so as to hold good for any value of the radius whatever.

(10.) It is obvious that when any trigonometrical formula is thus generalized every term in it will be the same abstract number as in the original formula; whatever powers or roots of the lines enter the formula they will always be divided by the same powers or roots of the radius R. The denominators will all be removed by multiplying each term by the highest power of R which enters, and the result will necessarily be a homogeneous expression; that is, every term will have the same dimensions, or will involve as factors the same number of lines. Hence, in order to generalize any trigonometrical formula, or to render it independent of any particular value of R, it will be necessary merely to introduce into the several terms such powers of R as will render them all of the same dimension. For example, the following

 $\sin_{-1}(A+B) = \sin_{-1}A \cos_{-1}B + \sin_{-1}B \cos_{-1}A;$ in which the term on the left is of one dimension, and the terms on the right are each of two dimensions, will become homogeneous by introducing the factor R into the left hand member, so that when this is the

value of the radius instead of unity, the formula will be

B:3:08 Cx 7 = 5 12

 $R \sin. (A+B) = \sin A \cos. B + \sin. B \cos. A$; each term being the product of two lines.

In like manner the formula $\cos 4 A = 8 \cos^4 A - 8 \cos^2 A + 1$, becomes when the radius is R instead of unity

 $R^3 \cos 4 A = 8 \cos^4 A - 8 R^2 \cos^2 A + R^4$; the powers of R being introduced so as to render each term of four dimensions.

From the preceding definitions and remarks the following simple

properties are immediately deducible, viz.

 The sine of an arc is equal to half the chord of twice that arc.
 The chord of 60° being equal to the radius (Geom. p. 122), therefore, the sine of 30°, or the cosine of 60°, is equal to half the radius.

3. Hence, from the expression for the secant at the top of the preceding page, the secant of 60° is equal to the diameter of the circle.

4. The tangent of 45° is equal to the cotangent, and, therefore, to

the radius, (see fig. to art. 7.)
(11.) We shall terminate this introductory chapter with a table exhibiting the correlative values of the trigonometrical lines, situated in different quadrants; it is readily constructed from the values of the sine and cosine, by help of the relations in (9), bearing in mind that an arc and its supplement have the same sine.

Table of the Correlative Values of the Trigonometrical Lines.

arc.	sin.	cos.	tan.	cot.	sec.	cosec.
00	0	1	0	œ	1	œ
ω	+ sin. ω	+ cos. ω	+ tan. ω	+cot. ω	+ sec. ω	+cosec. ω
900	1	0	œ	0	œ	1
90∘ + ω	+cos. ω	— sin. ω	— cot. ω	—tan. ω	— cosec. ω	+ sec. w
180°	0	- 1	0	— œ	- 1	- ∞
180° + ω	— sin. ω	— cos. ω	+tan. ω	+cot. ω	— sec. ω	— cosec. ω
270°	- 1	0	œ	0	— ∞	- 1
270° + ω	— cos. ω	+sin. ω	— cot. ω	— tan. ω	+ cosec. ω	— sec. ω
360°	0	1	0	00	1	œ

This last line is the same as the first; and any line will, obviously, remain unaltered if we add to the corresponding arc a whole circumference or any number of circumferences. If we take ω negatively, we may extend the table as follows:

trical lines would obviously recur as before. It is obvious that the cosine of a negative arc, whether less or greater than a quadrant, is the same as the cosine of the same arc, taken positively; but the sine of a negative arc, although the same in magnitude as that of an equal positive arc, has an opposite sign: hence, by the equations at (9), the sine, tangent, cotangent, and cosecant, will have opposite signs to those of the same arc taken positively; but the cosine

and secant will have the same signs.

CHAPTER II.

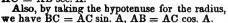
FORMULAS AND RULES FOR THE SOLUTION OF PLANE TRIANGLES.

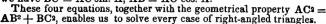
(12.) We shall now proceed to investigate rules for the solution of all the cases of plane triangles.

Right-angled triangles.

As right-angled triangles are those whose several parts are the most easily determined we shall consider them first.

Let ABC be any right-angled plane triangle, and with AB as a radius describe the arc Ba. If AB were unity BC would be the tangent, and AC the secant of the angle A; as it is, however, these lines are equal to AB times the trigonometrical tangent and secant (5), that is, BC = AB tan A, $\mathbf{AC} = \mathbf{AB} \sec \mathbf{A}$.





(13.) In applying these formulas, it must be remembered that the trigonometrical lines which they involve are according to the scale of radius = 1; they are computed and registered in the tables of natural sines and tangents. The tables of logarithmic-sines and tangents are not, however, computed to this radius, on account of the inconvenience which would attend the continual use of negative indices in all the sines and cosines; but they are computed to a radius of 1010. Hence, in all formulas of trigonometry, intended for logarithmic computation, the radius R must always be introduced, so as to make the terms homogeneous; and, although in the formulas which will be hereafter given, we shall but seldom encumber the expressions by actually inserting in them R, and its powers, yet the computist must not fail to take account of them in the logarithmic process.

Introducing R into the foregoing equations we may write them thus:

$$\frac{\mathbf{R}}{\mathbf{A}\mathbf{B}} = \frac{\tan \mathbf{A}}{\mathbf{B}\mathbf{C}}, \quad \frac{\mathbf{R}}{\mathbf{A}\mathbf{B}} = \frac{\sec \mathbf{A}}{\mathbf{A}\mathbf{C}}; \quad \frac{\mathbf{R}}{\mathbf{A}\mathbf{C}} = \frac{\sin \mathbf{A}}{\mathbf{B}\mathbf{C}}, \quad \frac{\mathbf{R}}{\mathbf{A}\mathbf{C}} = \frac{\cos \mathbf{A}}{\mathbf{A}\mathbf{B}}$$

and all these equations may be comprehended in a single rule expressed as below. As the tabular radius

: the radius in the figure

:: any tabular line

: the corresponding line in the figure;

and from this it immediately follows that

Any tabular line

: corresponding line in the figure,

:: any other tabular line

: corresponding line in the figure;

which proportion, obviously, comprehends the former.

It appears from this rule that when we want to find a side, we must begin the proportion with a given tabular line, that is, either with the tabular radius, of which the logarithm is 10, or else with the tabular sine, cosine, &c. of a given angle; but when we want to find an angle then we must invert this proportion, beginning with a given side which must be made the geometrical radius, as no other tabular line but the radius will be given, seeing that angles are in this case unknown.

(14.) In operating with logarithms, the logarithm of the first term of

the proportion must be subtracted from the sum of the logs. of the other two, to obtain the logarithm of the sought fourth term; and thus the logarithmic process will consist of five lines or rows of figures. If, however, the first term, or that to be subtracted were 10, we might save a line, by adding the two other logs. together, and rejecting 10 in the index; when the first term is not 10 we may still save a line by the following artifice, viz. instead of putting down for the first term the log. given by the table, put down its deficiency from the number 10, which may be done with as much readiness as transcribing the number itself, provided we begin at the left-hand figure and subtract each in succession from 9, till we come to the last significant figure, which must be taken from 10; we shall thus have instead of the logarithm, what is called its arithmetical complement, which, being added in with the other two terms, rejecting 10 from the index, must give the same result as if we had subtracted the log. of the first term from the sum of the other two. An example or two will fully illustrate what has now been said.

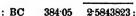
EXAMPLES.

(15.) 1. Given the angles and the base to find the perpendicular and hypotenuse, viz. $A = 53^{\circ} \otimes$, AB = 288.

1. To find the Perpendicular BC.

As a side is here required, we must begin with a tabular line; we shall choose for simplicity the tabular radius, to save a reference to the table, as we know the log. of this to be 10. Taking then the known line AB for radius in the figure, we have

Rad. . . 10 : AB 288 2:4593925 :: tan. A 53° 8 10:1249898



BC might have been found by making any other side radius, although not quite so easily, as we should then have had to seek out in the table the tabular line for the first term, corresponding to the known line AB; thus if AC had been made radius, then the tabular line we should have commenced with, would have been that corresponding to AB, viz. the cosine of the angle A. If CB had been made radius we should have commenced with the cotangent of A, that is, the tangent of C, for such would be the tabular lines corresponding to BA.

II. To find the Hypotenuse AC.

Preserving the same radius we have,

Rad. . . . 10 : AB 288 24593925 :: sec. A 53° 9 10-2218814 : AC 480-036 2-6812739,

If we had made AC radius, the proportion would have been cos. A: AB:: rad.: AC. By way of showing the use of the arithmetical complement, let us determine AC by this proportion

cos. A		arit	h. c	omp.	0.2218814
: AB	288	•	•	•	2.4593925
:: Rad.	•	•	•	•	10
: AC	480-036				2.6812739

Given the two perpendicular sides to find the hypotenuse and angles, viz. AB = 472, BC = 765, (see last fig.)

I. To find the Angle A.

We must here, agreeably to the rule, begin with a given side, say AB, which we shall make radius.

AB	472 arith. com	
: Rad. :: BC	765 .	10 2 [.] 8836614
: tan. A	* 58° 19' 32"	10-2097194

II. To find the Hypotenuse.

Here we must begin with a tabular line; we shall choose the radius

	AB	472	2·6739420
	sec. A	58° 19' 32'	10·2797645
:	AC	898.89	2.9537065.

Or without employing the angle A we may determine AC by the formula. $AC = \sqrt{AB^2 + BC^2}$.

3. Given two sides and the included angle of an isosceles triangle ABC to find the other parts

AC = BC = 288, ACB = 78° 12.

Let the perpendicular CD be drawn, then since it will bisect the angle C, we shall have given in the right-angled triangle

ADC, AC = 288, ACD = 30° 6 \therefore A = 90° — 39° 6 = 50° 54; hence to find AD, we have have the since it and according to the since it is a s

by making AC radius.



Rad. : AC :: cos. A	288 50° 54⁄	10 2.4593925 9·7998062
: AD	181-635	2-2591987

AB = 363.270.

- 4. Given the base AB = 53.42, and the perpendicular BC 75.18, to
- 4. Given the base AB = 35 22, and the perpendicular BC 15 16, to find the hypotenuse and angles?

 A = 54° 36° 14° , C = 35° 23° 46° , AC = 72° 23.

 5. Given the hypotenuse AC = 643° 7, and the base AB = 473° 8 to find the other parts? A = 42° 36 12° , C = 47° 23° 48° , BC = 35° 87.

 6. Given the angle A = 37° 29° 43° , and the hypotenuse AC = 173° 2 to find the other parts? C = 52° 57° 17° , AB 138° 24, BC = 104° 34.

 (16.) We shall now proceed to investigate rules and formulas for
- the solution of triangles in general.

Oblique-Angled Triangles.

Let ABC be any plane triangle, and let us denote the angles by the capital letters A, B, C, at their vertices, and the sides opposite to them by the small letters a, b, c.

From either vertex, as C, draw the perpendicular CD to the opposite side.

Then the sine of A to the radius b will, obviously, be the line C D, and the value of this sine in terms of the trigonometrical sine of the same angle to radius 1 is (art A



For the method of determining the angle corresponding to any tabular number to seconds, see the introductory explanation prefixed to the tables.

5.) $CD = b \sin A$. In like manager the sine of B to the radius a, is the same line CD, whose value, the same in term of the trigonometrical sine, is CD = a sin. B; consequently, by equating these two values of CD, we have $a \sin B = b \sin A$

 $\therefore \frac{a}{b} = \frac{\sin. A}{\sin. B}.$ This equation immediately furnishes us with an im-

portant rule, which may be expressed as follows.

Any side of a triangle is to any other side as the sine of the angle, opposite to the former, is to the sine of the angle opposite to the latter.

Whenever, therefore, we know two sides and an angle opposite to one of them, or two angles and a side opposite to one of them, the other three parts of the triangle may always be determined by help of this rule.

The cosine of A, to the radius b, is the line AD; and, therefore, AD, in terms of the trigonometrical cosine of A, is AD = b cos. A. In like manner the cosine of B to the radius BC, is BD, which, in terms of the trigonometrical cosine, is $BD = a \cos B$; if the angle B is obtuse, as in the second of the above diagrams, cos. B will be negative; hence whether it be acute or obtuse we shall have for the side AB the expression $c = a \cos B + b \cos A$; in which the proper signs of the cosines are supposed to be involved in their expressions.

If instead of drawing the perpendicular from C we had drawn it from B, it is easy to see the result we should have obtained; for then considering B the vertical angle instead of C, or supposing the triangle to be turned about till B actually becomes the vertical angle, then commencing at the vertex, the arrangement of the angles will now be B, C, A;

these, therefore, should respectively be substituted for C, A, B, in the above formula; also the arrangement of the sides will be a, b, c, instead of b, c, a, as at first, so that these letters must be replaced by the former: consequently, our equation will become $b = c \cos A + a \cos C$.

If, on the contrary, A be made the vertical angle, then the order of the angles will be A, B, C, and of the sides c, a, b, and these must supply the places, of C, A, B, and b, c, a, in the first formula, so that we shall then have $a = b \cos C + c \cos B$. Collecting these equations together we have,

 $a = b \cos C + c \cos B$ $b = c \cos A + a \cos C$ $c = a \cos B + b \cos A$

and these equations contain the whole theory of plane trigonometry. They involve all the six parts of a triangle, the three angles, and the three sides; and, as the equations are three in number, any three of the parts, considered as unknown quantities, may be determined, provided only the other three are known; but fewer than three being given will not be sufficient to determine the others, as then there would be a greater number of unknowns than of equations.

We must remark too that the three given quantities must not be the three angles simply, because the three other quantities a, b, c, severally enter the three terms of each equation, so that if we were to multiply each equation, by any assumed factor whatever, m, the values resulting from the elimination of A, B, C, would, obviously, be the same for ma, mb, mc, as for a, b, c; thus, showing that the data are not sufficient to determine any triangle, but belong equally to innumerable triangles, all, however, similar to each other.

(17.) It appears then that the solutions to all the cases of plane triangles are derivable from the equations (1), under different hypotheses, as to the three unknown quantities, and we might now with but little trouble proceed to deduce these solutions, one after another, from these equations: thus suppose the three sides a, b, c, were given, then multiply the first equation by a, the second by b, and the third by c, we $a^2 = ab \cos C + ac \cos B$

 $b^2 = bc \cos A$ and $a \cos C$ $c^2 = ac \cos B$ $c \cos A$;

and subtracting each of these from the sum of the other two, we get

$$b + c - a^{2} = 2bc \cos A \cdot \cos A = \frac{b^{2} + c^{2} - a^{2}}{2bc}$$

$$c^{2} + c^{2} - b^{2} = 2ac \cos B \cdot \cos B = \frac{a^{2} + c^{2} - b^{2}}{2ac}$$

$$c^{3} + b^{2} - c^{2} = 2ab \cos C \cdot \cos C = \frac{a^{2} + b^{2} - c^{2}}{2ab}$$

and thus the values of the cosines of the required angles become known, and by searching in the table of natural sines and cosines we shall find

the angles to which they belong.

It is necessary to remark here that in almost every trigonometrical calculation it is advisable to conduct the operation by means of logarithms, in order to avoid lengthy and tiresome multiplications, divisions, and extractions; so that it becomes a matter of consequence to express all our general rules and formulas in a form, adapted as much as possible to logarithmic calculation, that is, the operations indicated by the formulas should be those of multiplication, division, involution, and evolution, and not those of addition and subtraction.

The formulas just deduced for the angles of a triangle, when the sides are given, do not appear in a form adapted to logarithmic computation; and the same would be found to be the case with the various other formulas directly deducible from the general equations (1); nor would it be easy, without the aid of other and independent properties, to convert these expressions into the desired form. Although, therefore, it is true, as we have stated above, that formulas for all the cases of plane trigonometry may be deduced from the equations (1), yet, on account of the inconvenient form these formulas assume, it becomes necessary for us to seek assistance from other sources. Now there exist two general trigonometrical formulas, which may be considered as forming the foundation of the whole theory of angular magnitude, and which, in conjunction with what is laid down above, will enable us to deduce formulas suited to logarithmic calculation for all the cases of plane triangles.

(18.) There are various ways of investigating these formulas; we shall adopt that which appears to us the most simple and general.

It was given by M. Sarrus in the Annales des Mathematiques, tom. xi.

Given the sines and cosines of two arcs or angles, to find the sine and cosine of their sum and difference.

Let AM = a, and AN = a', be any two arcs of the circle, the radius being unity, then drawing the chord of the arc NM = a - a', we shall

being unity, then drawing the chord of the arc NM = a - a', we shall have from the triangle NMG right angled at G. $MN^2 = NG^2 + MG^2 = (CQ - CP)^2 + (PM - NQ)^2$; which may

 $MN^2 = NG^2 + MG^2 = (CQ - CP)^2 + (PM - NQ)^2$; which may be written thus, $chd^2(a-a') = (cos. a' - cos. a)^2 + (sin. a - sin. a')^2$.

By actually squaring the expressions in the righthand member of this equation, and recollecting that $\sin 2 a + \cos 2 a = 1 \sin 2 a' + \cos 2 a' = 1$

 $\sin 2 a + \cos 2 a = 1$, $\sin 2 a + \cos 2 a = 1$, we have $\cot 2 (a - a) = 2 - 2 \cos a \cos a - 2 \sin a \sin a$. (1).

As this expression is true for any arc whatever, it is true for the arc a - d, so that $chd.^2(a - d) = 2 - 2cos.(a - d)...(2)$.

^{*} This property is also proved in the Geometry, p. 92, Scholium.

Comparing together the second members of (1) and (2) we obtain $\cos.(a-a')=\cos.a\cos.a'+a\sin.a'$ sin. a' (1). As this is true for all values a', a', it is true when a-a' is put for a', so that $\cos.a'=\cos.a\cos.(a-a')+\sin.a\sin.(a-a')$; in which equation, if we substitute the value of $\cos.(a-a')$ given by (1), we have cos. $a' = \cos a^2 \cos a' + \cos a \sin a \sin a' + \sin a \sin (a-a')$; from which, by putting for $\cos a$ its value $1 - \sin a$, we get

 $\sin (a - a') = \sin a \cos a' - \sin a' \cos a \dots$ (n). Lastly, putting (a + a') for a, in the equations (I) and (II), we have,

cos. $a = \cos$. $(a + a')\cos$. $a' + \sin$. $(a + a')\sin$. a'. \sin . $a = \sin$. $(a + a')\cos$. $a' - \cos$. $(a + a')\sin$. a'.

In order to obtain from these equations the expressions for $\sin (a + a)$, and $\cos (a + a)$, multiply the first by $\sin a$, the second by $\cos a$, and add, and we thus get, sin. $(a+a') = \sin a \cos a' + \sin a' \cos a$. (m).

Multiply the first by cos. a', the second by sin. a', and subtract, and we get cos. $(a + a') = \cos a \cos a' - \sin a \sin a' \dots (iv)$. The four general formulas thus deduced may be written as follows:

sin.
$$(a \pm a') = \sin a \cos a' \pm \sin a' \cos a$$

cos. $(a \pm a') = \cos a \cos a' \mp \sin a' \cos a'$
. . . (4).

(19.) The first of these immediately furnish the two following, viz.

 $\frac{\sin \cdot (a+a') + \sin \cdot (a-a')}{\sin \cdot (a+a') + \sin \cdot (a-a')} = \frac{2 \sin \cdot a \cos \cdot a'}{\sin \cdot a \cos \cdot a}; \text{ from which } \\
\frac{\sin \cdot (a+a') + \sin \cdot (a-a')}{\sin \cdot (a+a') + \sin \cdot (a-a')} = \frac{\sin \cdot a}{\cos \cdot a}. \qquad \frac{\cos \cdot a'}{\sin \cdot a} = \frac{\tan \cdot a}{\tan \cdot a'}$ $\frac{\cos \cdot a'}{\sin \cdot a'} = \frac{\tan \cdot a}{\tan \cdot a'} (art.8).$ If, therefore, we put

a+a'=A, a-a'=B $\therefore a=\frac{1}{2}(A+B)$, $a'=\frac{1}{2}(A-B)$, shall have $\sin A+\sin B$ $tan. \frac{1}{2}(A+B)$ Now we have

we shall have $\frac{1}{\sin A - \sin B} = \frac{1}{\tan A + \sin B}$ Now we have al-

ready seen that in any plane triangle sin. A: sin. B:: a:b... sin. A + sin. B: sin. A - sin. B:: a+b:a-b; sonsequently from the equation above a+b tan. $\frac{1}{2}$ (A.

consequently, from the equation above, $\frac{a-b}{a-b} = \frac{a-b}{\tan \frac{1}{a}(A-B)}$ $\tan A (A + B)$

that is to say, in any plane triangle the sum of any two sides is to their difference as the tangent of half the sum of the opposite angles is to the tan-

gent of half their difference.

By help of this rule we may determine the remaining parts of the triangle, when we know two sides a, b, and the included angle C; for knowing C we know also $\frac{1}{2}(A + B) = \frac{1}{2}(180^{\circ} - C)$; and $\frac{1}{2}(A - B)$ is determined by the rule; therefore, as the half sum added to the half difference of two quantities gives the greater, and subtracted gives the less; we thence readily obtain the angles A and B, and then the third side c, by (16.) We have thus deduced commodious rules fitted for logarithmic computation, for the solution of the first two cases of plane triangles: it remains to furnish a rule for the third case.

(20.) Referring to the expression for cos. A at (17), it is plain that since $b^2 + c^2 = (b + c)^3 - 2bc$, and therefore, $b^2 + c^2 - a^2 = (b + c + a)(b + c - a) - 2bc$; that expression may be put under the form cos. $A = \frac{(b + c + a)(b + c - a)}{2bc} - 1$.

Now supposing the arcs a, a', in equation (A), to be equal to each other, and to 1 A, we have from the second of them

 $\cos A = \cos A + \sin A$ $1 = \cos 2 A + \sin 2 A$ by addition, cos. $A = 2 \cos 4 A - 1$ by subtraction, cos. $A = 1 - 2 \sin A$;

by substituting the first of these values in the foregoing equation, and putting for brevity S for the sum of the three sides of the triangle, we have $\cos \frac{1}{4} A = \sqrt{\frac{1}{8} \frac{8(\frac{1}{4} S - a)}{1}}$

We can just as readily obtain a second formula by means of the other

we can just as readily obtain a second formula by means of the other expression for cos. A; for substituting it in equation (2), art. (17), we have $2 \sin 2 A = 1 - \frac{b^2 + c^2 - a^2}{2bc} = \frac{a^3 - b^2 - c^2 + 2bc}{2bc} = \frac{a^3 - (b - c)^2}{2bc} = \frac{(a + b - c)(a - b + c)}{2bc};$ consequently, $\sin A = \sqrt{\frac{(a - b)(a - b)}{bc}} \dots (2);$

$$= \frac{a^3 - (b-c)^2}{2bc} = \frac{(a+b-c)(a-b+c)}{2bc}$$

and by dividing this expression by the former we get a third formula, viz. $\tan \frac{1}{4} A = \sqrt{\frac{\frac{1}{4} S - b}{1} \frac{S(1 S - c)}{1}}$. (3). $\frac{1}{2}S(\frac{1}{2}S-a)$

(21.) We thus have three distinct formulas for the determination of the angles of a triangle when the three sides are given, and all of them are adapted to logarithmic computation. It is not, however, always a matter of indifference which of these formulas we employ, as in certain cases one may be prescrable to another. Thus, if we knew beforehand, or could foresee that the sought angle ! A would be very nearly equal to 90°, then it would be improper to employ the formula (2), because we should be very likely to commit error in taking out the angle, seeing that for an angle very near 90° the seven first decimals in the sine coincide with those in the sines of several other angles in its vicinity, or which differ each from the proposed angle by only a few seconds.

If the logarithmic tables, which we employ, are calculated to seconds, as the large tables, of Taylor or of Bagay, then the sought angle when near 90°, may be accurately determined to the nearest second, either from its cosine or from its tangent, as the values of these trigonometrical lines, at this part of the table differ considerably from each other, even when the arcs are nearly equal. But if the table employed is not calcu-- lated to seconds, then the sought angle, when near 90°, should be determined from its cosine, and not from its tangent; because in approaching to 90° the tangents increase by very unequal differences, and, as, in proportioning for the seconds, we proceed on the supposition that the tangents increase equally through 60", we shall be in danger of committing error in thus determining the seconds. As the cosines decrease more regularly towards the extremity of the quadrant than the tangents increase, it will, therefore, be safest to determine such arcs from their cosines.

When the sought angle is very small it will be best to determine it

from its sine; although the tangent may be used with safety.

Solution of Plane Triangles in general. (22.) We shall now proceed to apply the rules and formulas which we have just investigated to the several cases of plane triangles, repeating the rule at the head of each case.

CASE 1. When a side and its opposite angle are among the given parts.

RULE.—Sine of given angle, RULE 2. Also, any given side, : sine of its opposite angle : its opposite side

:: sine of any other angle :: any other side

: its opposite side. : sine of its opposite angle.

As the same sine belongs both to an angle and to its supplement, it may seem doubtful in determining an angle of a triangle from its sine, whether to take the acute angle given by the tables or the obtuse angle which is its supplement.

The following precepts will remove all doubt on this point.

If the given angle is obtuse the sought angle must be acute. This
is obvious, because a triangle cannot have two obtuse angles.

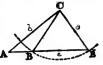
2. If the given angle be acute, and the side opposite to it greater than the side opposite to the sought angle, this must be acute; for the greater

angle must be opposite to the greater side.

3. But when the side opposite to the greater side.

3. But when the side opposite to the given angle is less than that opposite to the sought angle, this may be either acute or obtuse, so that two triangles exist under the proposed conditions, and the problem in question admits, therefore, of two solutions. The annexed diagram shows that with two given sides AC, CB, and the acute angle A, opposite to one of them, we may always constructive triangles ABC.

may always construct two triangles, ABC, ABC; where the angle B, opposite to the other given side in the one triangle, will be the supplement of the corresponding angle B' in the other, provided CB is less than CA.



EXAMPLES.

(23.) 1. In the triangle ABC are given AB=137, AC=153, $B=78^{\circ}13$, to find the remaining parts.

1. To find the Angle C.

As AC . : sin. B . :: AB .	153 78° 13 137	•	arith.	comp.	7·8153086 9·9907502 2·1367206
: sin. C	61° 13′ 4	71			9.9427794.

The obtuse angle, which is the supplement of this, is not admissible, because the side opposite to the given angle is greater than the side opposite the required one.

II. To find the side CB.

The angle A is equal to $180^{\circ} - (B+C) = 180^{\circ} - 139^{\circ} 26 47' =$ 40° 33' 13": therefore

As sin. B : AC :: sin. A	78° 13' 153 40° 33' 13'		arith.	comp.	0·0092498 2·1846914 9·8130198
: CB	101-617				2.0069610.

2. In the plane triangle ABC are given AC = 216, CB = 117, and $A = 22^{\circ} 37$, to find the rest.

1. To find the Angle B.

As BC : sin. A :: AC	117 22° 37 216 .		arith.	comp.	7·9318141 9·5849685 2·3344538
: sin. B	45° 13′ 55″ (or 134°	46' 5"		9.8512364

The angle B is, in this example, ambiguous, because the side opposite the given angle is less than that opposite the required one.

II. To find the third side AB.

The angle C is equal to $180^{\circ} - (A + B) = 112^{\circ} 9'5'$, provided we take B acute; therefore,

As sin. A : BC :: sin. C	22° 37' 117 112° 9'	5''		arith.	0·4150315 2·0681859 9·9667005
: AB	281			•	2·4499179

SCHOLIUM.

In each of the foregoing examples where two sides, and an angle opposite to one, are given, we have found it necessary to find the angle opposite to the other given side before we could apply the rule to the determination of the third side; so that the determination of this third side requires two proportions, and there is no logarithmic method which will lead us to it by a shorter process. It may, however, be deduced directly from the formula at (17), viz. cos. $A = \frac{b^2 + c^3 - a^2}{c^2}$

which gives $c = AB = b \cos A \pm \sqrt{a^2 - b^2 \sin^2 A}$; which expression is, however, not adapted to logarithmic computation. 3. In the plane triangle ABC are given

 $A = 44^{\circ} 13' 24''$, $B = 79^{\circ} 46' 38''$, AB = 368, to find the rest.

1. To find the side AC.

The angle C is equal to 180° — $(A + B) = 55^{\circ} 59' 58'$, therefore, As sin. C 55° 59' 58' arith. comp. 0.0814286 368 : AB 2.5658478 :: sin. B 79° 46' 38' 9.9930503 : AC 436.844 2.6403267

II. To find the side CB.

55° 59' 58" As sin. C arith. comp. 0.0814286 : AB 368 2.5658478 :: sin A 44° 13' 24" 9.8435174

: CB 309.595 2.4907938 4. In the plane triangle ABC are given AB = 408 yards, $A = 74^{\circ} 14$,

 $B = 49^{\circ} 23'$; to find the other two sides, C = 371.9 ye AC = 371.9 yards and BC = 486.02 yards. 5. In the plane triangle ABC are given AB = 408 yards, $A = 58^{\circ}$ 7,

 $B = 22^{\circ} 37$; to find the other two sides,

27 9° 16' AC = 158 98 yards and BU = 501 V 7 9° 16' AC = 158 98 yards and BU = 100 V 7 9° 16' AC = 158 98 yards and BU = 501 V 7 9° 16' AC = 158 98 yards and BU = 501 V 7 9° 16' AC = 158 98 yards and BU = 501 V 7 9° 16' AC = 158 98 yards and BU = 501 V 7 9° 16' AC = 158 98 yards and BU = 501 V 7 9° 16' AC = 158 98 yards and BU = 501 V 7 9° 16' AC = 158 98 yards and BU = 501 V 7 9° 16' AC = 158 98 yards and BU = 501 V 7 9° 16' AC = 158 98 yards and BU = 501 V 7 9° 16' AC = 158 98 yards and BU = 501 V 7 9° 16' AC = 158 98 yards and BU = 501 V 7 9° 16' AC = 158 98 yards and BU = 501 V 7 9° 16' AC = 158 98 yards and BU = 501 V 7 9° 16' AC = 158 98 yards and BU = 501 V 7 9° 16' AC = 158 98 yards and BU = 501 V 7 9° 16' AC = 158 98 yards and BU = 1 32° 40; to find the angle C, Case n. (24.) When two sides and the included angle are given.

RULE, (ART 19.)

As the sum of the two given sides,

: their difference,

:: tangent of half the sum of the opposite angles : tangent of half their difference.

Having thus found the half difference of the unknown angles, we obtain the angles themselves, by first adding and then subtracting this half difference from the half sum. The angles being thus known, as well as two sides, the third side is found by the first case.

The student will find a more compendious method of solution for this case in Prob. 1., Part IV.; but the rule here given will be more

easily remembered.

EXAMPLES.

1. In the triangle ABC are given AB = 137, AC = 153, $A = 40^{\circ}$ 33 19'; to find the other parts.

1. To find the other two Angles.

The sum of the other two angles is $(B+C) = 180^{\circ} - A = 139^{\circ} 26 48^{\circ}$. therefore

$\begin{array}{c} As AB + AC \\ : AC \sim AB \\ : tan. \ \ (B+C) \end{array}$	290 16 69° 43' 24"	arith. com	p. 7·5376020 1·2041200 10·4324460
: tan. 1 (B ~ C)	8° 29' 37"	•	9.1741680

78° 13' 1" == greater angle B. 61° 13' 47" == less angle C. By adding By subtracting

U. To find the third Side BC.

As sin. B	78° 13' 1"		arith.	comp.	0.0092493
	153 .			•	2.1846914
:: sin. A 4	10° 33′ 12′	•	•	•	9.8130173

2.0069580. : BC 101.616

2. In the triangle ABC are given AC = 378, BC = 526, $C = 32^{\circ} 18^{\circ} 26^{\circ}$; to find the other parts.

1. To find the Angles.

The sum of the angles A, B is $(A + B) = 180^{\circ} - 32^{\circ} \cdot 18^{\circ} \cdot 26^{\circ} = 147^{\circ}$ 41' 34'.

As AC + BC	904		arith.	om	p. 7·0438316
: $AC - BC$	148		•		2.1702617
:: tan. 1 (A+)	B) 73° 50'	47"			10.5381278

103° 10' 21" = greater angle B. By adding, By subtracting, 44° 31' 13" = less angle A.

II. To find the side AB,

A	s sin. A	440	31	13"		arith.	comp.	0.1541818
		526						2.7209857
::	sin. C	320	18	26"	•	•	•	9.7279143

: AB 400.942 2.6030818.

If we wish to obtain the third side of the triangle immediately, without first finding the angle, we may do so by means of the formula at (17), adverted to in the scholium to last case; but as the computation will not be adapted to logarithms, it will in general be the shortest method to proceed as above, by two proportions.

3. In the triangle ABC are given AB = 1637, AC = 2065,

A = 132° 7' 12'; to determine the remaining parts.
B = 26° 52' 424'', C = 21° 0' 54'', BC = 3387'974.
4. In the triangle ABC are given AB = 1686, BC = 960, $B = 128^{\circ} 4$; to find the rest.

A = 18° 21' 20', C = 33° 34' 40', AC = 2400'364.

Case m. (25.) When the three sides are given.

A rule for this case, easy to be remembered, may be deduced

from the following simple geometrical investiga-

Take the longest side AB of the triangle for base, and demit upon it the perpendicular CD from the vertex, which will necessarily fall within the base. With centre C and radius CA equal to the longer of the two sides AC, CB, describe a circle, and produce the sides AB, BC, to meet the circumference; then it is plain that



$$GB = AC + CB, BF = AC - CB, BE = AD - DB.$$
Now (Geom. Prop. 24, book 6).
$$GB \cdot BF = AB \cdot BE \therefore AB \cdot (AD - DB) = (AC + CB) \cdot (AC - CB)$$

$$AB : AC + CB :: AC - CB : AD - DB \text{ hence the following rule.}$$

RULE I.

Consider the longest side of the triangle as the base, and demit upon it a perpendicular from the opposite vertex, dividing the base into two segments; then say, As the base,

: the sum of the other two sides,

:: the difference of those sides

: the difference of the segments of the base.

Having thus the sum and difference of the segments, each segment becomes known, and, therefore, in each of the two right-angled triangles into which the proposed is divided, there will be known the base and hypotenuse, and this is enough to determine all the other parts.

$$\cos \frac{1}{4} A = \sqrt{\frac{\frac{1}{4} S (\frac{1}{4} S - a)}{bc}}, \sin \frac{1}{4} A = \sqrt{\frac{(\frac{1}{4} S - c)(\frac{1}{4} S - b)}{bc}}$$

$$\tan \frac{1}{4} A = \sqrt{\frac{(\frac{1}{4} S - b)(\frac{1}{4} S - c)}{\frac{1}{4} S (\frac{1}{4} S - a)}}$$

Both these rules are adapted to logarithmic computation, and this last is much the shortest; when, however, the three sides are small numbers, it will be best to operate without logarithms, by means of the formula (20), cos. $A = \frac{(b+c+a)(b+c-a)}{2} - 1$.

In applying the logarithmic formulas in Rule 2 to the determination of any particular angle, it will generally be best, when this angle is opposite to the longest side of the triangle, to use the first formula, and when it is opposite to the shortest side to use the second; the third may be used when the required angle is opposite to the mean side. If two sides of the triangle are equal, then, of course, neither of these formulas will be used, as the unknown parts will be more readily found as in Example 3, p. 17.

 $\therefore A = 132^{\circ} 7 12.$

```
2. The three sides of the triangle ABC are AB = 98, BC = 95 12, AC = 162 34; to determine the angle A. Using the third formula in the second rule, we have
                 a = 95.12
                 b = 162.34
                 c = 98
                   2)355.46
                S = 177.73 arith. comp.
                                                  7.7502393
        18 - a = 82.61 arith. comp.
                                                  8.0829674
                                                   1.1872386
        8 - b = 15.39
                                                   1.9016218
        18-c = 79.73
                                                2)18:9220671
      tan. 1 A = 16° 7 261"
                                                   9.4610335
                       .. A = 32° 14' 531".
   3. In the triangle ABC are given AC = 6, AB = 5.523,
BC = 1.372; required the angle A.
   Applying the second formula to this example we have
           a = 1.372
                                                   9.2218487
            b=6
                         arith. comp.
            c = 5.523 arith. comp.
                                                   9.2578250
              2)12.895
         8 = 6.4475
    18 - b = .4475
                                                    1.6577930
    18 - c = .9245
                                                    1.9659069
                                                2)18:0963736
   \sin A = 6^{\circ} 24' 55'
                                                    9.0481868
                              . A = 12° 49′ 50″.
 4. The three sides of a plane triangle are AB = 137, AC = 153, BC = 101.616; required the three angles,

A = 40° 33' 12'', B = 78° 13' 1'', C = 61° 13' 47''.

5. The three sides of a plane triangle are AB = 1686, BC = 960,
```

AC = 2400.364; required the angle B

 $B = 128^{\circ} 4$. 6. Required the angles when the sides are 4, 5, and 6. The angles are 41° 24' 35", 55° 46' 16", and 82° 49' 9".

CHAPTER III.

APPLICATION OF PLANE TRIGONOMETRY TO THE MENSURATION OF HEIGHTS AND DISTANCES.

PROBLEM. 1.

A person on one side of a river observes an obelisk on the opposite side, and, being desirous to ascertain its height, he took with a quadrant the angle $B=55^{\circ}$ 54, which the obelisk subtended at the place where he stood, then going back the distance BA = 100 feet, he again measured the subtended angle, and found it to be A = 33° 20; what was the height of the obelisk?

In the triangle of ABC are given the angle $A = 33^{\circ} 20$, the angle $ACB = 55^{\circ} 54 - 33^{\circ} 20 = 22^{\circ} 34$, and the side AB; and, therefore BC may be found by Case I. of oblique angled triangles. Again, in the triangle BCD, we shall have given the side BC, and the angle B to find CD, which belongs to Case 1. of right angled triangles.

The actual computation, however, will be shortened by combining

these two rules in a single formula, thus for the first

 $\frac{1}{\sin ACB}$, and from the second $CD = BC \sin CBD$

 $\therefore CD = \frac{AB \sin. A \sin. CBD}{B}$ sin. ACB 22° 34 arith. comp. 0.4159424 sin. ACB 330 20 sin. A 9.7399748 sin. CBD 55° 54' 9.9186620 AB 100

> CD 118.57* 2.0739792.

The problem may be solved still more readily as follows. If we take CD for radius, DB will be the tangent of the angle DCB, and DA the tangent of DCA, therefore, AB is the difference of those tangents; but by referring to the table of natural tangents, we find that to radius 1

nat. tan. $56^{\circ} 40^{\circ} = 1.5204261$ nat. tan. 34° 6′ = difference = .8433752

∴ 8433752 : 1 :: 100 : 118.57, as before.

PROBLEM II.

A person at A wishes to know his distance from an in accessible object at C, but he has no instrument for taking angles. He, therefore, sets up a staff at A, from tion B, 38 feet from the former A, and he finds the diagonal distances AB', BA', to be respectively 97 feet and 81 feet. From these data it is required to determine the distance of A from the object C.



All the three sides of the triangle A'AB are given, therefore to find

the angle A'AB we have, by using the first formula at (25), A'B = 81A'A = 60 arith. comp. 8.2218487 AB = 38 arith. comp. 8.4202164

> 2)179 1 S = 1.951823018-A'B=8.50.9294189 2)19.5233070

 $\cos \cdot A AB = 54^{\circ} \cdot 41' \cdot 56''$ 9.7616535 $\therefore A'AB = 109^{\circ} 23' 52' \therefore CAB = 70^{\circ} 36' 8'$

he

* To the height of the object thus determined the height of the observer's eye, or of the instrument, must be added.

Again, by applying the same formula to the triangle BBA, we have $\mathbf{B}'\mathbf{A} = 97$ B'B = 86 arith. comp. 8.0655015 AB = 38 arith. comp. 8.42021642)221 110.5 2.0433623 1.1303338 13·5 2)19.6594140

cos. B'BA = 47° 29' 50" 9.8297070

 $\therefore B'BA = 94\circ 59 \cdot 40' \cdot \therefore CBA = 85\circ 0' \cdot 20'$ $\therefore C = 180 - (CAB + CBA) = 24\circ 23' \cdot 40'.$ Consequently, in the triangle ABC, we have all the angles and one side AB given; hence, by Case 1.

sin. C 24° 23' 40' arith. comp. 0.3840330 : AB 38 1.5797836 :: sin. B 85° 0' 20" 9·9983479 : AC 91.657 1.9621645.

PROBLEM III.

At the top of a castle, which stood on a hill near the sea-shore, the angle of depression HTS, of a ship at anchor, was observed to be 40.52; at the bottom of the castle the angle of depression OBS was 4° 2'. Required the horizontal distance AS of the vessel, and the height of the hill above the level of the sea, the height of the castle being 60 feet.

As TH, BO, are parallel to AS, we have $TSA = 4^{\circ}52$, and BSA = 4° 2. Bearing this in mind we have

In
$$\triangle$$
 TSB, $\frac{SB}{BT} = \frac{\sin. ATS}{\sin. TSB}$

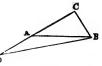


In \triangle BSA, AS = SB cos. BSA, AB = SB sin. BSA $; AB \cdot R = \frac{BT \sin. ATS \sin. BSA}{BSA}$ BT sin. ATS cos. BSA sin. TSB sin. TSB

	AS	4100	-4				3.6128250,	AB	289.12		2.4610847.
	BSA BT	40		•			9·9984315 9·9989230 1·7781513	sin	BSA	:	8·8471827 1·7781513
sin.		0° !	50′		•	comp.	1.8373192				1·8373192 9·9984315

PROBLEM IV.

The distances of three objects A, B, C, from each other, are as follow, viz. AB = 462 yards, AC = 328 yards, and BC = 297 yards; a person at D, wishing to know his distance from each object, takes the angle ADB, and finds it to be 34° 16 21"; it is required to determine DA, DC, and DB.



As the three sides of the triangle ABC are given we may find the angle CAB, and, consequently, the supplemental angle DAB, so that we shall have in the triangle DAB the two angles D, A and the side AB to find the rest. The computation will, therefore, be as follows.

I. To find the angle CAB.

BC = 297

AC = 328 arith. comp. 7.4841262 AB = 462 arith. comp. 7.3353580

2)1087

2.3334473 215.5 2.9111576

2)19.0640891

9.5320445 ∴ DAB = 180° - 39° 48' 28' = 140° 11' 32' ∴ DBA = 15° 32' 7'.

II. To find AD.

24° 16' 21" arith. comp. 0.3860770 $\mathbf{A}\mathbf{s}\sin \mathbf{D}$: AB 462 2.6646420 :: sin. B 15° 32' 7" 9.4278619

301.01 2.4785809 : AD $\therefore DC = DA + AC = 629.101 \text{ yards.}$

III. To find BD.

As sin. D 24° 16' 21" arith. comp. 0.3860770 : AB 462 2.6646420 :: sin. A 140° 11' 32" 9.8063252

: BD 719.5222.8570442

Hence we have the three distances, viz. DA = 301.01, DC = 629.101, DB = 719.522.

PROBLEM V.

Suppose that from the top of a mountain, three miles high, the angle of depression of the remotest visible point of the earth's surface is taken and found to be 2° 13' 27'; it is required thence to determine the diameter of the earth, supposing it to be a perfect sphere.

Let O be the centre of the earth, BA the mountain, AC the visual ray or line touching the earth's surface in C. Draw the tangent BD, and join OD, OC; then the angle of depression EAC being given, we have also the angle BAD, the complement of it, equal to 87° 46° 33". Also since the tangents BD, CD, are equal, (Geom. p. 106,) we have the angle BOD = $DOC = \frac{1}{2}$ comp. $A = 1^{\circ} 6' 491''$, and, therefore, $BDO = 88^{\circ} 53' 16''$.



Now in the right-angled triangle ABD we have BD = AB tan. A; and in the right-angled triangle OBD, OB = BD tan. BDO; hence by substitution, OB = AB tan. A tan. BDO; the computation is, therefore, 0.4771213 as follows: AB =

870 46 33" tan. A 11.4107381 tan. BDO 88° 53' 164" 11.7119309

3979.15 3.5997903;

hence the diameter is 7958 3 miles.

PROBLEM VI.

Given the distances between three objects A, B, C, and the angles subtended by these distances at a point D in the same plane with them; to determine the distance of D from each object.

Let a circle be described about the triangle ADB, and join AE, EB, then will the angles ABE, BAE, be respectively equal to the given angles ADE, BDE, (Geom. p. 52); thus all the angles of the triangle AEB are known, as also the side AB; we may find, therefore, the remaining sides AE, EB. Again, the sides of the triangle ABC being known, we may find the angle BAC; hence the angle CAE becomes known, so that in the triangle CAE we shall have the two sides AE, AC, and the included angle given, from which we may find the angle AEC in fig. 1, or the angle ACE in fig. 2, and thence its supplement AED or ACD; this with the given side AE and angle ADE, in the first figure, or with the given side AC and angle ADC in the second, will enable us to find AD, one of the required lines, and

thence DC and DB, the other two.





Or the solution may be conducted more analytically as follows. Put x for the angle DAC, and x for the angle DBC; also call the given angles ADC, BDC, a and a', then a, b, c, representing as usual the sides opposite to A, B, C, we have

$$\frac{\sin \cdot a}{\sin \cdot x} = \frac{b}{DC}, \frac{\sin \cdot a'}{\sin \cdot x'} = \frac{a}{DC} \cdot \dots \cdot (1) \therefore \frac{\sin \cdot a \sin \cdot x'}{\sin a' \sin \cdot x} = \frac{b}{a}$$

$$\therefore a \sin \cdot a \sin \cdot x' = b \sin \cdot a' \sin \cdot x \dots \cdot (2).$$

This is one equation between the unknown quantities x, x. Another is easily obtained; for since the four angles of the quadrilateral ADCB make up four right angles or 360°, we have x+x+a+a'+ACD+BCD=360°; the two latter angles may be considered as known, since in the triangle ABC the angle C is determinable from the three given sides; therefore all the terms in the first member of this equation are known except x and x. Call the sum of these known quantities β , and we shall thus have $x = \beta - x$, and, consequently, by substitution, equation (2) becomes, $a \sin a \sin (\beta - x) = b \sin a \sin x$

or dividing by
$$\sin x$$
, $b \sin a' = a \sin a (\sin \beta \cos x - \cos \beta \sin x)$;

$$\therefore \cot x = \frac{b \sin a'}{a \sin a \sin \beta} + \frac{\cos \beta}{\sin \beta} = \frac{b \sin a'}{a \sin a \sin \beta} + \cot \beta$$
.

The first term of this second member may be easily calculated by logarithms, and this added to the natural cotangent of β gives the nat. cot. of x, and thence x is known from the equation $x = \beta - x$, and CD from either of the equations (1).

PROBLEM VII.

Given the angles of elevation of an object taken at three places on the same horizontal straight line, together with the distances between the stations; to find the height of the object and its distance from either station.

Let AB be the object, and C, C', C'', the three stations, then the triangles BCA, BC'A, BC'A, will all be right angled at A; and, therefore, to radius BA, AC, AC', AC", will be the tangents of the angles at B, or the cotangents of the angles of elevation; hence putting a, a', a'', for the angles of elevation, x for the height of the object, and a, b, for the distances C C', C C'', we shall have AC = x cot. a, AC' = x cot. a'. AC'' = x cot. a'.



Now if a perpendicular AP be drawn from A to C C", we shall have (Geom. p. 35,) from the triangle ACC

 $AC^2 = AC'^2 + C'C^2 - 2C'C \cdot CP$; and from the triangle AC'C''

 $AC'^2 = AC'^2 + C''C'^2 + 2C''C' \cdot C'P$; that is, we shall have the two equations $x^2 \cot^2 a = x^2 \cot^2 a' + a^2 - 2a \cdot C'P$.

 $x^2 \cot x^2 = x^2 \cot x^2 + b^2 + b^2$ tiply the first by b, the second by a, and add and we shall have

$$x^{2} (b \cot^{2} a + a \cot^{2} a'') = (a + b) x^{2} \cot^{2} a' + ab (a + b)$$

$$\therefore x = \sqrt{\frac{ab (a + b)}{b \cot^{2} a + a \cot^{2} a'' - (a + b \cot^{2} a')}}$$

If the three stations are equidistant, then a = b, and the expression

becomes

The height AB being thus determined, the distances of the stations from the object are found by multiplying this height by the cotangents of the angles of elevation.

Three objects A, B, and C, whose distances are AC = 8 miles, BC = 71 miles, and AB = 12 miles are visible from one station D, in the line joining A and B, at which point the line joining A and C subtends an angle of 107° 56° 13". Required the distances of the objects from the station.

AD = 5 miles, DC = 4°892 miles, DB = 7 miles. PROBLEM 1X.

Suppose the angle of elevation of the top of a steeple to be 40° when the observer's eye is level with the bottom, and that from a window 18 feet directly above the first station, the angle of elevation is found to be 37° 30°. Required the height and distance of the steeple.

Height = 210°44 feet. Distance 250°79 feet.

PROBLEM X

In order to determine the horizontal distance between two remote objects A, B, a base line A' B' of 536 yards was measured, and then a flagstaff being set up at each extremity, these four angles were taken from them, viz. at A' the angular distance between A and B, 57° 40, and the angular distance between B and B', 40° 16', also at B' the angular distance between A and B, 71° 7, and the angular distance between A' and A, 42° 29. Required the distance between the objects. 939.52 yards.

PROBLEM XI.

Three objects A, B, C, are in the same straight line, and of known distances from each other, viz. AB = 3626 yards, and BC = 8374 yards, the angular distance of A, B, from a station D, where all the objects are visible, is 19°, and the angular distance of B, C, is 25°. Required the distance of each object from the place of observation.

DA = 9.471 yards, DB = 10.861, DC = 16.848.

PROBLEM XII.

At three points in the same horizontal straight line the angles of elevation of an object was found to be 36°50, 21°24 and 14°, the middle station being 84 feet from each of the others. Required the height of the object. 53.964 feet.

PROBLEM XIII.

There are three towns A, B, and C, whose distance apart are as follow: from A to B six miles; from A to C, 22 miles; and from B to C, 20 miles. A messenger is despatched from B to A, and has to call at a town D in a direct line between A and C. Now in travelling from B

to D, he walks uniformly at the rate of 4 miles an hour, and from D to A at the rate of 3 miles an hour. Supposing him to perform his journey in 3 hours, it is required to determine the position of the town D.

The distance of D from A is 4.72 miles.

The student who has the practical applications of Plane Trigonometry more immediately in view, may pass over the following chapter, on the theory of the trigonometrical lines, and proceed to the first chapter of part iii., which contains the application of Trigonometry to Navi-

CHAPTER IV.

INVESTIGATION OF TRIGONOMETRICAL FORMULAS.

(26.) The formulas hitherto investigated are those only which are immediately connected with the business of plane trigonometry, properly so called, that is, with the solutions of the several cases of plane triangles. Having disposed of all these cases, we shall now proceed to develop the theory of the trigonometrical lines more at large, dismissing all considerations of the sides of triangles.

The following general expressions have already been established, viz.

$$\begin{array}{l} \sin. \ (A+B) = \sin. \ A \cos. B + \sin. B \cos. A \\ \sin. \ (A-B) = \sin. \ A \cos. B - \sin. B \cos. A \\ \cos. \ (A+B) = \cos. A \cos. B - \sin. A \sin. B \\ \cos. \ (A-B) = \cos. A \cos. B + \sin. A \sin. B \end{array} \right\} \ . \ (2).$$

From these equations we get 1. By addition,

$$\sin. (A + B) + \sin. (A - B) = 2 \sin. A \cos. B$$

 $\cos. (A + B) + \cos. (A - B) = 2 \cos. A \cos. B$. . (3).

2. By subtraction,

$$\sin. (A + B) - \sin. (A - B) = 2 \cos. A \sin. B$$

 $\cos. (A - B) - \cos. (A + B) = 2 \sin. A \sin. B$... (4).

It is worth while to remark here that if we make $A = 60^{\circ}$, then since cos. 60° A 4, (p. 14,) the first of these formulas furnish the equation $\sin B = \sin (60^{\circ} + B) - \sin (60^{\circ} - B) ... (V);$

which is a useful expression in the work of computing tables.

3. By multiplication,

$$\sin (A + B) \sin (A - B) = \sin A \cos B - \sin B \cos B$$

 $\cos (A + B) \cos (A - B) = \cos A \cos B - \sin B$
Or eliminating $\cos A$, $\cos B$
of the conditions $\sin A + \cos A - \cos B$

of the conditions $\sin^2 A + \cos^2 A = 1$; $\sin^2 B + \cos^2 B = 1$; the second members of them become, respectively, $\sin^9 A - \sin^9 A \sin^9 B - \sin^9 B + \sin^9 B \sin^9 A$, or $\sin^9 A - \sin^9 B$;

 $1 - \sin^2 B - \sin^2 A + \sin^2 A \sin^2 B - \sin^2 A \sin^2 B$, or $\cos^2 B \sin^2 A$; $\begin{array}{l} \sin\left(A+B\right)\sin\left(A-B\right)=\sin^2A-\sin^2B=\left(\sin A+\sin B\right)\left(\sin A-\sin B\right)\\ \cos\left(A+B\right)\cos\left(A-B\right)=\cos^2B-\sin^2A=\left(\cos B+\sin A\right)\left(\cos B-\sin A\right) \end{array}$

$$\begin{array}{c} \mathbf{A} \cdot \mathbf{B} \cdot \mathbf{y} \cdot \mathbf{cos} \cdot \mathbf{A} - \mathbf{B} \cdot \mathbf{b} = \mathbf{cos}^{2}\mathbf{B} - \mathbf{sin}^{2}\mathbf{A} = (\mathbf{cos} \cdot \mathbf{B} + \mathbf{sin} \cdot \mathbf{A})(\mathbf{cos} \cdot \mathbf{B} - \mathbf{sin} \cdot \mathbf{A}) \\ \mathbf{A} \cdot \mathbf{B} \cdot \mathbf{y} \cdot \mathbf{division}, & \frac{\sin \cdot (\mathbf{A} + \mathbf{B})}{\sin \cdot (\mathbf{A} - \mathbf{B})} = \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{B} + \sin \cdot \mathbf{B} \cdot \mathbf{cos} \cdot \mathbf{A}}{\cos \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} - \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{B} - \sin \cdot \mathbf{A} \cdot \mathbf{sin} \cdot \mathbf{B}} \\ \frac{\cos \cdot (\mathbf{A} + \mathbf{B})}{\cos \cdot (\mathbf{A} + \mathbf{B})} = \frac{\cos \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{B} - \sin \cdot \mathbf{A} \cdot \mathbf{sin} \cdot \mathbf{B}}{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{B} + \sin \cdot \mathbf{A} \cdot \mathbf{sin} \cdot \mathbf{B}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{B} - \sin \cdot \mathbf{A} \cdot \mathbf{sin} \cdot \mathbf{B}}{\cos \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{B} + \sin \cdot \mathbf{A} \cdot \mathbf{sin} \cdot \mathbf{B}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{B} + \sin \cdot \mathbf{A} \cdot \mathbf{sin} \cdot \mathbf{B}}{\cos \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{B} + \sin \cdot \mathbf{A} \cdot \mathbf{sin} \cdot \mathbf{B}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}}{\cos \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}}{\cos \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}}{\cos \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}}{\cos \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}}{\cos \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}}{\cos \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}}{\cos \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}}{\cos \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}}{\cos \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}}{\cos \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}}{\cos \cdot \mathbf{A} \cdot \mathbf{A}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}}{\cos \cdot \mathbf{A}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}}{\cos \cdot \mathbf{A}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}}{\cos \cdot \mathbf{A}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}}{\cos \cdot \mathbf{A}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}}{\cos \cdot \mathbf{A}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{cos} \cdot \mathbf{A}}{\cos \cdot \mathbf{A}} \\ \frac{\sin \cdot \mathbf{A} \cdot \mathbf{co$$

The right hand number of these equations will assume other useful forms by dividing both numerator and denominator of each by certain

expressions: thus, let the divisors for the first equation be

:

cos. A cos. B, sin. A sin. B, sin. A cos. B; those for the second, cos. A sin. B, sin. A cos. B, cos. A cos. B; and those for the third the same as those for the first; we shall then have

$$\frac{\sin. (A+B)}{\sin. (A-B)} = \frac{\tan. A + \tan. B}{\tan. A - \tan. B} = \frac{\cot. B + \cot. A}{\cot. B - \cot. A} = \frac{1 + \cot. A \tan. B}{1 - \cot. A \tan. B}$$

$$\frac{\cos. (A+B)}{\cos. (A-B)} = \frac{\cot. B - \tan. A}{\cot. B - \tan. A} = \frac{\cot. A - \tan. B}{\cot. A - \tan. B} = \frac{1 + \cot. A \tan. B}{1 - \tan. A \tan. B}$$

$$\frac{\sin. (A \pm B)}{\cos. (A \pm B)} = \frac{\tan. A \pm \tan. B}{1 + \tan. A \pm an. B} = \frac{\cot. A + \tan. B}{\cot. A \cot. B \mp 1} = \frac{1 \pm \cot. A \tan. B}{\cot. A \mp \tan. B}$$
(6).

cos.
$$(A \pm B)^- 1 \mp \tan A \tan B^- \cot A \cot B \mp 1^- \cot A \mp \tan B$$

The last of these immediately gives

$$\tan (A + B) = \frac{\tan A + \tan B}{1 - \tan A \tan B}, \tan (A - B) = \frac{\tan A - \tan B}{1 + \tan A \tan B}$$

cot. $(A + B) = \frac{\cot A \cot B - 1}{\cot B + \cot A}, \cot (A - B) = \frac{\cot A \cot B + 1}{\cot B - \cot A}$

If $A = 45^\circ$, then $\tan A = \cot A = 1$, therefore,

$$\tan (45^\circ + B) = \frac{1 + \tan B}{1 - \tan B}, \tan (45^\circ - B) = \frac{1 - \tan B}{1 + \tan B}$$

cot. $(45^\circ + B) = \frac{\cot B - 1}{\cot B + 1}, \cot (45^\circ - B) = \frac{\cot B + 1}{\cot B - 1}$

$$\therefore \tan (45^\circ + B) - \tan (45^\circ - B) = \frac{4 \tan B}{1 - \tan B} \cdot \cdot \cdot \cdot (8)$$

cot. $(45^\circ - B) - \cot (45^\circ + B) = \frac{4 \cot B}{\cot B - 1} \cdot \cdot \cdot \cdot \cdot (9)$.

Such are the most useful theorems respecting the sums and differences

$$\tan. (45^{\circ} + B) = \frac{1 + \tan. B}{1 - \tan. B}, \tan. (45^{\circ} - B) = \frac{1 - \tan. B}{1 + \tan. B}$$

$$\cot. (45^{\circ} + B) = \frac{\cot. B - 1}{\cot. B + 1}, \cot. (45^{\circ} - B) = \frac{\cot. B + 1}{\cot. B - 1}$$

$$\therefore \tan. (45^{\circ} + B) - \tan. (45^{\circ} - B) = \frac{4 \tan. B}{1 - \tan.^{\circ} B} . . . (8)$$

$$\cot (45^{\circ} - B) - \cot (45^{\circ} + B) = \frac{4 \cot B}{\cot^{2} B - 1} . . . (9).$$

Such are the most useful theorems respecting the sums and differences of two unequal arcs, and they may be converted into other expressions involving three or more arcs by simply substituting B+C+D+dx for B. We shall briefly consider the case of three arcs, or angles, because of a curious property belonging to them whenever they make up either 180° or 90°.

Let A, B, C, be any three arcs, and consider A + B as one, then by equa. (1)

$$\begin{array}{l} \sin \left({A + B + C} \right) = \sin \left({A + B} \right)\cos C + \cos \left({A + B} \right)\sin C \\ = \left({\sin .\,A\cos .\,B + \cos .\,A\sin .\,B} \right)\cos C + \cos C + \sin C + \cos C$$

Let now the sum of the three arcs be 180°, or, indeed, any multiple of 180°, then the sine of this sum will be 0, so that the first of these equations gives \sin A \cos B \cos C + \cos A \sin B \cos C + \cos A \cos B \sin C = \sin A \sin B \sin C;

dividing both sides of this equation by cos. A cos. B cos. C, we have

$$\frac{\sin. A}{\cos. A} + \frac{\sin. B}{\cos. B} + \frac{\sin. C}{\cos. C} = \frac{\sin. A}{\cos. A} \cdot \frac{\sin. B}{\cos. B} \cdot \frac{\sin. C}{\cos. C};$$

that is, tan. A + tan. B + tan. C = an. A tan. B tan. C; a remarkable property of the angles of a plane triangle.

Again, let the sum of the three arcs be 90°, or any multiple thereof, then the cosine of this sum will be 0, so that the second general equation above becomes cos. A cos. B cos. C = A cos. B cos. C + sin. A cos. B sin. C + cos. A sin. B sin. C;

dividing both sides by sin. A sin. B sin. C, we have cot. A cot. B cot. $C = \cot A + \cot B + \cot C$.

for A + B in the preceding expressions. We thus get from (1)

```
sin. nA = \sin A \cos (n-1)A + \sin (n-1)A \cos A \cos nA = \cos A \cos (n-1)A - \sin A \sin (n-1)A;
so that putting for n, 1, 2, 3, &c. successively, we have
            \sin. A = \sin. A \sin. 2 A = 2 \sin. A \cos. A
            \sin 3 A = \sin A \cos 2 A + \sin 2 A \cos A

\sin 4 A = \sin A \cos 3 A + \sin 3 A \cos A
                                                                                                                                             (10)
                               &c.
            \cos. A = \cos. A
            \cos 2 A = \cos^2 A - \sin^2 A
            \cos 3 A = \cos A \cos 3 A - \sin A \sin 2 A
                                                                                                                                              (11).
            \cos 4 A = \cos A \cos 3 A - \sin A \sin 3 A
We may put the general expressions for sin. nA, and cos. nA, under a different form, by making use of the second equation in (1) and (2),
thus putting (n-1) A for A, and A for B, these become \sin. (n-2) A = \sin. (n-1) A cos. A - \sin. A cos. (n-1) A cos. A + (n-1)
or, by transposing,

0 = -\sin A \cos (n-1) A + \sin (n-1) A \cos A - \sin (n-2) A

0 = +\cos A \cos (n-1) A + \sin A \sin (n-1) A - \cos (n-2) A;
adding these two equations to those above, there results
     \sin n A = 2 \sin (n-1) A \cos A - \sin (n-2) A \cos n A = 2 \cos (n-1) A \cos A - \cos (n-2) A
hence, \sin A = \sin A
                 \sin 2 A = 2 \sin A \cos A
                \sin 3 A = 2 \sin 2 A \cos A - \sin A
                                                                                                                                         (13)
                 \sin 4 A = 2 \sin 3 A \cos A - \sin 2 A
                         &c.
                                                               &c.
                 \cos. A = \cos. A
                 \cos 2 A = 2 \cos A \cos A - 1
                \cos 3 A = 2 \cos 2 A \cos A - \cos A

\cos 4 A = 2 \cos 3 A \cos 2 A - \cos 2 A
                                                                                                                                         (14).
                       &c.
                                                                         &c.
 (29.) The sines and cosines of multiple arcs may also be developed in terms of the powers of the sine and cosine of the simple arc, by help
 of a remarkable formula, known by the name of De Moivre's formula,
 which may be easily established, as follows.
      Multiply together the two expressions,
                      cos. A + \sin A \cdot \sqrt{-1} and cos. A_1 + \sin A_1 \cdot \sqrt{-1};
 and we shall have the product, cos. A cos. A_1 - \sin A \sin A_1 +
 (cos. A sin. A<sub>1</sub> + sin. A cos. A<sub>1</sub>) \sqrt{-1}; which, by the equations (1),
  (2), is the same as, cos. (A + A_1) + \sin((A + A_1) \sqrt{-1};
  which is of the same form as the original factors, consequently, multi-
 plying this by the new factor, cos. A_2 + \sin A_2. \sqrt{-1}, we must have for
  the product cos. (A + A_1 + A_2 + \sin \cdot (A + A_1 + A_2) \sqrt{-1},
  and thus by continually introducing a new factor, we must have
  generally
            (cos. A + sin. A. \sqrt{-1})(cos. A<sub>1</sub> + sin. A<sub>1</sub>. \sqrt{-1}) (cos. A<sub>2</sub> + sin. A<sub>2</sub>. \sqrt{-1}) &c. =
             \cos (A + A_1 + A_2 + &c.) + \sin (A + A_1 + A_2 + &c.) \sqrt{-1}.
   Suppose now that A = A_1 = A_2 = &c, then this equation will become
```

(cos. $A + \sin A \cdot \sqrt{-1}$)ⁿ = cos. $A + \sin A \cdot \sqrt{-1}$ or, writing the radical with the double sign,

(cos. $A \pm \sin A \cdot \sqrt{-1}$) $= \cos n A \pm \sin n A \cdot \sqrt{-1}$. (15); n is here a whole number, but, in order to show that the formula holds when the exponent is a fraction, put $a = \frac{\pi}{m} A$; then by this formula,

 $(\cos a \pm \sin a \cdot \sqrt{-1})^m = \cos ma \pm \sin m \cdot \sqrt{-1} =$ cos. $n A \pm \sin n A$. $\sqrt{-1} = (\cos A \pm \sin A \cdot \sqrt{-1})^n$; therefore, extracting the mth root of the first and last members, restoring the value of a, we have, $\cos \frac{n}{m} A \pm \sin \frac{n}{m} A \cdot \sqrt{-1} = (\cos A)$

 $\pm \sin A \cdot \sqrt{-1}$. (16); which is the formula of De Moivre.

If we take the reciprocal of each side of this question we shall have $\frac{1}{\cos \frac{n}{m} A \pm \sin \frac{n}{m} A \cdot \sqrt{-1}} = (\cos A \pm \sin A \cdot \sqrt{-1})^{\frac{n}{m}}$ and if we multiply both numerator and denominator of the first member

of this by cos. $\frac{n}{m} \mathbf{A} \mp \sin \frac{n}{m} \mathbf{A} \cdot \sqrt{-1}$, the denominator will then become $\cos^2 \frac{n}{m} A + \sin^2 \frac{n}{m} A = 1$; hence

$$\cos \frac{n}{m} \mathbf{A} \mp \sin \frac{n}{m} \mathbf{A} \cdot \sqrt{-1} = (\cos \mathbf{A} \pm \sin \mathbf{A} \cdot \sqrt{-1})^{-\frac{n}{m}} (17);$$

so that the formula (16) remains true, whether $\frac{n}{m}$ be positive or nega-

tive. If in (16) we make $\frac{n}{m}$ negative, the signs \pm , in the first member, will be inverted as here, because the sign of the sine is the same as that of the arc.

It may seem to the student that there is a want of generality in the first members of (16) and (17), which ought to contain m values, seeing that the mth root appears in the second members. But this defect is only apparent; for it must be remembered that while the lines sin. A, cos. A, in the second member have each a certain fixed value, the arcs A, to which these lines indifferently belong are innumerable. The first member involves a proposed fractional part, not of any particular one of these arcs, but of any one of them indifferently; it is easy to see, therefore, that the first member involves a variety of values, and they

may be shown to be in number m.

We are to show here that in formula to De Moivre, viz.

$$\cos \frac{n}{m} A \pm \sin \frac{n}{m} A \cdot \sqrt{-1} = (\cos A \pm \sin A \cdot \sqrt{-1})^{\frac{n}{m}}$$

the first member has m values as well as the second. This fact we shall easily establish, by means of the property adverted to in the text, viz. that to any given values of the lines sin. A, cos. A, there correspond innumerable different arcs, viz. every arc in the infinite series, A, $2\pi + A$, $4\pi + A$ $6\pi + A$, &c. so that the first member of the above formula involves in it the follow-

ing values, viz. cos.
$$\frac{n}{m}$$
 A \pm sin. $\frac{n}{m}$ A . $\sqrt{-1}$

oos.
$$\frac{n}{m}(3\pi + A) \pm \sin \frac{n}{m}(3\pi + A) \cdot \sqrt{-1}$$

here my is huppored to

cos.
$$\frac{n}{m} (4\pi + A) \pm \sin \frac{n}{m} (2\pi + A) \cdot \sqrt{-1}$$

cos. $\frac{n}{m} (6\pi + A) \pm \sin \frac{n}{m} (6\pi + A) \cdot \sqrt{-1}$

These values will continue different till we arrive at such a value, N, for one of the numerical coefficients, 2, 2, 4, 6, &c. as will render - N = a multiple of 2π, when the first of the foregoing values will obviously recur, so that by continuing the series we shall merely obtain a repetition of the former values. Now $\frac{n}{m}$ N π cannot become a multiple of 2π till N become equal to 2m; hence we shall have expressed all the different values involved in the first member of De Moivre's formula, when we have continued the above series of values as far as that in which the numeral coefficient is 2m-2; that is when we have written m values. Hence each member of the formula involves m

(30.) Let the first side of (15) be developed by the binomial theorem and the equation will become cos. * A $\pm n \cos$. * $\rightarrow 1$ Ap

$$+\frac{n(n-1)}{2}\cos^{n-2}Ap^2 \pm &c. = \cos \cdot n \pm \sin \cdot n A \cdot \sqrt{-1};$$

p being put for the imaginary sin. A. $\nu - 1$.

Now as in any equation the imaginaries on one side are together equal to those on the other, (Alg. p. 88,) we have by expunging all the imaginaries on both sides, the following expression for cos. n A, viz.

cos.
$$n A = \cos^{-n} A - \frac{n(n-1)}{2} \cos^{-n-2} A \sin^{-2} A + \frac{n(n-1)(n-2)(n-3)}{2 \cdot 3 \cdot 4} \cos^{-n-4} A \sin^{-4} A - &c.$$

In the like manner by expunging all the rational terms on each side of the same equation, and then dividing by $\sqrt{-1}$, there results for $\frac{n(n-1)(n-2)}{2}\cos^{n-1}A\sin$. A + &c.

$$\frac{h(n-1)(n-2)}{2\cdot 3}\cos^{n-2}A\sin^{3}A + &c.$$

From these two expressions may be obtained series for the value of the sine and cosine of an arc in terms of the arc itself.

For let $n = \frac{1}{0}$, and sin. A = 0 = A, then $nA = \frac{0}{0} = any$ finite

quantity
$$x$$
; hence by these substitutions the foregoing series become $\cos x = 1 - \frac{x^2}{1 \cdot 2} + \frac{x^4}{1 \cdot 2 \cdot 3 \cdot 4} - &c.$

$$\sin x = x - \frac{x^3}{1 \cdot 2 \cdot 3} + \frac{x^5}{1 \cdot 2 \cdot 3 \cdot 4 \cdot 5} - &c.$$

by means of which we may calculate the values of the sine and cosine of any arc x, in parts of the radius or linear unit, when we know the length of x itself, according to the same scale. The length of any are in parts of the radius is easily ascertained from the known value of 180° or of a semicircle, in those parts, which by putting π for the semicircumference to radius 1, is (see Geom. p. 139) $\pi=3.14159265358979$,

Sec. so that the length of an arc x degrees is $\frac{x}{190} \cdot \pi = \frac{x}{90} \cdot \frac{\pi}{2}$

As in calculating the sines and cosines x may be always taken less than

1,500 196 4

90, it follows that $\frac{x}{90}$ will be a decimal fraction; if we call this as we may write the foregoing series thus

ite the foregoing series thus,

$$\sin. (m \cdot 90^{\circ}) = m \frac{\pi}{2} - \frac{(\frac{1}{8}\pi)^{3}}{1 \cdot 2 \cdot 3} m^{3} + \frac{(\frac{1}{8}\pi)^{5}}{1 \cdot 2 \cdot 3 \cdot 4 \cdot 5} m^{5} - \csc.$$

$$\cos. (m \cdot 90^{\circ}) = 1 - \frac{(\frac{1}{8}\pi)^{3}}{1 \cdot 2} m^{2} + \frac{(\frac{1}{8}\pi)^{4}}{1 \cdot 2 \cdot 3 \cdot 4} m^{4} - \csc.$$

which series are now in a form suited to immediate calculation. Suppose, for example, the sine and cosine of 1' are required, then,

$$m = \frac{1}{90 \times 60} \cdot m \cdot \frac{\pi}{2} = 0002906882, &c., \cdot \sin 1 = 0002906882, &c. -\frac{1}{1 \cdot 2 \cdot 3} (0002906882) & f. + &c. = 0002906882, &c. \\ \cos 1 = 1 - \frac{1}{1 \cdot 3} (0002906882, &c.)^2 &c. = 9999999577, &c.$$

and from knowing the value of sin. I' and cos. I' we might compute the sines and cosines for every minute in the quadrant, by means of the tormula (3), which when B = I', becomes

 $\sin (A + 1') = 2 \sin A \cos 1' - \sin (A - 1'),$ in which A is to be made successively equal to 1', 2', 3', &c. But we shall not enter into the details of this computation here, our present object being to deduce formulas for the sines, cosines, &c. of multiple arcs.

From the general expressions already given for sin. nA, and cos. nA, rrom the general expressions already given for sin. nA, and cos. nA, those for tan. nA, cot. nA, &c. may be readily obtained by help of the equations at (9); we shall not, therefore, occupy the space by writing them down, but confine ourselves throughout the remainder of this article entirely to the consideration of double arcs, as formulas for these are in much more frequent request than for any higher multiple. The formulas of which we speak, may, of course, all be deduced from the general expressions investigated in the beginning of this article, but, for the sake of simplicity, we shall go nearer the first principles, and deduce them from the expressions in art. (26) deduce them from the expressions in art. (26).

Referring to the equations (1), (2), art. (28), we have when
$$A = B$$
, $\sin 2 A = 2 \sin A \cos A \dots$ (18) $\cos 2 A = \cos^2 A - \sin^2 A$, or $\cos 2 A = 2 \cos^2 A - 1$, or $\cos 2 A = 1 - 2 \sin^2 A \dots$ (19);

and from the last two of these we immediately get

cos. $A = \sqrt{\frac{1}{1 + \frac{1}{1}} \cos 2 A}, \sin A = \sqrt{\frac{1}{1 - \frac{1}{1}} \cos 2 A} \dots (20);$ and, therefore, by division, $\tan A = \frac{1 - \cos 2 A}{1 - \cos 2 A} = \frac{1 + \cos 2 A}{1 - \cos 2 A} \dots (20);$

$$\tan A = \sqrt{\frac{1 - \cos 2 A}{1 + \cos 2 A}}, \cot A = \sqrt{\frac{1 + \cos 2 A}{1 - \cos 2 A}}...$$
 (21); from which we get two new expressions for cos. 2 A, viz.

$$\cos 2 A = \frac{1 - \tan^2 A}{1 + \tan^2 A} = \frac{\cot^2 A - 1}{\cot^2 A + 1} \dots (22).$$

If instead of A we write $45^{\circ} - A$, then since $\cos (90^{\circ} - 2A) =$ sin. 2 A, we have

$$\sin 2 A = \frac{1 - \tan^2 (45^\circ - A)}{1 + \tan^2 (45^\circ - A)} = \frac{\cot^2 (45^\circ - A) - 1}{\cot^2 (45^\circ - A) + 1}$$

It may be worth while to remark that the radical in the above expressions for tan. A, cot. A, may be removed by multiplying the numerator and denominator of each fraction by its numerator: we thus have

tan.
$$A = \frac{1 - \cos 2 A}{\sin 2 A}$$
, cot. $A = \frac{1 + \cos 2 A}{\sin 2 A}$

For the tangent and cotangent of a double arc we have, by division, (18), (19), $\frac{\sin 2 A}{\cos 2 A} = \frac{2 \sin A \cos A}{\cos^2 A - \sin^2 A}$; that is, dividing numerator and denominator of the second member by cos. A, or by sin. A, and recollecting that $\frac{\sin}{\cos}$ = tan., and that $\frac{1}{\tan}$ = cot., we have

$$\tan 2 A = \frac{2 \tan A}{1 - \tan^2 A} = \frac{2 \cot A}{\cot^2 A - 1} = \frac{2}{\cot A} = \frac{2}{\cot A}$$

$$\cot 2 A = \frac{1 - \tan^2 A}{2 \tan A} = \frac{\cot^2 A - 1}{2 \cot A} = \frac{2}{1 (\cot A - \tan A)}$$
(23)

which expressions also immediately come from the values of tan. (A +B), cot. (A + B), at (26), by putting A = B. Comparing the above value of tan. 2A with the expression (8), art. (26), we have, 2 tan. 2 A = $\tan (45^{\circ} + A) - \tan (45^{\circ} - A)$; or which is the same thing, 2 tan. $A = \tan (45^{\circ} + \frac{1}{2} A) - \tan (45^{\circ} - \frac{1}{2} A) \dots (V)$

Formulas for the secants and cosecants of double arcs are easily deduced from those for the cosine and sine, because

sec.
$$=\frac{1}{\cos}$$
, and cosec. $=\frac{1}{\sin}$, thus, from equation (22) above,

we have sec. 2 A = $\frac{1 + \tan^2 A}{1 - \tan^2 A} = \frac{\sec^2 A}{2 - \sec^2 A}$; and from equation (18),

cosec.
$$2 A = \frac{1}{2 \sin A \cos A} = 1 \sec A \csc A$$
.

(31.) Another useful class of formulas are those for half arcs: they may be easily deduced from the expressions for the double arcs; thus putting 1 A for A, we have from (20).

sin.
$$\frac{1}{8}$$
 A = $\sqrt{\frac{1}{8} - \frac{1}{8}}\cos A$, $\cos \frac{1}{8}$ A = $\sqrt{\frac{1}{8} + \frac{1}{8}}\cos A$... (24);
also from (21), $\tan \frac{1}{8}$ A $\sqrt{\frac{1 - \cos A}{1 + \cos A}} = \frac{1 - \cos A}{\sin A}$
 $\cot \frac{1}{8}$ A = $\sqrt{\frac{1 + \cos A}{1 - \cos A}} = \frac{1 + \cos A}{\sin A}$... (25).

Other useful values of sin. $\frac{1}{4}$ A, and cos. $\frac{1}{4}$ A, are derivable from the equation (18) last article, for when $\frac{1}{4}$ A is put for A the equation is sin. $A = 2 \sin \frac{1}{4}$ A cos. $\frac{1}{4}$ A (26), and if this be either added to or subtracted from $1 = \sin \frac{n}{4}$ A + cos. $\frac{n}{4}$ A, the second member will become in each case a perfect square, viz.

$$1 + \sin A = (\sin A + \cos A)^{2}$$

$$1 - \sin A = (\sin A + \cos A)^{2}$$
;

hence,
$$\sqrt{1 + \sin A} = \sin A + \cos A$$

 $\sqrt{1 - \sin A} = \sin A - \cos A$

Let A be less then 90°, then the radical must be taken positive in the first, and negative in the second expression; hence, by addition and subtraction, sin. $\frac{1}{2}$ A = $\frac{1}{2}$ ($\sqrt{1 + \sin A} - \sqrt{1 - \sin A}$)

$$\cos A = (\sqrt{1 + \sin A} - \sqrt{1 - \sin A})$$
(V).

By means of these two expressions the accuracy of a table of sines and cosines may be examined; that is to say, from the calculated values sin. A, in the table, we may compute, by these equations, the values of sin. A, and of cos. A; if these agree with the tabular values, found by other means, we may conclude that the tables are correct in the parts thus verified. Formulas employed in this manner to put the accuracy

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of the tables to the test are called formulas of verification.
            given three of these, and marked them with the letter (V).
                  (32.) The following formulas involving the half sums and half differ-
           ence of two arcs are of frequent application: substitute \frac{1}{2}(A+B) for A and \frac{1}{2}(A-B) for B, in the equations (3), (4), at art. (26) and we have
               \begin{array}{l} \sin. \ A + \sin. \ B = 2 \sin. \frac{1}{2} (A + B) \cos. \frac{1}{2} (A - B) \\ \cos. \ A + \cos. \ B = 2 \cos. \frac{1}{2} (A + B) \cos. \frac{1}{2} (A - B) \\ \sin. \ A - \sin. \ B = 2 \cos. \frac{1}{2} (A + B) \sin. \frac{1}{2} (A - B) \\ \cos. \ B - \cos. \ A = 2 \sin. \frac{1}{2} (A + B) \sin. \frac{1}{2} (A - B) \end{array}
                                                                                                                                                                                                                                (27);
         and from these we get, by division,
         \frac{\sin A + \sin B}{\cos A + \cos B} = \tan \frac{1}{2} (A + B); \frac{\sin A - \sin B}{\cos B - \cos A} = \cot \frac{1}{2} (A + B). (28)
                                                          = \tan \frac{1}{4}(A-B); \frac{\sin A + \sin B}{\cos B - \cos A} = \cot \frac{1}{4}(A-B). (29).
         sin. A - sin. B
                        In each of these expressions let A = 90^{\circ}, and we shall have
         1+\sin B = 2\sin (45^{\circ} + \frac{1}{2}B)\cos (45^{\circ} - \frac{1}{2}B) = 2\sin^{2}(45^{\circ} + \frac{1}{2}B)
            cos. B. = 2\cos.(45^{\circ} + \frac{1}{8}B)\cos.(45^{\circ} - \frac{1}{8}B) = 2\cos.^{2}B - 1, by eq. 18
  1 — sin. B = 2 cos. (45^{\circ} + \frac{1}{4} B) sin. (45^{\circ} - \frac{1}{4} B) = 2 cos. (45^{\circ} + \frac{1}{4} B)
= 2 sin. (45^{\circ} - \frac{1}{4} B)
1 — cos. B = 2 sin. (45^{\circ} + \frac{1}{4} B) sin. (45^{\circ} - \frac{1}{4} B) = 2 sin. (45^{\circ} + \frac{1}{4} B) speq. 19,
         \frac{1 - \cos B}{1 + \sin B} = \tan (45^{\circ} + \frac{1}{2}B) \frac{1 - \sin B}{\cos B} = \cot (45^{\circ} + \frac{1}{2}B) \frac{1 - \sin B}{\cos B} = \cot (45^{\circ} + \frac{1}{2}B)
= \tan (45^{\circ} - \frac{1}{2}B),
 \begin{cases} \frac{\cos B}{1 + \sin B} = \tan \frac{(45^{\circ} - 1B)}{1 - \sin B}, & \frac{1 + \cos B}{1 - \cos B} = \cot \frac{(45^{\circ} - 1B)}{1 - \cos B} = \cot \frac{1B}{1 - \cos B} = \cot \frac{1B}{1 - \cos B}. \end{cases}
         Again, dividing (28) by (23), we have \frac{\sin A + \sin B}{\sin A - \sin B} = \frac{\tan \frac{1}{2}(A + B)}{\tan \frac{1}{2}(A - B)}, \frac{\sin A - \sin B}{\sin A + \sin B} = \frac{\cot \frac{1}{2}(A + B)}{\cot \frac{1}{2}(A - B)}(30).
                 Lastly, substituting A + B for A in (26) last article, we have
         sin. (A + B) = 2 \sin \frac{1}{2} (A + B) \cos \frac{1}{2} (A + B); and dividing this by
         each of the formulas (27) in succession, there results
                                                                       \cos \frac{1}{4} (A + B) \sin (A + B)
                                                                                                                                                                                             sin. 1 (A + B)
           \sin A + \sin B =
                                                                        \frac{1}{\cos A} + \frac{1}{(A-B)}; \frac{1}{\cos A} + \cos B = \frac{1}{\cos A}
                                                                          \sin \frac{1}{4} (A + B) \sin (A + B) \cos \frac{1}{4} (A + B)
               \sin (A + B)
           \frac{1}{\sin A - \sin B} = \frac{1}{\sin A - \cos A} = \frac{1}{\sin A} 
                 (33.) We shall conclude this chapter on the theory of the trigono-
         metrical lines, with two curious and useful propositions.
                 1. To express the sine and cosine of a real arc by means of imaginary
         exponentials. By the exponential theorem,*
         e^x = 1 + x + \frac{x^2}{2} + \frac{x^3}{2 \cdot 3} + \frac{x^4}{2 \cdot 3 \cdot 4} + &c. where e represents the base of
         the Naperian logarithms, that is, e = 2.7182818, &c. For x substitute
         x\sqrt{-1}, and -x\sqrt{-1} successively, and we have these developments
         e^{x\sqrt{-1}} = 1 + x\sqrt{-1} - \frac{x^2}{2} - \frac{x^3\sqrt{-1}}{2 \cdot 3} + \frac{x^4}{2 \cdot 3 \cdot 4} + &c. (1);
\frac{x^{2}}{2} \sqrt{-1} = 1 - x \sqrt{-1} - \frac{x^{2}}{2} + \frac{x^{2} \sqrt{-1}}{2 \cdot 3} + \frac{x^{4}}{2 \cdot 3 \cdot 4} - \&c. (2);
                  See the "Elementary Essay on the construction of Logarithms," p. 68; or Young's
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Algebra, just published by Carey, Lea, & Co. Philadelphia.

hence, by addition,

$$e^{x\sqrt{-1}} + e^{-x\sqrt{-1}} = 2\left(1 - \frac{x^2}{2} + \frac{x^4}{2 \cdot 3 \cdot 4} - &c.\right)$$

But by art. (30) the series on the right is the development of cos. s, hence $\cos x = \frac{e^x \sqrt{-1} + e^{-x} \sqrt{-1}}{2}$

By subtracting (2) from (1) we have
$$e^{x\sqrt{-1}} - e^{-x\sqrt{-1}} = 2\sqrt{-1} (x - \frac{x^3}{2 \cdot 3} + \frac{x^5}{2 \cdot 3 \cdot 4 \cdot 5} - 6c.)$$

But by art. (30) the series on the right is the development of sin. z; hence, sin. $x = \frac{e^x \sqrt{-1} - e^{-x} \sqrt{-1}}{2 \sqrt{-1}}$.

2. To develop sin." x, cos." x, in terms of the sine and cosine of the multiples of x.

Put
$$\cos x + \sin x$$
. $\sqrt{-1} = u$ $\cos x - \sin x$. $\sqrt{-1} = v$ (1) ,

then art. (29),
$$\cos nx + \sin nx \cdot \sqrt{-1} = u^{n}$$

$$\cos nx - \sin nx \cdot \sqrt{-1} = v^{n}$$

$$(2);$$

from which, by addition and multiplication, we get $u^n + v^n = 2 \cos nx$, $u^n v^n = 1 \dots (3)$. Add together the equations (1); there will result cos. $x = \frac{1}{2} (u + v)$; and, therefore,

$$\cos^n x = \frac{1}{2^n} (u + v)^n = \frac{1}{2^n} (v + u)^n; \text{ hence, by the binomial theorem,}$$

$$\cos^{n} x = \frac{1}{2^{n}} \{ u^{n} + n u^{n} - 1 v + \frac{n(n-1)}{2} u^{n} - v^{2} + \delta c. \},$$

or, $\cos^n x = \frac{1}{2^n} \{ v^n + nv^{n-1} u + \frac{n(n-1)}{2} v^{n-2} u^2 + &c. \}$ adding these equations together, and dividing by 2, we have

$$\cos^{n} x = \frac{1}{2^{n} \sqrt{12}} \left\{ u^{n} + v^{n} + nuv \left(u^{n} - 2 + v^{n} - 2 \right) + \frac{n(n-1)}{2} u^{2} v^{2} \left(u^{n} - 4 + v^{-4} \right) + &c. \right\}$$

But from (3)
$$u^n + v^n = 2 \cos nx$$
 $u^n - \frac{1}{2} + v^n - \frac{1}{2} = 2 \cos (n-2) x$ $u^2 - \frac{1}{2} + v^n - \frac{1}{2} = 2 \cos (n-4) x$ $u^2 + \frac{1}{2} + \frac{$

$$\cos^{n} x = \frac{1}{2^{n}} \{ \cos nx + n \cos (n-2) x + \frac{n(n-1)}{2} \cos (n-4) x + & c. \}$$
 (4).

Again, subtract the second of (1) from the first, and we have

$$2 \sin x \cdot \sqrt{-1} = u - v \therefore \sin x = \frac{u - v}{2\sqrt{-1}};$$

and, consequently,
$$\sin^n x = \frac{(u-v)^n}{(2\sqrt{-1})^n}$$
.

?

H

1. Let n be even, then (Algebra, p. 149,) $(u-v)^n = (v-u)^n$; hence, $\sin^n x = \frac{1}{(2\sqrt{-1})^n}(u-v)^n$, or $\sin^n x = \frac{1}{(2\sqrt{-1})^n}(v-u)^n$; and by adding these equations together after having developed (* - *), and (v - u), we have

 $2\sin^{n} x = \frac{1}{(2\sqrt{-1})^{n}} \{u^{n} + v^{n} - nuv(u^{n-2} + v^{n-2}) + \frac{n(n-1)}{2}u^{2}v^{2}(u^{n-4} + v^{n-4}) - &c.\};$

and making the same substitution as before in virtue of (3), and recollecting that, because n is even, $(\sqrt{-1})^n = \mp 1$, the upper sign having place when n is either of the numbers 2, 6, 10, &c. and the lower sign when a is either of the numbers 4, 8, 12, &c. we have for the development of sin."x

$$\sin^{n} x = \mp \frac{1}{2^{n}} \{\cos nx - n \cos (n - 2)x + \frac{n(n-1)}{2} \cos (n-4)x - \csc \} . . . (5).$$

 $\frac{n(n-1)}{2}\cos.(n-4)x-&c.; . . . (5).$ 2. Let n be odd, then $(u-v)^n=(-1)^n(v-u)^n=-(v-u)^n;$ therefore.

 $\sin^n x = \frac{1}{(2\sqrt{-1})^n} (u-v)^n, \text{ or } \sin^n x = -\frac{1}{(2\sqrt{-1})^n} (v-u)^n;$ and developing $(u-v)^n, (v-u)^n$ as before, and taking the sum of these equations, we have

 $2\sin^n x = \frac{1}{(2\sqrt[4]{-1})^n} \{u^n - v^n - nuv(u^{n-2} - v^{n-2}) +$ $\frac{n(n-1)}{2}u^2v^2(u^{n-4}-v^{n-4})-\&c.$

But from the equations (2), $u^n - v^n = 2 \sin nx \sqrt{-1}$, $u^n v^n = 1$; consequently, since $(\sqrt{-1})^{n-1} = \mp 1$, the foregoing development

becomes
$$\sin^n x = \mp \frac{1}{2^n} \{ \sin nx - n \sin (n-2) x + 2^n \}$$

+

$$\frac{n(n-1)}{2}\sin(n-4)x - &c.$$

the upper sign having place when n-1 is either of the numbers 2, 6, 10, &c. and the lower sign having place when n-1 is either of the numbers, 4, 8, 12, &c. The general term of the first series of numbers is 4m+2, that of the second series 4m.

و ها و فالشمط بيد " وأديث . ووق بها بيساها

for if is or or be negative the terms involving their odd powers much be negative

PART II.

ELEMENTS OF SPHERICAL TRIGONOMETRY.

CHAPTER I.

ON THE SPHERE.

(34.) A Sphere is a solid whose surface is every where equally distant from a certain point within it, called the centre. It may be generated by the revolution of a semicircle about the diameter.

Any line drawn from the centre to the surface of the sphere is called the radius; and the line through the centre having both its extremities

in the surface, is the diameter.

A plane surface, or simply a plane, is that in which if any two points whatever be taken, the straight line which joins them shall lie wholly

in that surface.

A plane may be drawn through any three points, taken at random in space, but not through more than three; for having joined two of the proposed points by a straight line, we may pass a plane through this line in any direction, and we may turn it round upon this line till it arrives at the other point. Three points, therefore, not in the same straight line, fix the position of a plane.

It follows from this, that the common intersection of two planes must be a straight line; for, if among the points in the intersection there be three which are not in the same straight line, the two planes passing

through them must coincide and form but one.

A straight line is said to be perpendicular to a plane when it is per-pendicular to every straight line in that plane, drawn through its foot, or the point where the perpendicular meets the plane. These definitions will suffice for the purpose of establishing the necessary preliminary theorems of spherical Geometry.

(35.) If a sphere be any how cut by a plane, the section must be a circle.

Let C be the centre of the sphere, and ADB
the plane section; draw Cc perpendicular to this plane, and from c draw any line cD in the section and terminating at the surface; then the angle CcD must be a right angle. Join CD, then wherever the point D may be, CD will always be of the same constant length, being the radius of the sphere; and in consequence of the right angle c, $cD = \sqrt{CD^2 - Cc^2}$; hence CD must have the same constant length in whatever direc-

tion it be drawn, that is, the bounding line ADB is the circumference

of a circle of which c is the centre.

The circle is, obviously, the larger, as it is nearer to the centre C of the sphere, or as its perpendicular distance Cc is less, because CD being constant, cD increases as Cc diminishes, and becomes the greatest possible when Cc is 0, that is, when the section passes through the centre of the sphere; hence every circle whose plane passes through the centre

of the sphere is called a great circle of the sphere, and every other a small circle.

It is obvious that the circumference of a great circle may be drawn through any two points on the surface of a sphere, because a plane may be drawn through these two points and through the centre also, but a great circle cannot be drawn through three points on the surface, taken at random, because then a plane might be drawn through four points taken at random; a circle of some kind, however, may always be drawn through three points on the surface of the sphere, since a plane may be

drawn through them.

The line C_c from the centre of the sphere perpendicular to the plane of the circle passes, as we have seen, through its centre c; if this line be Produced both ways to the surface of the sphere, the opposite points P, P, are called the *poles* of the circle. Thus every circle on the sphere has two poles diametrically opposite, the diameter which joins them being perpendicular to the plane of the circle. The poles of a small circle are unequally distant from its plane, the inequality of distance amounting to twice Cc; but in a great circle this inequality vanishes, and the poles are equidistant from the circle.

As the poles of any circle are at the extremities of a diameter of the sphere, an infinite number of great circles may be drawn through them; indeed, every circle passing through them will necessarily be a great circle, because the entire diameter joining them must be comprised in every plane drawn through them. The distance of any circle from either of its poles, measured upon any of these infinite number of great circles, is constantly the same, that is, the distances or arcs PB, PD, PD, PA, &c. are equal, because the constant line Pc is the common versed sine of all these arcs to the common radius CP; hence the other distances P'B, P'E, &c. must be equal. Every arc of a great circle is thus distant from either pole by a quadrant or 90°.

(36.) Two great circles always intersect in two points at the distance of a semicircle from each other, that is, the circumferences bisect each other. For as the plane of each circle passes through the centre of the sphere their intersection must be a diameter common to both circles, and it is at the extremities of this diameter that the circumferences cross each

other.

From this we learn that if from any point on the sphere two quadrantal arcs can be drawn to two points in any great circle, the distance between the points being less than 180°, then the first point must be the pole of this great circle; for it is necessarily the pole of some great circle passing through the proposed points, and as only one great circle can pass through two points, which are not 180° apart, the pole must

belong to the circle in question.

In spherical trigonometry, the arcs of great circles only are concerned, and the angle included between two such arcs, that is to say, a spherical angle, is measured in a manner analogous to that in which a plane angle is measured. For the measure of a plane angle we take the intercepted arc of that circle whose centre is at the vertex, and whose radius is some assumed unit: in like manner for the measure of a spherical angle we take the intercepted arc of that circle whose pole is at the vertex, and whose radius is some fixed unit, viz. the radius of the sphere on whose surface the angle is: thus, in the foregoing figure the spherical angle DPD' is measured by the intercepted arc QQ' of which the pole is P, and radius, CQ, that of the sphere.

It is as easy to justify the propriety of adopting this mode of measuring spherical angles as it is to justify the method of measuring plane angles, for in both cases the intercepted arc varies as the angle; this, by the by, is true of the intercepted arc DD' of any small circle whose pole is P, but we are compelled to refer the measure to a great circle, in order that all the trigonometrical lines concerned in the same inquiry may be related to a common radius, for as we have before remarked, the sides of a spherical triangle are always arcs of great circles.

From what we have just said it appears that a spherical angle DPD has the same measure as either of the equal plane angles QCQ', DcD', &c. situated in the planes of the circles whose common pole is P, and whose sides are formed by the intersection of these planes with those of the two great circles, forming the sides of the spherical angle. If at P tangents were drawn to the two great circles PD, PD', and in their planes they would obviously include the same angle as the lines CQ, CQ', to which they are parallel; indeed if we conceive the plane of the circle HQQ', to move parallel to itself towards the pole, P, the path of C being along the line CP, the angle QCQ' will successively coincide with QCQ', DcD', &c. till C coincides with P, when the lines CQ, CQ', will become tangents to the circles at P, and will remain each in the plane along which it has moved; hence the measure of the angle included between these tangents is also the measure of the spherical angle.

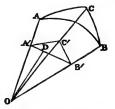
(37.) If in the plane of HQI perpendiculars be drawn from C to each of the planes of the circles PQP', PQ'P', these will be perpendicular to the lines CQ, CQ', and will therefore, include the same angle, which angle will be measured by the arc of HQI, which the said perpendiculars intercept; but these perpendiculars will meet the surface at the poles of the circles to whose planes they are perpendicular; hence the great circle distance between the poles of two intersecting great circles.

measures their angle of intersection.

Every great circle which passes through the poles of another is at right angles to it. Thus the great circle PDQP', through the poles of HQQ'I, is at right angles to HQQ'I; for if a tangent were drawn to PQP' at the point Q it would be in the same plane with and parallel to CP, and if a tangent were drawn to HQI at the point Q it would be in the same plane with and parallel to CH; hence if these two tangents were to move simultaneously to themselves, the path of their point of concourse Q being along QC, they would necessarily coincide with the perpendiculars CP, CH, when Q arrived at C: these tangents, therefore, form a right angle; hence the great circles are perpendiculars to each other, or the spherical angle at Q is a right angle.

(38.) Any one side of a spherical triangle is less than the sum of the other two.

Let ABC be any spherical triangle, and O the centre of the sphere; draw the radii OA, OB, OC, then there will be about O three angles in three distinct planes respectively, measured by the arcs AB, BC, CA. Let AB be the greatest of these arcs, then it will only be necessary to show that AB < AC + CB, or that AOB < AOC + BOC. In the plane of AOB draw any line A'B', and then draw OD, making an angle B'OD equal to BOC; make OC' equal to OD, and join C'B', C'A'



Then since by construction the two sides B'O, OD, and the included angle, are respectively equal to the two sides B'O, OC', and the included angle, B'D = B'C'. But in the plane triangle A'B'C'. $A'B' > A'C' + B'C' \cdot A'C'$; hence the two sides OA', OD, of the triangle A'OC', or are equal to the two sides OA', OC', of the triangle A'OC', of the former is less than the third side A'C' of the latter, and,

consequently, A'OD < A'OC'; hence, since B'OD has been made equal to B'OC', it follows that

 $\mathbf{A}'\mathbf{O}\mathbf{D} + \mathbf{B}'\mathbf{O}\mathbf{D} = \mathbf{A}'\mathbf{O}\mathbf{B}' < \mathbf{A}'\mathbf{O}\mathbf{C}' + \mathbf{B}'\mathbf{O}\mathbf{C}' :: \mathbf{A}\mathbf{B} < \mathbf{A}\mathbf{C} + \mathbf{C}\mathbf{B}.$

(39.) The sum of all the three sides of a spherical triangle is less than the circumference of a great circle.

Let ABC be any spherical triangle; produce the

sides AB, AC, till they meet again in D, then the arcs ABD, ACD, will be semi-circumferences, since (36,) two great circles always bisect each other. But in the triangle BCD we have BC < BD + CD, and, consequently, by adding AB + AC to both, we shall have AB + AC + BC < ABD + ACD; that is to say, the sum of the three sides is less than a whole circumference.



By help of this theorem we may show that the sum of the sides of any spherical polygon whatever is less than the circumference of a great

circle.

Take the spherical pentagon ABCDE for example. Produce the sides AB, DC, till they meet in F; then since BC < BF + CF, the perimeter of the pentagon will be less than the quadrilateral AEDF. Again, produce the sides DE, ABA till they meet in G, was shall have FA. BA, till they meet in G; we shall have EA EG + AG; hence the perimeter of the quadri-lateral AEDF is less than that of the triangle DFG; which last is itself less than the circum-

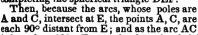


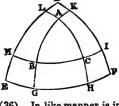
ference of a great circle; the perimeter of the original polygon is, therefore, less still.

(40.) If from the three vertices of a spherical triangle, taken as poles, arcs be described, forming a new triangle, then the vertices of the new triangle will be the poles of the other triangle.

For let ABC be any spherical triangle,

and with the pole A, and circular radius AG equal to a quadrant, describe the arc EF; in like manner with the pole B and same radius describe the arc FD, meeting the former in F; and, lastly, with the pole C and same radius describe the arc ED, completing the spherical triangle DEF.





is less than 180°, E must be the pole of AC (36). In like manner is it shown that F is the pole of AB, and D the pole of BC.

The triangle DEF is sometimes, from the mode of its construction, called the polar triangle, and the original one ABC the primitive triangle.

(41.) Any angle of the primitive triangle is the supplement of the side opposite to it of the polar triangle, and any angle of the polar triangle is the supplement of the side opposite to it in the primitive triangle.

For EH being the radius of HL is $= 90^{\circ}$, and FG being the radius of GK is also $= 90^{\circ}$, and the sum of these radii, namely, EF + GH $= 180^{\circ}$, therefore, GH, which is the measure of the angle A, is the supplement of the side EF opposite to it. In like manner it is shown that B is the supplement of DF, and C the supplement of DE. Again, BI being the radius of ID, and CM the radius of MD, the sum of these MI + BC= 180° therefore, BC is the supplement of MI, which measures the

hole of that a

 angle D. On account of the property just demonstrated, the triangles
 ABC, DEF, are frequently called supplemental triangles.
 It is proper to remark here, as Legendre has done, that besides the triangle DEF three others might be formed by the intersection of the three arcs DE, EF, DF. But the proposition immediately before us is applicable only to the central triangle, which is distinguished from

the others by the circumstance that the two angles A and D (see preceding fig.) be on the same side of BC, the two B and E on the same side of AC, and the two C and F on the same side of

(42.) From the foregoing proposition it follows that three angles of every spherical triangle are together greater than two right angles, and less than



For the sides of the supplemental triangle DEF are together less than four right angles (39), and as these are supplements of the angles A, B, C, and therefore when added to them make six right angles, these last must together exceed two right angles. But they cannot amount to six right angles, for in that case the sum of the sides of the supplemental triangle would be 0, which is absurd. Hence, unlike plane triangles, a spherical triangle may have all its angles right angles or all obtuse angles.

(43.) The foregoing geometrical properties comprise all that we require, for the foundation of the analytical theory of spherical Trigonometry: we need not, therefore, enumerate any more. We shall, however, in conclusion, endeavour to establish the fact that the arc of a great circle joining two points is the shortest line that can be drawn on the

sphere from the one to the other.

The following proof of this property is by Legendre.

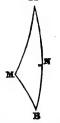
Let ANB be the arc of the great circle which joins the points A and B; and without this line, if possible, let M be a point in the shortest path, between A and B. Through the point M draw

MA, MB, arcs of great circles; and take BN = MB.

Then, by (38), the arc ANB is shorter than AM + MB; take BN = BM, respectively from both; there will

remain AN < AM.

Now, the distance of B from M, whether it be the same with the arc BM or with any other line, is equal to the distance of B from N; for, by making the plane of the great circle BM revolve about the diameter, which passes through B, the point M may be brought into the position of the point N; and the shortest line between M and B, whatever it may be, will then be identical with that between N and B: hence the two paths from A to B, one passing through M, the other through N, have an equal

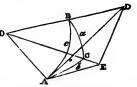


part in each, the part from M to B equal to the part from N to B. first path is the shorter by hypothesis; hence the distance from A to M must be shorter than the distance from A to N; which is absurd, the arc AM being proved greater than AN; hence no point of the shortest line from A to B can be out of the arc ANB; hence this arc is itself the shortest distance between its two extremities.

CHAPTER II.

INVESTIGATION OF FORMULAS, AND RULES FOR THE SOLUTION OF SPHERICAL TRIANGLES.

(44.) Let ABC be a triangle traced on the surface of a sphere of which the centre is O, and the radius equal to the linear unit. The angles of this triangle we shall represent by the letters at their vertices, A, B, C, and the sides opposite to them by the small letters a, b, c; so that having



drawn the two tangents AD, AE, to meet the radi OB, OC, produced through the other extremities of the arcs AB, AC, we shall have

awn the two tangents AD, AE, to meet the radi OB, OC, production the other extremities of the arcs AB, AC, we shall have
$$AD = \tan c = \frac{\sin c}{\cos c}, AE = \tan b = \frac{\sin b}{\cos b}$$

$$OD = \sec c = \frac{1}{\cos c}, OE = \sec b = \frac{1}{\cos b}$$
Oraw DE, then in the two triangles ODE, ADE, we have (17)

Draw DE, then in the two triangles ODE, \overrightarrow{ADE} , we have (17) $\overrightarrow{DE^2} = \overrightarrow{OE^2} + \overrightarrow{OD^2} - 2 \overrightarrow{OE} \cdot \overrightarrow{OD} \cos a$ $\overrightarrow{DE^2} = \overrightarrow{AE^2} + \overrightarrow{AD^2} - 2 \overrightarrow{AE} \cdot \overrightarrow{AD} \cos A$;

recollecting that (p. 43-44) the plane angle DAE measures the spherical angle A. Substituting in these equations the values given by (1),

they become DE² = sec.
$2b$
 + sec. $^2c - \frac{2\cos a}{\cos b \cos c}$

$$DE^2 = \tan \cdot ^2b + \tan \cdot ^2c - \frac{2\sin b \sin c \cos A}{\cos b \cos c} \therefore \text{ by subtraction}$$

$$0 = 1 + 1 + (\sin b \sin c \cos A - \cos a) \frac{2}{\cos b \cos c}$$

Hence multiplying by $\frac{\cos b \cos c}{2}$, and transposing, we have

 $\cos a = \cos b \cos c + \sin b \sin c \cos A$; which is a general expression for the cosine of any side in terms of the other two sides, and their included angle. If we had taken the side b instead of a, the other two would have been a, c, and their included angle B; and if we had taken the side c the other two would have been a, b, and their included angle C; we have, therefore, the three following symmetrical equations, viz.

cos.
$$a = \cos b \cos c + \sin b \sin c \cos A$$

cos. $b = \cos a \cos c + \sin a \sin c \cos B$
cos. $c = \cos a \cos b + \sin a \sin b \cos C$
and these equations embody the whole theory of spherical trigonometry

and are sufficient to supply rules for the solution of every case.

(45.) Some interesting geometrical properties flow also from these

equations.

1. Suppose two sides b, c, of the triangle are equal, that is, let it be isosceles, then it will follow from the two last of these equations that, like as in the isosceles plane triangle, the angles opposite the equal sides will be equal. For taking the difference of these two equations on the supposition that b = c; we have $0 = \sin a \sin b \cos B$

 $-\sin a \sin b \cos C$; and, consequently, B = C. 2. If a = b = c, then it is in a similar manner proved that A = B = c

*C, that is, every equilateral spherical triangle is equiangular.

3. The arc which bisects the vertical angle A of a spherical isosceles

triangle also bisects the base a. For let p represent this bisecting arc, and m, m' the parts into which it divides the base, then the two spherical triangles thus formed give, by the above equations,

cos. $m = \cos b \cos p + \sin b \sin p \cos A$ cos. $m' = \cos a \cos p + \sin a \sin p \cos A$ therefore, since by hypothesis a = b, we have m = m', that is, the arc bisecting the vertical angle also bisects the base, and the student will

find no difficulty in further showing that this same arc is also perpen-

dicular to the base.

4. If two sides and the included angle in one triangle are equal to two sides, and the included angle in another, the third side of the one must be equal to the third side of the other. This is obvious from the first of (A), which shows that cos. a, and therefore a, becomes fixed when the other two sides b, c, and their included A, is fixed; moreover, the remaining angles of the one triangle are equal to the remaining angles of

the other; for by the second and third of (A), cos. B, cos. C, and therefore, B, C, become fixed when a, b, and c, are fixed.

5. If the three sides of one triangle are severally equal to the three sides of another, the three angles of the one are also severally equal to those of the other, the equal angles being opposite to the equal sides. For with fixed values for a, b, c, the formulas (A) give fixed values for cos. A, cos. B, cos. C, and, therefore, for A, B, C. We may, in like manner, infer the equality of the sides from that of the angles, but perhaps the inference is a little more obvious from the equations (B), p.

51, following.
In these deductions the student will observe that we have abstained from saying that the triangles are equal in all respects as in the analogous theorems of plane geometry; because two spherical triangles may exist, of which the several parts of the one may be equal to the several parts of the other, and yet not admit of coincidence, as plane triangles would under like conditions. Thus, if two plane triangles, of which the sides in the one are equal to those in the other, be joined together by a cor-responding side of each, and if we turn one of the triangles about this common side either above or below the plane on which they are situated till it comes to that plane again, we know that we shall thus obtain a perfect coincidence between the two; but if the sides of the triangles thus joined are the chords of two spherical triangles, these triangles will, as we have seen, have all their parts equal, each to each, because, the chords being equal, the arcs must be equal, and yet it is very plain that the corresponding parts of the two triangles cannot be brought into coincidence as in plane triangles, and only in the particular case in which the two triangles are isosceles can they coincide, by being laid the one over the other. We cannot therefore, say, as in plane triangles, that two triangles, whose corresponding parts are equal, have equal surfaces, without distinct proof. This proof will be given in Part iv.

We shall add here but one more inference from the fundamental

equations (A).

6. By the first of (A) if the sides b, c, are fixed, cos. a will necessarily diminish as cos. A diminishes; that is, a will increase as A increases: hence if two triangles have two sides in the one equal to two sides in the other, but the included angle in the first greater than the included angle in the second, then the third side of the first triangle must be greater than the third side of the second.

Let us now proceed with the analytical discussion.

The three general equations above involve all the six parts of a tri-. angle, the sides, and the angles; and in order to solve them, fewer than three of these parts will be insufficient; but, knowing any three, the others may be determined from them by the usual algebraical process

of elimination; yet, as in the general formulas for the solution of plane triangles, so here, the result thus obtained would require considerable modification in certain cases to fit them for logarithmic computation, and on this account it is better to deduce particular formulas by a less direct process. Thus, in order to ascertain the relation between the sides and opposite angles of a spherical triangle, we proceed as follows.

(46.) From the equation (A),
$$\cos A = \frac{\cos a - \cos b \cos c}{\sin b \sin c}$$
... (1)

$$\therefore \sin. A = \sqrt{1 - \cos^2 A} = \frac{\sqrt{\sin^2 b \sin^2 c - (\cos. a - \cos. b \cos. c)^2}}{\sin. b \sin. c}$$
or since $\sin^2 b \sin^2 c - (1 - \cos^2 b)(1 - \cos^2 c)$

or, since sin. * $b \sin$. * $c = (1 - \cos$. * $b) (1 - \cos$. * c)

$$\sin A = \frac{\sqrt{1 - \cos^2 a - \cos^2 b - \cos^2 c + 2\cos a \cos b \cos c}}{\sin b \sin c}.$$
 (2)

$$\therefore \frac{\sin. A}{\sin. a} = \frac{\sqrt{1 - \cos. 2a - \cos. 2b - \cos. 2c + 2\cos. a\cos. b\cos. c}}{\sin. a\sin. b\sin. c}$$

Now the second side of this equation is plainly of such a form, that, however we interchange the quantities a, b, c, the value of the expression remains unaltered; so that if we had set out with cos. B, as given by the second of (A), instead of with cos. A, we should have had the

very same result for
$$\frac{\sin B}{\sin b}$$
; hence $\frac{\sin A}{\sin a} = \frac{\sin B}{\sin b} = \frac{\sin C}{\sin c}$(3). that is, in any spherical triangle the sines of the sides are to each other as the sines of the opposite angles; so that when two of the three given quantities are a side and its opposite angle, the unknown, which is

opposite to the third given quantity, may be determined by a simple

proportion, or by an easy logarithmic process.

(47.) The equation (2) above might serve to find an angle, from knowing the three sides; it is, however, much less simple than the original expression (1), but neither of them are adapted to logarithms.

In order to obtain one that is adapted, add 1 to each member of (1) and there results (form 24, p. 38), $1 + \cos A = 2 \cos^2 A$ and there results (som 24, p. 38), $1 + \cos A = 2 \cos^2 A$ and $1 + \cos A = 2 \cos A = \cos A$

$$= \frac{\cos a + \sin b \sin c - \cos b \cos c}{\sin b \sin c} = \frac{\cos a - \cos (b + c)}{\sin b \sin c}$$

but a and b+c are respectively the difference and sum of the two arcs $\frac{1}{2}(a+b+c)$, and $\frac{1}{2}(b+c-a)$; hence (form 4, p. 32), cos. $a-\cos(b+c)=2\sin\frac{1}{2}(a+b+c)\sin\frac{1}{2}(b+c-a)$; therefore, putting 8 for the sum of the three sides, we have

$$\cos \frac{1}{2} A = \sqrt{\frac{\sin \frac{1}{2} S \sin \left(\frac{1}{2} S - a \right)}{\sin b \sin a}} . . . (1).$$

If instead of adding 1 to each side of (1) art. 46 we subtract each side from 1, and proceed as above, we shall obtain for sin. A the value,

$$\sin \frac{1}{4} A = \sqrt{\frac{\sin (\frac{1}{4}S - b)\sin (\frac{1}{4}S - c)}{\sin b \sin c}} (2)$$

and, by dividing this equation by the former, we have

$$\tan \frac{1}{2} A = \sqrt{\frac{\sin \left(\frac{1}{2} S - b\right) \sin \left(\frac{1}{2} S - c\right)}{\sin \frac{1}{2} S \sin \left(\frac{1}{2} S - a\right)}}....(3)$$

and all these expressions are adapted to logarithms.

It is unnecessary to put down the corresponding expressions for the other angles, as they may be obtained from these by simply changing the letters: thus for sin. ‡ B, we have, by changing A for B and b for a

in (2), the formula
$$\sin \cdot \frac{1}{2}B = \int \frac{\sin \cdot (\frac{1}{2}S - a)\sin \cdot (\frac{1}{2}S - c)}{\sin \cdot a \sin \cdot c}$$
,

whence $\frac{\sin \cdot \frac{1}{4} A}{\sin \cdot \frac{1}{4} B} = \sqrt{\frac{\sin \cdot a \sin \cdot (\frac{1}{4} S - b)}{\sin \cdot b \sin \cdot (\frac{1}{4} S - a)}}$

from which it appears that if a > b, sin. $\downarrow A > \sin \cdot \downarrow B$, and therefore A > B; also if b > a, sin. $\downarrow B > \sin \cdot \downarrow A$; and therefore B > A. Consequently the greater side is always opposite to the greater angle,

If b = c, the equation (2) becomes $\sin \frac{1}{2} A = \frac{\sin \frac{1}{2} a}{\sin b}$

(48.) We have thus got convenient formulas for the determination of the unknown parts, when two sides and an opposite angle are given, when two angles and an opposite side are given, and when all the three sides are given. We shall now seek the solution to the case in which two sides and the included angle are given, or two angles and the interjacent side; that is to say, we shall proceed to deduce an equation involving only the four quantities a,b,A and C.

For cos. on the first of equations (A) substitute its value, as given

For cos. c in the first of equations (A) substitute its value, as given by the third, and there results, after putting $1 - \sin^2 b$, for its equal $\cos^2 b$, $\cos a = \cos a - \cos a \sin^2 b + \sin a \sin b \cos b \cos C + \sin c \cos A$; or cancelling $\cos a$ on each side, dividing by $\sin b$, and transposing, $\cos a \sin b = \sin a \cos b \cos C + \sin c \cos A$. (1). For $\sin c$ in this equation substitute its value given by (3, p. 49), viz.

 $\sin a = \frac{\sin a \sin C}{\sin A}$; and it becomes $\cos a \sin b = \sin a \cos b \cos C$

 $+\frac{\sin a \sin C \cos A}{\sin A}$ that is dividing by sin. a,

cot. $a \sin b = \cos b \cos C + \sin C \cot A$; which is the equation we proposed to deduce, and from which we at once get an expression for cot. A, when the two sides a, b, and their included angle C, are given, or for cot. a when the two angles A, C, and interjacent side b are given. The remaining parts of the triangle may, obviously, be found by the relation (p.49) between the sides and opposite angles; but if the third side, in terms of the other two, and the included angle, is required in a single formula, we must then recur to the fundamental equations (A), which obviously furnish that formula. But neither this nor that which we have just deduced are calculable by a single logarithmic operation; by the introduction, however, of a subsidiary are the solution may be conducted by logarithms, although two operations will be necessary. But we shall explain this artifice in the next chapter, which will contain the practical application of the formulas deduced in this.

(49.) It now only remains for us to furnish a formula for the side of a spherical triangle in terms of the three angles, and this we may easily do by help of the formulas already given for an angle in terms of the sides, availing ourselves of the property of the supplemental triangle, viz. that the angles and sides of this are supplements of the sides and angles of the former (41). For let the formulas (47) refer to the supplemental triangle of that in question, then, by marking the letters of the former with an accent for distinction sake we have $A' = 180^{\circ} - 4$.

the former with an accent for distinction sake we have $A' = 180^{\circ} - a$, $a' = 180^{\circ} - A$, $b' = 180^{\circ} - B$, $c' = 180^{\circ} - C$, $S' = 540^{\circ} - S$; S' being the sum of the sides of the triangle in (47), and S the sum of the angles of the triangle with which we are now occupied. Consequently, $\cos \frac{1}{4}A' = \cos .90^{\circ} - \frac{1}{4}a) = \sin .\frac{1}{4}a$, $\sin .b' = \sin .(180^{\circ} - B) = \sin .B$ $\sin .c' = \sin .(180^{\circ} - C) = \sin .C$, $\sin .\frac{1}{4}S' = \sin .(270^{\circ} - \frac{1}{4}S) = -\cos .\frac{1}{4}S$; $\sin .(\frac{1}{4}S' - a') = \sin .[90^{\circ} - (\frac{1}{4}S - A)] = \cos .(\frac{1}{4}S - A)$; therefore by substituting these values the formula (2) becomes

$$\sin \frac{1}{4}a = \sqrt{\frac{-\cos \frac{1}{4} S \cos (\frac{1}{4} S - A)}{\sin B \sin C}};$$

and the other two become $\cos \frac{1}{2}a = \int \frac{\cos (\frac{1}{2}S - B)\cos (\frac{1}{2}S - C)}{\cos (\frac{1}{2}S - C)}$ sin. B sin. C

 $\tan A = \sqrt{\frac{-\cos A}{\cos (A - B)} \cos (A - B)}$

As 1 S exceeds 90° but falls short of 270° art. (42), cos. 1 S is always negative, and, therefore, the numerators, of the first and third of these expressions although appearing with a negative sign, are in reality, positive

(50.) By means of the polar triangle it is obvious that we may, in all cases as well as in this, convert any formula involving the sides and angles of a triangle into another, similarly involving the angles and sides; the sides in the one formula being replaced by the angles opposite to them in the other, and the angles being replaced by the opposite To effect this change we need only write, instead of sin. and cos in the original formula, sin. and —cos. of the opposite arc, whether side or angle.

Thus the fundamental equations (A) become in this manner changed

into the following

$$\cos A = \cos a \sin B \sin C - \cos B \cos C
\cos B = \cos b \sin A \sin C - \cos A \cos C
\cos C = \cos c \sin A \sin B - \cos A \cos B$$
... (B).

which plainly show that if the three angles of one triangle are equal to the three angles of another, the sides of the former must also be equal to those of the latter; and also that if two angles B, C, and interjacent side, a, of one triangle are respectively equal to two angles, and the interjacent side of another, the remaining angle A of the one must be equal to the remaining angle of the other; and thus all parts of the one triangle are

equal severally to those of the other.

(51.) The theory now delivered is sufficient for the solution of every case of spherical triangles; but we shall add two more theorems appli-, cable to the case in which the two sides and included angles are given to find the other angles, and to that in which two angles and the inter-jacent side are given to find the other sides. These theorems have the advantage of being very simple, and are of a form easily retained in the memory. They were first given by *Lord Napier*, and are known by the name of Napier's Analogies.

By the equation (1), page 50, we have

 $\sin c \cos A = \cos a \sin b - \sin a \cos b \cos C$.

Similarly,

$$\sin c \cos B = \cos b \sin a - \sin b \cos a \cos C$$

$$\therefore \sin c (\cos A + \cos B) = \sin (a + b) (1 - \cos C) (1).$$
Now from the equations (3) page 49, we have

Now from the equations (3), page 49, we have \sin . A \sin . $c = \sin$. a \sin . C

$$sin. B sin. c = sin. b sin. C$$

$$c. B) sin. c = (sin. a + sin. b) sin. C$$

(sin. A \pm sin. B) sin. $c = (\sin a \pm \sin b) \sin C \dots (2)$.

Dividing (2) by (1) there results

$$\frac{\sin \cdot \mathbf{A} \pm \sin \cdot \mathbf{B}}{\cos \cdot \mathbf{A} + \cos \cdot \mathbf{B}} = \frac{\sin \cdot \mathbf{a} \pm \sin \cdot \mathbf{b}}{\sin \cdot (\mathbf{a} + \mathbf{b})} \cdot \frac{\sin \cdot \mathbf{C}}{1 - \cos \cdot \mathbf{C}}$$

that is, arts. (32) and (31) taking the upper and lower signs separately.

$$\tan \cdot \frac{1}{2} (A + B) = \frac{\cos \cdot \frac{1}{2} (a - b)}{\cos \cdot \frac{1}{2} (a + b)} \cot \cdot \frac{1}{2} C$$

$$\tan \cdot \frac{1}{2} (A - B) = \frac{\sin \cdot \frac{1}{2} (a - b)}{\sin \cdot \frac{1}{2} (a + b)} \cot \cdot \frac{1}{2} C.$$

For the supplemental triangle the corresponding formulas are tan. $\frac{1}{2}(a+b) = \frac{\cos \frac{1}{2}(A-B)}{\cos \frac{1}{2}(A+B)} \tan \frac{1}{2}c$

$$\tan \frac{1}{a}(a+b) = \frac{\cos \frac{1}{a}(A-B)}{\cos \frac{1}{a}(A+B)} \tan \frac{1}{a}$$

 $tan. \frac{1}{2} (a - b) = \frac{\sin \frac{1}{2} (A + B)}{\sin \frac{1}{2} (A + B)}$ tan. 1 c; and these are the four equations which furnish the Analogies of Napier, viz.

cos.
$$\frac{1}{2}(a+b)$$
: cos. $\frac{1}{2}(a-b)$:: cot. $\frac{1}{2}$ C: tan $\frac{1}{2}(A+B)$ sin. $\frac{1}{2}(a+b)$: sin. $\frac{1}{2}(a-b)$:: cot. $\frac{1}{2}$ C: tan. $\frac{1}{2}(A-B)$

$$\begin{array}{l} \cos \frac{1}{4}(A+B) : \cos \frac{1}{4}(A-B) : : \tan \frac{1}{4}c : \tan \frac{1}{4}(a+b) \\ \sin \frac{1}{4}(A+B) : \sin \frac{1}{4}(A-B) : : \tan \frac{1}{4}c : \tan \frac{1}{4}(a-b) \end{array}$$
 (3)

As the arcs $\frac{1}{2}(a-b)$, and $\frac{1}{2}$ C, are always less than 90°, the two means in the first of these analogies are positive, and, therefore, the two extremes must have the same signs, that is, they must either be both positive or both negative: hence $\frac{1}{2}(a+b)$, and $\frac{1}{2}(A+B)$, must either be both acute or both obtuse, and consequently the arcs a+b. A + B, must be either both less or both greater than 180°. From this circumstance we may always avoid doubtful solutions to the cases in which the given parts are two sides and an opposite angle, or two angles and an opposite side, as will be exemplified in next chapter.

CHAPTER III.

SOLUTIONS OF THE DIFFERENT CASES OF SPHERICAL TRIANGLES.

(52.) WE are now to show the application of the preceding theory to the actual determination of any of the six parts of a spherical triangle when three of them are known; and as in Plane Trigonometry, so here, we shall find it convenient to begin with right-angled triangles.

Right-Angled Spherical Triangles.

The formulas for which all the rules for right-angled triangles are derived are those marked (A), (B), and 3, (p. 49), in the preceding sin. C

chapter, viz.
$$\frac{\sin A}{\sin a} = \frac{\sin B}{\sin b} = \frac{\sin C}{\sin c}$$
. (1)

$$\cos A = \cos a \sin B \sin C - \cos B \cos C$$

 $\cos B = \cos b \sin A \sin C - \cos A \cos C$
 $\cos C = \cos c \sin A \sin B - \cos A \cos B$

cos.
$$a = \cos b \cos c + \sin b \sin c \cos A$$

cos. $b = \cos a \cos c + \sin a \sin c \cos B$
cos. $c = \cos a \cos b + \sin a \sin b \cos C$

Let ABC be a spherical triangle, right-angled at C; then from the first of these formulas we have, since $\sin C = 1$, the equations

 $\sin a = \sin c \sin A$, $\sin b = \sin c \sin B$. (4). Two different expressions for sin. a, sin. b, may also be obtained from the first and second of (2).

Thus C being 90° these two equations give cos. $A = \cos$. ϵ sin. B, cos. $B = \cos$. δ sin. A . (5); substituting in these the values of sin. A. sin. B, as deduced from (1) they become

$$\cos A = \frac{\cos a}{\sin a} \sin A \sin b, \cos B = \frac{\cos b}{\sin b} \sin B \sin a$$

 \therefore sin. $b = \tan a \cot A$, sin. $a = \tan b \cot B$. For the hypotenuse c we get from the third of (2) the expression

$$\cos c = \frac{\cos A \cos B}{\sin A \sin B} = \cot A \cot B,$$

and from the third of (3) the expression $\cos c = \cos a \cos b$. In the equations (5) substitute for sin. A, sin. B, their values in (4), and for cos. a, cos. b, their values in (6), and they then take the form

cos. $A = \tan b \cot c$, cos. $B = \tan a \cot c$. Collecting together all these equations, we have $\sin a = \tan b \cot B = \sin c \sin A$ $\sin b = \tan a \cot A = \sin c \sin B$ $\cos c = \cot A \cot B = \cos a \cos b$ $\cos A = \tan b \cot c = \cos a \sin B$

 $\cos B = \tan a \cot c = \cos b \sin A;$ and these furnish solutions to every possible case of right-angled triangles; for it is plain that whichever two of the five quantities a. b, c, A, B, are given, any one of the others may be immediately found by one or other of these equations. Instead, however, of deducing from these five equations so many distinct rules for the solution of the various cases, the whole, by help of an ingenious contrivance, may be comprehended in two rules of very remarkable simplicity.

Before announcing these rules we shall, however, just stop to mention an inference from the first of this group of equations which will be useful hereafter, viz. that from any point on a sphere to a given great circle the shortest great circle are that can be drawn is the perpendicular; for by the equation referred to sin. a exceeds sin. c, since sin. A is less than If the point is the pole of the proposed great circle, then, indeed, (p. 43) $\sin a = \sin c$, and $\sin A = 1$, all great circle arcs from the point to the circle being perpendicular. From the last of the preceding equations we infer that cos. B, cos. b, always have the same sign, that is, either side is of the same affection as its opposite angle. From the middle equation we see that the hypotenuse is acute if the sides are of the same affection, or if the angles opposite to them are of the same affection, but otherwise the hypotenuse is obtuse.

The rules to which we have adverted above were invented by Baron Napier, the celebrated inventor of logarithms, and are called Napier's Rules for the Circular Parts. We shall now explain them.

In a right-angled triangle we are to recognise but five parts, viz. the three sides and the two angles A and B. If we take any one of these as a middle part, the two which lie next to it, one on each side will be adjacent parts: thus taking A for a middle part (last fig.), b and c will be the adjacent parts; if we take c for the middle part, A and B will be the adjacent parts; if we take B for the middle part, c and a will be the adjacent parts; but if we take a for the middle part, then, as the part C is not recognised we do not consider it as intervening between a and b, and, therefore, we call in this case B and b, the adjacent parts; and, lastly, if b is the middle part then the adjacent parts are A and a. The two parts immediately beyond the adjacent parts, one on each side, still disregarding the right-angle, are called the opposite parts; thus if A is the middle part the opposite parts are a, next to the adjacent part b, and b next to the adjacent part c. This being understood, Napier's two rules may be expressed as follows, carefully observing to use the complements of the two angles and of the intervening hypotenuse instead of these parts themselves.

Rad. X sin. middle part = product of tan. adjacent parts.
 Rad. X sin. middle part = product of cos. opposite parts.

Both these rules may be comprehended in a single expression, thus

rad. sin. mid. = prod. tan. adja. = prod. cos. opp.; and to retain this in the memory we have only to remember that the vowels in the contractions mid., adja., opp., are the same as those in the contractions sin., tan., cos., to which they are joined.

That these rules comprehend all the equations given above will be seen by taking a, b, c, &c. in succession for the middle part, as in the subjoined table, keeping in mind the condition just stated, that instead of A, B, and c, we are to use their complements.

Middle part.	Adjacent parts.	Opposite parts.
(sin.)	(tan.)	(cos.)
a.	b, comp. B	comp. c, comp. A
b .	a, comp. A	comp. c, comp. B
comp. c	comp. A, comp. B	a, b
comp. A	b, comp. c	a, comp. B
comp. B	a, comp. c	b, comp. A

As in the solution of right-angled triangles two parts are given tofind a third, we must in the application of Napier's rule choose for the middle of these three parts that which causes the other two to become either adjacent parts or opposite parts.

EXAMPLES.

(53.) 1. In the right-angled triangle ABC are given the two perpendicular sides, viz. $a=48^{\circ}$ 24′ 16″, $b=59^{\circ}$ 38′ 27″, to find the hypotenuse c.

Here the hypotenuse being made the middle part the other two will, obviously, be the opposite parts, being separated from the hypotenuse by the intervening angles A, B. Hence by the rule

 $rad \times sin. comp. c = cos. a \times cos. b$;

that is, rad. $\cos c = \cos a \cos b \cdot \cos c = \frac{\cos a \cos b}{\text{rad.}}$; and as $\cos a$, $\cos b$, are both positive, $\cos c$ is positive, and, therefore, c is acute.

2. In the spherical triangle ABC, right-angled at C, are given $b = 46^{\circ} 18' 23''$, $A = 34^{\circ} 27' 39''$, to find the other oblique angle B.

Making B the middle part, the other two will be the opposite parts. Consequently, by the rule, rad. \times sin. comp. B = cos. $b \times$ cos. comp. A; that is, rad. cos. B = cos. b sin. A \therefore cos. B = $\frac{\cos b}{\text{rad.}}$;

and as cos b, sin. A, are both positive, B is acute,

3. In the spherical triangle, right-angled at C, are given the two per pendicular sides, viz. $a=116^{\circ}$ 30′ 43″, $b=29^{\circ}$ 41′ 32″, to find the angle A.

Making b the middle part, the others will be the adjacent parts, and, therefore, by the rule rad. $\times \sin b = \tan a \times \tan c$

that is, rad. $\sin b = \tan a \cot A \cdot \cot A = \frac{\operatorname{rad. sin. } b}{\tan a}$; and as $\sin b = \cos b \cot a$ positive, and $\tan a$ negative, $\cot A$ will be negative, and, therefore, A will be obtuse, or the supplement of the angle given by the tables,

cot. A 103 52 48 . 9:3928670.

4. In a spherical triangle, right-angled at C, are given $b=29^\circ$ 12'50", and $B=37^\circ$ 26' 21", to find the side a.

Taking a for the middle part, the other two will be adjacent parts; hence, by the rule, rad. \times sin. $a = \tan b \times \tan \cos B$

that is, rad. $\sin a = \tan b \cot B : \sin a = \frac{\tan b \cot B}{\text{rad.}}$

In this case there are two solutions, viz. a and the supplement of a, both of which have the same sine. As sin. a is necessarily positive, b and B must necessarily be always of the same species, that is, either both acute or both obtuse, so that, as observed at p. 53, the sides including the right-angle are always of the same species as the opp. angles, a circumstance which must be attended to in framing examples.

sin. a 46° 55′ 2′ or 133° 4′ 58″ . 9.8635411.

It appears, therefore, that there exists two right-angled priangles, having an oblique angle, and the opposite side in one equal to an oblique angle and the opposite side in the other, but the remaining oblique angle in the one the supplement of the remaining oblique angle in the other. These triangles are situated, with respect to each other, on the sphere, as the triangles ABC, AB'C, in the annexed diagram, in which, with the exception of the common side,

diagram, in which, with the exception of the common side, AC, and the equal angles B, B', the parts of the one triangle are supplements of the corresponding parts of the other.

5. Given the angle $A = 23^{\circ}$ 28', the side $b = 49^{\circ}$ 17', to find the hypotenuse c. $c = 51^{\circ}$ 42' 37''.

tenuse c. $c = 51^{\circ} 42' 37''$. 6. Given the hypotenuse $c = 66^{\circ} 32'$, the side $a = 37^{\circ} 48'$, to find the angle B. $B = 70^{\circ} 19' 18''$.

7. Given the perpendicular sides $a = 59^{\circ}$ 38' 27", $b = 48^{\circ}$ 24' 16". to find all the other parts. $c = 70^{\circ}$ 23' 42", $A = 66^{\circ}$ 20' 40", $B = 52^{\circ}$ 32' 55". 8. Given $b = 121^{\circ}$ 26' 25", and the opposite angle $B = 111^{\circ}$ 14' 37", to find all the other parts.

Solution of Quadrantal Triangles.

(54.) The rules for right-angled triangles will serve also for the solution of quadrantal triangles, or those in which one side is a quadrant. For by changing such a triangle for its supplemental triangle, we shall then have to consider a right-angled triangle, of which the hypotenuse will be the supplement of the angle opposite the quadrantal side, the two perpendicular sides supplements of the other two angles of the proposed triangle, and the two oblique angles of the new triangle supplements of the oblique sides of the primitive or quadrantal triangle being a, b, and $c = 90^{\circ}$ and its angles A, B, c, the sides of the supplemental triangle will be $180^{\circ} - A$, $180^{\circ} - B$, and $180^{\circ} - C$, this latter being the hypotenuse; and the opposite angles will be $190^{\circ} - a$, $180^{\circ} - b$, and 90° . But the parts of a quadrantal triangle may be determined without the aid of the supplemental triangle. Thus let AD be the quadrantal side in the triangle ABD. Produce ABD. Produce ABD. The ABD is necessary, till ABD becomes a quadrant, and draw the ABD.

let AD be the quadrantal side in the triangle ABD. Produce DB, if necessary, till DC becomes a quadrant, and draw the arc AC, which will, obviously, measure the angle D, since D will be the pole of the arc AC, and C will be a right angle: also the angle CAB will be the complement of the angle BAD in the proposed triangle, and the angle ABC will either be identical with ABD in the proposed, or supplemental to it, accordingly as DC exceeds, or falls short of, a quadrant; hence all the parts of the proposed triangle are easily determined from those of the right-angled triangle ABC.

If the angle DAB is less than 90°, or than the angle DAC, the side DB must, obviously, be acute; but if DAB is greater than 90°, DB will be obtuse, and conversely. Hence the angles adjacent to the quadrantal side are of the same species as the sides opposite to them. The same

may be inferred from the polar triangle.

It must be remarked that the solution will be ambiguous whenever the determination of the right-angled triangle becomes ambiguous, whether we employ the polar triangle or the triangle ABC in the above diagram. This ambiguity occurs only when the given parts in the right-angled triangle are one of the perpendicular sides and the angle opposite to it. (See solution, p. 54.)

EXAMPLES.

In the triangle DAB, DA = 90°, A = 54° 43′, and D = 42° 12′, required the other parts.

As the angle DAB is less than 90°, that is, less than the angle DAC, DB is less than a quadrant, and the angle DAC, DB is less than a quadrant, and the angle DAC. and, therefore, the right-angled triangle ABC is situated as in the figure, BC being the prolongation of DB. Of the parts of this right-angled triangle we have given $A = 90^{\circ} - 54^{\circ} 43^{\circ} = 35^{\circ} 17^{\circ}$, and b =

42° 12′, to find the other parts.

Let A be the middle part, then b and c will be adjacent parts, therefore, rad. \times sin. comp. A =

tan. $b \times \tan$. comp. c,

D

that is, rad. cos. A =	tan. b cot. c	∴ cot. c =	tan. b	
rad. cot. A tan. b	35° 17′ 42 12		-	10·0000000 9·9118528 9·9574850
cot e	480 N Q	,,		9-9543678

Let B be the middle part, then A, b, will be opposite parts, and, consequently, rad. \times sin. comp. B = cos. b \times cos. comp. A;

that is, rad. cos. B = cos. b sin. A \therefore cos. B = $\frac{\cos b \sin A}{\sin A}$

rad. cos. b sin. A	42° 12′ 35 17				10·0000000 9·8697037 9·7616424
cos B	640 30/ 55	"	_	_	0-6313461

hence the angle ABD is 115° 20' 5"

It remains now to find a; let, therefore, B be the middle part, then a and c will be the adjacent parts; hence

rad. \times sin. comp. $B = \tan a \times \tan c$

rad. cos. B that is, rad. cos. $B = \tan a \cot c \therefore \tan a =$ ant e

rad.	-			_	-	10.0000000
cos. B			-	•	-	9.6313461
cot. c	-	-	-	-	-	9.9543678
ton o	O.	(a or, ow)				0.6760700

tan. a 25° 25′ 20′′

therefore, the side DB, which is the complement of this, is 64° 34′ 40″. 2. In the triangle DAB, DA = 90° , A = $112^{\circ} 2' 9''$, and AB = 67° 3' 14", to find the other parts.

Since in this example A is obtuse, DB is obtuse.

In the right-angled triangle ABC we have $A = 220^{\circ}$ 2' and AB = 67° 3' 14"; let A be the middle part, then AB, AC, will be adjacent parts, and we shall have

rad. \times sin. comp. $A = \tan b \times \tan \cdot \operatorname{comp} \cdot c$; that is, rad. $\cos A = \tan b \cot c$

therefore, the angle $D = 65^{\circ} 27' 9''$. Take now a for the middle part, then A and c will be opposite parts;

hence rad. \times sin. $a = \cos$. comp. $A \times \cos$. comp. c, sin. A sin. c that is rad. sin. $a = \sin A \sin c : \sin a =$ rad.

and a will be acute, because the opposite angle is acute

therefore BD = 110° 12' 44".

As we have now to find B, take a for the middle part, then b and B will be adjacent parts, therefore, rad. $\times \sin a = \tan b \tan \cosh B$; rad. sin. a.

that is, rad. $\sin a = \tan b \cot B \cdot \cot B =$ tan. b rad. 10.0000000 sin. 4

9.5384463 tan. b 10.3403408 cot. B 81° 1′ 58" 9.1981055.

- 3. Given the quadrantal side and the other two sides equal to 22° 53′ 30″, and 51° 4′ 35″, to find the angle opposite to the quadrantal side.
- $B = 70^{\circ} 3' 44''$ 4. In the quadrantal triangle ADB are given D = 69° 13′ 46", and $A = 72^{\circ} 12^{\circ} 4^{\circ\prime}$, to determine the other parts. $AB = 70^{\circ} 8' 39'', BD = 73^{\circ} 17' 29'', B = 96^{\circ} 13' 23''.$

These examples will suffice for the present, to show the application of Napier's rules to the solution of right-angled and quadrantal triangles. We shall, therefore, now give examples of the solution of the various cases of oblique-angled triangles in general.

Solution of Oblique Angled Spherical Triangles.

- (55.) The fundamental equations (A) show that in order to determine the several parts of a spherical triangle, three of those parts must be previously given. Now, three parts out of the six can be combined only in these different ways, viz.
 - 1. The three sides.
 - 2. The three angles.
 - 3. Two sides and the included angle.
 - 4. Two angles and the interjacent side.
 - 5. Two sides and an opposite angle.6. Two angles and an opposite side.

So that the complete solution of an oblique-angled spherical triangle presents six cases. These we shall solve in the order in which they are here enumerated.

CASE 1. (56.) Given the three sides to find the angles.

For the determination of any angle A we have by (47) the three following different expressions, viz.

$$\sin \cdot \frac{1}{4} A = \sqrt{\frac{\sin \cdot (\frac{1}{4} S - b) \sin \cdot (\frac{1}{4} S - c)}{\sin \cdot b \sin \cdot c}}$$

$$\cos \cdot \frac{1}{4} A = \sqrt{\frac{\sin \cdot \frac{1}{4} S \sin \cdot (\frac{1}{4} S - a)}{\sin \cdot b \sin \cdot c}}$$

$$\tan \cdot \frac{1}{4} A = \sqrt{\frac{\sin \cdot (\frac{1}{4} S - b) \sin \cdot (\frac{1}{4} S - c)}{\sin \cdot \frac{1}{4} S \sin \cdot (\frac{1}{4} S - a)}}$$

We may apply to these formulas the remarks made at (21) in the Plane Trigonometry. It will be sufficient to observe here that the first formula is generally the most suitable, because the angle A is rarely so large as to be very near 180°.

EXAMPLES.

sin. b 43 37 38 arith. comp. 0.1611739

1. In an oblique spherical triangle the three sides are $a = 68^{\circ}$ 46' 2" $b = 43^{\circ}$ 37' 38", $c = 37^{\circ}$ 10'; required the angle A. $a = 68^{\circ}$ 46' 2"

sin.
$$c$$
 37 10 0 arith. comp. 0·2188656

2)149 33 40

74 46 50

sin. ($\frac{1}{2}$ S - b) 31 9 12 - 9·7137678

sin. ($\frac{1}{2}$ S - c) 37 36 50 - 9·7855698

2)19·8793771

sin. $\frac{1}{2}$ A 60 29 53 - 9·9396885

 \therefore A = 120° 59′ 46″.

2. Given $a = 108°$, $b = 52°$ 12′, and $c = 74°$ 30′, to find A.

a 108° 0′

sin. b 37 48 arith. comp. 0·2126054

sin. c 74 30 arith. comp. 0·0160895

2)220 18

110 9

sin. ($\frac{1}{2}$ S - b) 72 21 - 9·9790594

sin. ($\frac{1}{2}$ S - c) 35 39 - 9·7655436

2)19·9732979

sin. $\frac{1}{2}$ A 75 51 56 - 9·9866489

3. Given $a = 70^{\circ}$ 4' 18", $b = 63^{\circ}$ 21' 27", and $c = 59^{\circ}$ 16' 23", to find the angles A and B.

A = 81° 38' 20", B = 70° 9' 38".

4. Given $a = 67^{\circ}$ 25' 2", $b = 80^{\circ}$ 2' 25", $c = 23^{\circ}$ 27' 46", to find the angle A.

A = 54° 55' 19".

5. Given $a = 61^{\circ}$ 32' 12", $b = 83^{\circ}$ 19' 42", $c = 23^{\circ}$ 27' 46", to find A. $A = 20^{\circ}$ 39' 48"

1

CASE II. (57.) Given the three angles to find the sides.

By (49) we have the following formulas for any side a in terms of the

three angles, viz.
$$\sin \cdot \frac{1}{4} = \sqrt{\frac{-\cos \cdot \frac{1}{4} \cdot 8 \cos \cdot (\frac{1}{4} \cdot 8 - A)}{\sin \cdot B \cdot \sin \cdot C}}$$

 $\cos \cdot \frac{1}{4} \cdot a = \sqrt{\frac{\cos \cdot (\frac{1}{4} \cdot 8 - B) \cos \cdot (\frac{1}{4} \cdot 8 - C)}{\sin \cdot B \cdot \sin \cdot C}}$
 $\tan \cdot \frac{1}{4} \cdot a = \sqrt{\frac{-\cos \cdot \frac{1}{4} \cdot 8 \cos \cdot (\frac{1}{4} \cdot 8 - A)}{\cos \cdot (\frac{1}{4} \cdot 8 - B) \cos \cdot (\frac{1}{4} \cdot 8 - C)}}$

It may be remarked here that the first two only of the expressions in this and in the former case need be berne in the memory, as the third is an immediate consequence of them. If the expressions in the former case be recollected, these can scarcely fail to be recalled at the same time, as they differ from them only in this, viz. that the sides are replaced by their opposite angles, and, except in the denominators, cosines are written for sines, and sines for cosines.

EXAMPLES.

l. The three angles of a spherical triangle are, $A=130^{\circ}$ 3′ 11″, $B=31^{\circ}$ 34′ 26″, $C=30^{\circ}$ 28′ 12″, required the side a.

A 130° 3′ 11″

sin. B: 31 34 26 arith.comp. 0.2810023 sin. C 30 28 12 arith.comp. 0.2949174

- 2. The three angles of a spherical triangle are, $A = 103^{\circ}$ 59' 57", $B = 46^{\circ}$ 18' 7", $C = 36^{\circ}$ 7' 52"; required the side a.
- 3. The three angles of a spherical triangle are 120° 43′ 37″, 109° 55′ 42″, and 116° 38′ 33′; required the three sides.

 115° 13′ 26″, 98° 21′ 40″, and 109° 50′ 22.″

Case III. (58.) Given two sides a, b, and the included angle C, to find the other parts. By Napier's analogies,

$$\cos \frac{1}{2}(a+b) : \cos \frac{1}{2}(a-b) : \cot \frac{1}{2}C : \tan \frac{1}{2}(A+B) \sin \frac{1}{2}(a+b) : \sin \frac{1}{2}(a-b) : \cot \frac{1}{2}C : \tan \frac{1}{2}(A-B).$$

These serve to determine the angles A, B, opposite to the given sides; after which the third side c may be determined by either of the remaining two analogies of Napier, viz.

$$\cos \frac{1}{2}(A + B) : \cos \frac{1}{2}(A \sim B) :: \tan \frac{1}{2}c : \tan \frac{1}{2}(a + b)$$

 $\sin \frac{1}{2}(A + B) : \sin \frac{1}{2}(A \sim B) :: \tan \frac{1}{2}c : \tan \frac{1}{2}(a - b)$.

EXAMPLES.

1. In a spherical triangle are given $a=38^{\circ}30'$, $b=70^{\circ}$, and $C=31^{\circ}34'$ 26'', to find the other parts.

1 To find A and B.

cos. $\frac{1}{2}$ (a + b) 54° 15'ar. comp. 0.2334015 ar. comp. sin. cos. $\frac{1}{2}$ (a - b) 15 45 . 9.9833805 sin. cot. $\frac{1}{2}$ C 15 47 13 10.5486359

0-0906719 9-4336746 10-5486358

 $\tan \frac{1}{4}(A+B)80$ 15 41 10.7654172, $\tan \frac{1}{4}(A-B)$ 49° 47' 30" 10.0729817 $\frac{1}{4}(A+B)$ must be acute, because $\frac{1}{4}(a+b)$ is acute.

By taking the sum and difference of these results we have, $B = 130^{\circ}$ 3' 11", and $A = 30^{\circ}$ 28' 11".

n. To find c.

cos.
$$\frac{1}{4}$$
 (A ~ B) 49° 47′ 30″ arith. comp. 0·1900575 cos. $\frac{1}{4}$ (A + B) 80 15 41 . . . 9·2282812 tan. $\frac{1}{4}$ (a + b) 54 15 0* 9·5610683 cos. c = 40° 0′ 0″.

When in the case we are considering, the only part required happens to be the side opposite the given angle, the finding of the other two angles then becomes merely a subsidiary operation, and the determination of the required side, by Napier's analogies, seems somewhat lengthy. But a shorter method of solution is deducible from the fundamental formula, $\cos c = \cos a \cos b + \sin a \sin b \cos C$. (1).

For substituting cos. $a \tan a$ for its equal sin. a it becomes $\cos a = \cos a (\cos b + \tan a \sin b \cos C)$.

Assume tan.
$$a \cos C = \cot \omega = \frac{\cos \omega}{\sin \omega}$$
;

then
$$\cos c = \cos a \frac{\sin \omega \cos b + \sin b \cos \omega}{\sin \omega} = \frac{\cos a \sin (\omega + b)}{\sin \omega}$$

Hence, to find the side c, we must first determine a subsidiary angle ω from the equation cot. $\omega = \tan a \cos C$. (2); after which c is found by the equation $\cos c = \frac{\cos a \sin (\omega + b)}{\sin \omega}$ - - (3).

2. The same parts being given as in the last example, to determine == by these formulas,

by these formulas, tan.
$$a$$
 38° 30′ 0′′. 9.9006052, cos. a . 9.8935444 cos. C 31 34 26 . 9.9304221, sin. ω , ar. comp. 0.0620652 cot. ω 55 52 304 . 9.8310273, sin. (ω + b) 9.9086437 cos. ε 40° . 9.8842533.

Other formulas for the determination of c might be easily deduced from the same equation (1), but this is as short and as convenient as any. We might also introduce here a distinct formula for the determination of one of the angles A, by help of a subsidiary arc ω ; but as little or nothing would be gained, in point of brevity, over the process by Napier's analogies, we shall not stop to investigate it.

^{*} There will be no necessity to refer to the tables for the tangent of this arc, we shall obtain it by subtracting the right-hand arithmetical complement in the preceding logarithmic process from that on the left, adding 10 to the index. For calling the right-hand complement p, and the left q, and recollecting that \log tan. = $10 + \log$ sin. — \log cos. = 10 + (10 - p) - (10 - q), we have \log tan. = 10 + q - p.

3. In a spherical triangle are given $a = 43^{\circ}$ 37' 38", $b = 37^{\circ}$ 10', c = 68° 46' 2". $C = 120^{\circ} 53^{\circ} 46^{\circ\prime}$, to find the side c.

4. In a spherical triangle are given the two sides, equal to 37° 10' and 68° 46' 2', and the included angle equal to 39° 23'; required the other two angles.

33° 45' 3' and 120° 59' 49". two angles.

5. Given the two sides equal to 44° 13' 45" and 84° 14' 29", and the

included angle equal to 36° 45' 28"; to find the other parts.

The angles are 32° 26' 6", and 130° 5' 22", and the side 51° 6' 12".

CABE IV. (59.) Given two angles A, B, and the interjacent side c, to find the other parts.

The solution of this case as well as the former, is comprehended in Napier's analogies; the one pair, viz.

$$\cos \cdot \frac{1}{2}(A+B) : \cos \cdot \frac{1}{2}(A-B) : \tan \cdot \frac{1}{2}c : \tan \cdot \frac{1}{2}(a+b)$$

 $\sin \cdot \frac{1}{2}(A+B) : \sin \cdot \frac{1}{2}(A-B) : \tan \cdot \frac{1}{2}c : \tan \cdot \frac{1}{2}(a-b);$
determining the unknown sides a, b , and either of the other pair, viz.

cos.
$$\frac{1}{2}(a+b)$$
: cos. $\frac{1}{2}(a-b)$:: cot. $\frac{1}{2}$ C: tan. $\frac{1}{2}(A+B)$ sin. $\frac{1}{2}(a+b)$: sin. $\frac{1}{2}(a-b)$:: cot. $\frac{1}{2}$ C: tan. $\frac{1}{2}(A-B)$; enabling us to find the unknown angle C.

EXAMPLES.

1. In a spherical triangle are given two angles equal to 39° 23' and 33° 45′ 3", and the interjacent side equal to 68° 46' 2"; to find the remaining parts.

1. To find the Sides.

 $tan. \pm (a+b) 40 2349 9.9299161, \tan \frac{1}{2}(a-b)3^{\circ}13'48''8.7515426$ $\therefore a = 43^{\circ} 37' 37'', b = 37^{\circ} 10' 1''.$

II. To find the Angle.

sin.
$$\frac{1}{4}(a-b)$$
 3° 13′ 48″ arith. comp. 1°2491502 sin. $\frac{1}{4}(a+b)$ 40° 23° 49° 98116281 tan. $\frac{1}{4}(A-B)$ 2 48° 58 $\frac{1}{4}$ 8° 6918985 cot. $\frac{1}{4}$ C 60° 29° 53 9°7526768 \therefore C = 120° 59′ 46″.

If the angle opposite to the given side be the only part required, a more compendious method of solution may be obtained by introducing a subsidiary arc, as in last case. Thus the formula (B) art. (50) becomes when cos. A tan. A is substituted for sin. A, cos. $C = \cos A (\tan A \sin B \cos c - \cos B);$

CO8. ω or assuming tan. A cos. $c = \cot \omega =$

$$\cos C = \cos A \frac{\sin B \cos \omega - \sin \omega \cos B}{\sin \omega} = \frac{\cos A \sin (B - \omega)}{\sin \omega}$$

Hence, having found a subsidiary angle ω by the equation cot. ω = tan. A cos. c (1); the sought angle is determined by the equation cos. C = $\frac{\cos A \sin \cdot (B - \omega)}{\sin \omega}$ sin. a

 $^{^{\}circ}$ The log. tangent of this are will be equal to log. sin. — log. cos., before given, increased by 10.

2. The given quantities being the same as in last example, to determine the angle C.

tan. A 39° 23′ 0″ 9°9143020 cos. A 9°8881335 cos. c 68 46 2 9°5588979 sin. ω, ar. comp. 0°0183921 cot. ω 73 26 331 9°4731999 sin. (B — ω) 39° 41′ 30½″ 9°8052688

cos. 59° 0′ 13″ 9.7117938.

As $(B - \omega)$ is negative, cos. C must be negative; hence C is the supplement of this, viz. 120° 59′ 47″.

- 3. Given $A = 30^{\circ}$ 28' 11", $B = 130^{\circ}$ 3' 11", and $c = 40^{\circ}$; to determine the other parts. $a = 38^{\circ}$ 30', $b = 70^{\circ}$, and $C = 31^{\circ}$ 34' 26".
- 4. Given $A = 31^{\circ} 34' 26''$, $B = 30^{\circ} 28' 12''$, and $C = 70^{\circ} 2' 3''$; to find the angle C. $C = 130^{\circ} 3' 11''$.
- 5. Given $A = 34^{\circ}$ 15' 3", $B = 42^{\circ}$ 15' 13", and $C = 76^{\circ}$ 35' 36"; to find a and b. $a = 40^{\circ}$ 0' 10", $b = 50^{\circ}$ 10' 30".
 - 6. Given $A = 51^{\circ} 30'$, $B = 131^{\circ} 30'$, and $c = 80^{\circ} 19' 12''$; to find C. $C = 59^{\circ} 15' 59''$.

Case v. (60.) Given two sides a, b, and the angle A opposite to a; to find the other parts B, C, c.

- 1. To find the angle B we have, by (46) the proportion, $\sin a: \sin b: \sin A: \sin B.....$ (1).
- 2. To find C and c, we have, by Napier's analogies,

cos. $\frac{1}{4}(a - b)$: cos. $\frac{1}{4}(a + b)$:: tan. $\frac{1}{4}(A + B)$: cot. $\frac{1}{4}C$ cos. $\frac{1}{4}(A - B)$:: cos. $\frac{1}{4}(A + B)$:: tan. $\frac{1}{4}(a + b)$: tan. $\frac{1}{4}c$ }...(2).

Or after either C or c is found by one of these analogies, the other part may be found by the proportion sin. A: sin. C:: sin a: sin. c(3); although we shall prefer Napier's analogy to this in order that all ambiguity may be avoided.

If only one of the parts C, c, be required, then it will be best to find first the angle B, by the proportion (1), which operation must be regarded entirely as subsidiary to the determination of the required part, by one of the analogies (2). The part determined by the proportion (1) admits of a double value, since two arcs answer to the same sine; it becomes necessary, therefore, for us to inquire under what circumstances both these values are admissible, and how we may know which to choose when but one solution exists. Referring to the fundamental formula

(A), we have $\cos B = \frac{\cos b - \cos a \cos c}{\sin a \sin c}$; in which expression we

may remark that if $\cos b$ is numerically greater than either $\cos a$ or $\cos c$, the second member must take the sign of $\cos b$, consequently, B and b must be of the same species if $\sin b < \sin a$, or $\sin b < \sin b <$ that is, an angle must be of the same species as its opposite side, if the sine of this side is less than the sine of either of the other sides. But if $\cos b$ is numerically less than $\cos a$, then whether the right hand member be + or — will depend upon the magnitude of $\cos c$, or $\cos c$ will have two values corresponding to $+\cos b$, and $-\cos b$; hence an angle has two values, when the sine of its opposite side is greater than the sine of the other given side.

EXAMPLES.

1. Given the side $a = 63^{\circ}$ 50', the side $b = 80^{\circ}$ 19', and the angle $A = 51^{\circ}$ 30'; to determine the other parts.

I. To find the Angle B.

63° 50' arith. comp. 0-0469582 sin. a : sin. b 80 19 9.9937679 :: sin. A 51 30 9.8935444

: sin. B 59° 15′ 47″ - 9°9342705 The angle B admits of two values, because sin. $b > \sin a$, so that there exist two triangles, having the data proposed. We shall, however, take the acute value of B.

n. To find the Angle C.

cos.
$$\frac{1}{2}(a \sim b)$$
 8° 14′ 30″ arith. comp. 0°0045086
: cos. $\frac{1}{2}(a+b)$ 72 4 30 - 9′4882288
:: tan. $\frac{1}{2}(A+B)$ 55 22 53 - 10′1609412
: cot. $\frac{1}{2}$ C 65 44 53 - 9′6536786
∴ C = 131° 29′ 46″.

III. To find the Side c.

cos. $\frac{1}{2}$ (A \sim B)	3° 52′ 53″	arith. comp. 0.0009973
: cos. $\frac{1}{2}$ (A + B)	55 22 53	9.7544333
:: tan. $\frac{1}{2}$ (a + b)	72 4 30	10.4901618
: tan. 🛊 c	60 24 0 2	10-2455924

c = 120 48 0

2. Given $a = 40^{\circ} 36' 37''$, $b = 91^{\circ} 3' 25''$, and $A = 35^{\circ} 57' 15''$ to determine C.

1. To find the subsidiary Angle B.

sin. a : sin. b : sin. A	91	36′ 37′ 3 25 57 15	 0·1864788 9·9999261 9·7687401
: sin. B	64	24 19	 9.9551450

or 115 35 41 The angle B admits of two values, because sin. $b > \sin a$. We shall suppose the particular triangle under consideration to have B obtuse

n. To find C.

cos.
$$\frac{1}{2}(a \sim b)$$
 25° 13′ 24″ arith. comp. 0.0435177
: cos. $\frac{1}{2}(a + b)$ 65 50 1 - 9.6121350
:: tan. $\frac{1}{2}(A + B)$ 75 46 28 - 10.5959988
: cot. $\frac{1}{2}C$ 29 15 28 - - 10.2516515

.. C = 58 30 56.

- 3. Given $a = 40^{\circ} 18' 29''$, $b = 67^{\circ} 14' 28''$, and $A = 34^{\circ} 22' 17''$; to determine the other parts when B is acute.
- B = 53° 35′ 15″, C = 119° 13′ 31″, c = 89° 47′ 6.″ 4. Given a = 84° 14′ 29″, b = 44° 13′ 45″, and A = 130° 5′ 229″;

to determine the other parts.

B = 32° 26′ 64″, C = 36° 45′ 28″, c = 51° 6′ 12″.

5. Given a = 97° 18′ 39″, b = 86° 53′ 46″, and A = 97° 21′ 26″; $c = 89^{\circ} 21' 37''$ to determine c.

CASE VI. (61.) Given two angles A, B, and the side a opposite to one of them, to find the other parts.

1. To find b we have sin. A: sin. B:: sin. a: sin. b.

2. And to find C and c we may employ Napier's analogies, which need not be here repeated.

The nature of the arc b may be discussed, as in the preceding case. Thus the formula (B), art. (50), gives cos. $b = \frac{\cos B + \cos A \cos C}{2}$

sin. A sin. C from which it follows, as in the foregoing case, that if cos. B is numerically greater than cos. A, B and b, will be of the same species. If cos. B is numerically less than cos. A, then both the values of b, given by the above proportion, will be admissible, for C may be determined so as to render cos. b positive or negative. Hence any side will be of the same species as its opposite angle, if the sine of this angle be less than the sine of either of the other angles; and the species of the side b will be indetermined if the sine of its opposite angle B be greater than the sine of the other given angle A. There cannot, therefore, be two solutions unless a and A are of the same species.

EXAMPLES.

1. In an oblique-angled spherical triangle ABC are given, $A = 32^{\circ}$ 26' 6\frac{1}{2}'', $B = 130^{\circ}$ 5' 22'', and the side $a = 44^{\circ}$ 13' 42''; to determine the other parts.

I. To find the Side b.

As sin. A 32° 26′ 61″ arith. comp. 9.8836842 : sin. B 130 5 23 0-2705556 :: sin. a 44 13 45 9.8435629

: sin. b 84 14 29 9.9978027 : b has two values, because the sine of B is greater than that of A. We shall take the acute value.

11. To find the Side c.

As $\cos \frac{1}{4}(A \sim B)$ 48° 49′ 37 $\frac{1}{4}$ ″ arith. comp. 0·1815543 : $\cos \frac{1}{4}(A + B)$ 81 15 44 $\frac{1}{4}$ - 9·1815890 :: $\tan \frac{1}{4}(a + b)$ 64 14 7 - 10·3163591 25 33 9.6795024 : tan. 1 c 2 c = 51 6 19.

III. To find the Angle C.

As $\cos \frac{1}{2}(a \sim b)$ 20° 0′ 22″ arith, comp. 0′ 0270310 : $\cos \frac{1}{2}(a + b)$ 64 14 7 - 9′ 6381663 :: $\tan \frac{1}{2}(A + B)$ 81 15 44‡ - 10′ 8133436 10.4785408 : cot. I C 18 22 44 2

 $\therefore C = 36 \ 45 \ 28.$

2. Given $A = 103^{\circ}59'57\frac{1}{2}''$, $B = 46^{\circ}18'7\frac{1}{2}''$, and $a = 42^{\circ}8'48''$; to find C=36° 7′ 521″. the angle C. 3. Given $A = 17^{\circ} 46' 161''$, $B = 151^{\circ} 43' 52''$, and $a = 37^{\circ} 48'$; to find $b = 108^{\circ}, c = 74^{\circ} 30^{\circ}.$

the remaining sides, b being obtuse.

SCHOLIUM.

Previously to closing this second part it may be worth while to re-mark, that if, in the foregoing investigations, we consider the radius of the sphere, upon which the triangles concerned are described, to be infinite, then, as any finite portion of the spheric surface may be considered as a plane, the spherical triangles will become plane triangles, and the sines and tangents of their sides will become identical with the sides themselves; so that all the foregoing rules and formulas, into which cosines, cotangents, secants, or cosecants, of the sides do not enter, are applicable as well to plane as to spherical triangles.

Professor Vince, at page 43 of his Trigonometry, has the following

note. "Difficulties have frequently arisen in consequence of its being supposed that an arc of 90° has a tangent and secant, each infinite. For instance, in a right-angled spherical triangle, radius : cosine of the angle at the base :: tangent of the hypotenuse: tangent of the base; now when the base = 90°, the hypotenuse = 90°; and therefore, these arcs being equal, if they have any tangents, of whatever value they may be, they must be equal; and, therefore, radius = cosine of the angle at the base, whatever that angle may be. This false conclusion arises from the supposition that an arc increases till it becomes 90°; the tangent and secant increase without limit; and at 90° the arc ceases to have either a tangent or secant, by their definition. As the arc, by increasing, passes through 90°, the tangent and secant increase without limit, cease to exist at 90°, and then begin again at a quantity indefinitely great. And thus in other cases where the tangent or secant of an arc enter into the computation, when the arc becomes 90°, we can draw no conclusion on which we can depend."

The foregoing reasoning is very much calculated to mislead the young student, although it does in reality tend to overturn the author's own hypothesis, and to show that the tangent of 90° must necessarily be in-

Taking the example chosen above, by Mr. Vince, we have for the true solution cos. < at base = rad. $\frac{\tan . 90^{\circ}}{\tan . 90^{\circ}}$; which must necessarily involve the absorbity necessarily involve the absurdity noticed above, except tan. 90° be either 0 or ∞; but when the proper value ∞ is put for tan. 90°, then we have $\cos < at$ base \mathbf{z} rad. $\frac{\infty}{\infty}$ \mathbf{z} rad. $\frac{0}{0}$; and as $\frac{0}{0}$ admits not only of the particular value 1.

fixed upon by Mr. Vince, but of an indefinite number of values, so does cos. < at base.

Upon the same grounds that Mr. Vince has rejected the tangent of 90°, he should have rejected the cosine of 90°, which, however, he admits to be 0.

For sin. < at base = rad. $\frac{\cos \cdot <$ at vertex $\cos \cdot$; but, when both base and hypotenuse are 90°, the angle at the vertex is 90°, and we ought, therefore, to have, according to Mr. Vince, single base = rad, which is, indeed, one solution, but by no means the only one, because the walues of are innumerable.

PART III.

APPLICATION OF PLANE AND SPHERICAL TRIGONOMETRY TO THE PRINCIPLES
OF NAVIGATION AND NAUTICAL ASTRONOMY.

(62.) Having in the two preceding parts of the present treatise pretty fully explained and illustrated the principles of plane and spherical trigonometry, we shall now, for the purpose of showing the practical ntility of these principles, apply them to the solution of one of the most important mathematical problems that has ever engaged the attention of man, viz. to determine the place of a ship at sea.

When a ship sails from any known place, and a correct account is kept of her various directions, and rates of sailing, her situation at any time may be readily ascertained by the rules of plane trigonometry, and the solution of the problem from these data belongs to Navigation.

But it is impossible to measure a ship's course and the distance sailed exactly; so that after a long passage it would be unsafe to compute the place of the ship from the ship's reckoning. In such cases, therefore, the solution must be effected from other data, independent of the ship's account; these are furnished by astronomical observation, and the computation is performed by the rules of spherical trigonometry; the problem then becomes one of Nautical Astronomy. We shall devote a distinct chapter to each of these important branches.

CHAPTER I.

THE PRINCIPLES OF NAVIGATION.

Definitions.

(63.) 1. The earth is very nearly spherical. For the purposes of Navigation it may be considered as perfectly so. It revolves round one of its diameters, called its axis, in about twenty-four hours. This rotation is from the west towards the east, causing the heavenly bodies to have an apparent motion from the east towards the west.

2. The great circle, whose poles are the extremities of the axis, is called the *equator*. The poles of the equator are called also the poles of the earth; the one being the north pole, and the other the south pole.

3. Every great circle which passes through the poles, and which, therefore, cuts the equator at right-angles, is called a meridian circle. Through every place on the surface of the earth such a great circle is supposed to be drawn; it is the meridian of the place. It is expedient for the purposes of Geography and Navigation to fix upon one of these meridians as a first meridian, from which the meridians of other places are measured.

The English have fixed upon the meridian of Greenwich Observatory

for the first meridian.

4. The longitude of any place is the arc of the equator, intercepted between the meridian of that place and the first meridian; the longitude, therefore, is the measure of the angle between the two meridians. The longitude is east or west, according as the place is situated on the right or on the left of the first meridian, when we look towards the north pole.

5. The difference of longitude between two places is the arc of the equator intercepted between the meridians of those places, or the measure of the angle which they include; hence, when the longitudes of the places are of the same denomination, that is, either both east or both west, the difference is found by subtracting the one from the other; but when they are of contrary denominations the difference is found by adding the one to the other.

6. The latitude of a place is its distance from the equator, measured on the meridian of the place. Latitude, therefore, is north or south, according to the pole towards which it is measured, and cannot exceed

90°.

7. The small circles drawn parallel to the equator are called parallels of latitude. The arc of a meridian, intercepted between two such parallels, drawn through any two places, measures the differences of latitude of those places: when the latitudes are of the same denomination the difference of latitude is found by subtraction, but when the denominations are not the same the difference of latitude is found by

addition, like difference of longitude.

8. The horizon of any place is an imaginary plane, conceived to touch the surface of the earth at that place, and to be extended to the heavens; such a plane is called the sensible horizon, and one parallel to it, but passing through the earth's centre is the rational horizon of the place. A line drawn across the horizon and through the place, in the plane of its meridian, is the meridian of the horizon, or the north and south line; the horizontal line through the same point, and perpendicular to this, is the east and west line. Besides the North, South, East, and West, points thus marked on the boundary of the horizon, this boundary is conceived to be subdivided into other intermediate points, corresponding to the divisions in the circle below.

9. The course of a ship is the angle which her track makes with the meridians; so long as this angle remains the same, the ship is said to sail on the same rhumb line or loxodromic curve. The magnitude of

the angle or the course is indicated by the mariner's compass.

10. The Mariner's compass consists of a circular card whose circumference is divided into thirty-two equal parts, called points, and each of these are subdivided into four equal parts, called points; across this card is fixed a slender bar of magnetized steel, called the needle; the tapering extremities of which point to two diametrically opposite divisions of the card. These opposite divisions are marked N. and S., corresponding to the north and south poles, or ends, of the magnetized bar. The diameter W. E., at right angles to the diameter

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N. S., point out the west and east points; these four are called the cardinal points, and the others are marked as in the sub-

joined diagram.

Thus one point from the north towards the east is north by east; two points, north, north east; three points, north-east by north; and so on. (See the table of Rhumbs at the end, p. 306:)

The card thus furnished being now suspended horizontally, and so as to allow the needle to settle itself freely, will point out the four cardinal points of the horizon, as

also the several intermediate points, provided only that it is the property of the magnetic needle to point due north and south. Such, however, is not strictly the case, as the needle is found from accurate observations, to deviate from this position, and at some places very considerably, and this deviation is itself subject to variation. But the true

direction of the compass, or the angle it makes at any place with a line pointing duly north and south, may be ascertained at any time by astronomical observations, and thus the deviation of the compass-points, from the corresponding points of the horizon, may always be found and allowed for.

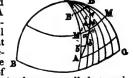
The compass is so placed on ship-board that the vertical plane, cutting the ship from stem to stern, may pass through the centre of the card, so that that point of the compass which is directed to the ship's head shows the compass-course, and the proper correction for variation being applied the true course will be obtained.

11. A ship's rate of sailing is determined by means of an instrument, called the Log, and an attached line called the log-line. The log is a piece of wood forming the sector of a circle, and its rim is so loaded with lead that when heaved into the sea it assumes a vertical position, with its centre barely above the water. The log line is so attached as to keep the face of the log towards the ship, that it may offer the greater resistance to be dragged after the ship by the log-line, as it unwinds from a reel on board, by the advancing motion of the ship. The length of line thus unwound in half a minute, gives the rate of sailing. For convenience the log-line is divided into equal parts, called knots, of which each measures the 120th of a nautical or geographical mile,* and as half a minute is the 120th of an hour, it follows that the number of knots, and parts of a knot, run in half a minute expresses the number of miles and parts of a mile, run in an hour, at the same rate of sailing.

On Plane Sailing.

(64.) Let the annexed diagram represent a portion of the earth's surface, P being the pole, and EQ the equator.

Let AB be any rhumbline, or track described by a ship in sailing on a single course from A to B. Conceive the path of the ship to be divided into portions Ab, bc, cd, &c. so small that each may differ insensibly from a straight line, and draw meridians through these seve-



ral divisions, as also the parallels of latitude B
bb',cc', dd', &cc.; we shall thus have a series of
triangles described on the surface of the globe, but so small that each
may be considered as a plane triangle. These triangles are all similar,

may be considered as a plane triangle. These triangles at a and a similar, for the angles at b', c', d', &c. are right angles, and the ship's path cuts all the meridians at equal angles; hence (Geom. prop. 9, Book 6,) Ab : Ab' :: bc : bc' :: cd : cd', &c. therefore, (Geom. prop. 5, Book 5,) Ab : Ab' :: Ab + bc + cd + &c. :: Ab' + bc' + cd' + &c.But Ab + bc + cd + &c. is the whole distance sailed, and Ab' + bc + cd' + &c. Ab : Ab', is the difference of latitude between A and B; consequently, if a right-angled triangle ABB', similar to the small triangle Abb', be constructed that is one in which the angle Abb' is constructed that is one in which the angle Abb' is constructed. angle Abb', be constructed, that is, one in which the angle A is equal to the course, and if the hypotenuse AB represent the dis-tance sailed, the side AB will represent the difference of latitude. Moreover, the other side BB', or that opposite to the course, will represent the sum b'b+c'c+d'd+&c. of all the minute departures which the ship makes from the successions. sive meridians which it crosses; for as the triangle ABB', in this last diagram, is similar to the small triangle Abb', in the former, we have Ab: bb':: AB: BB' but in the first figure we have Ab: bb'::bc: cc':: cd: dd', &c. $\therefore Ab:bb'::Ab+bc'+cd+&c.:bb'+cc'+dd'+&c.$

^{*} The geographical mile is one minute of the earth's circumference. T diameter at 7916 English miles, the geographical mile will be about 6079 feet. Taking the

consequently, since the three first terms of (1) are respectively equal to those of (2), the remaining terms BB',bb'+cc'+dd'+&c. must be equal. This last quantity is called the *departure* of the ship in sailing from A to B. It follows, therefore, that the distance sailed, the difference of latitude made, and the departure, are correctly represented by the hypotenuse and sides of a right-angled plane triangle, in which the angle opposite the departure is the course, so that when any two of these four things are given the others may be found simply by the resolution of a rightangled plane triangle; as far, therefore, as these particulars are con-cerned the results are the same as if the ship were sailing on a plane surface, the meridians being parallel straight lines, and the parallels of latitude cutting them at right-angles; and hence that part of Navigation in which only distance sailed, departure, difference of latitude, and course are considered, is called Plane sailing.

EXAMPLES.

1. A ship from latitude 47° 30' N. has sailed S. W. by S. 98 miles, What latitude is she in, and what departure has she R made?

Let C be the place sailed from, CB the meridian, the angle C=3 points = 33° 45′ and CA=98 miles, the distance sailed; then CB will be the difference of latitude, and BA the departure

1Õ : Distance 98 1.9912261 :: cos. course 33° 45' 9.9198464

As rad. : Dist. :: sin. course

1.9912261 9.7447390

1.9110725 : Diff. of lat. 81.48 Latitude left 47° 30' N.

: Departure 54.45

1.7359651

Diff. of lat. = 81.48 minutes = 1° 22' S. Dep. = 54.45 miles W.

Latitude in 46 8 N.

2. A ship sails for 24 hours on a direct course, from lat. 38° 32′ N., till she arrives at lat. 36° 56′ N.; the course is between the S. and E., and the rate 5½ miles an hour. Required the course, distance, and departure.

Lat. left 38° 32' N. Lat. in 36 56 N.

 $24 \times 51 = 132$ miles, the distance.

Diff.	1 :	36 = 96 miles.
As Dist.	132	2 1205739
: Rad.		10
:: Diff. lat.	96	1.9822712
	40-0	

As rad. 10 2.1205739 : Dist. 9.8364771 :: sin. course

: cos. course 43° 20′ 9·8616973 | : Dep. 90·58 | 1·9570510 |
Hence the course is S. 43° 20′ E., and the departure 90·58 miles E.

3. A ship sails from lat 3° 52′ S. to lat. 4° 30′ N., the course being N. W. by W. ½ W.; required the distance and departure.

Distance 1065 miles, Departure 9389 miles W. 4. Two ports lie under the same meridian, one in latitude 52° 30′ N., and the other in latitude 47° 10′ N. A ship from the southernmost sails due east at the rate of 9 miles an hour, and two days after meets a sloop which had sailed from the northernmost port; required the sloop's direct course and distance run.

Course S. 53° 28' E., or S. E. ‡ E.; the distance run 5376 miles:

5. If a ship from lat. 48° 27' S., sail S. W. by W., 7 miles an hour, in what time will she arrive at the parallel of 50° S. ? In 23°914 hours.

6. If after a ship has sailed from lat. 40° 21' N. to lat. 46° 18' N., she be found 216 miles to the eastward of the port left; required her course and distance sailed. Course N. 31° 11' E., dist. 417'3 miles.

prefixed.

Traverse Sailing.

(65.) When a ship in going from one place to another, sails on different courses, it is called traverse sailing; and the determination of the single course and distance from the one place to the other is called vorking or compounding the traverse. To effect this, it is obviously merely necessary to find the difference of latitude, and departure, due to each distinct course, to take the aggregate of these for the whole difference of latitude and departure, and from these to find, as in last article, the single course and distance. It is usual in thus compounding courses to form a table consisting of six columns, called a traverse table, and in the first column to register the several component courses, and against them, in the second column, the proper distances; the next two columns, marked N. and S., are to receive the several differences of latitude, whether N. or S., due to each course, and distance, and the two remaining columns marked E. and W. are to receive, in like manner, the corresponding eastings and westings, that is, the departures. When these several particulars are all inserted, the columns are added up, and the difference of the results of the N. and S. columns will be the required difference of latitude, and the difference of the results of the E. and W. columns will be the corresponding departure.

The columns appropriated to the differences of latitude and departures are usually filled up from a table already computed to every quarter point of the compass, and to all distances from one mile up to a hundred or 120; so that, by entering this table with any given course and distance, the proper difference of latitude and departure is found by inspection. Most books on navigation contain also a second and more enlarged traverse table, being computed to every course from a quarter of a degree up to forty-five degrees. This latter table we have not thought it necessary to insert in our collection, but the former we have given (Table IV.), and its use is fully explained in the introduction

But there is another mode of finding the direct course and distance, much practised by seamen, viz. by construction. To facilitate this construction the mariner's scale is employed, which is a two-foot flat rule exhibiting several scales on each side, by help of which and a pair of compasses the usual problems in sailing may be all solved. One of these scales is a scale of chords, commonly called a scale of rhumbs, being confined to every quarter point of the compass; and another is a more enlarged scale of chords, being to every single degree. Both these scales are constructed in reference to the same common radius, so that the chords on the scale of rhumbs belong to that circle whose radius equals the chord of 60° on the scale of chords; and the method of laying down a traverse from these scales, and one of equal parts, and of

thence measuring the equivalent single course, and distance made good, will be at once understood from the following examples.

EXAMPLES.

1. A ship sails from a place in lat. 24° 32' N., and has run the fol-

lowing courses and distances, viz.

Ist, S. W. by W., distance 45 miles; 2d, E. S. E., distance 50 miles; 3d, S. W., distance 30 miles; 4th, S. E. by E., distance 60 miles; 5th, S. W. by S. ‡ W., distance 63 miles: required her present latitude, with the direct course and distance from the place left to the place arrived at.

Traverse	

Courses.	Dist.	Differe	nce of Lat.	Dep	arture.
S. W. by W. E. S. E. S. W. S. E. by E. S. W. by S. ‡ W.	45 50 30 60 63	N.	8. 25·0 19·1 21·2 33·3 50·6	E. 46·2 49·9	W. 37·4 21·2 37·5
			149-2	96·1	96.1

It appears from the results of this table that the difference of latitude made by the ship during the traverse is $149.2 \text{ S.} = 2^{\circ} 29' \text{ S.}$

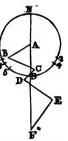
Lat. left - - - 24° 32′ N. Diff. lat. - - - 2 29 S.

Lat. in - - - 22 3 N.

It appears also that the departures east are equal to the departures west, so that the ship has returned to the meridian she sailed from, consequently the direct course from the place left to that come to is due south, and the distance is equal to the difference of latitude, which is 149-2 miles.

The construction of this traverse is as follows.

With the chord of 60°, taken from the line of chords on the mariner's scale, describe the horizon circle, and draw the north and south line N.S. From the line of rhumbs take the chords of the several courses, and as these are all southerly, they must be laid off from the south point S, those which are westerly to the left, and those which are easterly to the right, their extremities being marked 1, 2, 3, &c. in the order of the courses. This done, lay off from any convenient scale of equal parts, and in the direction A1 the distance AB sailed on the first course; then in the direction parallel to A2, the distance BC sailed on the second course; in the direction parallel to A3, the distance CD on the third course; in the direction parallel to A4, the distance DE on the



in the direction parallel to A4, the distance DE on the fourth course; and, lastly, in the direction parallel to A5, the distance EF on the third course; then F will represent the plane of the ship at the end of the traverse; FA, being applied to the scale of equal parts, will show the distance made good, and the chord of the arc included between this distance, and the meridian, being applied to the line of rhumbs, will show the direct course. In the present case the intercepted arc will be 0, showing that F is on the meridian of A.

2. A ship from lat. 28° 32' N., has run the following courses, viz. 1st, N. W. by N., 20 miles; 2d, S. W., 40 miles; 3d, N. E. by E., 60 miles; 4th, S. E., 55 miles; 5th, W. by S., 41 miles; 6th, E. N. E., 66 miles. Required her present latitude, the distance made good, and the direct course from the place left to that come to.

The direct course is due east, and distance 70.2 miles, the ship being in the same latitude at the end as at the beginning of the traverse.

3. A ship from lat. 41° 12' N., sails S. W. by W., 21 miles; S. W. ‡ S. 31 miles; W.S.W. ‡ S., 16 miles; S. ‡ E., 18 miles; S. W. ‡ W., 14 miles; and W. ‡ N., 30 miles: required the latitude of the place arrived at, and the direct course and distance to it.

Lat. 40° 5' N.; course S. 52° 49' W.; distance 111.7 miles.

4. A ship from Cape Clear, in lat. 51° 25′ N., sails 1st, S. S. E. ‡ E., 16 miles; 2d, E.S.E., 23 miles; 3d, S.W. by W. ‡ W., 36 miles; 4th, W. ‡ N., 12 miles; 5th, S.E. by E. ‡ E., 41 miles: required the distance made good, the direct course, and the latitude in ?

Traverse Table.

Courses.	Dist.	Difference of Lat.		Depa	rture.
S. S. E. ‡ E. E. S. E. S. W. by W. ‡ W. W. ‡ N. S. E. by E. ‡ E.	16 23 36 12 41	N. 1·8	S. 14·5 8·8 17·0 21·1	E. 6·3 21·3	31·8 11·9
		1.8	61·4 1·8	63·3 43·7	43.7
			59.6	19.6	1

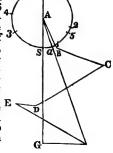
Lat. in

As diff. lat. 59·6 . 1·7752463 | As sin. course : rad. . . 10· : departure 19·6 . 1·2922561 :: rad . . . 10·

: tan. course 18° 12′ 9.5170098 | : distance 62.74 . 1.7976356 therefore, as the difference of latitude is south, and the departure east, the direct course is S. 18° 12′ E., and the distance made good 62.74 miles.

To construct this traverse, describe, as before, the horizon circle, with a radius equal to the chord of 60°, and taking from the line of rhumbs the chord of the first course, 2‡ points, apply it from S. to 1, to the right of S.N., as this course is south-easterly; apply, in like manner, the chord of the second course, 6 points from S. to 2, also to the right of the meridian line; apply the chord of the third course, 5½ points from S. to 3, to the left of the meridian, the chord of the fourth course, 7½ from N. to 4, to the left of N. S., this course being north-westerly, and

lastly, apply the chord of the fifth course, 5½ points, from S. to 5, to the right of S. N. In the direction A1, lay off the distance AB = 16 miles from a scale of equal parts; in the direction parallel to AQ, lay off the distance BC = 23 miles; in the direction parallel to A3, lay off CD = 36 miles; in the direction parallel to A4, lay off DE = 12 miles; and, lastly, in the direction parallel to A5, lay off EF = 41, then F will be the place of the ship at the end of the traverse; consequently, AF will be the distance made good, and the angle FAS the direct course; applying, therefore, the distance AF to the scale of equal parts, we shall find it reach from 0 to 62½; and applying the distance Sa to the line of chords, we shall find it reach from 0 to 189.



5. A ship runs the following courses, viz. 1st, S. E., 40 miles; 2d, N.E., 28 miles; 3d, S.W. by W., 52 miles;

4th, N.W. by W., 30 miles; 5th, S.S.E., 36 miles; 6th, S.E. by E., 58 miles: required the direct course and distance made good.

Direct course S. 25° 59′ E., or S.S.E. ‡ E. nearly; distance 95 87 miles.

6. A ship in latitude 37° 10′ N. is bound to a port in the latitude of 33° 0′ N. which lies 180 miles west of the meridian of the ship; but by reason of contrary winds, she sails the following courses, viz. S. W. by W. 27 miles, W. S. W. ‡ W. 30 miles, W. by S. 25 miles, W. by N. 18 miles, S. S. E. 32 miles, S. S. E. ‡ E. 27 miles, S. E. 25 miles, S. 31 miles, and S. S. E. 39 miles. Required the latitude the ship is in, and her departure from the meridian, with the course and distance to her intended port?

The difference of latitude and departure made on each course, will be seen by sketching a traverse table; hence it appears that the difference of latitude made good is 1694 miles, the departure 474 miles, and by plane sailing, the course S. 15° 38′ W. and distance 175.9 miles; and the course to the intended port S. 58° 42′ W., distance 155.2 miles; the

latitude being 34° 21' N.

These examples will, perhaps, suffice to illustrate the principles of plane sailing, in which course, distance, difference of latitude, and departure, are the only things concerned. The determination of the difference of longitude made on any course cannot be effected by these principles, for this element is not the same as if the meridians were all parallel to each other, as is the case with the other elements. The finding of the difference of longitude is the easiest when the ship sails due east or due west, that is, upon a parallel of latitude; this is called parallel sailing.

Parallel Sailing.

(66.) The theory of parallel sailing is comprehended in the following proposition, viz.

The cosine of the latitude of the parallel is to the distance run as the radius to the difference of longitude. This may be demonstrated as follows.

In the figure, at page 42, let IQH represent the equator, and BDA any parallel of latitude; CI will be the radius of the equator, and cB the radius of the prallel. Let BD be the distance sailed, then the difference of longitude will be measured by the arc IQ of the equator, and since (Geom., prop. 12, Cor. 2, B. 7) similar arcs are to each other as the radii of the circles to which they belong, we have

cB: CI:: dist. BD: diff. long. IQ.

But cB is the cosine of the latitude IB to the radius CI, that is, cB is CI times the trigonometrical cosine of the latitude; hence the above

proportion is CI × cos. lat. : CI :: distance : diff. long.

cos. lat.: Rad. (=1) :: distance: diff. long. . . . (1). Corollary: hence if the distance between any two meridians, measured in a parallel in latitude L be D, and the distance of the same meridians, measured on a parallel, in latitude L' be D', we shall have, (Geom., prop. 15, Cor. 2, Book 5, cos. L: D:: cos. L': D' . . . (2). Hence if one of the legs of a right-angled triangle represent

Hence if one of the legs of a right-angled triangle represent the distance run on any parallel, and the adjacent acute angle be equal to the degrees of lat. of that parallel, then the hypotenuse will represent the difference of longitude, since this hypotenuse will be determined by the foregoing proportion (1). It follows, therefore, that any problem in parallel sailing may be solved by the traverse table, com-

proportion (1). It follows, therefore, that any problem in parallel sailing may be solved by the traverse table, computed to degrees, as a simple case of plane sailing; for by considering the latitude as the course, and the distance as the difference of latitude, the corresponding distance in the table will express the difference of longitude.

1. A ship from latitude 53° 56' N., longitude 10° 18' E., nas sailed due west, 236 miles: required her present longitude. By the rule; As cos. lat. 53° 56' 9.7699134 10 : radius 2.3729120 :: distance : diff. long. 408.87 2-6029986 10° 18' E. Long. left Diff. long. $=\frac{400}{60}$ degrees =

3 38 E.

and then due N., till she reaches lat. 73° 26' N.; how far must she sail W. to reach the meridian of the North Cape?

Here the ship sails on two parallels of latitude, first on the parallel of 71° 10′, and then on the parallel of 73° 26′, and makes the same difference of longitude on each parallel. Hence, by the corollary,

As cos. lat. 71° 10′ arith. comp. 0.4910444

: distance 126 2 1003705 :: cos. lat. 73 26 . 9.4550441

: distance 1113 . . 2 0464590.

3. A ship in latitude 32° N., sails due east; till her difference of loagitude is 384 miles; required the distance run. 325.6 miles.

4. If two ships in latitude 44° 30' N., distant from each other 216 miles, should both sail directly south till their distance is 256 miles, what latitude would they arrive at? 32º 17' S.

5. Two ships in the parallel of 47° 54' N., have 9° 35' difference of longitude, and they both sail directly south, a distance of 836 miles: required their distance from each other at the parallel left, and at that 385.5 miles, and 479.9 miles. reached.

Middle Latitude Sailing.

(67.) Having seen how the longitude which a ship makes when sailing on a parallel of latitude may be determined, we come now to examine the more general problem, viz. to find the longitude a ship

makes when sailing upon any oblique rhumb.

There are two methods of solving this problem, the one by what is called middle latitude sailing, and the other by Mercator's sailing. The first of these methods is confined in its application, and is moreover somewhat inaccurate even where applicable; the second is perfectly general, and rigorously true; but still there are cases in which it is advisable to employ the method of middle latitude sailing, in preference to that of Mercator's sailing; it is, therefore, proper that middle latitude sailing should be explained, especially since, by means of a correction to be hereafter noticed, the usual inaccuracy of this method may be rectified.

Middle latitude sailing proceeds on the supposition that the departure

or sum of all the meridional distances b'b, c'c, d'd, &c. from A to B, is equal to the distance M'M of the meridians of A and B, measured on the middle parallel of latitude between A and B.

This supposition becomes very inaccurate when the course is small, and the distance run great; for it is plain that the middle latitude



distance will receive a much greater accession than the departure, if the track of B cuts the successive meridians at a very small angle.

The principle approaches nearer to accuracy as the angle A of the course increases, because then as but little advance is made in latitude, the several component departures lie more in the immediate vicinity of the middle latitude parallel. But still, as in very high latitudes, a small advance in latitude makes a considerable difference in meridional distances, this principle is not to be recommended in such latitudes if much accuracy is required.

By means, however, of a small table of corrections, recently constructed by Mr. Workman, and judiciously introduced by Mr. Riddle in the second edition of his valuable Treatise on Navigation, the imperfections of the middle latitude method may be removed, and the results of it rendered in all cases accurate. This table we have given at the end of the present volume, and have explained its construction in the

introductory explanation to the Tables. The rules for middle latitude sailing may be thus deduced.

It has been seen at (64) that the difference of latitude, departure, and distance, sailed on any oblique rhumb, will be all accu-A' rately represented by the sides AB', B'B, AB, of a plane triangle. Now, by the present hypothesis, the departure B'B is equal to the middle latitude distance between the meridians of the places sailed from, and arrived at, so that the difference of longitude of the two places of the ship is the same as if it had sailed the distance B'B, on the middle latitude parallel; the determination of this difference of longitude is, therefore, reduced to a case of parallel sailing, for BB' now representing the distance on the parallel, and an angle A'BB' being made equal to the latitude of that parallel, we shall have the difference of longitude, represented by the hypotenuse A'B. We thus

have the following theorems, viz. in the triangle A'B'B, cos. A'BB': BB':: radius: BA'; that is, t. Cos. mid. lat. : departure :: radius : diff. of long. In the triangle A'BA, sin. A': AB::sin. A: A'B; that is, II. Cos. mid. lat.: distance :: sin. course: diff. long. In the triangles ABB', A'BB',

AB' tan. A = B'B; A'B cos. A'BB' = B'B; therefore,

AB': A'B:: cos. A'BB': tan. A; that is, m. Diff. lat.: diff. long.:: cos. mid. lat.: tan. course.

These three proportions comprise the theory of middle latitude sailing, and when to the middle latitude the proper correction, taken from Mr. Workman's table is added, these theorems will be rendered strictly accurate.

EXAMPLES.

1. A ship, in latitude 51° 18' N., longitude 22° 6' W., is bound to a place in the S.E. quarter, 1024 miles distant, and in lat 37° N.: what is her direct course and distance, as also the difference of longitude between the two places.

Lat. from 51° 18' N. Sum of latitudes 89º 18' 0 N. Lat. to 37 Mid. lat. 44 9

18 = 858 miles. Diff. lat. 14

For the course. For the diff. long. 3.0103000 cos. mid. lat. 44° 9' ar. com. 0.1441668 As distance 1024 : tan.course 33 5 : radius 9.8138993 2.9334873 :: diff. lat. 2.9334873 :: diff. lat. 858 858

: cos. course 33° 5′ 9.9231873 : diff. long. 2.8915534 779

In this operation the middle latitude has not been corrected, so that the difference of longitude here determined is not without error. To find the proper correction look for the given middle latitude, viz. 44° 9' in the table of corrections, the nearest to which we find to be 45°; against this and under 14° diff. of lat. we find 27', also under 15°, we find 31', the difference between the two being 4': hence corresponding to 14° 18' the correction will be about 28'. Hence the corrected middle

latitude is 44° 37′, therefore, cos. corrected mid. lat. 44° 37′ ar. comp. 0.1483780 9.8138993 : tan. course 33 :: diff. lat. 2-9334873

> : diff. long. 786.6 2.8957646:

therefore, the error in the former result is about 71 miles.

2. A ship sails in the N. W. quarter, 248 miles, till her departure is 135 miles, and her difference of longitude 310 miles: required her

course, the latitude left, and the latitude come to.

Course N. 32° 59′ W.; lat. left 62° 27′ N.; lat. in 65° 55′ N.

3. A ship, from latitude 37° N., longitude 9° 2′ W., having sailed between the N. and W., 1027 miles, reckons that she has made 564 miles of departure; what was her direct course, and the latitude and longitude reached ?

Course N. 33° 19′ W. or N. W. by N. nearly; lat. 51° 18′ N.; long 28° 8′ W.

4. Required the course and distance from the east point of St. Michael's, lat. 37° 48' N., long. 25° 13' W., to the Start Point, lat. 50° 13' N., long. 3° 38', the middle latitude being corrected by Workman's Course N. 51º 11' E.; distance 1189 miles.

Mercator's Sailing.

(68.) It has been already seen that when a ship sails on any oblique rhumb, the difference of latitude, the departure, and the ordistance run, are truly represented by the sides of a right-angled plane triangle. The departure B'B repre-B' sents the sum of all the very small meridian distances, or elementary departures, b'b, c'c, &c. in the diagram, at page 74, the difference of latitude AB represents the sum of all the corresponding small difference in the figure p referred to; and the distance AB, the sum of all the distances to which these several departures and differences A

belong, and each of these elements are supposed to be taken so excessively small as to form on the sphere a series of triangles, differing

insensibly from plane triangles.

Let Ab'b in the annexed diagram represent one of these elementary triangles, b'b will be one of the elements of the departure, and Ab', the corresponding difference of latitude; and as b'b is a small portion of a parallel of latitude, it will be to a similar portion of the equator, or of the meridian, as the cosine of its latitude to radius (66). This similar portion of the equator, or of the meridian, being the difference of longitude between b' and b. Suppose now the distance Ab prolonged to p, till the departure p'p is equal to the difference of longitude of b', and b, then b'b will be to p'p as the cosine of the latitude of b'b to the radius; but b'b:p'p:Ab':Ap'; hence the proper difference of latitude Ab' is to the increased difference Ap' as the cosine of the latitude of b'b to the radius. Calling, therefore, the proper difference of latitude d, the increased difference D, the latitude of b'b, C, and the radius R, we

have $D = \frac{Rd}{\cos l} = Rd$ sec. l; the ship, therefore, having made the small

departure b'b, and the difference of latitude Ab', must continue her course till the difference of latitude becomes D, in order that her departure may become equal to the difference of longitude corresponding to bb. Conceiving all the elementary distances to be in this manner increased, the sum of all the corresponding increased departures will necessarily be the whole difference of longitude made by the ship during the course; to represent, therefore, the difference of longitude due to the departure B'B, and difference of latitude AB', we must prolong AB' till AC' is equal to the sum of all the elementary differences increased as above, and the departure C'C, due to this difference of latitude, will represent the difference of longitude actually made in sailing from A The determination of AC' requires the previous determination of all its elementary parts; if d be taken equal to 1, each of these parts will be expressed by D = 1 sec. l, from which equation the values of D, corresponding to every minute of l, from the equator to the pole, may be calculated; and by the continued addition of these there will be obtained, in succession, the values of the increased latitude corresponding to 1', 2', 3', &c. of proper latitude; these values are called the meridional parts, corresponding to the several proper latitudes, and when registered in a table, form a table of meridional parts, given in all books on Navigation.

The following may serve as a specimen of the manner in which such a table may be constructed, and, indeed, of the manner in which the first table of meridional parts was actually formed by Mr. Wright, the pro-

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poser of this ingenious and valuable method.
Mer. pts. of 1' = nat. sec. 1'.
Mer. pts. of 2' = \text{nat. sec. } 1' + \text{nat. sec. } 2'.

Mer. pts. of 3' = \text{nat. sec. } 1' + \text{nat. sec. } 2' + \text{nat. sec. } 3'.

Mer. pts. of 4' = \text{nat. sec. } 1' + \text{nat. sec. } 2' + \text{nat. sec. } 3' + \text{nat. sec. } 4'.
                                                         &c.
                                                                                                                    &c.
```

Hence, by means of a table of natural secants, we have

```
Nat. secs. Mer. parts.
Mer. pts. of l' =
                                                         1.00000000 = 1.00000000
Mer. pts. of 3' = 1.0000000 + 1.0000002 = 2.0000002

Mer. pts. of 3' = 2.0000002 + 1.0000004 = 3.0000006

Mer. pts. of 4' = 3.0000006 + 1.0000007 = 4.0000013
```

There are other methods of construction, but this is the most simple and obvious; we shall, however, presently have to advert to another process of computation, by which the meridional parts for any latitude may be found independently of previous calculations. The meridional parts, thus determined, are all expressed in geographical miles, because in the

general expression D=1' sec. l, 1' is a geographical mile. Having thus formed a table of meridional parts, (see Riddle's Navigation, or Robertson's Treatise,) if we enter it with the latitudes sailed from, and come to, and take the difference of the corresponding parts in the table, the remainder will be the meridional difference of latitude, or the line AC' in the preceding diagram, and the difference of longitude C'C will then be obtained by this proportion, viz.

1. As radius is to the tangent of the course, so is the meridional difference of latitude to the difference of longitude; or if the departure be given

instead of the course then the proportion will be 2. As the proper difference of latitude is to the departure, so is the meridional difference of latitude to the tangent of the course. Other proportions immediately suggest themselves from the preceding figure.

(69.) As an example of Mercator's, or more properly of Wright's, sailing, let us take the following.

certic 1000

 Required the course and distance from the east point of St. Michael's to the Start Point.

lat. 50° 13' N. Mer. pts. 3494.8 long. 3° 38′ W. Start St. Michael's lat. 37 48 N. Mer. pts. 2453-1 long. 25 13 W.

> 12 25 Mer. diff. lat. 0141.7 diff. long. 21 35 W. 60

Proper diff. lat. 745 miles. 1295 miles. For the distance. For the course. As Mer. diff. lat. 1041.7 3.0177427 9.7971501 As cos. course : radius : prop. diff. lat. 2.8721563 :: diff. long. 3.1122698:: rad. 10 : tan. course 51° 11' E. 10 0945271 : distance 1189 3.0750062

(70.) In the absence of a table of meridional parts, a table of logarithmic tangents may be employed for the same purposes; and, indeed, the meridional parts corresponding to any given latitude may be expeditiously computed by help of such a table, and independently of any previous computations.

It was shown, at page 76, that if a ship in latitude x, vary her latitude by a very small portion Δx , and that she continue her course till her departure equals the difference of longitude due to the difference of latitude Δx , then the enlarged difference of latitude (Δy), due to this departure, will be $\Delta y = \sec x \, \Delta x \, \therefore \, \frac{-y}{\Delta x}$ $\frac{\Delta y}{\lambda}$ = sec. x. This expression, it must be remembered, is nearer the truth the smaller we suppose Az to be, and is, therefore, accurately true only when $\Delta x = 0$; in other words, sec. x is the value to which the ratio $\frac{\Delta y}{\Delta x}$ continually approaches, as we continually diminish Δx , (and in consequence Δy ,) and which value it actually becomes only when the terms of the ratio vanish, and the fractions take the form $\frac{\sigma}{0}$. By adopting the language of the Differential Calculus we have, in this case, $\frac{dy}{dx} = \sec x \cdot dy = \sec x dx = dx$ $\therefore y = \log$. tan. (45° + $\frac{1}{4}x$), see Int. Calculus, p. 69; the logarithm here used is the Naperian. To change it into a common logarithm we must multiply by the modulus 2 302585, &c.; it must be observed, however, that it is the logarithm of the natural tangent which is here expressed, and not the tabular logarithmic tangent; it is, therefore, equal to the tabular logarithmic tangent minus 10. Hence, employing the table of logarithmic tangents, we may compute y from the formula $y = 2 \cdot 302585$ [log. tan. $(45^{\circ} + 1x) - 10! \times \text{Rad.}$ and thus, as stated above, the meridional parts, y, corresponding to any given latitude x, may be expeditiously computed, independently of any previous computations.

The tables of meridional parts are usually expressed in nautical miles, and we shall have the number of miles in y, if, instead of multiplying by the radius of the earth, we multiply by the number of miles or minutes in it. Now in every circle the radius is equal to 34:3774679 mi-34: nutes of that circle, because 3 14159, &c.: 1800 :: 1: 343 774679 minutes hence for the number of miles in y the expression is 7915-7044679 $\{\log \tan (45^{\circ} + \frac{1}{4}x) - 10\}$; or, since $\tan 45^{\circ} + \frac{1}{4}x = \cot 45^{\circ} - \frac{1}{4}x$

 $\frac{R^3}{\tan} = 20 - \tan .$; this expression and, since, moreover, \log . \cot . = \log .

may be written thus, 7915-7044679 $\{10 - \log \tan (45^{\circ} - \frac{1}{2}z)\}$, which gives the rule in the text. We had intended to have introduced here some other particulars relating to Mr. Wright's projection of the meridian line, but we are precluded from doing so, as this treatise has already exceeded the limits assigned to it. We must, therefore, content ourselves with referring the student to Robertson's Nav. vol. n. p.135—146.

The practical rule is as follows, viz. if the log. tangent of half the complement of any latitude be subtracted from 10, and the remainder be multiplied by 7915.7044679, &c. the product will give the meridional parts

in miles, corresponding to that latitude.

From this rule the method of operating with logarithmic tangents, instead of with meridional parts, may be easily derived. Call t, t', the logarithmic tangents of the half complements of the latitudes left and reached, and put a for the constant multiplier 7915 7044, &c. Then, by the rule just given, the meridional difference of latitude will be

$$a\{(10-t')-(10-t)\}=a(t-t')=(t-t')\ 10000+\frac{10000}{a}$$

Now log. $\frac{10000}{a}$ = 1015104, therefore, the logarithm of the meridional difference of latitude is found by removing the decimal point in the difference t-t' four places to the right, and then subtracting the constant number 1015103. Hence, if instead of the logarithm of the radius 10, we use 10 1015104, and instead of the meridional parts the logarithmic tangents t, t', of the complements of the half latitudes, taking care in setting down the difference of these to remove the decimal point four places to the right, the proportion (1), at page 77, may be still employed. Thus, taking the foregoing example, the operation by this

method will be as follows.
Let Co. lat. St. Michael's 26° 6'
$$\therefore t = 9.6901030$$

Start 19 53 $\therefore t' = 9.5585051$
 $t-t' = 1315.979$

1315.979 arith. comp. 6.8807448 : Const. log. 10.1015104 :: diff. long. 3.1122698

: tan. course N. 51° 11' E. 10.0945250

The reason why the resulting logarithm here does not exactly comcide with that obtained by using the meridional parts, is that the meridional parts have been computed to but one place of decimals; if they had been computed to two or three places, the two results would have been exactly the same.

2. Given the Lizard in lat. 49° 55' N. Barbadoes in lat. 13° 10' N. and

their difference of longitude 53°, or 3180′ W.; to determine the course and distance. Course S. 49° 59′ W.; distance 3429 miles.

3. A ship sails from lat. 37° N. long. 22° 56′ W., on the course N., 33° 19′ E., till she arrives at lat. 51° 18′ N.: required the distance sailed, and the longitude arrived at.

Distance 1027 miles; longitude in 9° 45' W.

We shall here terminate the present chapter on the principles of Navigation, having now discussed the several cases of sailing which actually occur in practice. But the student who is desirous of prosecuting his inquiries on this very important branch of practical science to greater extent, will, of course, consult works expressly devoted to the subject. Of these, the most elaborate in our language is the valuable "Elements" of Robertson, in two octavo volumes. The Treatise of Mr. Riddle is also an excellent work abounding with practical examples very accu-

rately solved, and upon the whole, better adapted to modern practice, as well as more compendious, than Robertson's. Mr. Norie's Navigation is also a good practical book, and so is that of Dr. Bowditch.

CHAPTER IL

APPLICATION OF SPHERICAL TRIGONOMETRY TO ASTRONOMICAL PROPLEME.

(71.) The solution of Astronomical Problems forms one of the most useful and agreeable applications of the theory of spherical Trigonometry. To such inquiries the theory itself, no doubt, owes its origin, as well as many of the successive improvements which it has gradually received, so that a specimen of its use in the solution of astronomical problems may reasonably be looked for in a book on Trigonometry.

For the purpose of measuring the angular distances of the heavenly bodies from each other, and from the horizon, it is convenient to suppose them all situated as they really appear to an observer on the earth, viz. in a spherical concave surrounding our earth and concentric with it. This imaginary concave is called the celestial sphere, or the apparent heavens; in it all the apparent motions of the heavenly bodies are, for the convenience of trigonometrical application, supposed actually to take place; and the entire celestial sphere to revolve daily round the earth, as if this were at rest in its centre. All this is allowable, because the applications of which we speak are not affected by the inquiry, whether the motions which the heavenly bodies present to an observer on the earth are really as they appear or not.

At the opening of last chapter we defined several lines which geographers had found it convenient to consider as described on the surface of the earth; most of these, astronomers extend to the heavens. Thus the plane of the earth's equator, when extended to the heavens, marks on the celestial sphere the great circle called the equinoctial, and in like manner, the meridians being extended to the heavens, mark out the celestial meridians; also the axis of the earth, about which its real motion takes place, when extended to the heavens, is the axis about which the apparent motion of the celestial sphere takes place: this axis marks

out the north and south poles of the heavens.

As the sun performs its apparent revolution about the earth in 24 hours it passes over 15° in an hour; if then we consider, as astronomers do, that the day at any place commences at noon, or when the sun is on the meridian of that place, the time shown by the sun in any position will be expressed in degrees by the arc of the equinoctial, intercepted between the fixed meridian of the place, and that passing through the sun, or it will be expressed by the angle included by these meridians. Celestial meridians are, therefore, also called hour circles, and the angle between the meridian of the place and that through the sun is called the hour angle, or the horary angle. That meridian which is at right-angles to the meridian of the place is the six o'clock hour circle, since the sun obviously reaches it when half way between noon and midnight.

Besides these lines, thus transferred from the earth to the heavens, there are others peculiar to the celestial sphere, which must be meanioned; these are, 1st, ecliptic, which is the great circle path described by the sun among the fixed stars in its apparent annual motion about the earth: in reality it is the path of the earth moving in a contrary direction about the sun. This circle crosses the equinoctial at an angle subject to an exceedingly small variation, determinable by observation and computation; its inclination to the equinoctial is about 23° 28', but it is always given with the minutest attainable accuracy in the Nautical

Almanack. The points where the ecliptic crosses the equinoctial are called the equinoctial points: the sun enters these points about the 21st of March and the 23d of September; the former being called the vernal equinox, and the latter the autumnal equinox. These names are given because at such times the nights are equal in length to the days all over the world; for as the two poles of the earth are at these times symmetrically situated with respect to the sun, the circular boundary, which separates the enlightened hemisphere from the darkened, must pass through both poles; and hence any point on the earth will be as long in being carried, by the earth's uniform rotation, through the enlightened part as through the dark part. The meridian through the equinoctial points is called the equinoctial colure.

The position of any point on the celestial sphere, like the position of a point on the terrestrial sphere, is marked out by its latitude and longitude. On the celestial sphere the circle of longitude is the ecliptic; and perpendiculars to this, passing, therefore, through the poles of the ecliptic, are the circles of celestial latitude; the point from which longitude is measured is the vernal equinoctial point. Commencing at this point, too, the ecliptic is divided into twelve parts, called signs; a sign is therefore 30°. The twelve signs are named, and symbolically ex-

pressed, as follow:

1. % Aries. | 4. Cancer.

2. % Taurus. | 5. \(\) Leo.

3. \(\) Gemini. | 6. \(\) Virgo. | 10. V3 Capricornus.

The first six of these signs are on the north of the equinoctial, the others on the south, and the vernal equinoctial point is called the first point of Aries. The longitude is measured from this point in but one

direction, viz. in the order of the signs.

Besides the above method of marking out the position of a celestial body, by means of its latitude and longitude, there is another way, viz. by means of its Right Ascension and Declination. The right ascension is measured on the equinoctial from the first of Aries, in the order of the signs, and the declination is measured on the perpendicular to this, or circle of declination passing through the object. We see, therefore, that what on the terrestrial sphere is latitude and longitude, is on the celestial sphere declination and right ascension; and parallels of latitude on the one correspond to parallels of declination on the other. Of these the two which are 23° 28' from the equinoctial, one on each side, and which therefore touch the ecliptic in the first points of Cancer and Capricorn, are called the tropics of Cancer and of Capricorn. These first points of Cancer and Capricorn are respectively called the summer and winter solstice; because for a day or two before and after the sun enters them he appears to be stationary, and the days to be of equal length, so slowly does his declination at those times change, for his motion is obviously very nearly parallel to the equinoctial. The meridian, through the solstitial points, is called the solstitial colure, and that through the equinoctial points, the equinoctial colure.

Having described the principal circles and points of the celestial sphere which are considered as permanent, or which do not alter with the situation of the observer on the earth, we come now to describe those which change with his place. The principal of these is the horizon, which has been defined already (63), and vertical circles which are perpendicular to the horizon, and on which the altitudes of celestial objects

are measured.

These vertical circles all meet in two points diametrically opposite, viz., the poles of the horizon; that one which is directly over the head of the observer is called his zenith, and the opposite one his nadir. That vertical which passes through the east and west points of the horizon is called the prime vertical; it necessarily intersects the meridian of the place (which passes through the north and south points) at rightangles.

The azimuth of a celestial object is an arc of the horizon, comprised between the meridian of the observer and the vertical circle through the object, and hence vertical circles are sometimes called azimuth circles.

The amplitude of a celestial object is the arc of the horizon, comprised between the east point and the point where the object rises, or between the west point and that where it sets; the one is called the rising amplitude, the other the setting amplitude. These definitions and remarks will suffice to render the following problems intelligible.

(72.) Given the sun's right ascension and declination to determine his

longitude and the obliquity of the ecliptic.

Let n EsQ represent the celestial meridian through the first of Cancer and Capricorn, that is, let it be the solstitial colure, ns the axis of the sphere, EQ the equator, eC the ecliptic, and nSs the

declination circle, passing through the sun S; then ARS is a right angle, and in the right-angled spherical e triangle ARS there are given the right ascension AR, and the declination RS to find the longitude AS, and the obliquity SAR, which is an easy operation in right-angled spherics. It is necessary, however, to remark

that as celestial longitude and right ascension are measured from A, the first point of Aries in the direction AS of the signs quite round the celestial sphere, when, of the four quantities in the problem, the obliquity and the declination are given to find the others, we must know on what side of the equinoxial the sun is, that is, whether the declination is north or south, for if the sun have the north declination RS, the longitude will be AS; but if it have the equal south declination R'S', the longitude being measured in the direction ASC round the globe to S', will be,

instead of A'S', 360° - A'S'.

It is moreover necessary to know not only on which side of the equinoctial the sun is, but also on which side of the tropic; for the sun, in passing from a tropic to the equinox, descends through the same gradations of declination as it ascended through in passing from the preceding equinox to the tropic, although its longitude and right ascension goes on increasing; in addition, therefore, to knowing whether the declination is north or south, we must also know whether it be increasing or decreasing, in order to determine the longitude and right ascension without ambiguity; and these particulars will be known from knowing the time of the year when the proposed declination is observed; thus from the 21st of March to the 21st June, during which time the sun is in the first quadrant of the ecliptic, the sun's declination is north and increasing; it afterwards continues to decrease, still remaining north, during the second quadrant, that is till the 23d of September, from which, till the 21st of December, that is, during the third quadrant, the declination is south and increasing, after which or during the fourth quadrant, the declination still south, decreases till the 21st of March.

1. Given the sun's right ascension on the 17th of May, 53° 38', and its declination 19° 15′ 57"; required his longitude and the obliquity of the ecliptic.

Applying Napier's rule to the right-angled triangle ARS, we have Rad. \times cos. AS = cos. AR cos. RS.

Rad. sin. $AR = \tan$. RS cot. $A : \cot$. $A = \frac{\text{Rad. sin. } AR}{2}$

Hence the computation for AS and A is as follows.

For the obliquity A For the longitude AS. cos. AR 53° 38' 0" 9.9059247 9.7730185 sin. AR 0.4565209 cos. RS 19 15 57 9.9749710 tan. RS arith. comp.

cos. AS 55 57 43 9-7479895 | cot. A 23° 27′ 501″ 10.3624456

2. On the 31st of March, 1816, the sun's declination was observed at Greenwich to be 4° 13′ 31½": required his right ascension, the obliquity of the ecliptic being 23° 27′ 51". The right ascension was 9° 47′ 59". on the ecliptic being 23° 27' 51". The right ascension, the obliquity 3. Required the sun's longitude on the 28th of November, 1810, when his declination was 21° 16' 4", and his right ascension, in time, 16' 14" 58'4", or in degrees 243° 44' 36".

The longitude

The longitude was 245° 39' 10", or 8 signs 5° 39' 10."

4. The sun's longitude being 8' 7° 40' 56", and the obliquity of the ecliptic 23° 27' 42\frac{1}{4}": required his right ascension in time. The right ascension is 16^k 23^m 34^s.

PROBLEM II.

Giving the sun's declination to find the time of his rising and setting

at any place whose latitude is known.

Let nEsQ represent the meridian of the place, Z being the zenith, and HO the horizon, and let s's" be the apparent path of the sun on the proposed day, cutting the horizon in S. Then the arc EZ will be the latitude of the place, and consequently EH, or its H equal QO, will be the colatitude, and this measures the angle OAQ; also RS will be the sun's declination, and AR, expressed in time, will express the time of sunrise from 6 o'clock, for nAs is the 6 o'clock hour circle.

Hence, in the right-angled triangle ARS, we have given RS and the opposite angle A to find AR, the time from 6 o'clock.

Required the time of sunrise at latitude 52° 13' N., when the sun's declination is 23° 28'.

By Napier's rule, Rad. sin. AR = cot. A tan. RS = tan. lat. tan. dec. tan. 23° 28′ - 9.6376106

tan. 52 13 10.1105786

9.7481892 sin. 34 3 211"

24 16' 13" 25" AR in time 6

43 46 35 = time of rising.

SCHOLIUM.

It should be here remarked that the time thus determined is apparent, time, which is that which would be shown by a clock so adjusted as to pass over 24 hours during one apparent revolution of the sun, or from its leaving the meridian to its return to it again, the index pointing to 12, when the sun is on the meridian. But it is impossible that any clock can be so adjusted, because the interval between the successive return of the sun to the meridian is continually varying, on account of the unequal motion of the sun in its orbit, and of the obliquity of the ecliptic; each of these varying intervals is called a true solar

Degrees are converted into hours by multiplying by 4 and dividing by 60.

day, and it is the mean of these during the year which is measured by the 24 hours of a well regulated clock, this period of time being a mean solar day; hence, at certain periods of the year, the sun will arrive at the meridian before the clock points to 12, and at other periods the clock will precede the sun; the small interval between the arrival of the index of the clock to 19 and of the sun to the meridian is called the equation of time, and it is given in page ii. of the Nautical Almanack for every day in the year; this correction, therefore, must always be applied to the apparent time determined by trigonometrical calculation to obtain the true time, or that shown by a well regulated clock or chronometer.

Another circumstance too must be taken into account, in order to determine the apparent time with rigorous accuracy, viz. the change in the declination of the sun from sunrise to noon. In the Nautical Almanack the declination of the sun is given for every day at noon, and if this be used in the computation, we shall assume that the declination has not varied from sunrise to noon, which is not the case; hence it will be necessary to compute the declination for the time of sunrise, as determined above, and then to resolve the problem with this corrected declination. The correction is obtained by taking from the Nautical Almanack the variation of declination in 24 hours, and then finding by proportion the variation for the time required.

2. Required the time of sunrise at latitude 57° 2′ 54″, when the sun's

declination is 23° 28' ? 34 11# 490.

3. How long is the sun above the horizon in latitude 58° 12′ N., when is declination is 18° 40′ S.? his declination is 18° 40' S.?

PROBLEM III.

Given the latitude of the place, and the declination of a heavenly body, to determine its altitude and azimuth when on the six o'clock hour circle.

Let HZPO be the meridian of the place, Z the zenith, HO the horizon, S the place of the object on the six o'clock hour circle PSp, which of course passes through the east and west points of the horicon, and ZSB the vertical circle passing through the sun. Then in the right-angled triangle SBA, the given quantities are AS, the declination, and the arc OP, or angle SAB, the latitude of the place, to find the altitude BS, and the azimuth BO from the north point O of



the horizon; or to find the complement AB of this azimuth, that is, the sun's bearing from the east.

EXAMPLES.

1. What was the altitude and azimuth of Arcturus, when upon the six o'clock hour circle of Greenwich, lat. 51° 28′ 40″ N., on the 1st of April, 1822; its declination on that day being 20° 6′ 50″ N.? By Napier's rule we have Rad. sin. BS = sin. A sin. AS.

Rad. cos. A Rad. $\cos A = \tan AB \cot AS \cdot \cot BO =$ cot. AS For the altitude For the azimuth. 51° 28′ 40″ 20 6 50 9.8934103 | cos. A 9-7943619 sin. A 9.5364162 cot. AS 10-4369645 sin. AS 20

9.4298265 cot. BO 77° 9′ 4″ 15 36 27 9-3561067 Hence the altitude is 15° 36' 27", and the azimuth 77° 9' 4" N.

At latitude 62° 12' N. the altitude of the sun at 6 o'clock in the morning was found to be 18° 20′ 23"; required his declination and azimuth. Declination 20° 50′ 12" N., Azimuth 79° 56′ 11" from N.
 On the 20th of November, 1822, the declination of Aldebaran was

3. On the 20th of November, 1822, the declination of Aldebaran was 16° 8′ 36″ N., what was its altitude and azimuth when on the six o'clock hour circle of Greenwich, lat. 51° 28′ 40″ N.?

Altitude 12° 32' 3", Azimuth 79° 46' 50" from N.

PROBLEM IV.

The latitude of the place and the declination of the sun being given to find the time when it is due east, or upon the prime vertical, and the altitude at that time.

Having drawn the meridian of the plane as before, the vertical circle ZAN, at right-angles to it, will be the prime vertical, A being the east point of the horizon HAO: also P being the elevated pole, and S the place of the sun, ZP will be the colatitude, PS the codeclination, ZS the coaltitude, and ZPS the hour angle, or time from noon; hence, in the right-angled spherical triangle SZP, there are given SP and PZ, to find SZ and the angle P. If the declination is not of

SP and PZ, to find SZ and the angle P. If the declination is not of the same name as the latitude, the sun will arrive at the prime vertical at S' before it rises: in this case the declination is to be considered as negative.

negative.

By Napier's rule Rad. cos. $P = \cot$. $SP \tan$. $PZ = \tan$. dec. cot. lat.

Rad. cos. $SP = \cos$. $SZ \cos$. $PZ \therefore \sin$. alt. $= \frac{Rad. \sin. dec}{\sin. lat}$.

EXAMPLES.

1. On the 1st of August, 1831, the sun's declination was 18° 10' 22' N., at what hour was he due east at Greenwich; and what was his altitude at that time?

For the hour angle. tan. dec. 18° 10′ 22″ cot. lat. 51 28 40	9·5162138 9·9009509	For the altitude. sin. dec 9.4939924 sin. lat 9.8934103
cos.hor.angle 74 51 7	9.4171647	sin. alt. 23° 29′ 37″ 9·6005821
4 ³ 59** 24* 28* 12		•

7~0~35~32. Hence the time is 35 seconds and a half past 7 o'clock, and the altitude $23^\circ~29'~37''.$

2. Given the sun's declination 5° 8' 26" N., and his altitude when due east 16° 53' 10"; required the latitude of the place.

Latitude 17° 58' N.

3. If the declination of a celestial object be 18° 4′ S., what is its altitude when on the prime vertical of latitude 27° 42′ S., and its distance from the meridian in time?

Altitude 41° 51'; Merid. distance in time 3h 26m 20°.

PROBLEM V.

To find the time when the apparent motion of a celestial object is perpendicular to the horizon, from having its declination and the latitude of the place given.

8

Let s s' represent the parallel of declination, or the apparent diurnal path of the body, and let the vertical ZSN be drawn to touch it in S; then S will be the place of the body when its apparent motion is in the direction SZ of the vertical, and therefore perpendicular to the horizon: through S draw the hour circle PS, which being the shortest distance from P to ZN, is perpendicular to it (p. 53); hence the triangle PSZ is right-angled at S, and in which we have given the colatitude ZP, and the codeclination PS, to find the hour



angle ZPS.

It is obvious that this problem will be impossible when 'Ps' exceeds PZ; that is when the declination is less than the latitude.

PROBLEM VI.

To determine upon what vertical a celestial object must be, in order that a small error, committed in taking its altitude, may have the least

possible effect upon the hour angle.

Let S be the place of the sun or other body, but by an error in taking its altitude let it be referred to S'. Draw S' S" parallel to the horizon, and meeting the parallel of declination ss' in S", then when the body is at S" it will really have the coaltitude ZS" = ZS', which it was erroneously supposed to have at S, so that in the determination of the hour angle P, from the colatitude, the coaltitude, and the codeclination, the small angle S' PS" will be the amount of the error.



As the triangle SS' S" is, of course, exceedingly small, it may be regarded as a rectilinear triangle, right-angled at S'; therefore SS' = SS" sin. S" and SS" = sin. PS SSS", (see page 73,) consequently,

$$SS' = \sin. S'' \sin. PS \cdot \angle SPS'' \therefore SPS'' = \frac{SS''}{\sin. S'' \sin. PS} . (1)$$

Now the angle S" is equal to the angle ZSP, because S' SS" is the complement of each, and therefore, by the relation between the sides and angles of a spherical triangle, we have

sin. S": sin PZ:: sin. SZP: sin. PS ∴ sin. S" sin. PS = sin. PZ sin. SZP.

Substituting the second member of this equation in (1), we have SS error in alt.

 $SPS'' = \frac{SS}{\sin PZ \sin SZP} = \frac{\cos \text{lat. sin. azimuth}}{\cos \text{lat. sin. azimuth}}$

This expression will obviously be the least possible when the sine of the azimuth is the greatest possible, or when the azimuth is 90°; that is, when the body is on the prime vertical.

Hence, indeducing the time from an altitude of any celestial body, it will be best to make the observation when the body is either exactly,

or nearly due east or due west.

PROBLEM VII.

The latitudes and longitudes of two celestial objects being given to

determine their distance apart.

Let P represent the pole of the ecliptic, and PS, PS', two arcs of celestial latitude, drawn to the two objects S S'; then will these arcs represent the colatitudes, the angle P will be the difference of longitude, and the arc SS' will be the distance sought, so that we have two sides and their included angle given to find the third side. In order to this, we must first de- S-



termine agreeably to the method explained at page 60, a subsidiary angle, ω , by the equation $\cot \omega = \tan PS \cos P$; after which the side SS' is found by the equation $\cos SS' = \frac{\cos PS \sin (\omega + PS')}{\sin \omega}$

EXAMPLES.

1. Required the distance between Procyon and Capella, the latitude of Procyon being 15° 58′ 14″ S., and its longitude 3° 22° 55′ 42″; also the latitude of Capella being 22° 51′ 57″ N., and longitude 2° 18° 57′ 57″?

Taking the difference of the longitudes, we have for the angle P, $P = 33^{\circ} 57' 45''$; and for the polar distances we have $PS = 105^{\circ} 58' 14''$, $PS = 67^{\circ} 8' 3''$; hence the logarithmic process will be as follows: tan. $PS = 105^{\circ} 58' 14'' - 10^{\circ} 5433466 \cos$, $PS = 9^{\circ} 4395590 \cos$. $PS = 33^{\circ} 57^{\circ} 45' - 9^{\circ} 187658 \sin$, ω , ar. comp. $0^{\circ} 4865396 \cos$. $OS = 160^{\circ} 57^{\circ} 46^{\circ} - 10^{\circ} 4621124 \sin$, $(\omega + PS') = 9^{\circ} 7978326 \cos$. $OS = 10^{\circ} 8^{\circ} 3^{\circ} \cos$, $OS = 10^{\circ} 3^{\circ$

 $\omega + PS' = 228 \quad 5 \quad 49.$

In this example cot. ω is negative, because tan. PS is negative, and tos. P positive; also cos. SS' is positive, because cos. PS is negative, sin. ($\omega + PS'$) negative, and sin. ω positive. The operation will obviously be similar, when, instead of the latitudes and longitudes, the right ascensions and declinations of the two bodies are given to find their distance apart.

- 2. The latitude and longitude of a star S. are 38° 40′ 26″ N., and 39° 2° 4′ 40′; and of a star S′., 13° 26′ 11″ N., and 9° 11° 41′ 26″; required their angular distance apart.

 Distance 127° 7′ 11″.
- 3. What is the distance between Sirius and Procyon, the right ascension of Sirius being 99° 0' 21", and its declination 16° 26' 35" S.; and the right ascension of Procyon 112° 6' 47", and its declination 5° 45' 3" N.

 Distance 25° 42' 10".

PROBLEM VIII.

Given the latitude of the place and the sun's declination to find the

beginning and end of twilight.

Twilight commences in the morning and ends in the evening, when the sun is about 18° below the horizon. Hence, if PZ (see the diagram to next problem) represent that portion of the meridian which is intercepted between the elevated pole and the zenith, and S' be that point in the sun's apparent path on any day which is 108° from Z, S' will be the place of the sun at the commencement of morning twilight, or at the termination of evening twilight; also PS' will be the codeclination, and PZ the colatitude; we thus have the three sides of the triangle PS'Z, to find the angle P. Hence, calling the sum of the three sides S, the formula for computing the hour angle P will be

sin.
$$\frac{1}{2}$$
 P = $\sqrt{\frac{\sin.(\frac{1}{2}S - ZP)\sin.(\frac{1}{2}S - PS')}{\sin. ZP\sin. PS'}}$; which is the same as $\sin.\frac{1}{2}$ P = $\sqrt{\frac{\sin.\frac{1}{2}(lat + 18^\circ + colec.)\sin.\frac{1}{2}(dec. + 18^\circ + colat.)}{\cos. lat. \cos. dec}}$;

a very convenient form for computation.

EXAMPLES.

1. At what time did twilight commence at Edinburgh, lat. 55° 57′ 20″ N., on the 20th of August, 1831, when the sun's declination was 12° 38′ 9″ N.?

sin. # P 760 54' 541" 9.9885745.

Hence $P = 153^{\circ} 49' 49'' = (in time) 10^{\circ} 15^{\circ} 191'$, so that twilight commenced in the morning at 14 44m 404, and ended in the evening at 104 15m 194s.

2. At what time does the twilight begin at latitude 48° 38′ 56″ N., when the sun's declination is 8° 28′ 54″ N.? Twilight begins at 3° 20...

3. At what time does twilight end at latitude 52° 12′ 35′ N. the sun's declination is 15° 55′ 25″ N.? Twilight ends at 10° I Twilight ends at 104 124".

PROBLEM IX.

Given the latitude of the place to determine on what day of the year the twilight is the shortest, and its duration on that day.

Let HO represent the horizon, and ho the parallel to it, 180 below it; also let PS be the declination circle, passing through the sun at sunset, and PZ, that passing through the zenith. Conceiving these two circles to revolve with S, PS will come to PS' when S comes to S', and IPZ will take some determinate position PZ'. Now, since the angles ZPS, Z' PS', are equal,



we have, by taking from each the common part Z'PS, ZPZ' = SPS'; but SPS', converted into time, expresses the duration of twilight, ZPZ' is therefore the least possible when the twilight is the shortest possible. Now since the sides PZ, PZ', are both given, the side ZZ' will be the shortest when the opposite angle, P, is the least; (see equa. (A) p. 47,) hence when ZZ' is the shortest, the twilight is the shortest; but as the two sides Z'S', ZS, of the triangle ZZ'S', are given, the third side will be shortest when the angle S' is the least possible, and this is the case when Z' falls on ZS', for then the angle is 0. Hence the twilight is chortest when the angle PSZ is considered to the part of the

shortest when the angle PSZ is equal to the angle PS'Z.

Let then z be the proper position of Z'; we shall have $Zz = Zh' - zh' = zS' - zh' = h'S' = 18^\circ$, and because PZ = Pz, the arc Pn, bisecting the angle ZPz, will also bisect the base Zz, and be perpendicular to

it (54); consequently, sin.
$$ZPn = \sin \cdot \frac{1}{8}SPS' = \frac{\sin \cdot Zn}{\sin \cdot PZ} = \frac{\sin \cdot 9^{\circ}}{\cos \cdot \text{lat.}}$$
 (1); also cos. $Pn = \frac{\cos \cdot PZ}{\cos \cdot Zn}$; and, in the right-angled triangle PnS' , $\cos \cdot PS' = \cos \cdot n \cdot S' \cos \cdot PZ = \frac{\cos \cdot n \cdot S' \cos \cdot PZ}{\cos \cdot Zn}$; that is, sin. dec. $= \frac{\sin \cdot 9^{\circ} \sin \cdot \text{lat.}}{\cos \cdot Zn} = \frac{\sin \cdot 9^{\circ} \sin \cdot \text{lat.}}{\cos \cdot Zn} = -\tan \cdot 9^{\circ} \sin \cdot \text{lat.}$ (2).

cos. 9º

The declination being known by this equation, the day of shortest twilight is also known, (Naut. Alm.) The declination will be of a contrary name with the latitude as its sine is negative. Equation (1) expresses the duration of the twilight. Since the angles ZPz, SPS, are equal, the hour angles for the beginning and ending of the morning twilight, or for the ending and beginning of the evening twilight, are ZPS', zPS'. Now, in the right-angled triangle PaS', we have

$$\sin nPS' = \frac{\sin S'n}{\sin PS'} = \frac{\sin 99^{\circ}}{\cos dec} = \frac{\cos 9^{\circ}}{\cos dec}$$
 (3)

The sum of (1) and (3) gives the angles ZPS', and their difference the angle zPS' = ZPS, and thus we have the hour angles for the beginning and end of the twilight.

EXAMPLES.

1. Required the time and duration of the shortest twilight at Green-

wich, lat 51° 25° 40°, 11	i me year ic			
For the day.		Fo	or the duration.	
tan. 9° .	9.1997125	sin	90 .	9.1943324
sin. 51° 28′ 40″	9.8934103	COS.	510 28' 40"	9.7943612
sin. dec. 7 7 5	9.0931228	sin.	14 32 49	9.3999712
The declination is the				Alm.) cor-
responds to March the				125.110.)

Also the hour angle SPS' is 29° 5' 38", which, in time, is 1^h 56^m 224,

the duration sought.

To find the times of beginning and ending of the twilight, we have, from the equation (3)

The angle *nPS', thus determined, is obtuse, because its opposite side is greater than PS, and this is opposite to a right-angle. This angle, converted into time, is 6* 22* 5‡*. Adding therefore, to this the angle ZP*, in time, that is half the duration, or 58* 11‡*, we have 7* 20** 154* the time when the evening trillight ends Also by subtract 164, the time when the evening twilight ends. Also, by subtracting the same quantity, we have 5, 23, 54 for the time when the evening twilight commences. These results respectively taken from 12, leave the time when the morning twilight begins and ends.

CHAPTER III.

ON THE PRINCIPLES OF NAUTICAL ASTRONOMY.

(73.) In our chapter on Navigation we have laid down several methods of determining the place of a ship at sea, by help of the account kept on board of its progress through the water, that is, of the course and distance sailed; and, if confidence could be placed in this account, even when kept with the utmost care, the art of Navigation would be perfect. Such perfection, however, it is hopeless to expect; for it does not seem possible to measure, with strict accuracy, either a ship's rate or the direction in which she moves, both of which may indeed be continually varying. In order, therefore, to determine the place of a ship at sea, with that accuracy which the safety of navigation requires, it is absolutely necessary that we be furnished with methods entirely independent of the dead reckoning, and these methods it is the business of Nautical Astronomy to teach. 8+

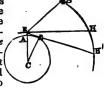
"It must not, however, be understood that the dead reckoning is without its value; on the contrary, when combined with astronomical observations, it is of considerable utility in detecting the existence and velocity of currents, and is indispensably necessary to fill up the short intervals which may occur in unfavourable weather between celestial conservations. But the too general practice of relying exclusively upon it cannot be sufficiently deprecated, and numerous instances might be adduced of the fatal consequences of this reliance, in the loss of vessels, from errors of such magnitude that they might have been detected by the most superficial knowledge of nautical astronomy, and the aid of even a good common watch." (Capt. Kater's Nautical Astronomy in the Ency. Met.)

On the Corrections to be applied to the observed Altitudes of Celestial Objects.

(74.) The true altitude of a celestial object is always understood to mean its angular distance from the rational horizon of the observer. This is not obtained directly by observation; but is the result of certain corrections applied to the observed altitude. These we shall now enumerate and explain.

Of the Dip or the Depression of the Horizon.

(75.) Let Erepresent the place of the observer's eye, and S the situation of any celestial body; the first object is to obtain its apparent altitude above the horizontal line EH; that is, the angular distance SEH. Now, as to the observer, the visible horizon is EBH', the altitude given by the instrument is the angle SEH'; hence we must subtract from this observed altitude the angle HEH', called the Dip or Depression of the Horizon, in order to obtain the apparent altitude SEH.



The angle HEH', or its equal C, is calculated for various elevations, AE of the eye above the surface of the sea from the proportion,

 $CE : EB = \sqrt{EC^2 - CB^2} :: rad. : sin. C;$

and the results are registered in a table.

Of the Semidiameter.

(76.) When the foregoing correction for dip has been applied, the result will be the apparent altitude of the point observed above the horizontal plane through the observer's eye. If this point be the uppermost or lowermost point of the disc of the sun or moon, a further correction will be necessary to obtain the apparent altitude of the centre; that is, we must apply the angular distance due to the semidiameter. quantity, both for the sun and moon, is given in the Nautical Almanac. But in the case of the moon the semidiameter itself requires a small correction depending upon the observed altitude. For the semidiameter, furnished by the Nautical Almanac, is the apparent horizontal semidiameter, or the angle it subtends when in the horizon; but as the moon approaches the zenith, her distance from the observer diminishes, and therefore her semidiameter is viewed under a greater angle. As she is nearer to the observer when in the zenith than when in the horizon, by one semidiameter of the earth, and as her distance from the earth's centre is about 60 semidiameters of the earth, the horizontal semidiameter will in the zenith become increased by about $\frac{1}{6}$ th part, and at intermediate elevations the increase will be as the sine of the altitude. On this principle is formed the Table at the end, entitled Augmentation of the Moon's Semidiameter, and containing the proper correction to be added to the given horizontal semidiameter to obtain the true semidiameter.

On account of the great distance of the sun, no such correction of his

semidiameter is necessary.

The corrections for dip and semidiameter being thus applied, the result is called the apparent altitude of the centre. In the case of the stars the only correction for the apparent altitude is the dip. It must, however, be here remarked, that if the centre of the object were visible, and its altitude, instead of that of the limb, were to be taken, we should not, after applying the correction for dip, obtain precisely the same result as that which we have just called the apparent altitude of the centre, but should get a value somewhat less. The reason of this is, that every vertical arc in the heavens is shortened by refraction, as we shall shortly explain, so that the centre would not exceed the observed altitude of the lower limb, or fall short of that of the upper, by so great a quantity as the true semidiameter. Hence, from the apparent altitude of the limb, a small quantity should in strictness be subtracted, and this small correction becomes necessary when the longitude is to be determined with accuracy. This correction was first proposed by Dr. Thomas Young. A table for it is given at the end.

To obtain the true altitude requires two other corrections, viz. for refraction and for parallax. The former of these has indeed an effect upon the two preceding corrections, dip, and semidiameter, which require certain modifications in consequence. One of these we have adverted to above, and the other will be noticed more particularly in

the following article.

Of Refraction.

(77.) It is a universal fact in optics, that if a ray of light pass obliquely out of one medium into another of greater density, it will be bent out of its original direction at the point when it enters the new medium, and proceed through it in a direction more nearly perpendicular to its surface at that point. Hence the rays of light, proceeding from the celestial bodies, become bent downwards as soon as they enter the atmosphere, their course being directed more nearly towards the centre of the earth, so that the rays which enter the eye of an observer, and by which any celestial object becomes visible to him, would, if not thus bent down, pass over his head; the object is therefore seen by him above its true place; the angle between this apparent direction, and the true direction of the object, measures the refraction; and, like the correction for dip, it is always subtractive; it increases from the horizon, where it is greatest, to the zenith, where it vanishes, as the rays from objects in the zenith enter the atmosphere perpendicularly.

It is the refraction which causes the sun and moon, when near the horizon, to present sometimes an elliptical appearance, the vertical diameter (and, indeed, every oblique diameter) seeming to be shorter than the horizontal, because the lower limb, or edge, being more elevated by refraction than the upper, the two are brought, in appearance, more

nearly together.

At the end of the volume we have given a table of refractions for different altitudes, from the horizon to the zenith, and adapted to the mean state of the atmosphere; but, as the actual state of the atmosphere generally differs from this, it becomes necessary, where the true altitude of the body is required with the utmost accuracy, to apply a correction to the numbers in this table, so as to adapt them to the existing temperature and density of the atmosphere at the time of observation,

as is indicated by the thermometer and barometer. The table of corrections is annexed to the table of mean refractions. It should, however, be observed that below 4° the refraction is very variable and uncertain, and such low altitudes should be avoided as much as possible at sea.

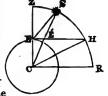
It will be unnecessary to use this annexed table for correcting the altitude of a celestial object when the latitude of the ship is the only object of the observation, as such a correction could seldom make a difference so great as half a mile in the resulting latitude; but in determining the longitude by the *Lunar observations*, the neglect of these small corrections would sometimes introduce an error in the resulting longitude of more than 30 miles.

It should be remarked here, that the dip, as determined in article (75), is on the supposition that refraction has not elevated the apparent horizon, but as such is not the case, the dip requires a correction; the amount of this correction is very uncertain, on account of the irregularity of the horizontal refractions although it is unquestionable that some correction is requisite. It is usual to allow about $1 \text{ or } \frac{1}{10}$ of the computed dip for the correction. In our table $\frac{1}{10}$ is allowed, which is according to Dr. Maskelyne, but Lambert and Legendre make it $\frac{1}{14}$.

When the foregoing corrections have been applied to the observed altitude, the result will be the true altitude of the centre above the visible horizon, and it remains now to apply the correction necessary to reduce this to the true altitude of the centre above the rational horizon; that is, to the altitude which the body would have if the observer were situated at the centre of the earth instead of on its surface.

Of the Parallax.

In order to explain the nature and effect of parallax, let S represent the place of the object observed from the surface of the earth, at E; then the angle SEH, that is, the observed angle when corrected for dip semidiameter, and refraction, will be the true altitude of the object, in reference to the observer's sensible horizon EH; and the angle SCR will be the true altitude, in reference to the rational horizon CR; and the difference of these angles is the parallax in altitude. If the



body be at H, in the sensible horizon, then the difference of which we speak is the entire angle HCR; this is called the horizontal parallax. Since the angle SEH is equal to the angle SCR, we have for the parallax in alt., SEH—SEH = ESC; that is, the parallax is the angle which the semidiameter of the earth subtends at the object; it is

angle which the semidiameter of the earth subtends at the object; it is obviously greatest in the horizon, and nothing in the zenith, and is the quantity which must be added to the true altitude above the sensible

horizon, to obtain the true altitude above the rational horizon.

The sun's parallax in altitude is given in a Table at the end; and the moon's horizontal parallax is given for the noon and midnight at Greenwich, of every day of the year, in the Nautical Almanack: and from the horizontal parallax thus obtained the parallax in altitude must be calculated. This is easy; for since in the triangle SEC, we have the proportion SC: EC:: sin. SEC = sin. SEZ = cos. SEH: sin ESC; it follows that the sine of the parallax in altitude varies as the cosine of the altitude, so that, as rad is to the cosine of the altitude, so is the sine of the horizontal parallax, to the sine of the parallax in altitude. In other words, the log. sine of the horizontal parallax, added to the log. cosine of the altitude, abating 10 from the index, will give the log. sine

of the parallax in altitude; but as the parallax is always a very small

angle it is usual to substitute the arc for its sine, so that

log. hor. par. in seconds + log. cos. alt. - 10 = log. par. in alt. in seconds. We must observe here that the horizontal parallax, given in the Nautical Almanack, is calculated to the equatorial radius of the earth; and, therefore, except at the equator, a small subtractive correction will be necessary, on account of the spheroidal figure of the earth. A table of such corrections is given at the end, and explained in the introduction to the tables.

Such are the corrections necessary to be applied to the observed altitudes of celestial objects in order to obtain their true altitudes. A few other preliminary, but very simple, and obvious operations must also be performed upon the several quantities taken out of the Nautical Almanack, in order to reduce them to their proper value at the time and place of observation; for the elements furnished by the Nautical Almanack are computed for certain stated epochs, and their values for any intermediate epoch must be found by proportion. But ample directions for these preparatory operations are contained in the "Explanation of the Articles in the Nautical Almanack," by the late Dr. Maskelyne, which accompanies every edition of that work.

Example of the Corrections.

1. On the 14th of January, 1833, suppose the observed altitude of the sun's lower limb to be 16° 24′, the observer's eye to be 18 feet above the level of the sea, the barometer to stand at 29 inches, and the thermometer at 58°: required the true altitude of the sun's centre.

Observed alt. O's L. L.	16°	36′	4"
Depression of the horizon -	_	4	4
App. alt. of L. L Refraction Correction for Barometer - Correction for Thermometer	16	32 3	0 14 6·5 3·2
True alt. of L. L. above visible horizon Sun's semidiameter (Naut. Alm.) Parallax in altitude	16	28 16 +	36·3 17·3 8·4
True altitude of Sun's centre - 1	16	45	2.

2. On the 20th of May, 1833, suppose that in longitude about 77° 30 west, and lat. about 48° north, at 3° apparent time, the altitude of the moon's lower limb is observed to be 18° 8′ 34″, the height of the eye being 20 feet, the barometer 28°5 inches, and the thermometer 46°: required the true altitude of the sun's centre. Here the object being the moon, it will be necessary to compute the parallax in altitude, from having the horizontal parallax corresponding to the time at Greenwich.

The horizontal parallax is given in the Nautical Almanack for every noon and midnight; and, therefore, to find it for any other intermediate time, we must say as 12^h is to its variation in 12^h, so is the proposed

time to the variation due to that time.

In like manner must the moon's semidiameter be reduced, by proportion to the time of observation, since it sensibly varies in the course of a few hours. We shall begin, therefore, with finding in this way the true horizontal parallax and semidiameter for the time of the observation reduced to the meridian of Greenwich.

Longitude of the ship in time 5 10^m after Greenwich time. Apparent time at ship 3 0

	_			
Apparent time at Gr Hor. par. at noon (Naut. Alm Hor. par. at midnight .		Semidiam. at noon Semidiam. at midnight		′ 53″ 57
Variation in 124 .	0 14	Variation in 12 ^k	0	4
∴ 12 ^h : 8 ^h 10 ^m :: 14": Hor. par. at noon	9·5 58′ 17	.: 12 ^h : 8 ^h 10 ^m :: 4": Semidiameter at noon Hor. semidia. at re-	15′	2·7″ 53
Hor. par at reduced time	58 26·5 60		15	55·7″ 5·2
Ditto in seconds	3506.5			
Dim. of par. for lat. 48°	-6·3	True semidiameter	16	0-9
True hor. parallax	3500-2			
For t	he Appdren	t Altitude.		

Observed altitud Depression Semidiameter m	e of D		Ĺ.	•	180 8	Ļ	
Apparent alt.)'s cer	ntre		•	18 2	0	14.9.
For 1	he Par	rallaz	in A	ltitud	e.		
cos. D's app. all hor. parallax	. 180 20	Y 15"			9·97 3·54		
Par. in altitude	3322:5	''			3.52	14	1597
I	or the	true .	Altitud	e.			
Apparent alt.of) 's cen	tre			180 20		
Ref-action					_ 2		
Barometer					-	-	8.8
Thermometer		•	•		. +	-	1.4
True alt. above Parallax in altit			zon 3322-5				
True alt. of D's	centre				19 19	2	35.8.

True alt. of D's centre 19 12 35-8.

These two examples will serve for specimens of the corrections to be applied to an observed altitude, in order to deduce from it the true altitude of the body's centre. In the case of the moon, the corrections, when the utmost accuracy is sought, are rather numerous, as the last example shows. But in finding the latitude at sea, it is usual to dispense with some of these, more especially with the corrections for temperature, for the contraction of the moon's semidiameter, and for the spheroidal figure of the earth; because an error of a few seconds in the true altitude will introduce no error worth noticing in the resulting latitude. When, however, the object of the observer is to deduce the longitude of the ship, all the data, furnished by observation, should be as accurate as possible; for the problem is one of such delicacy that by neglecting to allow for the influence of temperature would alone introduce in some cases an error of from 30 to 40 miles in the longitude.

When the object observed is a star, several of the foregoing corrections vanish: the only corrections, in this case requisite, are those for dip and refraction, modified as usual for the temperature.

(78.) To determine the latitude at sea from the meridian altitude of any clestial object whose dectination is known.

The determination of the latitude, by a meridian altitude, is the easiest, and in general the safest, method of finding the ship's place on the meridian; for both the observations and the subsequent calculations being few, they are readily performed, and with but little liability to error in the result; this method, therefore, is always to be used at sea,

unless foggy or cloudy weather render it impracticable.

The declination of the object observed is supposed to be given in the Nautical Almanack for the meridian of Greenwich; it may therefore be reduced to the meridian of the ship by means of the longitude by account, which will always be sufficiently accurate for this purpose, although it should differ very considerably from the true longitude, because declination changes so slowly that even an error of an hour in the longitude would cause an error in the declination too small to deserve notice.

Having then thus found the distance of the object from the equinoctial, and having, by means of the observed altitude properly corrected, obtained the distance of the same object from the ship's zenith, the distance of the zenith from the equinoctial, that is, the latitude, imme-

diately becomes known.

1. Let S be the object observed, the zenith Z being to the north of it, and the object itself north of the equinoctial EQ, then the latitude EZ is equal to the zenith distance, or coaltitude ZS + the declination, and it is north.

2. Let S' be the object, still north of the equinoctial, but so posited that the zenith is south of it, then the latitude EZ is equal to the difference between the zenith distance S'Z, and declination S'E, and is

still north.

3. Let now the object be at S", south of the equinoctial, and the zenith to the north of the object, then the latitude EZ is equal to the difference between the zenith distance S"Z and declination S"E, and it is north.

We have here assumed the north to be the elevated pole, but if the south be the elevated pole, then we must write south for north, and north for south. Hence the following rule for all cases. Call the



zenith distance north or south, according as the zenith is north or south of the object. If the zenith distance and declination be of the same name, that is, both north or both south, their sum will be the latitude; but, if of different names, their difference will be the latitude, of the same name as the greater.

EXAMPLES.

1. If on the 2d of May, 1833, the meridian altitude of the sun's lower limb be 47° 18′, height of the eye 20 feet, and longitude by account 32° E.: required the latitude, the sun being south at the time of observation.

The longitude in time is 2^h 8^m east, so that time at Greenwich is 2^h 8^m before the noon of the 2d of May; hence, to find the corresponding declination, we have, by the Nautical Almanack, 24^h : 2^h 8^m : 18^r 1^r : 1^r 1^r 1^r so that, 1^r 1^r 1^r 1^r the variation in 2^h 8^m , must be subtracted from 15° 23^r 21^r 1^r $1^$

Observed alt. of ⊙'s L. L.	47° 18′ 0″
Dip.	— 4 17
App. alt. of ©'s L. L.	46 13 43
Refraction	- 56
Parallax	+ 6
Semidiam. (Naut. Alm.)	15 53
True alt. of O's centre Zenith distance	46 28 46 43 31 14 N. 15 21 43 N.

Latitude 58 52 57 N.

2. On the first of January, 1820, the meridian altitude of Capella was 27° 35′, the zenith being south of the star, and the height of the eye 22 feet; required the latitude,

Observed altitude Dip -	•	27° 35′ 0″ — 4 30
Apparent altitude - Refraction	. •	27 30 30 - 1 51
True altitude Zenith distance Star's dec. (Naut. Alm.)	· · ·	27 28 39 62 31 21 S. 45 48 39 N.

16 42 42 S.

Latitude - - -

3. On the 19th of February, 1823, the ship being in longitude 40° W, the observed meridian altitude of the moon's lower limb was 55° 6'; the zenith north of the moon; and the height of the eye 16 feet: required the latitude.

Here the time of observation at the ship is not given, it must therefore be calculated, and we have these data for this purpose, viz. that the ship is 40° W. of Greenwich, and that the moon is on its meridian.

The following process therefore immediately suggests itself.

The moon passed the merid. of Green wich Feb. 19 (Naut. Alm.) 6^h 56^m 0

Fig. 20 Feb. 2

Interval between the two passages - 24 + 1 3 0. Hence 1^h 3^m is the moon's retardation in 25^h 3^m, and by proportion using for the longitude 40° W., its value in time 2^h 40^m, we have,

25h 3m: 1h 3m: 2h 40m: 0h 6m 42;

that is, the moon is retarded 6^m 42^s in passing from the meridian of Greenwich to that of the ship, and, therefore, instead of the apparent time at the ship being 6^h 56^m , as it necessarily would be if there were no retardation, it will be 6^m 42^s later. Hence

Apparent time at the ship Ship's longitude W. - 7^{h} 2^{m} 42^{m} 42^{m}

Time at Greenwich - - 9 42 42.

Having thus got the apparent time at Greenwich when the observation was made, we may, by a reference to the Nautical Almanack and a subsequent proportion, find the moon's declination at that time: thus

Moon's declination at Greenwich, Feb. 19 at noon 26° 38′ 17″ 26 54 39

Change of declination in 12 hours - - - 16 22. .: 12^h: 9^h 42^m 42^s:: 16' 22'': 13' 15''; hence 13' 15" is the amount of the change of declination, from noon to 9*43", on the supposition, however, that the motion of the moon in declination may be considered as equable during the twelve hours. But on account of the irregular motion of the moon, this supposition introduces a sensible error, which may however be corrected by means of the table of "Equation of second Differences," given in the Nautical Almanack, and explained in Dr. Maskelyne's accompanying "Explanation." The correct change of declination is thus found to be 14' 16". But from the year 1833, the declination of the moon will be given in the Nautical Almanack to every three hours, and the change for any shorter interval may then be obtained with the requisite accuracy by proportion, as above. Taking in the present case 14' 16" for the correct change, we

above.	Taking in the present case 14 10	101 the correct change, we
have	Declination for preceding noon Increase of Declination -	26° 38′ 17″ N. 14 16
duce the Observe Dip. Semidie	Declin. at the time of observation re we can find the proper correction e apparent altitude of the centre, ed altitude of) 's L. L. ameter (Naut. Alm.)	26 52 33 N. for parallax, we must de- 55° 6′ 0′′ — 3 50 16 13 13
Hor. pa	nt alt. of)'s centre r. in seconds at 9 th 43 th (Naut. Alm.) x in altitude in seconds	55 18 36 cos. 9·7552161 3572 log. 3·5529115 2033 log. 3·3081276
thereio	re the correction for parallax is 33′ 53	S''.

Having thus reduced all the corrections to the time of observation, we readily obtain the true altitude, and thence the latitude as follows,

Apparent alt. of Refraction Parallax in altitu	D's centre		55°	48' 36" — 40 33 53
True altitude Zenith distance Declination	:	٠	55 34 26	51 49 8 11 N. 52 33 N.
Latitude .	_	_	61	0 44 N

SCHOLIUM.

These examples will, no doubt, be found sufficient to put the student in possession of the method of applying the various corrections to the observed meridian altitude of a celestial object, in order to deduce from it the latitude of the ship. But it should be remarked, that in most works on Nautical Astronomy, subsidiary tables are inserted for the purpose of abridging some of the foregoing corrective operations; such tables, therefore, offer very acceptable aid to the practical navigator. The most esteemed works of this kind are Dr. Mackay's "Treatise on the Theory and Practice of finding the Longitude at Sea;" the "Nautical Tables" of J. De Mendoza Rios, and Mr. Riddle's book on Navigation and Nautical Astronomy.

It should also be observed here, that in the preceding examples the celestial object is supposed to be on the meridian above the pole; that is, to be higher than the elevated pole. But, if a meridian altitude be taken below the pole, which may be done if the object is circumpolar,

or so near to the elevated pole as to perform its apparent daily revolution about it without passing below the horizon, then the latitude of the place will be equal to the sum of the true altitude, and the codeclination or polar distance of the object; for this sum will obviously measure the elevation of the pole above the horizon, which is equal to the latitude.

(79.) To determine the latitude at sea, by means of two altitudes of the

sun, and the time between the observations.

In the preceding article we have shown how to determine the latitude of the ship by the meridian altitude of the sun, or of any other heavenly body, whose declination may be found. But, as already remarked, the object we wish to observe may be obscured when it comes to the meridian, and this may happen for many days together, although it may be frequently visible at other times of the day. As therefore the opportunity for a meridian observation cannot be depended upon, it becomes an important problem to determine the latitude at sea, by observations made out of the meridian; and considerable attention has accordingly been paid, by scientific persons, to the method of finding the latitude by "double altitudes," and various tables have been computed to facilitate the operation. But the direct method, by spherical trigonometry, though rather long, involving three spherical triangles, will be more readily remembered, and more easily applied by persons familiar with the rules and formulas of Trigonometry, than any indirect or approximative process; we shall therefore explain the direct method.

Let P be the elevated pole, Z the zenith of the ship, and S, S' the two places of the sun when the altitudes are taken. Then, drawing the great circle arcs as in the figure, we shall have these given quantities, viz. the codeclinations PS, PS'; the coaltitudes ZS, ZS', and the hour angle SPS', which measures the interval between the observations; and the quantity sought is the coaltitude ZP. Now, in the triangle PSS', we have given two sides and the included angle

to find the third side SS', and one of the remaining angles, say the angle PSS'. In the triangle ZSS' we have given the three sides to find the angle S'SZ; having then the angles PSS', S'SZ, the angle ZSP becomes known, so that we have lastly, two sides and the included angle in the triangle ZSP, to find the third side ZP.

Before the application of the trigonometrical process, the observed altitudes must, of course, be reduced to the true altitudes, as in the preceding examples. Moreover, as the ship most probably sails during the interval of the observation, an additional reduction becomes necessary; the first altitude must be reduced to what it would have been if taken at the place where the second was taken: this correction will be known if we know the number of minutes the ship has sailed directly towards or directly from the sun, upon leaving the place where the first observation was made. To find this, take the angle included between the ship's course and the sun's bearing, at the first observation; and considering this angle as a course, and the distance sailed as the corresponding distance, find by the traverse table, or by the operation of plane sailing, the difference of latitude, which will be the amount of the approach to, or departure from, the sun. This must be added to the first altitude if the angle is less than 90°, because the ship will have approached towards the sun; but it must be subtracted when the angle exceeds 90°. If the angle is 90° no correction for the ship's change of place will be necessary.

The truth of this correction will be immediately seen by considering that if the sun's centre were the elevated pole, what is in reality the

coaltitude would then be the colatitude, and, therefore, that, by whatever quantity this latter is increased or diminished by the ship's motion, on the one hypothesis, by the same quantity will the former be increased

or diminished on the other hypothesis.

Where great accuracy is aimed at, account should be taken of the ships change of longitude during the interval of the observations; when converted into time it must be added to the interval of time between the observations when the ship has sailed eastward, and subtracted when she has sailed westward. This correction is very easily applied.

Having thus mentioned the necessary preparative corrections, we

shall now give an example of the trigonometrical operation.

Let the two zenith distances corrected be (see last fig.) $ZS = 73^{\circ} 54'$ 13", ZS' = 47° 42° 51", the corresponding declinations 8° 18' and 8° 15' north, and the interval of time three hours; to determine the latitude.

Considering SS' to be the base of an isoceles spherical triangle, of which one of the equal sides is $\frac{1}{2}(PS + PS') = 81^{\circ} 43' 30''$, and the vertical angle equal to 3^h or 45°, let the perpendicular PM be drawn, then we have in the triangle PMS right-angled at M, PS = 81° 43' 30''

20						as follows.
	•		from th	se trian	gle PM	
sin. PS 81° 43 sin. P 22 30						9·9954547 9·5828397
sin. SM 22 15		3	•	•		9-5782944
88' = 44 30	22.6	- 5.				
n. To	find	PSS'	from	the tric	ingle Ps	38'.
sin. 88' 44°	30' 2	2.6"	-	ari	th. comp	0. 0.1542898
sin. PS' 81		0	-	-		9.9954822
sin. SPS' 45	0	0	-	-		9.8494850
sin. PSS' 86			-		-	9.9992570
This angle is acute	e like	its of	posite	side, (see art. (60.)
m. 2	To fin	nd ZS	S' in t	he trian	gle ZSS	3'
ZS' 47	0 45	51"				
sm. ZS 73	54	13	•	aritl	h. comp.	0.0173696
sin. 28 73 sin. 88' 44	30	22-6	-	aritl	ı. comp.	0-1542898
2)166						
´ <u> </u>						
1 Sum = 8						0.0000000
L (1 Sum — ZS)	9 11	50.07	-	•	•	9-2030206
. (i Sum — SS') 3	0 34	90-7	-	•	•	9.7949179
					2)19-1695969
sin. 1 ZSS' 2	2 36	26:4			_	9.5847985
			/ AS	12' 52	-9//	5 5011000
	٠.	Z 55	= 50	- LO UO	0	
am. y 200 x				38 58		

1v. To find ZP in the triangle ZSP.

tan. PS 81° 42′ 0″ - 10·8359917, cos. PS - 9·1594364
cos. PSZ 41° 26′ 5·2′ - 9·8748930, sin. ω, ar. comp. :7189561
cot. ω 11′ 0 41·2′ - 10·7108847, sin. (ω + ZS) 9·9989874

3 54 54.2 sin. 48° 49′ 59.7″

9-8766779

 $\omega + ZS = 84 54 54 2.$

Hence the latitude is 48° 50'.

2. The two corrected altitudes are 42° 14' and 16° 5' 47", the corresponding declinations 8° 16' 30" and 8° 15', and the time between the observations 3 hours; required the latitude of the place.

Upon the same principle may the latitude be determined from the altitudes of two fixed stars, taken at the same time; in this case S, S', in the preceding figure, will represent the two stars; PS, PS', their known polar distances, and the angles SPS' the difference of their right ascensions; the same quantities are therefore given as in the case of the sun, but as in the case of two stars PS, PS', may differ very considerably; SS' cannot be considered as the base of an isosceles triangle, but must be computed from the other two sides and their included angle. In the Nautical Almanack for 1925 Dr. Brinkley has computed for 1822, and tabulated, the distances SS' for certain pairs of stars, conveniently situated for observation, and has annexed the change of distance corresponding to 10 years. The same table shows also the difference of right ascension for each pair of stars, with the change in 10 years; so that by help of this table the computation for finding the latitude from the simultaneous altitudes of two fixed stars becomes considerably abridged.

For other methods of determining the latitude, the student may consult "Mackay on the Longitude," vol. 1., and Captain Kater's Nautical Astronomy, in the Ency. Metropolitan, &c.

On finding the Longitude by the Lunar Observations.

(80.) There are several astronomical methods of determining the longitude of a place, which cannot be accurately employed at sea, on account of the great difficulty of managing a telescope on shipboard; we shall not, therefore, enter here into any explanation of these methods, but shall confine ourselves to the lunar method of determining the longitude, which is justly regarded as the principal problem in Nautical Astronomy. Before entering upon the solution of this problem it will be necessary to make a few introductory remarks.

The determination of the longitude of a place always requires the solution of these two problems, viz. 1st, to determine the time at the place at any instant; and, 2d, to determine the time at the first meridian, at the same instant; for the difference of the times converted into degrees, at the rate of 15c to an hour, will obviously give the longitude.

at the rate of 15° to an hour; will obviously give the longitude.

When the latitude of the place is known, (and it may be found by the methods already explained,) the time may be computed from the altitude of any celestial object whose declination is known; for the coaltitude, codeclination, and colatitude, will be three sides of a spherical triangle given to find the hour angle, comprised between the codeclination and the colatitude. But to find the time at Greenwich requires the aid of additional data, besides those furnished by observations made at the place. The Greenwich time may, indeed, be obtained at once, independently of any observations at the place, by means of a chronometer,

carefully regulated to Greenwich time, provided it be subject to no irregularities after having been once properly adjusted. A ship furnished with such a timepiece always carries the Greenwich time with her,* and the longitude then becomes reduced to the problem of finding the time at the place. Chronometers are now brought to such a state of perfection that very great dependence can be placed on them, and they are accordingly always taken out on long voyages for the purpose of showing the Greenwich time, and are thus of great use to the mariner. Still, however, as the most perfect contrivance of human art is subject to accident, and the more delicate the machine the more liable is it to disarrangement, from causes which we may not be able to control, it becomes highly desirable, in so important a matter as finding the place of a ship at sea, to be possessed of methods altogether beyond the influence of terrestrial vicissitudes, and such methods the celestial motions alone can supply. The angular motion of the moon in her orbit is more rapid than that of any other celestial body, and sufficiently great to render the portion of its path passed over in so short a time as two or three seconds, a measurable quantity even with a small portable instrument (the sextant).

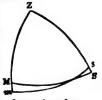
It is obvious, therefore, that if the distance of the moon's centre from any celestial body, in or near her path, be computed for any Greenwich time, and this distance be found the same as that given by actual observation at any place, then the difference between the time of observing the phenomenon and the time at Greenwich, when it was predicted to happen, will give the longitude of the place of observation. Now in the Nautical Almanack the distances of the moon from the sun, and from several of the fixed stars near her path, are given for every three hours of apparent Greenwich time, and for several years to come; and the Green wich time, corresponding to any intermediate distance, is obtained by simple proportion, with all requisite accuracy; so that by means of the Nautical Almanack we may always determine the time at Greenwich

when any distance observed at sea was taken.

The distances inserted in the Nautical Almanack are the true angular distances between the centres of the bodies, the observer being considered as at the centre of the earth, and to the true distance therefore every observed distance must be reduced; it is this reduction which constitutes the trigonometrical difficulties of the problem; and it consists in clearing the lunar distance from the effects of parallax and refrac-

tion; how to do this it is now our business to explain.

Let m, s, be the observed places of the moon and sun, or of the moon and a fixed star, and let M, S, be their true places. M will be above m, because the moon is depressed by parallax more than it is elevated by refraction; but S will be below s, because the sun is more elevated by refraction than it is depressed by parallax. Observation gives the apparent distance ms, and the apparent zenith distances Zm, Zs: by applying the proper corrections to these latter we also deduce the true zenith distances ZM, ZS, and with these data we are to determine the true distance, MS, by computation.



Put d for the apparent distance. D true distance. apparent altitudes.

true altitudes.

^{*}As chronometers show mean time, the equation of time must be applied to obtain the apparent time at Greenwich.

```
cos. D — sin. A sin. A'
 Then in the triangle MZS, we have cos. Z -
                                                                              cos. A cos. A'
and in the triangle #Zs, cos. Z = \frac{\cos a - \sin a \sin a'}{\cos a \cos a'}
 hence, for the determination of D, we have this equation, viz.
             cos. D — sin. A sin. A' = cos. d — sin. a sin. a'
                   cos. A cos. A'
 from which we immediately get
cos. D == (cos. d - sin. a sin. a') \frac{\cos. A \cos. A'}{\cos. a \cos. a'} + sin. A sin. A'
\frac{\cos d + \cos (a + a') - \cos a \cos a'}{\cos A \cos A' + \sin A} \sin A'
                        cos. a cos. a'
= \frac{2\cos.\frac{1}{4}(a+a'+d)\cos.\frac{1}{4}(\overline{a+a'} \sim d)\cos.A\cos.A'}{\cos.(A+A').(1)}
                                 cos. 4 cos. 4'
= \frac{2\cos A}{(a+a'+a)\cos A}\cos A\cos A' - 1\cos(A+A');
                         \cos a \cos a' \cos (A + A')
or calling the first term within the brackets 2 \cos^2 F, \cos D = (2 \cos^2 F - 1) \cos (A + A') = \cos 2 F \cos (A + A'). (2). The formulas marked (1) and (2) are both of them convenient for the computation of D; a third formula may be obtained from (1), as follows.
Subtract each side of (1) from 1; then since (p. 37,)
1-\cos D=2\sin^2\frac{1}{2}D, 1+\cos (A+A')=2\cos^2\frac{1}{2}(A+A'),
we have, after dividing by 2,
\sin^{2} D = \cos^{2} (A+A') - \frac{\cos A(a+a'+d)\cos A(a+a'-d)\cos A\cos A\cos A'}{\sin^{2} D\cos B\cos B\cos A\cos A'}
                                                                   cos. a cos. a'
=\cos^{\frac{1}{2}}(A+A')\left\{1-\frac{\cos\frac{1}{2}(a+a'+d)\cos\frac{1}{2}(a+a'-d)\cos.A\cos.A'}{\cos^{\frac{1}{2}}(a+a'+d)\cos^{\frac{1}{2}}(a+a'-d)\cos.A\cos.A'}\right\};
cos. a cos. a' cos. a' (A + A') or, calling the second term within the brackets \sin^2 \theta,
\begin{array}{c} \sin^2\frac{1}{\theta}D=\cos^2\frac{1}{\theta}(A+A')\cos^2\theta\\ \therefore \sin\frac{1}{\theta}D=\cos\frac{1}{\theta}(A+A')\cos\theta\\ \end{array}
This latter is Borda's formula.
    We shall solve an example by each of these formulas.
                                                EXAMPLES.
1. Suppose the apparent distance between the centres of the sun and moon to be 83° 57′ 33″, the apparent altitude of the moon's centre 27° 34′ 5″, the apparent altitude of the sun's centre 48° 27′ 32″, the true
attitude of the moon's centre 28° 20′ 48″, and the true altitude of the sun's centre 48° 26′ 49″; then we have d=83^\circ 57′ 33″, a=27^\circ 34′ 5″, a'=48^\circ 27′ 32″; A=28^\circ 20′ 48″, A'=48^\circ 26′ 49″;
and the computation for D, by the first formula is as follows:
           \begin{cases} d & 83^{\circ}55' \ 33'' \\ a & 27 \ 34 \ 5 \end{cases}
                                                                     0523390
                                              comp. cos.
           (a' 48 27 32
                                                                     1783835
                                              comp. cos.
               2)159 59 10
                                              log. 2
                                                                     3010300
l sum
                    79 59 35
                                                           cos. 9:2399686
                                                           cos. 9.9989587
sum \sim d
                    3 57 58
                   28 20 48
                                                           cos. 9.9445275
             A' 48 26
                                                           cos. 9.8217187
(Reject 40 from index) 1.5369260 = log. .3442921 +
                         True distance 83° 20′ 54″
                                                                             nat. cos. 1158326.
```

By glancing at the formula (1), we see that 30 must be rejected from the sum of the above column of logarithms, so that the logarithmic line resulting from the process is 9.5369260. Now, as in the table of logsines, log. cosines, &c., the radius is supposed to be 10¹⁰, of which the log. is 10, and in the table of natural sines, cosines, &c., the rad. is 1, of which the log. is 0; it follows that when we wish to find, by help of a table of the logarithms of numbers, the natural trigonometrical line corresponding to any logarithmic one, we must diminish this latter by 10 and enter the table with the remeinder. Hence the sum of the fore-10, and enter the table with the remainder. Hence the sum of the foregoing columns of logarithms must be diminished by 40, and the remainder will be truly the logarithm of the natural number represented by the first term in the second member of the equation (1). If this natural number be less than nat. $\cos (A + A')$, which is to be subtracted from it, the remainder will be negative, in which case **D** will be obtuse.

By the second formula the process is as follows:

d a a'	83° 27 48	34			•	comp.	cos.	0·0523390 0·1783835
2)159	59	10					
isum isum ∼ d A A A + A	3 28 48	20 26			-	•	cos.	9-2399686 9-9989587 9-9445275 9-8217187 0-6411909 —
							2)1	9.8770869
F	29	46	3	•	•		cos.	9.9385434
2 F	59	32	6				cos.	9.7050182+
							_	

True distance 83° 20' 54" cos. 9.0638273.

In adding up the logarithms to find cos. *F, 20 must be rejected from the index; and the logarithm marked —, is to be subtracted from that marked +. Moreover, if A + A and 2 F are both acute or both obtuse.

We shall now exhibit the process by Borda's formula.

d 83° 57′ 33″ a 27 34 5 a′ 48 27 32	comp. cos. 0.0523390 comp. cos. 0.1783835
2)159 59 10	
3 57 58 A 28 20 48 A 48 26 49	- cos. 9-2399686 cos. 9-9989587 cos. 9-9445275 - cos. 9-8217187
A + A' 76 47 37	2)39-2358960
1 (A + A) 38 23 481	19·6179480 cos. 9·8941654 +
8 31 57 53½	- sin. 9.7237826

cos. 9-9985870 +

D 41º 40' 27" sin. 9-8227524 \therefore D = 83 20 54, the true distance.

An estimate may now be formed of the relative advantages of these three methods, as regards practical facility. We are inclined to pre-fer the first method, which we believe is new, as fewer references to the tables are requisite, and as, moreover, there are no arithmetical operations required, besides those which are actually exhibited. The second and third methods seem to offer nearly equal advantages; in the first of these, however, it may be observed that the trigonometrical lines involved are all of one name, viz. cosines, and that the final reference to the tables gives the true distance instead of its half, as in the last method.

Each of the foregoing processes may be shortened by using a subsidiary table, containing the various values of the expression cos. A cos. A' Such a table computed to every degree of the moon's cos. a cos. a'

apparent altitude, and to every 10 seconds of her horizontal parallax, forms Table ix. of the Requisite Tables, published by order of the Commissioners of Longitude. But a more complete table of this kind is given in the second volume of Dr. Mackay's work, on the Longitude. If each number in this table were increased by the constant number 3010300, the table itself would become somewhat simplified, and the process of clearing the distance by our first method would be rendered remarkably short and convenient.

The preceding example is taken from Woodhouse's Astronomy, part n., p. 859, where the day of observation is stated to be June 5, 1793. Now by the Nautical Almanack, for that year, we have

Distance at 15^h 83° 6′ 1″, Also at time of observation D = 83° 20′ 55″

at 18^h 84 28 26 at 15^h D = 83 6 1

Increase in 3^h 1 22 25, Incs. between 15 and time of obs. 0 14 54 ... 1° 22′ 25″: 14′ 54″ ... 3^h : 32″ 33′.

Hence, when the observation was made, the apparent time at Green-

wich was 15' 32" 33'.

To find the time at the ship, requires that we know the latitude of the place and the sun's declination. The former, therefore, must have been previously ascertained, and the latter may now be found by means of the apparent Greenwich time just deduced, and the Nautical Almanack. We shall suppose the latitude to be 10° 16′ 40″S.; the sun's declination will be 23° 22′ 28″, and taking the true altitude of the sun = 48° 46′ 49″, we shall thus have, in order to find the time, three sides of a spherical triangle to find an angle. The computation is as follows.

coalt. 41° 33′ 11″ sin. colat. 79 43 20 arith. comp. 0°0070251 sin. sun's polar dist. 113 22 48 arith. comp. 0°0372078

2)234 39 19 117 19 39.5 37 36 19.5 9.7854864 3 56 51.5 8.8378712 sin. 2)18.6675905

sin. 12º 97' 174"

9.3337902

Hour angle = 94 54 35 = 1^{3} 39 38 3 in time.

Time at Greenwich

15 32 33

13 52 54·7.

L. in time, reckoning westward. Or, subtracting this from 24 hours, we have 104 7m 43s, for the longitude east, in time, and therefore the longitude in degrees is 151° 40

2. Given the apparent altitude of the moon's centre 8° 26′ 13″, the true altitude 9° 20′ 45″, the apparent altitude of a star 35° 40′, the true altitude 35° 38′ 49′, and their apparent distance 31° 13′ 26″; to determine the true distance.

The true distance is 30° 23′ 56″.

Those who are desirous of entering more at large into the problem of the Longitude, and of becoming acquainted with the best methods of shortening the computation by the aid of subsidiary tables, may advantageously consult, besides the works already referred to, the Quarto Tables of J. De Mendoza Rioz, Lynn's Navigation Tables, Captain Kater's Treatise on Nautical Astronomy, in the Encyclopædia Metropolitana, Kerrigan's Navigator's Guide and Nautical Tables, and Dr. Myers's translation of Rossel on the Longitude.

Variation of the Compass.

(81.) We shall conclude this part of our subject by briefly considering the methods of finding the variation of the compass, or the quantity by which the north point, as shown by the compass, varies easterly or

westerly from the true north point of the horizon

The solution of this problem merely requires that we find by computation, or by some means independent of the compass, the bearing of a celestial object, that we observe the bearing by the compass, and then take the difference of the two. The problem resolves itself, therefore, into two cases, the object whose bearing is sought being either in the horizon or above it: in the one case we have to compute its amplitude, and in the other its azimuth.

The computation of the amplitude is simply determining the hypotenuse of a right-angled triangle, of which one side is given, viz. the declination of the object, as also the angle opposite to it, viz. the colatitude. The computation of the azimuth requires the solution of an oblique spherical triangle, the three sides being given to find an angle; the three given sides are the colatitude; the zenith distance of the object and its polar distance: and the azimuth being measured by the angle at the zenith opposite the polar distance, this is the angle sought. We shall give an example in each of these cases of the problem.

EXAMPLES.

1. In January 1830, at latitude 27° 36' N., the rising amplitude of Aldebaran was, by the compass* E. 23° 30' N., required the variation. By the Nautical Almanack the declination of Aldebaran is 16° 9' 37" N., therefore since Rad. \times sin. dec. = sin. amp. \times cos. lat., the computation is as follows.

The compass amplitude must be taken when the apparent altitude of the object is equal to the depression of the horizon.

sin. declination 16º 9' 37" 9-4445527 cos. latitude 27 36 9.9475335 sın. Amptitude E. 18 18 17 N. 9.4970292

Magnetic Amptitude E. 23 30 0 N.

Variation 5 11 43.

As the object is farther from the magnetic east than from the true east, the magnetic east has therefore advanced towards the south, and therefore the magnetic north towards the east; hence the variation is

2. In latitude 48° 50' north, the true altitude of the sun's centre was 29° 2', the declination at the time was 10° 12' S., and its magnetic bearing 161° 32' east. Required the variation.

O's polar distance 100° 12° sin. zenith distance 67 58 arith. comp. 0.0329363 sin. colatitude 41 10 arith. comp. 0.1816080

2)209 20 sin. | B 104 40 9-9856129 8.8914209 sin. (18 — pol. dist.) 2)19:0915781 cos. 69° 25' 40" 9.5457895 2

O's true azimuth N. 138 51 20 E. Observed azimuth N. 161 32 0 E.

22 40 40 West.

The variation is west, because the sun's observed distance from the north, measured easterly, being greater than its true distance, intimates

53" N., its true altitude was found to be 37° 0' 16", and the observed azimuth S. 31° E.; required the variation of the compass. Variation 28° 2' West.

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MISCELLANEOUS TRIGONOMETRICAL INQUIRIES.

(82.) We now come to the final part of our subject, in which we propose to bring together several miscellaneous particulars which properly come under consideration in a treatise on Trigonometry. One or two of these, especially those which relate to certain compendious solutions of plane triangles, and to the trigonometrical lines of small arcs, might have been introduced much earlier, although we have preferred to postpone their consideration for a supplementary chapter, agreeing with Woodhouse, that it is better for the student first "to attend solely to the general solutions, and to postpone to a time of leisure and of acquired knowledge the consideration of the methods that are either more expeditious or are adapted to particular exigencies.

CHAPTER I.

ON THE SOLUTIONS OF CERTAIN CASES OF PLANE TRIANGLES, AND ON DETER-MINING THE TRIGONOMETRICAL LINES OF SMALL ARCS.

PROBLEM I.

(83.) Given two sides and the included angle of a plane triangle, to determine the third side, without finding the remaining angles. The general expression for the side c, in terms of the two sides a, b, and the included angle C, is (17), $c^2 = a^2 + b^2 - 2ab \cos C = (a - b)^2 + 2ab (1 - \cos C) = (a - b)^2 + 2ab \cdot 2\sin^2 \frac{1}{2} C = (a - b)^2 \left\{1 + \frac{4ab}{(a - b)^2} \sin^2 \frac{1}{2} C\right\}.$

Assume the second term within the brackets equal to $\tan \frac{a\theta}{\theta}$ then, since $1 + \tan \frac{a\theta}{\theta} = \sec \frac{a\theta}{\theta} = \frac{\operatorname{rad.}^2}{\cos \frac{a\theta}{\theta}}$, we have $c = (a - b) - \frac{\operatorname{rad.}^2}{\cos \theta}$.

Hence c is determined by these two formulas, viz. $\log \tan \theta = \log 2 + \frac{1}{4} \log a + \frac{1}{4} \log b + \log \sin \frac{1}{4} C - \log (a - b) \log c = \log (a - b) + 10 - \log \cos \theta$.

EXAMPLE.

Given a = 562, b = 320, and $C = 128^{\circ}$ 4', to find a log. 2 = 0.3010300 log. 562 = 1.3748681 log. 320 = 1.2525750 $log. sin. 64^{\circ}$ 2' 99537833

ar. comp. log. 242 7.6161846, log. 242 + 10 . .12.3838154

log. tan. θ 10·4984410 \therefore log. cos. θ = 9·4807177 log. c 800·01 \therefore 2·9030977.

PROBLEM II.

Given the logarithms of two sides of a plane triangle, as also the included angle, to determine the remaining angles.

Let log. a, log. b, and C, be given. Suppose a greater than b, and assume $r = \frac{\omega}{h} = \tan \theta$; then tan. θ being greater than 1, θ will exceed 45°. Also (19.) tan. 1 (A - B)

$$= \frac{a-b}{a+b} \cot \frac{1}{a} C = \frac{\frac{a}{b}-1}{\frac{a}{b}+1} \cot \frac{1}{a} C = \frac{\tan \theta - 1}{\tan \theta + 1} \cot \frac{1}{a} C$$

= tan. $(\theta - 45^{\circ})$ cot. $\frac{1}{2}$ C (p. 33).

Hence, introducing the radius, A - B is determined by these two formulas, viz. log. tan. $\theta = 10 + \log a - \log b$ log. tan. $\frac{1}{2}(A - B) = \log \tan (\theta - 45^{\circ}) + \log \cot \frac{1}{2}C - 10$.

log. tan.
$$\theta$$
 . $10.9445963 : \theta = 60^{\circ} 90' 35''$

 $0 - 45^{\circ} = 15^{\circ} 20' 35''$ Again, log. tan. 15°20' 35" 9.4383476 log. cot. 64 2 9.6875402

log. tan.
$$\frac{1}{4}$$
 (A - B) 9·1258878 $\therefore \frac{1}{4}$ (A - B) = 7° 36′ 40′ $\frac{1}{4}$ (A + B) = 25° 58

$$A = 33 34 40$$

 $B = 18 21 20$

This method of determining the angles A and B will always be the shortest, when instead of their sides their logarithms are given. Thus the solution of problem x., p. 31, becomes much facilitated by the application of this process.

PROBLEM III.

To determine the area of a plane triangle when any three parts except the three angles are given.

1. Let two sides b, c, and the included angle A, be given. (See fig.

p. 17.)

The area of the triangle is expressed by $\frac{1}{2}$ AB · CD; but CD = AC sin. A; hence the expression for the area, in terms of the given quantities, is Area = $\frac{1}{2}bc\sin A$.

2. Let two angles, A, B, and the interjacent side c, be given. Then, since sin. C : sin. B :: c : b, we have $b = \frac{\sin B}{\sin C}c \cdot bc \sin A = \frac{\sin A \sin B}{\sin C}c^2$; sin. A sin. B

we have
$$b = \frac{\sin B}{\sin C} c$$
 ... $bc \sin A = \frac{\sin A \sin B}{\sin C} c^2$

hence the expression for the area is Area = $\frac{\sin A \sin B}{2 \sin C}$.

3. Let the three sides be given.

By art. (20),
$$\sin \frac{1}{2} A = \sqrt{\frac{(\frac{1}{2}8 - b)(\frac{1}{2}8 - c)}{bc}}$$
, $\cos \frac{1}{2}A = \sqrt{\frac{\frac{1}{2}8(\frac{1}{2}8 - c)}{bc}}$

: 2 sin.
$$\frac{1}{4}$$
A cos. $\frac{1}{4}$ A, or (art. 31) sin. $A = \frac{2}{b^2} \sqrt{\frac{1}{4}S(\frac{1}{4}S - a)(\frac{1}{4}S - b)(\frac{1}{4}S - c)}$

Consequently, by substituting this value of sin. A in the first expres-

sion, we have, Area = $\sqrt{\frac{1}{18}} \frac{8(\frac{1}{18} - a)(\frac{1}{18} - b)(\frac{1}{18} - c)$;

which formula furnishes the well known rule, given in all books on mensuration, for the area of a triangle when the three sides are given. (See Geom. p. 202.) These expressions for the area of a plane triangle are all adapted to logarithmic computation.

PROBLEM IV.

To find the logarithmic sine of a very small arc.

By article (30) the expression for the sine of any arc x is,

$$\sin x = x - \frac{x^3}{1 \cdot 2 \cdot 3} + \frac{x^5}{1 \cdot 2 \cdot 3 \cdot 4 \cdot 5} - \cos x$$
. Now as the length of

an arc of one degree is 01745329, (see p. 36-7,) it is plain that, even when x is so great as this, the third term of the above series can have no significant figure in the first ten places of decimals.

Retaining therefore only the first two terms, we have, when x is small,

sin.
$$x = x - \frac{x^3}{1 \cdot 2 \cdot 3} = x \left(1 - \frac{x^2}{2 \cdot 3}\right) = x \left\{1 - \frac{x}{2} + \frac{x^4}{2 \cdot 3 \cdot 4}\right\}^{\frac{1}{6}}$$
 nearly; that is, (p. 36,) sin. $x = x \cos^{\frac{1}{6}} x$; hence, by introducing the radius, log. sin. $x = \log x - \frac{1}{6} (10 - \log \cos x) \dots (1)$.

Let the arc x contain n seconds, then $x = \frac{1}{120 \times 60 \times 60}$;

hence, by introducing the radius,

log.
$$x = \log_1 n + \log_2 3.14159$$
, &c. + 10 - $\log_1 180 \times 60^n$
= $\log_1 n + 4.6855749$; therefore, from (1),
log. sin. $x = \log_1 n + 4.6855749 - \frac{1}{4}$ arith. comp. log. cos. $x \dots (2)$; 2

hence this rule. To the logarithm of the arc reduced into seconds, with the decimal annexed, add the constant quantity 4 6855749, and from the sum subtract one third of the arithmetical complement of the log. cosine; the remainder will be the logarithmic sine of the given arc.

This rule will determine the log. sine of a very small arc with great

accuracy; it was first given, without demonstration, by Dr. Maskelyne, in his Introduction to Taylor's Logarithms. The above proof is from

Woodhouse's Trigonometry.

PROBLEM V.

To find the logarithmic tangent of a very small arc. Let x be the arc; then, as we have found in last problem,

$$\sin x = x \cos^{\frac{1}{2}} x \cdot \frac{\sin x}{\cos x} = \tan x = \frac{x}{\cos \frac{1}{2} x}$$
 Hence, introducing the

radius, log. tan. $x = \log_x x + \frac{1}{2} (10 - \log_x \cos_x x)$.

The second member of this equation is equal to the second member of (1) in last problem, plus the arithmetical complement of log. $\cos x$; hence, since the second member of (2) is equivalent to the second member of (1), we have

 $\log \tan x = \log n + 4.6855749 + 1$ arith. comp. $\log \cos x \dots (3)$; which furnishes this rule. To the logarithm of the arc reduced to seconds add the constant quantity 4 6855749, and two thirds of the arithmetical complement of the log. cosine, the sum is the log. tangent of the given arc.

PROBLEM VI.

To find a small arc from its log. sine or its log. tangent.

42 length of are to radius 1 -

1. Let the log. sine be given; then n being the number of seconds in the arc, the expression (2), in problem iv., gives $\log n = \log \sin x - 4.6855749 + 1$ arith. comp. $\log \cos x$ = log. $\sin x + 5 \cdot 3144251 - 10 + 1$ arith. comp. log. $\cos x$; therefore, we find the arc from the log. sine the rule is this. To the log. sine of the small arc add 5·3144251, and 1 of the arithmetical complement of the log. cosine; subtract 10 from the index of the sum, and the remainder will be the logarithm of the number of seconds in the arc. 2. Let the log. tangent be given; then from the expression (3), last problem, we have $\log_{10} n = \log_{10} \tan_{10} x - 4.6855749 - \frac{1}{2}$ arith. comp. $\log_{10} \cos_{10} x$ $= \log \tan x + 5.3144251 - 10 - \frac{1}{2}$ arith. comp. $\log \cos x$; that is, to the log tangent of the small are add 5.314251, and from the sum subtract 1 of the arithmetical complement of the log cosine, take 10 from the index of the remainder, and we shall have the logarithm of the number of seconds in the arc. Let us now apply each of the foregoing rules to an example. 1. Required the log. sine of 1' 4.8754". By the rule in problem iv. the process is as follows: log. 64.8754 1.8120801 Constant No. 4.6855749 6.4976550 arith. comp. log. cos. log. sin. 1' 4.8754" 6.4976550. By the tables the log. sine is found as follows: log. sin. 1'5" 6.4984889 log. sin. 1'4" 6.4917548 Difference 0067334 $\cdot \cdot \cdot \log \cdot \sin \cdot 1' \cdot 4.8754'' = 6.4917548 + 8754 \times 0067334 = 6.4976489.$ 2. Required the log. tangent of 7' 2'38". By the Rule in Problem V. By the tables. log. 422·38 - 2·6257033 Constant No. 4·6855749 log. tan. 7' 3" 7:3119158 log. tan. 7 2 7.3108879 erith. comp. log. cos. 0 0010279 log. tan. 7' 2.38" 7.3112782. $\therefore \log \tan 7' 2 \cdot 38'' = 7 \cdot 3108879 + \cdot 38 \times \cdot 0010279 = 7 \cdot 3112785$ 3. Required the arc whose log. sine is 6.4976550. By the Rule, Problem V. log. sine 6.4976550 Constant No. 5-3144961 n arith. comp. log. 64.8754 1.8120801 ... the arc is 1' 4.8754". By the Tables.

The proposed log, sine lies between log, sine 1'4" and log, sine 1'5", and the difference between these logs is 0067334; also the difference between the proposed log, and log, sine 1'4" is 59002; hence

required arc = $1'4'' + \frac{33003}{67334} = 1'4.876''$.

4. Required the arc whose log. tangent is 7:1644398. 7.1644398 By the Rule. log. tan. Constant No. 5.3144251 arith. comp.

> log. 301-2067 ... the arc is 5' 1.2067".

By the Tables.

2.4788646

The proposed log. is between log. tan. 5' 1" and log. tan. 5' 2"; the difference of these logs. is 0014404, and the difference of the proposed and log. tan. 5' 1" is 0002981.

 $\therefore \text{ the arc is 5' 1''} + \frac{2981}{14404} = 5' 1.2069''.$

CHAPTER II.

INVESTIGATIONS OF EXPRESSIONS FOR THE SURFACE OF A SPHERICAL TRIANGLE AND FOR THE SPHERICAL EXCESS.

(84.) It has been already shown (36) that two great circles always intersect in two points at the distance of a semicircle from each other. The space thus included by two great circles is called a lune, (see the

fig. at p. 42.)

The surface of a lune is to the surface of the whole sphere as the arc QQ', or as the angle P of the lune, is to the whole circumference IQHI. This is pretty obvious, but it may be rigorously proved in the same way as it is proved in plane Geometry, that in the same circle any sector is to the whole circle as its arc is to the circumference, Geom. prob. 23. Book 6). Hence, if we call the surface of the sphere 8, and the angle of the lune ω degrees, the expression from its area will

be $8\frac{\omega}{360}$; or if, instead of degrees, ω represents the absolute length of

those degrees to radius 1, then the expression may be written S where * stands for the number 3.14159, &c.

It can be proved, although not by the elementary principles of Trigonometry, that the surface of a sphere is equal to four times the area of one of its great circles; that is, r being the radius of the sphere $S=4\pi r^{a}$, so that the expression for the area of the lune is $2r^{a}\omega$. If we suppose r to be unity, the surface will be expressed by 2ω , that of the whole sphere being 4.

PROBLEM I.

To express the area of a spherical triangle in terms of its three angles.

Let ABC be any spherical triangle, and produce the sides AC, BC, till they meet again in C', forming the lune CC'. The triangle CAB will be a portion of an opposite lune equal to the lune CC'; and this portion will obviously be equal to the portion C'A'B', provided the arcs CA, CB, are equal to the arcs C'A', C'B'. Now AA' is equal to CC', each being a semicircle; hence, taking from each the common part CA', we have CA = C'A'. In like manner CB = C'B', and, therefore, the triangles ABC, A'B'C', are equal. Hence the surface of the hemisphere, whose base is AB'A'B', is equal to the sum of the three lunes AA', BB', CC', minus twice the triangle ABC; * See "The Elements of the Integral Calculus," page 144.

TRIGONOMETRICAL INQUIRIES. that is, calling the surface of this triangle Σ .

 $\therefore \Sigma = r^2 (A + B + C) - \frac{1}{4} S = r^2 \{(A + B + C) - \pi \}.$ where it must be observed that A, B, C, denote the lengths of the arcs of which measure the angles of the proposed triangle to radius unity.
But, if we take A, B, C, and π in degrees, then since

$$180^{\circ}: \pi :: A + B + C - 180^{\circ}: \{A + B + C - 180^{\circ}\} \frac{\pi}{180^{\circ}}$$
 the expression for Σ will be $\Sigma = r^{2}\{A + B + C - 180^{\circ}\} \frac{\pi}{180^{\circ}}$. (1).

If the radius of the sphere, on which the triangle is, be taken for unity,

It follows from this proposition that two spherical triangles are equal in surface, if the angles of the one are severally equal to those of the other, or, indeed, if the sum of the angles of the one triangle is equal to the sum of the angles of the other.

PROBLEM II.

To express the area of a spherical triangle, or the spherical excess in terms of two sides, and the included angle.

Calling as before the surface of the triangle to radius unity s, and, the sum of its three sides s, we have, by last problem,

 $\begin{array}{c} \mathfrak{c} = \mathfrak{s} - 180^{\circ} :: \cot \frac{\mathfrak{c}}{2} = -\tan \frac{1}{2} \mathfrak{s}. \\ \text{But (27), } \tan \cdot \frac{1}{2} \mathfrak{s} = \tan \cdot \frac{1}{2} (\mathbb{A} + \mathbb{B} + \mathbb{C}) = \frac{\tan \cdot \frac{1}{2} (\mathbb{A} + \mathbb{B}) + \tan \cdot \frac{1}{2} \mathbb{C}}{1 - \tan \cdot \frac{1}{2} (\mathbb{A} + \mathbb{B}) \tan \frac{1}{2} \mathbb{C}}; \\ \text{and, by Napier's analogy, } \tan \cdot \frac{1}{2} (\mathbb{A} + \mathbb{B}) = \frac{\cos \cdot \frac{1}{2} (a - b)}{\cos \cdot \frac{1}{2} (a + b)} \cot \cdot \frac{1}{2} \mathbb{C}; \end{array}$ hence, by substitution,

$$\cot \frac{\varepsilon}{2} = \frac{\cos \frac{1}{2}(a-b)\cot \frac{1}{2}C + \cos \frac{1}{2}(a+b)\tan \frac{1}{2}C}{\cos \frac{1}{2}(a-b) - \cos \frac{1}{2}(a+b)};$$

or multiplying the numerator by 2 sin. ‡C cos. ‡C, and the denominator by its equal, sin. C, (equa. 18, p. 37,)

$$\cot \frac{\epsilon}{2} = \frac{2\cos \frac{1}{\epsilon}(a-b)\cos^{2}\frac{1}{\epsilon}C + 2\cos \frac{1}{\epsilon}(a+b)\sin^{2}\frac{1}{\epsilon}C}{\cos \frac{1}{\epsilon}(a-b)\sin C - \cos \frac{1}{\epsilon}(a+b)\sin C};$$

that is, by the formulas (1) and (2), page 32,

$$\cot \frac{\epsilon}{2} = \frac{\cos \frac{\epsilon}{2} a \cos \frac{\epsilon}{2} + \sin \frac{\epsilon}{2} a \sin \frac{\epsilon}{2} b (\cos \frac{\epsilon}{2} C - \sin \frac{\epsilon}{2} C)}{\sin \frac{\epsilon}{2} a \sin \frac{\epsilon}{2} b \sin C};$$

but, (from 19, p. 37,)
$$\cos^2 \mathbf{i} \mathbf{C} - \sin^2 \mathbf{i} \mathbf{C} = \cos \mathbf{C}$$
; hence $\cot \frac{\epsilon}{2} = \frac{\cot \mathbf{i} \mathbf{a} \cot \mathbf{i} \mathbf{b} + \cos \mathbf{C}}{\sin \mathbf{C}} = \left\{ \frac{\cot \mathbf{i} \mathbf{a} \cot \mathbf{i} \mathbf{b}}{\cos \mathbf{C}} + 1 \right\} \cot \mathbf{C}$.

To adapt this expression to logarithmic computation suppose first that cos. C is positive, and that we assume $\frac{\cot \frac{1}{2} a \cot \frac{1}{2} b}{\cos C} = \tan \frac{a}{2} \theta_1$

then cot. $\{\epsilon = \sec^2 \theta \text{ cot. C}; \text{ suppose, secondly, that cos. C is negative.}$ then if $\frac{\cot \frac{1}{4}a \cot \frac{1}{4}b}{\cos C}$ is numerically less than radius, assume it equal

then To 190°, when radius = 1, as t evidently is it when my 1, seminimum bearing = mon

to sin. ² θ , and we shall have cot. $\frac{\epsilon}{\Omega} = \cos \theta$ cot. C; but if the same expression be numerically greater than radius, then assume it equal to sec. * θ , when we shall have cot. $\frac{\epsilon}{2}$ == tan. * θ cot. C.

It may be remarked that, with the proposed data, the excess may be otherwise easily determined, by first finding, by the common formula, the third angle of the triangle, and then applying Girard's theorem.

PROBLEM III.

To determine the spherical excess when the three sides are given. By formula 25, p. 38,

cot.
$$\frac{1}{2}a \cot \frac{1}{2}b = \frac{1 + \cos a}{\sin a} \cdot \frac{1 + \cos b}{\sin b} = \frac{1 + \cos a + \cos b + \cos a \cos b}{\sin a \sin b}$$

By formula (A) p. 47, cos. C =
$$\frac{\cos c - \cos a \cos b}{\sin a \sin b}$$
.

By formulas (1), (2), p. 49

Substituting these values in the expression for cot. $\frac{\epsilon}{\Omega}$, last problem, we have

eot.
$$\frac{s}{2} = \frac{1 + \cos a + \cos b + \cos c}{2\sqrt{\sin \frac{1}{2}} \sin \left(\frac{1}{2} - a\right) \sin \left(\frac{1}{2} - a\right) \sin \left(\frac{1}{2} - a\right) \sin \left(\frac{1}{2} - a\right)}$$
. (3).

We may investigate another expression for the excess, as follows:

By the formulas (1), (2), page 49

$$sin. \frac{1}{2} A cos. \frac{1}{2} B = \frac{\sin. (\frac{1}{2} S - b)}{\sin. c} \int \frac{\sin. \frac{1}{2} S \sin. (\frac{1}{2} S - c)}{\sin. b \sin. c}$$

$$sin. \frac{1}{2} B cos. \frac{1}{2} A = \frac{\sin. (\frac{1}{2} S - a)}{\sin. c} \int \frac{\sin. \frac{1}{2} S \sin. (\frac{1}{2} S - c)}{\sin. b \sin. a}$$

By adding, sin.
$$\frac{1}{2}(A + B) = \frac{\sin (\frac{1}{2} S - b) + \sin (\frac{1}{2} S - e)}{2 \sin \frac{1}{2} c \cos \frac{1}{2} C} \cos \frac{1}{2} C$$
By subtracting, sin. $\frac{1}{2}(A - B) = \frac{\sin (\frac{1}{2} S - b) - \sin (\frac{1}{2} S - a)}{2 \sin \frac{1}{2} c \cos \frac{1}{2} C} \cos \frac{1}{2} C$

By subtracting, sin.
$$\frac{1}{2}(A-B) = \frac{\sin (\frac{1}{2}S-b) - \sin (\frac{1}{2}S-a)}{2 \sin \frac{1}{2}\cos \frac{1}{2}$$

But by formula (27), page 39,

$$\sin \cdot (18-b) + \sin \cdot (18-a) = 2 \sin \cdot 16 \cos \cdot 16 (a-b) \sin \cdot (18-b) - \sin \cdot (18-a) = 2 \cos \cdot 16 \sin \cdot 16 (a-b)$$

Hence by substitution, sin. $\frac{1}{2}$ (A + B = $\frac{\cos \frac{1}{2}(a-b)}{\cos \frac{1}{2}c}\cos \frac{1}{2}$ Cos. $\frac{1}{2}$ C sin. $\frac{1}{2}$ (A - B = $\frac{\sin \frac{1}{2}(a+b)}{\sin \frac{1}{2}c}\cos \frac{1}{2}$ Cos. $\frac{1}{2}$ C.

$$\sin \frac{1}{a} (A - B) = \frac{\sin \frac{1}{a} (a + b)}{\sin \frac{1}{a} a} \cos \frac{1}{a} C$$

Proceeding in the same way with the expressions for cos. 1 A cos. 2 B. and sin. A sin. B,

there results cos.
$$\frac{1}{2} (A - B) = \frac{\sin \cdot \frac{1}{2} (a + b)}{\sin \cdot \frac{1}{2} c} \sin \cdot \frac{1}{2} C$$
,
 $\cos \cdot \frac{1}{2} (A + B) = \frac{\cos \cdot \frac{1}{2} (a + b)}{\cos \cdot \frac{1}{2} c} \sin \cdot \frac{1}{2} C$. Now, since

$$\cos \frac{1}{2}(A+B) = \frac{\cos \frac{1}{2}c}{\cos \frac{1}{2}c} \sin \frac{1}{2}C.$$

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= -\cos \frac{1}{4}(A+B+C) = \sin \frac{1}{4}(A+B) \sin \frac{1}{4}C - \cos \frac{1}{4}(A+B) \cos \frac{1}{4}C,
we have, by substituting in the second member the first and last of the
to regoing expressions, \sin \frac{\epsilon}{2} = \frac{\sin \frac{\epsilon}{4} a \sin \frac{\epsilon}{4} b}{\cos \frac{\epsilon}{4} c} \sin C; or substituting for
sin. C its value, as exhibited in last problem, and recollecting that (31),
\sin a \sin b = 4 \sin a \cos a \sin b \cos b,
we have \sin \frac{c}{2} = \sqrt{\frac{\sin \frac{1}{2} \operatorname{S} \sin \cdot (\frac{1}{2} \operatorname{S} - a) \sin \cdot (\frac{1}{2} \operatorname{S} - b) \sin \cdot (\frac{1}{2} \operatorname{S} - c)}{2 \cos \frac{1}{2} a \cos \frac{1}{2} b \cos \frac{1}{2} c}} (3);
an expression adapted to logarithms.
         By combining the formulas (2) and (3) various others may be deduced.
  Thus, by multiplying them together, we have
                                                                                \cos \frac{\varepsilon}{2} = \frac{1 + \cos a + \cos b + \cos c}{4 \cos 1 a \cos 1 b \cos 1 c}.
         But, formula (20), page 37,
Squaring this, 2\cos^2\frac{\epsilon}{2} = \frac{1+\cos a + \cos b + \cos c}{2(1+\cos a)(1+\cos b)(1+\cos c)};
\cos^2\frac{\epsilon}{2} = \frac{1+\cos a + \cos b + \cos c}{\sqrt{2(1+\cos a)(1+\cos b)(1+\cos c)}}....(5)
Squaring this, 2\cos^2\frac{\epsilon}{2} = \frac{(1+\cos a + \cos b + \cos c)^2}{(1+\cos a)(1+\cos b)(1+\cos c)};
 which, since \cos \epsilon = 2 \cos^2 \frac{\epsilon}{2} - 1, gives
 \cos cos. c = \frac{(1 + \cos a + \cos b + \cos c)^2 - (1 + \cos a)(1 + \cos b)(1 + \cos c)}{(1 + \cos a)(1 + \cos b)(1 + \cos c)} ... (6);
  also because 1 - \cos x = \text{vers. } c, we may change this into
 vers. \epsilon = \frac{1 - \cos^2 a - \cos^2 b - \cos^2 c + 2 \cos a \cos b \cos c}{(1 + \cos a)(1 + \cos b)(1 + \cos c)}
         Lastly, by squaring the expression (3) and multiplying by 2, we have
 2\sin^{\frac{c}{2}} = 1 - \cos \varepsilon = \text{vers.} \varepsilon = \frac{\sin \frac{1}{2} \operatorname{Sin.} (\frac{1}{2} \operatorname{S} - a) \sin \cdot (\frac{1}{2} \operatorname{S} - b) \sin \cdot (\frac{1}{2} \operatorname{S} - c)}{2\cos^{\frac{c}{2}} a \cos^{\frac{c}{2}} \frac{1}{2} b \cos^{\frac{c}{2}} \frac{1}{2} c} . (8).
           The expression, marked (2), is due to De Gua, as are those marked
  (4), (5), (6), and (7). The expression (3) is from Cagnoli, (Trigon. page
 329.) Since, \tan \frac{\epsilon}{4} = \frac{1 - \cos \frac{1}{4}\epsilon}{\sin \frac{1}{4}\epsilon}, we have, by combining the expres-
  sions (3) and (5),
 \tan \frac{\epsilon}{4} = \frac{1 - \cos^2 \frac{1}{4}a - \cos^2 \frac{1}{4}b - \cos^2 \frac{1}{4}c + 2\cos \frac{1}{4}a \cos \frac{1}{4}b \cos \frac{1}{4}c}{\sqrt{1 + \cos^2 \frac{1}{4}a - \cos^2 \frac
                                                     \sqrt{\sin (\frac{1}{2} S \sin (\frac{1}{2} S - a) \sin (\frac{1}{2} S - b) \sin (\frac{1}{2} S - a)}
  Now, 1 - \cos^2 \frac{1}{2} a - \cos^2 \frac{1}{2} b = \sin^2 \frac{1}{2} a - \cos^2 \frac{1}{2} b, by equa. 5, p. 32, = \sin^2 \frac{1}{2} a \sin^2 \frac{1}{2} b - \cos^2 \frac{1}{2} a \cos^2 \frac{1}{2} b; hence, the numerator of the above expression is equal to
   \sin^2 \frac{1}{2} a \sin^2 \frac{1}{2} b — (cos. \frac{1}{2} a \cos \frac{1}{2} b — cos. \frac{1}{2} c), which is the same as
                                                       \{\sin \cdot a \sin \cdot b + \cos \cdot a \cos \cdot b - \cos \cdot c\} \times
                                                       \frac{1}{3}\sin \frac{1}{4}a \sin \frac{1}{4}b - \cos \frac{1}{4}a \cos \frac{1}{4}b + \cos \frac{1}{4}c = 0; or as
    \begin{cases} \cos \frac{1}{2} (a-b) - \cos \frac{1}{2} c \\ \times \\ \cos \frac{1}{2} c - \cos \frac{1}{2} (a+b) \\ = (by equ 2.27, p.39); \\ 2 \sin \frac{1}{2} (\frac{1}{2} S - b) \sin \frac{1}{2} (\frac{1}{2} S - a) \times 2 \sin \frac{1}{2} S \sin \frac{1}{2} (\frac{1}{2} S - c).  Consequently, since (page 38), \sqrt{\frac{1}{2}} \tan \frac{1}{2} A = \frac{\sin \frac{1}{2} A}{\sqrt{\sin A}}, 
   the foregoing expressions for tan. \frac{\varepsilon}{4} takes this very remarkable form, viz.
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$$\tan \frac{c}{4} = V \tan \frac{1}{2} \operatorname{S} \tan \frac{1}{2} \left(\frac{1}{2} \operatorname{S} - a \right) \tan \frac{1}{2} \left(\frac{1}{2} \operatorname{S} - b \right) \tan \frac{1}{2} \left(\frac{1}{2} \operatorname{S} - c \right);$$

which is Lhullier's expression.

It follows from this problem that two spherical triangles are always equal in surface when the sides of the one are severally equal to those of the other, whether the triangles admit of coincidence or not.

PROBLEM IV.

Given the area of a spherical triangle on the surface of the earth in square feet, to determine the spherical excess.

Let the area of the triangle in feet be Σ , then, by problem I., $\epsilon = \frac{\Sigma}{r^2} \cdot \frac{180^{\circ}}{3.14159}.$

$$r = \frac{2}{r^2} \cdot \frac{1605}{3.14159}$$

Now the length of a degree, supposing the earth to be a perfect sphere, is 365154.6 feet; hence the earth's radius is $\frac{100}{3:14159} \times 365154.6$ feet;

 $\frac{180 \times (365154 \cdot 6)^2}{314159 \times 60^3}$ degrees; or if the excess be expressed consequently, ===

n seconds, then $\epsilon =$

ds, then
$$\epsilon = \frac{3 \cdot 14159 \ \Sigma \times 60^{9}}{180 \cdot (365154 \ 6)^{9}}$$
 seconds.
 $\therefore \log \epsilon = \log \ \Sigma + \log \ 62 \cdot 83185 \ &c. - 9 \log \ 365154 \ 6$
 $= \log \ \Sigma + 1 \cdot 7981799 - 11 \cdot 1249536$
 $= \log \ E - 9 \cdot 3267737$.

In from the logarithm of the area of the triangle in feet, substituting the second of the second

Hence, from the logarithm of the area of the triangle in feet, subtract the constant logarithm 9 3267737, and the remainder will be the logarithm of the excess in seconds.

This rule, which usually goes by the name of General Roy's rule, is in fact due to the late professor Dalby, by whom it was communicated to the General, when engaged with him in conducting the Trigonometrical Survey. (See the "Life of Mr. Dalby," in Leybourn's Reposi-

By means of the rule just given we may very readily compute the spherical excess, provided that we previously know the area of the tri-angle in feet. In trigonometrical surveying, the triangle on the surface of the earth, composed between any three stations, is necessarily so limited a portion of the whole sphere that its area, computed as a plane triangle from the measured data, cannot be affected with any error of consequence. On this hypothesis, therefore, the area of the triangle may be determined by one or other of the methods in prob. III., last chapter, and thence the excess ascertained by the above rule. Should the excess, thus deduced, exactly equal the excess of the three observed angles above two right-angles, we may be assured of the accuracy of the observations; but if they differ, the difference must be regarded as the amount of the errors with which the three observed angles are affected. If all of them were observed with equal care, so that there appear no reason why one should be more erroneous than another, the correction thus found must be distributed equally among them; but if it be suspected that one of the angles is less to be depended on than the others, then to this angle must be applied the greater part of the whole correction. The data being thus corrected, the required side or sides of the spherical triangle may be computed by the rules of spherical trigonometry; or the same object may be effected by plane trigonometry, with all requisite accuracy, provided we employ in the computation. not the corrected spherical angles, but these angles diminished each by one third of the spherical excess found as above, a truth which has been established by Legendre, (See the Appendix to Brewster's translation

of Legendre's Geometry.) Trigonometrical surveying is a very important application of the theory of trigonometry, but is too ample a subject to admit of being discussed in the present volume. The student will find a condensed account of these geodetical operations in the tenth section of Dr. Lardner's Trigonometry, and every requisite information in the Geodesic of M. Puissant and Col. Mudge's account of the Trigonometrical Survey of England and Wales.*

Miscellaneous Expressions involving the Sides and Angles of a Spherical Triangle.

(85). We shall terminate the present chapter by the insertion of a few general expressions, involving the three sides and the three angles of a spherical triangle. Those formulas which have already been given in the second part of the work, are amply sufficient for the so-lution of every case in spherical trigonometry, but the sides and angles of a spherical triangle possess many other remarkable relations which are often called in aid, in higher investigations concerning a sphere. are often cased in aid, in higher investigations concerning a sphere. A few of these, therefore, it may be proper to give. Let s represent half the sum of the sides a, b, c, and S, half the sum of the angles A, B, C, of a spherical triangle; then by multiplying together the expressions for $\sin \frac{1}{2}A$, $\cos \frac{1}{2}A$, in art. (47), and those for $\sin \frac{1}{2}a$, $\cos \frac{1}{2}a$, in art. (49), and squaring the results, we have these equations; $\sin \frac{1}{2}b \sin \frac{1}{2}c \sin \frac{1}{2}A = 4 \sin \frac{1}{2}s \sin \frac{1}{2}c \sin \frac{1}{2}A = 4 \cos \frac{1}{2}c \sin \frac{1}{2}a = -4 \cos \frac{1}{2}c \cos \frac{1}{2}c = -4 \cos \frac{1}{2$ $=4N^{2}(2)$ By multiplication, \cdot sin. $a \sin b \sin c \sin A \sin B \sin C = 4 N = (3)$. By division, $\frac{\sin b}{\sin B} \cdot \frac{\sin c}{\sin C} \cdot \frac{\sin A}{\sin a} = \frac{\pi}{N}$. But the first two factors of this expression are each of them the re- $\frac{\sin b}{\sin B} = \frac{\sin c}{\sin C} = \frac{\sin a}{\sin A}$ ciprocal of the last. But from (1), $\frac{\sin A}{\sin a} = \frac{2n}{\sin a \sin b \sin c} \cdot \frac{N}{n} = \frac{2n}{\sin a \sin b \sin c}$. (5) and from (2), 2N $\frac{\sin A}{\sin A} = \frac{21N}{\sin A \sin B \sin C} \cdot \cdot \cdot \frac{\pi}{N} = \frac{21N}{\sin A \sin B \sin C} \cdot \cdot \cdot \cdot (6).$ Substituting in (6) the value of N deduced from (5), and in (5) the value of n deduced from (6), we have, from the resulting equations, these expressions for n and N viz. $n = \frac{1}{4} \frac{3 \sin^2 a \sin^2 b \sin^2 c \sin^2 A \sin^2 B \sin^2 C}{1 + \frac{1}{4} \sin^2 a \sin^2 A \sin^2 A \sin^2 A}$ $N = \frac{1}{4} \left\{ \sin^2 A \sin^2 B \sin^2 C \sin a \sin b \sin c \right\}^{\frac{1}{4}} \dots$ (8); and, for their ratio $\frac{\pi}{N}$, we have from these, as also from (4), $\frac{n}{N} = \left\{ \frac{\sin a \sin b \sin c}{\sin A \sin B \sin C} \right\}^{\frac{1}{2}}$ expressions which are remarkable for their symmetry. Again, referring to the expressions for sin. A, and cos. A, at (47), we see that sin. $\frac{1}{2}$ A sin. $\frac{1}{2}$ B sin. $\frac{1}{2}$ C = $\frac{1}{\sin s}$ sin. $\frac{1}{2}$ sin n sin, s $\cos \frac{1}{4} A \cos \frac{1}{4} B \cos \frac{1}{4} C = \frac{\pi \sin \frac{1}{4} \sin \frac{1}{4} \sin \frac{1}{4}}{\sin \frac{1}{4} \sin \frac{1}{4} \sin \frac{1}{4}} . . . (11)$

^{*}Some additional particulars respecting the spherical excess will be found in the supplement.

∴
$$\tan \frac{1}{4} A \tan \frac{1}{4} B \tan \frac{1}{4} C = \frac{n}{\sin^2 x}$$
 . . . (19).

And by referring to the expressions for sin. 14, cos. 14, at (49), we see the truth of the following analogous equations; viz.,

$$\sin \frac{1}{4} a \sin \frac{1}{4} b \sin \frac{1}{4} c = \frac{-N \cos S}{\sin A \sin B \sin C} \cdot ... (13)$$

$$\cos \frac{1}{4} a \cos \frac{1}{4} b \cos \frac{1}{4} c = \frac{N^2}{-\cos S \sin A \sin B \sin C} ... (14)$$

: tan.
$$\frac{1}{2}a \tan \frac{1}{2}b \tan \frac{1}{2}c = \frac{\cos^2 8}{N}$$
 . . (15).

From (10),
$$\sin s = \frac{n^3}{\sin a \sin b \sin c \sin \frac{1}{2} A \sin \frac{1}{2} B \sin \frac{1}{2} C}$$
. (15)
= , by (5), $\frac{N}{2 \sin \frac{1}{2} A \sin \frac{1}{2} B \sin \frac{1}{2} C}$. (16).

From (11), $\sin s = \frac{\sin a \sin b \sin c \cos A \cos B \cos C}$

=, by (5),
$$2\frac{n}{N}\cos \frac{1}{2}A\cos \frac{1}{2}B\cos \frac{1}{2}C$$
. (17);

and, from (12),
$$\sin^2 s = \frac{\pi}{\tan \frac{1}{2} A \tan \frac{1}{2} B \tan \frac{1}{2} C}$$
. (18). In like manner, from (13), (14), (15), we have $\cos S = -\frac{\sin A \sin B \sin C \sin \frac{1}{2} a \sin \frac{1}{2} b \sin \frac{1}{2} c}{N}$

$$\cos S = -\frac{\sin A \sin B \sin C \sin \frac{1}{4} a \sin \frac{1}{4} b \sin \frac{1}{4} a}{N}$$

=, by (6), -2
$$\frac{N}{n}$$
 sin. $\frac{1}{2}a$ sin. $\frac{1}{2}b$ sin. $\frac{1}{2}c$. . (19)

cos. S =
$$-\frac{N^2}{\sin A \sin B \sin C \cos \frac{1}{2} a \cos \frac{1}{2} b \cos \frac{1}{2} c}$$

= , by (6), $-\frac{\pi}{2\cos \frac{1}{2} a \cos \frac{1}{2} b \cos \frac{1}{2} c}$. (90)

$$\cos^2 S = N \tan_{\frac{1}{2}} a \tan_{\frac{1}{2}} b \tan_{\frac{1}{2}} c = \frac{N}{\cot_{\frac{1}{2}} a \cot_{\frac{1}{2}} b \cot_{\frac{1}{2}} c}.$$
(21).

(86). In addition to these we shall here put down a few other useful expressions immediately deducible from the four equations which we had occasion to investigate at p. 114; and which are as follows:

con to investigate at p. 114; and which are as follow
$$\sin \frac{1}{2} (A + B) = \frac{\cos \frac{1}{2} C}{\cos \frac{1}{2} c} \cos \frac{1}{2} (a - b) . . . (28)$$

$$\sin \frac{1}{2} (A - B) = \frac{\cos \frac{1}{2} C}{\sin \frac{1}{2} c} \sin \frac{1}{2} (a - b) . . . (28)$$

$$\cos \frac{1}{2} (A + B) = \frac{\sin \frac{1}{2} C}{\cos \frac{1}{2} c} \cos \frac{1}{2} (a + b) . . . (24)$$

$$\cos \frac{1}{2} (A - B) = \frac{\sin \frac{1}{2} C}{\sin \frac{1}{2} c} \sin \frac{1}{2} (a + b) . . . (25).$$

From these equations we immediately deduce the following analo-

[•] This expression, as well as those marked 19, is usually given with an improper sign, viz. + instead of —, a mistake which seems to have arisen from confounding ν (cos. S · cos. S) with ν (— cos. S × — cos. S,) which are, in fact, distinct expressions; the one being + cos. S, and the other — cos. S. See the chapter on *Imaginary Quantities*, in Young's Algebra, just published by Carey, Lea, & Co. Philadelphia.

gous ones, viz.
$$\sin \frac{1}{2}(a+b) = \frac{\sin \frac{1}{2}c}{\sin \frac{1}{2}C} \cos \frac{1}{2}(A-B)$$
. (26)

$$\sin \frac{1}{2}(a-b) = \frac{\sin \frac{1}{2}c}{\cos \frac{1}{2}C} \sin \frac{1}{2}(A-B)$$
. (27)

$$\cos \frac{1}{2}(a+b) = \frac{\cos \frac{1}{2}c}{\sin \frac{1}{2}C} \cos \frac{1}{2}(A+B)$$
. (28)

$$\cos \frac{1}{2}(a-b) = \frac{\cos \frac{1}{2}c}{\cos \frac{1}{2}C} \sin \frac{1}{2}(A+B)$$
. (29).

From (22) and (23) we have,
$$\sin \frac{1}{2}(A+B) \cos \frac{1}{2}c = \cos \frac{1}{2}C \cos \frac{1}{2}(a-b)$$

$$\sin \frac{1}{2}(A-B) \sin \frac{1}{2}c = \cos \frac{1}{2}C \sin \frac{1}{2}(a-b)$$
. Hence, by addition,
$$\sin \frac{1}{2}(A-B) \sin \frac{1}{2}c + \sin \frac{1}{2}(A+B) \cos \frac{1}{2}c = \cos \frac{1}{2}C \cos \frac{1}{2}C$$
. (30).

In like manner, from (24) and (25),
$$\cos \frac{1}{2}(A-B) \sin \frac{1}{2}c + \cos \frac{1}{2}(A+B) \cos \frac{1}{2}c = \sin \frac{1}{2}C$$
. (31).

Again, from (26) and (27), we have
$$\sin \frac{1}{2}(a+b) \sin \frac{1}{2}(C = \sin \frac{1}{2}c \cos \frac{1}{2}(A-B);$$
and, by addition,
$$\sin \frac{1}{2}(a-b) \cos \frac{1}{2}C + \sin \frac{1}{2}(a+b) \sin \frac{1}{2}C = \sin \frac{1}{2}c . (32),$$
and, in like manner, from (28) and (29) we get
$$\cos \frac{1}{2}(a-b) \cos \frac{1}{2}C + \cos \frac{1}{2}(a+b) \sin \frac{1}{2}C = \cos \frac{1}{2}c . (33).$$

CHAPTER III.

ON THE RELATIONS BETWEEN THE CORRESPONDING VARIATIONS OF THE PARTS OF A TRIANGLE.

In the present chapter we propose briefly to examine into the effect produced on the sides and angles of a triangle, by a small change taking place in the magnitude of one of them; that is to estimate the amount of error affecting any part which may have been determined from data, not strictly accurate, and thence to ascertain under what circumstances a small inaccuracy in a proposed datum will least affect the accuracy of the result. This becomes a very essential matter of inquiry in all the more delicate practical operations of trigonometry, because, since the data furnished by observation necessarily fall short of strict accuracy, on account of the imperfections of instruments, and other unavoidable defects, we ought to know under what circumstances our observation should be made, so that the small error with which it is affected may have the least possible influence on the quantity to be determined from it. The following problems will sufficiently show the method of arriving at this knowledge.

PROBLEM I.

In a right-angled plane triangle, whose base is b, and altitude a, it is required to determine the error committed in calculating a by means of the given base b, and the observed angle opposite to a.

Let us consider a to represent the true angle opposite a, from which that given by observation varies by a small quantity, which we shall represent by δa , and call the variation of a, then the sought side which would be given by the equation $a = b \tan a$, is affected by an error δa ,

so that instead of a it is $a + \delta a$, and this we determine from the equation $a + \delta a = b \tan (a + \delta a)$; in which, by subtracting the preceding equation, we find the value of δa to be,

$$\delta a = b$$
} tan. $(a + \delta a) - \tan a$ } = $\frac{b \sin \delta a}{\cos a \cos (a + \delta a)}$ (art. 27):

Now, by hypothesis, δa is very small, so that we may substitute it for

its sine, and cos. a instead of cos. $(a + \delta a)$, $\therefore \delta a = \frac{\sigma a}{\cos^2 a}$;

in which expression & is the length of the arc to radius 1, which measures the angular error.

To determine what length b must be to render the variation θa the least possible under the same amount of error δa in a, we have

$$b = a \cot a \cdot ba = \frac{a \cot aba}{\cos^2 a} = \frac{aba}{\sin a \cos a} = 2 \frac{aba}{\sin 2a};$$

hence δa will be the least possible when sin. 2a is the greatest possible, that is when $a=45^\circ$: so that in order to determine the height of a tower or steeple, &c. with the utmost accuracy, by means of an observation of its angular altitude, we should make the observation at a distance from the object as nearly as possible equal to its height.

PROBLEM II.

In a right-angled spherical triangle is given one of the oblique angles to determine the variation of the opposite side, arising from a small variation of the hypotenuse.

Let A be the constant angle, a its opposite side, and c the hypotenuse; then $\sin a = \sin A \sin c$, $\sin (a + \delta a) = \sin A \sin (c + \delta c)$.

.. by subtraction, $\sin.(a+ba)-\sin.a=\sin.\Delta$ {sin. $(c+bc)-\sin.c$ }; that is, (page 39, equa. 27,)

 $2\cos(a+\frac{1}{2}\delta a)\sin(\frac{1}{2}\delta a)=2\sin A\cos(c+\frac{1}{2}\delta c)\sin(\frac{1}{2}\delta c)$

 $\therefore \sin \frac{1}{4} \delta a = \frac{\sin A \cos (c + \frac{1}{4} \delta c) \sin \frac{1}{4} \delta c}{\cos (a + \frac{1}{4} \delta a)}; \text{ and if } \delta a, \delta c, \text{ be very small,}$

 $\delta a = \frac{\sin. A \cos. c}{\cos. a} \delta c$; or, substituting for sin. A its value from the first

equation, $\delta a = \frac{\sin a}{\cos a} \cdot \frac{\cos c}{\sin a} \cdot \frac{\cos c}{\sin a} \cdot \frac{bc}{\sin a} = \tan a \cot c \cdot \delta c$; which variation will be the least possible when cot. c is least, or when $c = 90^\circ$. It would seem from the expression for δa , that in this case δa is absolutely 0, which we know cannot be. Indeed, no result deduced like that above, from a process in which certain small quantities are rejected, can be considered as perfectly accurate, although they may approximate so nearly to the truth as to be practically admissible as such. If we restore the $\frac{1}{2}\delta c$ which has been neglected, and write the above result thus, $\delta a = \tan a \cdot a \cot (c + \frac{1}{2}\delta c) \delta c$; then, in the case of $c = 90^\circ$, the expression becomes $\delta a = -\tan a \cdot a \tan \frac{1}{2}\delta c \cdot \delta c$; or, considering the very small arc $\frac{1}{2}\delta c \cdot \delta c$ to be equal to its tangent, we have in the case supposed $\delta a = -\frac{1}{2}\tan a \cdot (\delta c)^a$, the same expressions otherwise determined by Professor Airy in his Treatise on Trigonometry, in the Encyclopædia Metropolitana.

PROBLEM III.

In an oblique-angled spherical triangle are given two sides to determine the variation produced in the third side by a small variation of the opposite angle.

Let a, b, be the two given sides, C the included angle, and z the side

opposite to it. Then $\cos c = \cos a \cos b + \sin a \sin b \cos C$, $\cos \cdot (c + \delta c) = \cos \cdot a \cos \cdot b + \sin \cdot a \sin \cdot b \cos \cdot (C + \delta c);$... by subtraction, $\cos (c + \delta c) - \cos c = \sin a \sin b (C + \delta C) - \cos C$; that is, $2 \sin. (c + \frac{1}{4} \delta c) \sin. \frac{1}{4} \delta c = 2 \sin. a \sin. b \sin. (C + \frac{1}{4} \delta C) \sin. \frac{1}{4} \delta C$ Hence, if δC be very small, $\sin. c \delta c = \sin. a \sin. b \sin. C \delta C$ $\therefore \delta c = \frac{\sin. a \sin. b \sin. C}{\sin. a \sin. a \sin. a \sin. B \delta C};$ sin. c and δc is therefore the least possible when sin. C is the least possible, that is, when C = 0. To find the expression for δc , in this case, restore what has been rejected, and we shall have $\delta c = \frac{\sin \alpha \sin b \sin (C + \frac{1}{2} \delta C)}{\sin \alpha \sin b \sin (C + \frac{1}{2} \delta C)} \delta C$; which, when C = 0, and $\frac{1}{2} \delta C$ very small, becomes $\delta c = \frac{\sin a \sin b}{a}$ PROBLEM IV. In an oblique-angled spherical triangle are given, as before, two sides and the included angle, to find the variation produced in one of the opposite angles by a small variation in the included angle. Let a, b, be the given sides, C the included angle, then we have to find what influence a small variation in the value of the angle C will have on the angle A opposite a. For this purpose we shall deduce a suitable formula, as follows: substitute the expression for cos. c, on the opposite page, in the corresponding expression for cos. a, and we shall have the equation cos. A sin $c = \cos a \sin b - \sin a \cos b \cos C$; $\therefore \cos. A \frac{\sin. c}{\sin. a} = \cot. a \sin. b - \cos. b \cos. C. But \frac{\sin. c}{\sin. a} = \frac{\sin. C}{\sin. A};$ hence by substitution, cot. A sin. C = cot. $a \sin. b$ — cos. $b \cos. C$, cot. $(A + \delta A) \sin. (C + \delta C) = \cot. a \sin. b$ — cos. b — cos. $(C + \delta C)$; and by subtraction,

cot. $(A + \delta A) \sin(C + \delta C) - \cot A \sin C = \cos \delta \{\cos C - \cos(C + \delta C)\}$. ||
The first side of this equation is the same as $\cot(A + \delta A) \{\sin(C + \delta C) - \sin C\} + \sin C \{\cot(A + \delta A) - \cot A\};$ and the quantities within the brackets are respectively the same as $-\sin \delta A$

2 cos. (C + $\frac{1}{2}\delta$ C) sin. $\frac{1}{2}\delta$ C and $\frac{1}{\sin A \sin (A + \delta A)}$ Also the second side of the same equation is the same as

2 cos. $b \cdot 2$ sin. $(C + \frac{1}{2} \delta C)$ sin. $\frac{1}{2} \delta C$; consequently, sin. $C \sin \delta A = 2 \cos \delta \sin C + \frac{1}{2} \delta C \sin \delta C = \frac{\delta C}{\sin \Delta \sin \Delta \sin \Delta \cos \delta C + \frac{1}{2} \delta C}$ sin. $\frac{1}{2} \delta C$; and, therefore, when δC and δA are sin. $C \cos \delta \sin \Delta C \cos \delta \cos \Delta C \cos \delta \cos \Delta C \cos$

very small, cot. A cos. $C \delta C - \frac{\sin \cdot C}{\sin \cdot A} \delta A = \cos \cdot \delta \sin \cdot C \delta C$

 $\therefore \delta \mathbf{A} = \frac{\sin 3\mathbf{A}}{\sin \mathbf{C}} (\cot \mathbf{A} \cos \mathbf{C} - \cos \mathbf{b} \sin \mathbf{C}) \delta \mathbf{C}.$

The foregoing examples are those selected by *Professor Airy* in his Treatise on Trigonometry, before referred to, and we have here adopted his processes. But the instruments of investigation generally the best adapted to inquiries of this kind is the *Differential Calculus*.

SUPPLEMENT

ON SPHERICAL GEOMETRY, POLAR TRIANGLES, &c. BY T. S. DAVIES F. R. S. E., F. R. A. S. &C.

CHAPTER L

ON SPHERICAL GEOMETRY.

In the commencement of the Spherical Trigonometry, a small collection of propositions, such as were necessary in the character of fundamental principles upon which to build the subsequent analytical investigations was given. At the request of the author, we here propose to add a few others, and shall endeavour to select such as may serve the double purpose of facilitating our future inquiries, and of interesting the mind of the student in some of the most beautiful classes of Geometrical research that are yet known to exist; we shall com-mence with a few properties analogous to the more elementary propositions in Euclid, and which are very often assumed by writers in spherical trigonometry, both unnecessarily and improperly.

1. Let O be the spherical centre of a circle, and AB any great circle chord: the perpendicular* OK demitted from the centre upon AB will bisect it. Draw AO, BO. Then from the right-angled triangles AKO, BKO, we have,

cos. OA

cos. OK

cos. OK

cos. OK

cos. BK

cos. OK

cos. BK

cos. BK

cos. BK

 $=\frac{1}{\cos BK}$

But OA = OB, and ∴ AK = BK.
2. Conversely, if OK bisect AB, it will cut it at right angles.

For cos. AKO = $\frac{\cos. AO - \cos. AK \cos. KO}{\cos. AK \cos. KO}$ sin. AK sin. KO $\cos. BKO = \frac{\cos. BO - \cos. BK \cos. KO}{\cos. KO}$ sin. BK sin. KO

But the right-hand sides of these equations are equal, term for term, and therefore cos. AKO = cos. BKO, or AKO = BKO; and as AK, KB are one great circle, the angles at K are right angles: the tenth definition of the first book of Euclid applying to spherical as well as to plane

angles.

3. If the great circle chord AB, be bisected at right angles at K, by the great circle ZM, this perpendicular shall pass through the centre of the circle. For, assume for a moment that the centre is at O', not in the circle ZM; and draw the perpendicular O'K'. Now, we have seen that O'K' bisects AB in K' when O' is the centre, or that AK + KK' = BK - KK'; But, by hypothesis, AK = BK, and therefore, subtracting the latter equation, KK' = -KK', which is only true when K, K' coincide, that is, when O'K' coincides with OK, or when O' is in ZM. The centre is therefore in ZM.

 Always meaning a great circular perpendicular, except expressly stated otherwise. Equation (4/page 4) for AK = BK - KK' achow KK'= 4. If two great circles which cut one another at A, be intersected by a circle of the sphere in D, E, and H, L respectively, the rectangles of the tangents of the semi-segments into which they are divided shall be equal.

That is,

tan. AE tan. AD = tan. AH tan. AL. For find the centre G, draw AG meeting

the circle in B and C, draw the perpendicu-lars GF, GK, and join GD, GE, GH, GL. Then, cos. AK cos. KG = cos. AG = cos. AF cos. FG, cos. LK cos. KG = cos. GL = cos. FE cos. FG.

From these we have, by subtraction, addition, and subsequent division.

 $\frac{(\cos. AK - \cos. KL)}{(\cos. AK + \cos. KL)} = \frac{(\cos AF - \cos. FE)}{(\cos. AF + \cos. FE)};$ $(\cos. AK + \cos. KL)$ (cos. AK + cos. KL) (cos. AF + cos. FL) and hence, by dividing (28) by (29), page 39. tan. i(AK-KL) tan.i(AK + KL) = tan.i(AF - FE)tan.i(AF + FE), that is, tan.i AH tan.i AL = tan.i AD tan.i AE.

The analogue to Euclid in. 35, may be seen in another form in the

Math. Repository, No. 23, part II., p. 131, 2.

5. Let the secants in the case where A is without the circle take the position of tangents. Then D, E, F, coalesce, and so do H, K, L Then the equation just obtained becomes $\tan^2 AF = \tan^2 AK$, or AF = AK.

The tangents from any points to the circle are therefore equal. The case when the point is within the circle is demonstrated by Cagnoli, in his Trigonometry, but the other case he has not noticed.*

6. We may easily prove, also, that the great circle drawn through K at right angles to the ra-

dius, OK, touches the circle. For draw any other arc from O, as OL. Then, because K is a right-angle, we have cos. LK cos. KO = cos. LO. But cos. LK < 1, and therefore cos. LO < cos. KO, or LO > KO; and L will therefore fall without the circle; or, no part of KA falls within the circle whence KA is a tangent.

It is unnecessary to dwell at greater length upon these simple sub-jects; the nature of the inquiry, and the method of pursuing it, as well as its close analogy to the corresponding properties in the Elements of

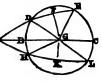
Euclid, must be at once apparent.

We may add that in the Repository, as above referred to, some other remarkable analogies to plain properties are derived by similar methods, to which we refer the inquiring reader.

Since this paper was written, Professor Lovery has sent me the enunciation of the proposition in the text, accompanied by the foregoing remark, and with the following corollaries subjoined, viz.

1. If an arc be drawn perpendicular to the diameter of a small circle of the sphere, the square of the tangent of half this arc will equal the product of the tangents of half the segments into which it divides the diameter.

2. If, from the extremities of the diameter of the small circle, arcs be drawn entities the circle in the same point as the perpendicular, then the sum of the aquares of the since of half these arcs will equal the square of the since of half these arcs will equal the square of the since of half the diameter of the small circle.



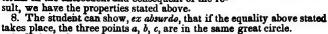


I.

7. Let any spherical triangle be cut by a transversal cba. Then the products of the sines of the alternate segments will be equal. That is, sin. Ac sin. Ba sin. Cb = sin. cB sin. aC sin bA.

For sin. Ac: sin. Ab:: sin. \(\beta \): sin. \(

Hence, multiplying, and effacing the common terms in the antecedent and consequent of the result, we have the properties stated above.



9. If through any point P on the surface of the sphere three great circles be described, which also pass through the angles of the triangle ABC, and cut the opposite sides in a, b, c, respectively, then sin. Ac sin. Ba sin. bC = sin. aC . sin. Bc sin. bA.

For the two spherical triangles BaA and CaA cut by the two transversals Cc, Bb, give respect-

ively $\sin AP \cdot \sin AB \sin bC = \sin AP \sin Bc \sin bA$

 $\sin aP \cdot \sin cB \sin cA = \sin AP \sin aC \sin cB;$ which multiplied, and the common terms effaced, give the enunciated

10. If through any point P in a given great circle Aa, which passes through an angle, of a spherical triangle, great circles be drawn to the remaining angles cutting the opposite sides in b, c, respectively, then the great circle be will always pass through the same point a' in the great circle BC, and

so divide it that sin. Ba: sin. ac:: sin. Ba': sin. a'C. For by (9 and 7) we have, respectively, sin. Ba: sin. aC:: sin. Bc sin. Ab:

sin. cA sin. bC sin. Ba': sin. a'C :: sin. Bc sin. Ab: sin. cA sin bC;

when, by equality of ratios, we have sin. Ba: sin. aC:: sin. Ba': sin. a'C.*

11. If three great circles be drawn

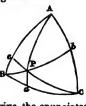
through the angles of a spherical triangle and through the same point on the surface of the sphere, cutting the sides in three points; three other great circles, each passing through two of these points, will intersect the sides of the triangle (produced or not as the case may require,) in the circumference of one and the same great circle.

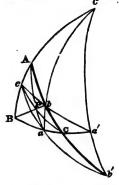
By (10) we have sin. Ba: sin. aC: sin. Ba': sin. a'C
sin. Cb: sin. bA:: sin. Cb': sin. b'A
sin. cA: sin. cB:: sin. c'A: sin. c'B;
or by multiplying vertically, and bearing (9) in mind,

* This division of an arc is analogous to that which in plane is called the harmonical division of a line. Some of the most interesting properties of elementary geometry. Sow from considerations respecting the mode of division; and the spherical properties have perfect analogies to those. A few of these may be seen in the paper above mentioned in the Repository; and others will appear in a future number. Some curious investigations on this subject, by Professor Lowry, may also be seen in vol. II., new series of the same work, quest 223. His processes however, are totally different from those just adverted to.

AABB; point P, culting sides in a, b, c; cb must Bb in a', ca meet Ab in b', ab meet BA in c' g a', b', c' are in ma







m

 $\sin \cdot Ba' \cdot \sin \cdot Cb' \sin \cdot c'A = \sin \cdot a'C \cdot \sin \cdot b'A \cdot \sin \cdot c'B$;

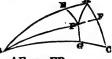
and hence by (8) the pr3position is established,*

12. If great circles be drawn from the angular points of any spherical polygon to a point on the surface of the sphere, the product of the sines of the alternate angles will be equal. In the triangle, (fig. to 9), sin. BP: sin. PA:: sin. BAP: sin. ABP sin. PA:: sin. PCA:: sin. PAC:: sin. PCA:: sin. PC

sin. PC: sin. PB:: sin. PBC: sin. PCB; and, by multiplica-tion, sin. BAP sin. PCA: sin. CBP = sin. ABP sin. PAC sin. PCB.

The student is required to prove it for four, five, &c. sided figures, and is recommended to complete the argument from the suggestions furnished by the particular cases of the general truth. This theorem is due to *Professor Lowry*, Math. Rep. old series, vol. 1., page 90.

Let ABC be a spherical triangle, and P a point on the surface of the sphere, from which perpendiculars PE, PF, PG, are drawn to the sides of the triangle: then the product of the cosines of the alternate segments will be equal to one another. For B.



cos. AE cos. EP = cos. AP = cos. AF cos. FP cos. BG cos. GP = cos. BP = cos. BE cos. EP cos. CF cos. FP = cos. PC = cos. CG cos. GP.

and multiplying the first and last columns vertically, we find

cos. AE cos. BG cos. CF = cos. AF cos. BE cos. CG.

Cor. If the triangle in triquadrantal, we shall have tan. AE tan. BG tan. CF = 1 = cot. AF cot. BE cot. CG.

14. We shall here give (although we forget from whom we take it, and what kind of demonstration was given of it,) another such property of the triquadrantal triangle; and the student who is versed in Analytical Geometry, will recognise in it the trigonometrical demonstration of a remarkable property of a point referred to rectangular coordinates.

Let D, E, be two points on the sphere, and ABC a triquadrantal triangle. Then we have this property, viz.

 \cos . $DE = \cos$. $DA \cos$. $AE + \cos$. $DB \Rightarrow \cos$. BE+ cos. DC cos. CE.

For \cos . DE = \cos . CD \cos . CE + sin. CD sin. CE cos. DCE and, by right angled triangles,

 $\sin. CD = \frac{\cos. AD}{}$ $\frac{\cos. AD}{\cos. AF}$ and $\sin. CE = \frac{\cos. AE}{\cos. AL}$.. (b). the angle DCE

is measured by $FL = AF \pm AL$; and hence (a) becomes

 $\cos DE = \cos CD \cos CE + \frac{\cos AD}{\cos AF} \cdot \frac{\cos AE}{\cos AL} \cos AF \cos AL$ sin. AF sin, AL

= cos. CD cos. CE + cos. AD cos. AE ∓ cos. AD cos. AE sin. AF sin. AL cos. AF cos. AL

But, by right angled triangles,

This remarkable proposition appears to have been discovered by Carnet, and was first published by him in 1803, and afterwards in 1806, in the Geometry of Position, and the Essay upon Transversals. It was subsequently and independently discovered by an eminent mathematician in this country, Mr. Whitey, who inferred it from the corresponding plane one, in the Ladies' Diary, 1817. The demonstration above given is taken entirely from Carnot, and it is a beautiful model for the method of conducting such inquiries. More ample information on these subjects may be had in the Beautiful with the Secretary of the success. in the Repository, ub supra.

cos. AD == cos. AF cos. FD, and cos. AE = cos. AL cos. LE; also, sin. $AF = \cos BF$, and $\mp \sin AL = \cos BL$. hence the last term of (c) reduces to

cos. FD cos. BF cos. LE cos. BL,

and by right-angled triangles, the first pair of these factors is equal to cos. BD, and the second pair to cos. BE, and thus is the proposed theorem established.*

Cor. 1. When D and E coincide, cos. DE = 1, and we have

$$\cos^2 AD + \cos^2 BD + \cos^2 CD = 1$$
,
 $\sin^2 DH + \sin^2 DG + \sin^2 DF = 1$.

Cor. 2. By (9) we have

sin. AF sin. BH sin. CG = sin. BF sin. AG sin. CH = cos. AF cos. BH cos. CG or, by division,

tan. AF tan. BH tan. CG = 1 = tan. AL tan. B1 tan. CK.

Cor. 3. When $DE = \frac{\pi}{\Omega}$ we have, cos. DA cos. AE + cos. DB cos. BE

+ cos. DC cos. CE == 0; (vide Young's Anal. Geom., p. 228, art. 182—just published by Carey, Lea, & Co. Philadelphia.)

15. The following propositions, dependent upon what has been done here, or else upon similar methods, are left as exercises for the student.

(a.) Let a transversal great circle cut any spherical polygon; dividing each side into two segments; the product of the sines of the one set of alternate segments will be equal to the product of those of the other set.

(b.) If a great circle bisect the angle of a triangle, (either interior or exterior,) the sines of the segments of the base have the same ratio as the sines of the sides.

(c.) The three bisectors pass through the same point on the sphere.
 (d.) Perpendiculars to the middles of the sides pass through the same

point, (centre of circumscribing circle.)

(c.) Perpendiculars from the angles of the triangle to the opposite

sides pass through the same point.

(f.) Great circles joining the middles of the sides to the opposite angles intersect in the same point.

(g.) Great circles joining the points of contact of the inscribed circles with the sides, and the opposite angles pass through the same point. (A.) Great circles passing through the points of contact of the circle

which touches a triangle exteriorly, and the opposite angles, pass through the same point.

(i.) Great circles bisecting the interior angles of a spherical triangle meet the opposite sides in three points, which are situated in one great circle of the sphere.

(k.) Show under what conditions the propositions (12) and (13) admit

of conversion.

(1.) Perpendiculars from the angles of a triangle upon the opposite sides intersect in three points, and the triangle formed by joining these

points has its angles bisected by the said perpendiculars.

It would have been easy to extend and to vary these subjects almost without limit. As the method of Transversals is the most powerful one yet known for the investigation of spherical determinate theorems, (seeming to make up for the deficiency of parallels and similar triangles the great organon in plane researches,) we thought it better to dwell

produce

^{*} It may be proper to mention here, that since the above demonstration was written I have remarked the same property in Dr. Luby's Trigonometry, p. 61-2; but I must have first met with it elsewhere, as I well recollect that it was unaccompanied with any proof. Dr. Luby's demonstration is a good deal similar to mine.

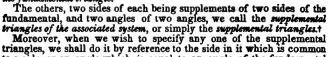
upon this sufficiently to give the student a real insight into the character of its processes and to furnish him with a few suitable exercises for his own improvement in such investigations.*

CHAPTER IL

ASSOCIATED TRIANGLES.

1. Let ABC be a spherical triangle, having its sides produced to meet again in A'B'C', respectively opposite to the angles A, B, C. Four triangles are thus formed which have a necessary relation to one another. These we propose to call c'the associated system of triangles, or simply the associated triangles.

That which was first drawn (ABC), and which serves as a basis of the rest, we call the fundamental triangle of the associated system, or simply the fundamental triangle.



Moreover, when we wish to specify any one of the supplemental triangles, we shall do it by reference to the side in it which is common to a side, or an angle which is equal to an angle of the fundamental triangle. Thus, to designate the triangles BA'C, CB'A, AC'B, we say the supplemental triangle taken with respect to A', (or a, as the case may be,) with respect to B', or with respect to C'.

As a uniformity of notation is essential in inquiries like these, related to classes of similar objects, we shall attempt to conform to the established notation as a basis. Thus, abc are the sides of ABC,

In which the number of subscribed accents points out the particular triangle designated, considering them to be ranged round the fundamental one in the order of the letters A', B', C'.

Again, for the angles, we have the angles

A number of important properties of spherical triangles, demonstrated geometrically, by Professor Lowry, may be seen in the first vol. of the old series of the Mathematical Repository, and some others in Howard's Spherical Geometry, 1798. The subject, however, is still open to indefinite research, and offers ample reward to those whose taste may lead them to cultivate it. See also note A.

if The term "supplemental" has been used by English Mathematicians to designate that triangle which is now universally denominated the "polar triangle." The word has ceased to be used in that sense for some years, and as it is so peculiarly adapted to express the triangles which are formed by producing the sides of the fundamental, we have not hesitated to adopt it. We give this notice, however, of the change in its appropriation, lest some confusion should arise in the mind of the young mathematician when he sees in Trigonometrical works, of the last age, a use different from our own of the word supplemental.

It may be remarked that the choice of the word for that purpose was not happy; for though it was so far a defining property as to give the species of the triangle, it did not give its position; an element quite as important, in many investigations, as the species keelf, and, indeed, that upon which several of its valuable properties depend.

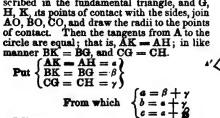
taken in the aforesaid order, we write r, r,, r,,, r,,... whilst, for the radii of the circumscribed circles, we put R, R,, R,,, R,,, respectively. The unaccented letters referring to the circles of the fundamental tri-

angles.

These triangles possess many beautiful properties when considered in their mutual association, which render them worthy of greater attention than has yet been bestowed upon them. Indeed, till very recently their existence has scarcely been alluded to by writers on spherical subjects, and even to the present day, not more than three of their properties have, we believe, been published.

2. Let O be the centre of the circle in-

scribed in the fundamental triangle, and G



Whence

Again, in the right-angled triangle BOG, we have tan. OG = sin. BG tan. OBG, that is, tan. $r = \sin \beta \tan \beta$; or by (1) just given and (3), upon page 49, applied to B, we have

$$\tan s = \sin s - b \left\{ \frac{\sin s - a \sin s - c}{\sin s \sin s - b} \right\}^{\frac{1}{2}}$$

$$= \frac{\sqrt{\sin s \sin s - a \sin s - b \sin s - c}}{\sin s \sin s - a \sin s - b \sin s - c} \dots (2)$$

Again, in the supplemental triangle BA'C, denoting the quantities BK', CH', and AK', by β_{γ_1} , α_{γ_2} , we shall have

a.

$$\frac{-a,+b,+c}{3}, = \frac{-a+x-b+x-c}{3} = \frac{a+b+c}{3} = s,$$

$$\frac{s,-b,+c}{3} = \frac{a-x-b+x-c}{3} = \frac{a+b-c}{3} = \frac{s-c}{3},$$

$$= \frac{a,+b,-c}{3}, = \frac{a+x-b-x-c}{3} = \frac{a-b+c}{3} = \frac{s-b}{3}.$$

Also $B_r = \pi - B_r$, and $\tan \theta + B_r = \cot \theta$. Hence, in the right angled triangle BO'G', we have $\tan \theta O'G' = \sin \theta$. BG $\tan \theta O'BG'$, that

is,
$$\tan r$$
, $-\sin \beta$, $\tan \beta$, $\tan \beta$, $\sin \beta - c$ $\left\{\frac{\sin \beta \sin \beta \sin \beta - b}{\sin \beta - a \sin \beta - c}\right\}$

$$-\sqrt{\sin \beta \sin \beta - a \sin \beta - b} \sin \beta - c$$

In exactly the same way we find the other associated inscribed radii, and the whole tabulated gives

These formulæ were first given by *Professor Lowry* (1829), Leyboum's Repository, vol. v. p. 3. Multiply these together, then we obtain $\tan r \tan r \sin r$, $\tan r$, $\tan r$, $\tan r$, $\tan r \sin s \sin s \sin (s-a) \sin (s-b) \sin (s-c)$. (4)

Divide (4) by the squares of each of the equations in art. (3), the first side by the first side, and the second by the second: then

$$\begin{array}{l}
\sin^2 s = \cot \cdot r \tan \cdot r_{,r} \tan \cdot r_{,r} \\
\sin^2 (s - a) = \tan \cdot r \cot \cdot r_{,r} \tan \cdot r_{,r} \\
\sin^2 (s - b) = \tan \cdot r \tan \cdot r_{,r} \cot \cdot r_{,r} \\
\sin^2 (s - c) = \tan \cdot r \tan \cdot r_{,r} \cot \cdot r_{,r}
\end{array}$$
(5); which remarkable

formulæ are due to Mr. Lowry (1819), vide Repository, wb. sup. Again, by multiplication of the terms in (3), we have

 $\tan r + \tan r + \tan r = \sin (s-b) \sin (s-c) + \sin s \sin (s-c)$

$$=\sin \cdot \frac{a+(b-c)}{2}\sin \cdot \frac{a-(b-c)}{2}+\sin \cdot \frac{b+c+a}{2}\sin \cdot \frac{(b+c)-a}{2}$$

$$=\sin \cdot \frac{a}{2}-\sin \cdot \frac{b-c}{2}+\sin \cdot \frac{b+c}{2}-\sin \cdot \frac{a}{2}=\sin \cdot b\sin \cdot c.$$

Taking also each of the other corresponding combinations, we obtain all the three following equations,

tan.
$$r$$
 tan. $r_{,+}$ tan. $r_{,,+}$ tan. $r_{,,-}$ = sin. b sin: c tan. $r_{,+}$ + tan. $r_{,+}$ tan. $r_{,,-}$ = sin. a sin. c tan. $r_{,,-}$ + tan. $r_{,,-}$ tan. $r_{,,-}$ = sin. a sin. b . (6).

Or, by addition, we have at once the following theorem.

tan.
$$\tau$$
 tan. τ , + tan. τ tan. τ _{...} + tan. τ tan. τ _{...} + tan. τ _{...} + tan. τ _{...} + tan. τ _{...} (7).

That is, in words, the sum of the binary products of the tangents of the four inscribed radii are equal to the sum of the binary products of the sines

of the sides. We may notice one beautiful theorem more, which is due to Mr.

Lowry, whi supra. It is tan. r, tan. r, + tan. r, tan. r, + tan. r, tan. r, = $\sin s \sin (s-a) + \sin (s-b) + \sin (s-c)$. For the several consequences of these theorems, and a continuation

of the inquiry, we must refer to the number xxiv. of Leybourn's Repository, now in the press, where expressions for the various trigonometrical functions of the sides and angles of the triangle, will be given in terms of the inscribed radii.

3. We now proceed to consider the circumscribed radii of the associated triangles. We shall immediately find these in terms of the angles, as we did those of the inscribed in terms of the sides.

Let Q be the centre of the circumscribing circle of the fundamental triangle, and draw the perpendiculars QM, QN, QP. Then M, N, P, bisect the sides a, b, c, respectively, and the several triangles BQC, CQA, AQB, are isceeles. Let the angles made by the radii QB, QC, with the side a be denoted by a; those with b, by β , and those with c by γ .* Then $A = \beta + \gamma$, $B = a + \gamma$, $C = a + \beta$. From which we have

$$a + \beta + \gamma = \frac{A + B + C}{2} = 8,$$

$$a = \frac{-A + B + C}{2} = (8 - A)$$

$$\beta = \frac{A - B + C}{2} = (8 - B)$$

$$\gamma = \frac{A + B - C}{2} = (8 - C)$$

But, by right-angled triangles BMQ, we have cot. QB = cos. QBM cot. BM, or cot. R = cos. a cot. 1 a; or, by (9) and (p. 50-1), we have at once

$$\cot \mathbf{R} = \sqrt{-\cos 8 \cos \overline{8 - A} \cos \overline{8 - B} \cos \overline{8 - C}}$$

$$-\cos 8$$

Proceeding with respect to the triangle BA'C, in a manner analogous to that employed in obtaining the three last equations of (3), using the values of a, β , γ , just given in (9), we shall have the following tablet of values,

[&]quot;These quantities being merely introduced as subsidiary ones, to be replaced in all general formulas by their values in terms of A, B, C, we have not transgressed our general rule in employing them to designete two different sets of unntities in this place as in art (3) which belong finally to the inquiry.

Q

cot.
$$R = \sqrt{\frac{-\cos S \cos \overline{S} - \overline{A} \cos \overline{S} - \overline{B} \cos \overline{S} - \overline{C}}{-\cos S}}$$

cot. $R_{,''} = \sqrt{\frac{-\cos S \cos \overline{S} - \overline{A} \cos \overline{S} - \overline{B} \cos \overline{S} - \overline{C}}{\cos S - \overline{A} \cos \overline{S} - \overline{B} \cos \overline{S} - \overline{C}}}$

cot. $R_{,''} = \sqrt{\frac{-\cos S \cos \overline{S} - \overline{A} \cos \overline{S} - \overline{B} \cos \overline{S} - \overline{C}}{\cos S - \overline{B} \cos \overline{S} - \overline{C}}}$

cot. $R_{,''} = \sqrt{\frac{-\cos S \cos \overline{S} - \overline{A} \cos \overline{S} - \overline{B} \cos \overline{S} - \overline{C}}{\cos \overline{S} - \overline{C}}}$

which, with the following beautiful theorem, analogous to Lowry's, at p. 128, (obtained by multiplying these together) is due to Dr. Lardner, (1826). Trig. p. 153. cot. R cot. R, cot. R, cot. R, =

 $-\cos S \cos S - A \cos S - B \cos S - C$. Divide (11) by the squares of each of the equations in (10), and we $\cos^2 S = \tan R \cot R \cot R \cot R \cot R$ have $\cos^2 S - A = \cot R \tan R \cot R_{ii} \cot R_{iii}$. (13).

 $\cos^2 S - B = \cot R \cot R$, $\tan R$, $\cot R$ $\cos^2 S - C = \cot R \cot R_i \cot R_{ii} \tan R_{iii}$

These elegant theorems, which are here published for the first time, were discovered by my learned friend, the Rev. H. F. C. Legan, Pro-fessor of Mathematics in the Catholic College of Prior Park. The first of them is a remarkable expression for the spherical excess in terms of the four circumscribed radii. The spherical excess in terms of the inscribed radii may be seen in the Repository before alluded to; and some theorems connected with the same function of the triangle will be given in a future page of this supplement. By combining (10) in the same way as (5) was combined to obtain (6), we shall have

cot. R cot. R, + cot. R,, cot. R,,, = sin. B sin. C cot. R cot. R,, + cot. R, cot. R,,, = sin. A sin. C cot. R cot. R,,, + cot. R, cot. R,, = sin. A sin. B

Hence, by addition, we get cot. R cot. R, + cot. R cot. R,, + cot. R cot. R,, + cot. R, cot. R,, + cot. R, cot. R,,, + cot. R, cot. R,,, + cot. R,, cot. R,, + cot. $= \sin A \sin B + \sin B \sin C + \sin C \sin A$ (14).

In the Repository (xxiv) will also be found expressions for the triconometrical functions of the elements of the triangle, in terms of R, R,, R,,, R,,; and we may here remark that by means of a theorem to be given at page 133-4 of this treatise, the expressions (10, 14, incl. and all of the same class) may be derived, by inspection, from those given in terms of sides and inscribed radii. It is by means of a property of the polar triangle. We shall, however, before proceeding to the theory of polar triangles, point the student's attention to two interesting propositions, the analytical expressions for which we have passed by without particular notice. We allude to the values of tan. r, and of cot. R, at particular notice. We allude pages 127, 129; and which are

tan. $\dot{r} = \sin \beta \tan \beta = \sin \beta (a + c - b) \tan \beta$ cot. $\dot{R} = \cos \alpha \cot \beta = \cos \beta (B + C - A) \cot \beta \alpha$

1. From the first of these we infer that if B and a+c-b are constant, r will he constant; that is to say, in any spherical triangle if the vertical angle (B) be constant, as also the difference between the base and sum of the other two sides, the radius and centre of the inscribed circle will continue fixed.

Ain 2 & cos 2 5. - 14

n

(a) be constant, as also the difference between the vertical angle, and the sum of the other two, the radius and centre of the circumscribed circle will ||||
be fixed; that is, the locus of the vertex will be a circle.

3. This last property suggests a remarkable simple method of de-3. This last property suggests a remarkable sumple method of demonstrating the beautiful theorem of Lexell which is this, viz. that if the base and area of the spherical triangle be constant, the locus of the vertex will be a circle. For, referring to the figure at page 129, let BC be the constant base, and ABC any one of the triangles. Produce the sides to meet in A', and call the angles at B and C below the base B' and C'. For the area of the triangle ABC we have the expressions $A + B + C - \pi = \text{constant}$. But A = A', $B = \pi - B'$, $C = \pi - C'$; hence, by substitution, $A' - (B' + C') + \pi = \text{const.} \therefore B' + C' - A'$.

= const. and, therefore, as the base BC or a' is also constant, it follows from the theorem just demonstrated that the locus of the vertex A' is the circle A'BC, and, consequently, the locus of A, which is the anti-podes of A', must be an equal circle. We ought to remark here that this demonstration is the same in substance as that given by M. Lowry

in Leybourn's Repository, vol. 1.*

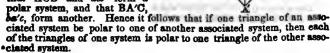
Polar Triangles.

We have already seen, (p. 45,) that if from the three angular points of a spherical triangle ABC we describe three great circles, they will form an associated system of triangles, one of which also has a remarkable relation to the triangle ABC: but it has not, so far as we know, been noticed, that if we complete the associated system, whose fundamental is ABC, then the two sets of associated triangles thus produced, will be separable into four pairs, (one of each system forming a pair) which will be related to one another precisely in the same way as the above named pair are related. Thus, if in the annexed figure, ABC be the fundamental triangle, abc its polar; then four pairs of polars will simultaneously be produced, viz.

(1) $\frac{ABC}{abc}$ (2) $\frac{AB'C}{ab'c}$ (3) $\frac{A'BC}{a'bc}$ (4) ABC'. abc'.

Now the first pair ABC, abc Hence B is the pole of ca, that is of bc; and since C is the pole of ab, therefore C' is the pole of ab, therefore C' is The the other pole of ab. points A, B, C' are the poles of the sides, therefore, of the triangle abc'. Whence, also, it follows by the reciprocity of the polar system, that a, b, c' are the poles of ABC'

In the same way it is shown that ACB' and ach' form a



In the Edinburgh Transactions the author of this supplement has investigated Lazal's theorem by a novel analysis,—the geometry of spherical coordinates, which determines in a direct manner the equation of the locus, and then shows its identity with the previously found equation of a circle.

[†] When we speak of parallel lines without specifying which is taken as the line of

This is not the only curious property of the figure before us: and we shall put down a small selection from those we are in possession of, not doubting that on many accounts they will be interesting to those geometers who indulge in trigonometrical speculations. An addition to these will appear in the 25th number of the Mathematical Repository.

Draw the great circle aA (next figure), and produce it to meet BC, be in G and H. Then, because a is the pole of BC, and that A is the pole of bc, the arcs aG, AH, are quadrants. Hence, aG + AH = aH+ AG = π, and the angles at G and H are right angles.

Let R, R', be the intersections of BC, bc; then, because the angles at G and H are right, R, R', are the poles of aA.

Let AB meet bc in K, BC meet ab in

L, AC meet bc in M, and ac meet Bc in N.

(Then $bH \sim Hc = GAC \sim GAB$ $\left\{bH + GAB = \frac{\tau}{2} = Hc + GAC.\right\}$

For bM = bH + HM = bH + HAM= bH + GAC. In like manner, cK =cH + HK = cH + HAK = cH + GAB

Also $bM = \frac{\pi}{2} = cK$, since b and c are the poles AM and CK.

Hence the propositions as stated are true

These are due to Professor Lowry, and were given by him, in 1800, in Leybourn's Repos. old series, No. 1, p. 44, 5. have not, that we are aware, been noticed in any other place.



Returning now to our original figure, let the three arcs, Aa, Bb, Cc, be drawn; these will pass through the same point O, because as has been just shown, they are perpendicular to the three sides BC, AC, AB, (vide p. 125). Also, because aA is perpendicular to bc, it will pass through the opposite pole a'. In like manner it will pass through A'. Or the points aAOa' A' are in the same great circle, whose poles are R, and R', the intersections of BC, bc.

In like manner #BOAB' are in one great circle, whose poles are S. S'.

In like manner bBOb'B' are in one great circle, whose poles are S, S', the intersections of AC, ac; cCOc'C' are in one great circle, whose poles are Q, Q', the intersections of AB, ab. Again, because R, R', are the poles of aa' the arcs RO, OR', are quadrants. In like manner SO, OS', and QO, OQ', are respectively quadrants; and as the quadrants are drawn from the poles of aa', bb', cc', respectively, R, O, R'; S, O, S', and Q, O, Q', are respectively in the same great circles.

Also since
$$OR = OR' = OS = OS' = OQ = OQ' = \frac{\pi}{2}$$
, the points R, R', S, S', A, Q', are in the same great circle, and O is its pole.

The complexity of the figure which would represent from a further detail of these interesting researches, compels us to leave them for the

reference, and knowing that the second is related to the first in the same way that the first is to the second, we simply denominate them parallels. The same practice also holds in speaking of two mutually supplemental angles. But when we previously fix upon one line or one angle, we say the parallel, or the supplemental in the singular number to express the other line or angle. Just so in respect to the two triangles which constitute the polar system, when we speak of both without assigning the referee, we call them polars, as a common epithet; but when we have fixed upon one already, as that to which the other is referred, we call it the primary and the other the solar triangle. polar triangle.

present to the industry and ingenuity of the student. They are exceedingly easy and furnish an excellent exercise in spherical investigations: and we therefore hope he will give it a proper degree of consideration. We proceed to view the subject algebraically.

Let abc, ABC, be the sides and angles respectively of a spherical triangle; Rr, the radii of the circumscribing and the inscribed circles; s, S, the semi sums of the sides and angles respectively; also let a'b'c'; A'B'C'; R', τ' ; S', s', be the same things in the triangle which is polar to abc. Put, as at page 116,

$$n^{2} = \sin s \sin s - a \sin s - b \sin s - c$$
 $n^{2} = \sin s \sin s' - a' \sin s' - b' \sin s' - c'$
 $n^{2} = \cos s \cos s - A \cos s - B \cos s - C$
 $n^{2} = -\cos s' \cos s' - A' \cos s' - B' \cos s' - C'$

Then we propose to prove that $n^2 = N^{\prime 2}$, and $n^{\prime 2} = N^2$.

For
$$a = \frac{1}{2}(a + b + c)$$

 $a - a = \frac{1}{2}(-a + b + c)$
 $a - b = \frac{1}{2}(a - b + c)$
 $a - c = \frac{1}{2}(a + b - c)$; and, in the polar tra-

angle, we have immediately $8' = \frac{3\pi}{2} - \frac{1}{4}(a + b + c) = \frac{3\pi}{2} - s$,

$$8' - A' = \frac{\pi}{2} - \frac{1}{2} (-a + b + c) = \frac{\pi}{2} - \frac{1}{2} - \frac$$

Hence,
$$-\cos B' = -\cos \left(\frac{3\pi}{2} - s\right) = \sin s$$
,
 $\cos B' - A' = \cos \left(\frac{\pi}{2} - \overline{s - a}\right) = \sin s - \overline{a}$,
 $\cos B' - B' = \cos \left(\frac{\pi}{2} - \overline{s - b}\right) = \sin s - \overline{b}$,
 $\cos B' - C' = \cos \left(\frac{\pi}{2} - \overline{s - c}\right) = \sin s - \overline{c}$.

Whence, by multiplication of the extreme vertical columns we have the quantities designated by $N^{\prime 2}$, and n^2 ; or, $N^{\prime 2} = n^2$. In exactly the same way, we find that $N^2 = n^{\prime 2}$. That is, $N^{\prime} = n$, and $N = n^{\prime}$.

$$\tan \frac{1}{2} \text{ A'} \tan \frac{1}{2} \text{ B'} \tan \frac{1}{2} \text{ C'} = \frac{\pi'}{\sin^2 \pi}; \cot \frac{1}{2} \text{ a cot. } \frac{1}{2} \text{ b cot. } \frac{1}{2} \text{ c} = \frac{N}{\cos^2 S'}$$

But $\frac{1}{4}(A' + a) = \frac{\pi}{2}$.. cot. $\frac{1}{4}a = \tan \frac{1}{2}A'$, and hence the left sides are equal. Also, cos. ${}^{2}S = \sin {}^{2}S$, therefore $N = \pi'$.

Had the mere proof of the property been our object, this would have been the preferable method: but the stages through which in the text we have passed are necessary in other inquiries, and we prefer therefore to give them in that form which, it may be remarked too, is the original one by which the property was obtained. See note B.

$$-\cos(3\pi - 25) = -\cos(\pi - 25) = -\cos(\frac{\pi}{2} - 5)$$

$$\cos(90 - 5) = \sin 5$$

^{*} These properties might have been more simply obtained, thus: by (18) and (21), page 117.

$$\tan r = \frac{n}{\sin s}$$
, $\tan r' = \frac{n'}{\sin s'}$; and, therefore, by (17, p. 117),

$$\tan r' = \frac{N'}{2\cos \frac{1}{4} \text{ A'}\cos \frac{1}{4} \text{ B'}\cos \frac{1}{4} \text{ C'}} = \frac{N'}{2\sin \frac{1}{4} \sin \frac{1}{4} \sin$$

$$\tan R = -\frac{\cos S}{N} = \frac{2\sin \frac{1}{2}a \sin \frac{1}{2}b \sin \frac{1}{2}c}{n}; \tan R' = -\frac{\cos S'}{N} = \frac{\sin s}{N'}.$$

Whence, recollecting that
$$N = n$$
, $\frac{\tan r}{\tan r} = \frac{2 \sin \frac{1}{2} a \sin \frac{1}{2} b \sin \frac{1}{2} c}{\sin \frac{1}{2} (a + b + c)}$

and
$$\frac{\tan R}{\tan R'} = \frac{9 \sin \frac{1}{2} a \sin \frac{1}{2} b \sin \frac{1}{2} c}{\sin \frac{1}{2} (a+b+c)} \cdot \frac{\tan r}{\tan r'} = \frac{\tan R}{\tan R'}$$

But we have a more useful result, as follows:

tan. R tan.
$$r' = \frac{2\sin \frac{1}{4} a \sin \frac{1}{4} b \sin \frac{1}{4} c}{n} \cdot \frac{N'}{2 \sin \frac{1}{4} a \sin \frac{1}{4} b \sin \frac{1}{4} c} \cdot = 1$$

or tan. R = cot. r', which is fulfilled by the relations

$$R + r' = \frac{\pi}{2}$$
, and $R + r' = \frac{3\pi}{2}$. The former of these relations holds

when the circles are referred to their nearest poles, and the latter when to their farther poles. In like manner, we also have, in the corresponding cases, $R' + r = \frac{\pi}{2}$ and $R' + r = \frac{3\pi}{2}$

From these we get
$$R + r' = R' + r$$

$$R-R'=r-r'$$

$$R-r=R'-r'.$$

Thus the remarkable relation between the polar triangles is continued even amongst the radii of the inscribed and circumscribing circles, viz. that the inscribed radius of one is the complement of the circumscribing radius of the other; or, taking diameters, the supplement of the other.

We have seen that in the two associated systems, having one pair of mutually polar fundamental triangles, the two systems, are triangle for triangle mutually polar; and hence collecting the whole result into one table, we have

$$R + r = \frac{\pi}{2}$$

$$R + r' = \frac{\pi}{3}$$

$$R' + t^{\frac{\pi}{2}} = \frac{\pi}{3}$$

$$R'_{r} + r_{r}^{*} = \frac{\pi}{2}$$

$$R_{r} + r'_{r} = \frac{1}{2}$$

$$R_{\prime\prime} + r_{\prime\prime} = \frac{\pi}{9}$$

$$R'_{\prime\prime\prime} + r_{\prime\prime\prime} = \frac{\pi}{2}$$

$$\mathbf{R}_{m} + \mathbf{r}_{m} = \frac{\pi}{9}$$

$$R' + r = \frac{3\pi}{9}$$

$$R + r' = \frac{3\pi}{9}$$

$$R', +r, = \frac{3\pi}{9}$$

$$R_{r}+r_{r}=\frac{1}{9}$$

$$R'_{'''} + r_{'''} = \frac{3}{9}$$

$$R_{'''} + r'_{'''} = \frac{3}{9}$$

Adding all these together, we have $R' + R'_{\prime\prime} + R'_{\prime\prime\prime} + R'_{\prime\prime\prime} = 4\pi \text{ (or 19 π)}.$

That is, the sum of all the sixteen radii of the primary and polar associated system is equal to the surface of the hemisphere if the first system of values is taken, or to three times that sum if the second system be taken.

The consideration of the latter system of values I owe to the Rev. Professor Logan; the former with its results is my own independent discovery, and was the origin of my researches on the subject of polar triangles, and of the associated triangles too.

Another property also comes immediately from this: viz. that the product of the tangents of the sixteen radii is equal to unity. Which is seen at once by $\tan r$, $\tan R' = 1$, &c.: or it may again be put

tan. r tan. r, tan. r, tan. r, tan. r tan. r, tan. r, tan. r, cot. R cot. R, cot. R, cot. R, cot. R' cot. R', cot. R', cot. R', or still differently,

 $\frac{\tan r \tan r \tan r, \tan r, \tan r, \tan r,}{\cot R \cot R, \cot R, \cot R,} = \frac{\cot r' \cot r', \cot r', \cot r',}{\tan R' \tan R', \tan R', \tan R',}$ cot. R cot. R, cot. R, cot. R,

Another neat relation may be put down here; we have already seen

 $\frac{\tan R}{\tan R'} = \frac{2\sin \frac{1}{4}a \sin \frac{1}{4}b \sin \frac{1}{4}c}{\sin \frac{1}{4}(a+b+c)}$; and by interchanging the pri-

mary and secondary polar triangles, still retaining the accent upon the same letters to distinguish them as the sides of the same triangle as

before, we have
$$\frac{\tan R'}{\tan R} = \frac{2 \sin \frac{1}{2} a' \sin \frac{1}{2} b' \sin \frac{1}{2} c'}{\sin \frac{1}{2} (a'+b'+c')}$$
.

Dividing these, we have

$$\frac{\tan^{2}R}{\tan^{2}R'} = \frac{\sin \frac{1}{2} a \sin \frac{1}{2} b \sin \frac{1}{2} c}{\sin \frac{1}{2} a' \sin \frac{1}{2} b' \sin \frac{1}{2} c'} \cdot \frac{\sin \frac{1}{2} (a'+b'+c')}{\sin \frac{1}{2} (a+b+c)}$$

But $\frac{1}{2}a = \frac{\pi}{\Omega} - \frac{1}{2}A$, &c. because the triangles are polar;

$$\frac{\tan^{-2}R}{\tan^{-2}R'} = \frac{\sin \cdot \frac{1}{2} a \sin \cdot \frac{1}{2} b \sin \cdot \frac{1}{2} c}{\cos \cdot \frac{1}{2} A \cos \cdot \frac{1}{2} B \cos \cdot \frac{1}{2} C} \cdot \frac{-\cos \cdot S}{\sin \cdot S}.$$

 $= \frac{\sin \cdot \frac{1}{2} a \sin \cdot \frac{1}{2} b \sin \cdot \frac{1}{2} c}{\cos \cdot \frac{1}{2} A \cos \cdot \frac{1}{2} B \cos \cdot \frac{1}{2} C} \cdot \frac{\cos \cdot \frac{1}{2} A \cos \cdot \frac{1}{2} C}{\cos \cdot \frac{1}{2} A \cos \cdot \frac{1}{2} C}$ Multiplying the

same equations we get 4 cos. A cos. B cos. C sin. sin. sin. sin. c = - cos. S sin. s; or in every spherical triangle we have

which, by the bye, is also an immediate consequence of the relations (17), (19), at page 117. Innumerable other interesting results may be obtained with equal facility, by means of the property of polar radii given above; but the limits of a work, like the present, prevent our enlarging upon them here. We may, however, refer for some of them to the Mathematical Repository, No. xxiv.

CHAPTER III.

SOME ADDITIONAL INQUIRIES RESPECTING THE SPHERICAL EXCESS.

WE shall now devote a short chapter to some miscellaneous inquiries respecting the Sphevical Excess, in continuation of what has been already done in Chapter II. Part IV. All the usual formulæ for the spherical excess have there been amply discussed; but there are still certain other combinations of data which have not yet been considered: these are, 1st, Two angles and the interjacent side; 2d, Two angles and a side opposite to one of them: and lastly, Two sides and an angle opposite to one of them. Expressions for the spherical excess in each of these cases may be readily deduced. In the last two, however, the formulæ which I have obtained are neither sufficiently symmetrical nor sufficiently simple to render them deserving of much notice, either for analytical beauty or for practical convenience; they involve, however, but one radical. The formula for the first of the above cases I investigate as follows.

To determine the Spherical Excess when two angles and the interjacent side are given.

Thus we shall have a choice of three forms, to suit the specific purpose we have in view. The last is the preferable on the ground of algebraical symmetry. Substituting these, we have

$$\cos \frac{E}{2} = \cos \frac{A+B}{2} \left\{ \cos^2 \frac{A-B}{2} \sin^2 \frac{c}{2} + \cos^2 \frac{A+B}{2} \cos^2 \frac{c}{2} \right\}^{\frac{1}{2}} \\ + \sin \frac{A+B}{2} \left\{ \sin^2 \frac{A-B}{2} \sin^2 \frac{c}{2} + \sin^2 \frac{A+B}{2} \cos^2 \frac{c}{2} \right\}^{\frac{1}{2}} \\ \sin \frac{E}{2} = \cos \frac{A+B}{2} \left\{ \sin^2 \frac{A-B}{2} \sin^2 \frac{c}{2} + \sin^2 \frac{A+B}{2} \cos^2 \frac{c}{2} \right\}^{\frac{1}{2}}$$

substitute the value of cos. e in terms of to . analtiply both terms by I or din & + eve - 2

$$+\sin \frac{A+B}{2} \cos^2 \frac{A-B}{3} \sin^2 \frac{\epsilon}{3} + \cos^2 \frac{A+B}{3} \cos^2 \frac{\epsilon}{3}$$

To determine the excess, when the three sides are given.

This case has been already discussed, but the following investigation may not be unacceptable. By (46, 4,)

$$\tan \frac{E}{4} = \frac{9 \sin. \frac{A + B + C - \pi}{4} \cos. \frac{A + B - C + \pi}{4}}{9 \cos. \frac{A + B + C - \pi}{4} \cos. \frac{A + B - C + \pi}{4}}$$

$$= \frac{\sin. \frac{A + B}{2} - \sin. (\frac{\pi}{2} - \frac{C}{2})}{\cos. \frac{A + B}{2} + \cos. (\frac{\pi}{2} - \frac{C}{2})} = \frac{\sin. \frac{A + B}{2} - \cos. \frac{C}{2}}{\cos. \frac{A + B}{2} + \sin. \frac{C}{2}} \text{ or by (art. 86)}$$

$$= \frac{\cos. \frac{a - b}{2} - \cos. \frac{c}{2}}{\cos. \frac{a + b}{2} + \cos. \frac{c}{2}} \cot. \frac{C}{2} = \frac{\sin. \frac{3 - a}{2} \sin. \frac{3 - b}{2}}{\cos. \frac{3}{2} \cos. \frac{3 - c}{2}} \cot. \frac{C}{2} \cdot (a).$$
But,
$$\cot. \frac{C}{2} = \sqrt{\frac{\sin. s \sin. s - c}{\sin. s - a \sin. s - b}}$$

$$= \sqrt{\frac{\sin. \frac{3}{2} \cos. \frac{3}{2} \sin. \frac{3 - c}{2} \cos. \frac{3 - c}{2}}{\sin. s - a \sin. s - b}}$$

Inserting (b) in (a), we have, after slight reductions,

$$\tan \frac{E}{4} = \sqrt{\tan \frac{s}{2} \tan \frac{s-a}{2} \tan \frac{s-b}{2} \tan \frac{s-c}{2}} \text{ which is the}$$

 $\frac{s-a}{\sin \frac{s-a}{2}\cos \frac{s-a}{2}\sin \frac{s-b}{2}\sin \frac{s-c}{2}}$

remarkable formula of Lhuillier.* Applying this to the polar triangles, some interesting results may be obtained as follows:

Denoting by S₁, S₂, S₂, the semi-sums of the sides of the supplementary triangles; by a_1 , b_2 , and c_3 , the sides of BA'C; a_{11} , b_2 , b_3 , b_4 , the sides of AB'C; and by a_{12} , b_{22} , b_3 , b_4 , b_4 , b_5 , the sides of AC'B. Then (see p.

187)
$$s, = \frac{a + \pi - b + \pi - c}{2} = \frac{a - b - c}{2} + \pi = \frac{-a + b + c}{2} = \pi - \frac{-s - a}{2} = \pi - s,$$

$$s, -b, = \frac{a - b - c}{2} + \pi - \pi - b = \frac{a + b + c}{2} = \pi - s,$$

$$s, -b, = \frac{a - b - c}{2} + \pi - \pi - b = \frac{a + b - c}{2} = s - c,$$

* The excess has also been obtained, by means of the modern analysis, by Euler in the Memoirs of the Royal Academy at Berlin, vol. ix. p. 256, and by Tedenat, in Gergonne's Annals of Mathematics, vol. vi. p. 48.

$$s, -c, = \frac{a-b-c}{3} + z - \overline{z-c} = \frac{a-b+c}{3} = s-k$$

Hence if E, E, E, denote the excesses of BA'C, AB'C, BC'A, we have by Lhuillier's theorem,

$$\tan \frac{E_{i}}{4} = \sqrt{\tan \frac{s_{i}}{2} \tan \frac{s_{i} - a_{i}}{2} \tan \frac{s_{i} - b_{i}}{2} \tan \frac{s_{i} - a_{i}}{2}},$$

that is:

$$\tan \frac{E_s}{4} = \sqrt{\cot \frac{s}{2} \cot \frac{s-a}{2} \tan \frac{s-b}{2} \tan \frac{s-c}{2}}$$

$$\tan \frac{E_{"}}{4} = \sqrt{\cot \frac{s}{2} \tan \frac{s-a}{2} \cot \frac{s-b}{2} \tan \frac{s-c}{2}}$$

$$\tan \frac{E_{"}}{4} = \sqrt{\cot \frac{s}{2} \tan \frac{s-a}{2} \tan \frac{s-b}{2} \cot \frac{s-c}{2}}$$

$$\tan \frac{E}{4} = \sqrt{\tan \frac{s}{2} \tan \frac{s-a}{2} \tan \frac{s-b}{2} \tan \frac{s-c}{2}}$$

in which Lhuillier's theorem is applied to each of the triangles in succession. If we multiply these together, we find
$$\tan \frac{E}{4} \tan \frac{E_{\prime\prime\prime}}{4} \tan \frac{E_{\prime\prime\prime}}{4} = \cot \frac{s}{2} \tan \frac{s-c}{2} \tan \frac{s-c}{2}$$
 (8).

Again, the angles of the triangle BA,C are $A_{r} = A_{r}, B_{r} = \pi - B_{r}, \text{ and } C_{r} = \pi - C_{r}.$

Hence similarly
$$\begin{cases}
\frac{E_{1}}{4} = \frac{\pi + A - B - C}{4} \\
\frac{E_{1/2}}{4} = \frac{\pi - A + B - C}{4} \\
\frac{E_{1/2}}{4} = \frac{\pi - A - B + C}{4} \\
\frac{E}{4} = \frac{\pi - A + B + C}{4}
\end{cases}$$
(3).

Also
$$\frac{\pi + A - B - C}{4} + \frac{\pi - A + B + C}{4} = \frac{\pi}{2}$$
, whence $\tan \frac{\pi - A + B + C}{4} = \cot \frac{E}{4} = \frac{\pi}{2}$

 $\frac{s}{s}$ tan. $\frac{s-a}{s}$ cot. $\frac{s-b}{s}$ cot. $\frac{s-c}{s}$; and by similar pro-

cesses with the other triangles, we get the following table;

$$\tan \frac{-A + B + C + \pi}{4} = \sqrt{\tan \frac{s}{2} \tan \frac{s - a}{2} \cot \frac{s - b}{2} \cot \frac{s - c}{2}}$$

$$\tan \frac{A - B + C + \pi}{4} = \sqrt{\tan \frac{s}{2} \cot \frac{s - a}{2} \tan \frac{s - b}{2} \cot \frac{s - c}{2}}$$

$$\tan \frac{A+B-C+\pi}{4} = \sqrt{\tan \frac{s}{2}\cot \frac{s-a}{2}\cot \frac{s-b}{2}\tan \frac{s-c}{2}}$$

$$\tan \frac{A+B+C-\pi}{4} = \tan \frac{s}{2} \tan \frac{s-a}{2} \tan \frac{s-b}{2} \tan \frac{s-c}{2}$$

The last of which is the common form of the area of a triangle given by Limitier, applied to the fundamental triangle.

Multiply all these together, and we shall have,

$$\tan^{A} \frac{a+b+c}{4} = \tan. \frac{A+B+C-\pi}{4} \tan. \frac{A+B-C+\pi}{4}$$

$$\tan. \frac{A-B+C+\pi}{4} \tan. \frac{-A+B+C+\pi}{4} \dots (5).$$

Also, giving to the terms of Lhuillier's theorem, their unabbreviated values, we shall see a striking analogy in their general form between that and the one just obtained. For in $\tan^2 \frac{A+B+C-\pi}{A}$

$$\tan \frac{a+b+c}{4} \tan \frac{a+b-c}{4} \tan \frac{a-b+c}{4} \tan \frac{-a+b+c}{4}$$
 (6).

we see the only difference, as to general form, is, that π enters into all the angular functions, and not into those of the sides. Again, since the three last factors in the right hand member of equation (5) are cot. $\frac{E_{ii'}}{4}$, cot. $\frac{E_{i'}}{4}$, and cot. $\frac{E_{i'}}{4}$; and the remaining factor is tan. $\frac{E}{4}$, we have (5) converted into

$$\tan^2 \frac{a+b+c}{4} = \tan \frac{E}{4} \cot \frac{E}{4} \cot \frac{E}{4} \cot \frac{E}{4} \cdots$$
 (7).

By the principle of the symmetry of the triangles, and of their expressions, we at once infer from (7) that

But
$$s_{r} = \frac{a + \overline{a - b} + \overline{a - c}}{2} = \pi - \frac{a + b + c}{2}$$

$$\therefore \tan \frac{s_{r}}{2} = \cot \frac{s - a + b + c}{2} = \cot \frac{s - a}{2}.$$

Applying the same principle of reduction to the other supplemental triangles, and collecting the results, we have

$$\tan^{\frac{3}{2}} = \tan \cdot \frac{E}{4} \cot \cdot \frac{E_{1}}{4} \cot \cdot \frac{E_{11}}{4} \cot \cdot \frac{E_{11}}{4}$$

$$\cot^{\frac{3}{2}} = \cot \cdot \frac{E}{4} \tan \cdot \frac{E_{1}}{4} \cot \cdot \frac{E_{11}}{4} \cot \cdot \frac{E_{111}}{4}$$

$$\cot^{\frac{3}{2}} = \cot \cdot \frac{E}{4} \cot \cdot \frac{E_{1}}{4} \cot \cdot \frac{E_{111}}{4} \cot \cdot \frac{E_{111}}{4}$$

$$\cot^{\frac{3}{2}} = \cot \cdot \frac{E}{4} \cot \cdot \frac{E_{11}}{4} \cot \cdot \frac{E_{111}}{4} \cot \cdot \frac{E_{111}}{4}$$

Let us resume equations (3), and multiply by (4) then we have

$$\begin{array}{l}
 A + B + C - \pi = E \\
 A - B - C + \pi = E, \\
 - A + B - C + \pi = E, \\
 - A - B + C + \pi = E, \\
 \end{array}$$
(9).

add them, then $E + E_{,+} + E_{,,+} + E_{,,,-} = 2 \pi$. (10). Add the first of these to each of the others successively, then

Inserting these values in the usual formula for finding a side, we get

nserting these values in the usual formula for finding a side, we get
$$\cot^2 \frac{1}{2} a = \frac{\sin \frac{E_{\prime\prime}}{2} \sin \frac{E_{\prime\prime\prime}}{2}}{\sin \frac{E}{2} \sin \frac{E_{\prime\prime}}{2}} \quad \cot^2 \frac{1}{2} b = \frac{\sin \frac{E_{\prime\prime}}{2} \sin \frac{E_{\prime\prime\prime}}{2}}{\sin \frac{E}{2} \sin \frac{E_{\prime\prime\prime}}{2}}$$
and
$$\cot^2 \frac{1}{2} c = \frac{\sin \frac{E_{\prime}}{2} \sin \frac{E_{\prime\prime\prime}}{2}}{\sin \frac{E}{2} \sin \frac{E_{\prime\prime\prime}}{2}},$$

$$= \frac{\sin \cdot \frac{E_{\prime}}{2}}{\sin \cdot \frac{E}{2}} \cdot \frac{\sin \cdot \frac{E_{\prime \prime}}{2}}{\sin \cdot \frac{E}{2}} \cdot \frac{\sin \cdot \frac{E_{\prime \prime \prime}}{2}}{\sin \cdot \frac{E}{2}} = \frac{\sin \cdot \frac{E_{\prime}}{2} \cdot \sin \cdot \frac{E_{\prime \prime}}{2} \sin \cdot \frac{E_{\prime \prime \prime}}{2}}{\sin \cdot \frac{E}{2}} \cdot \frac{\sin \cdot \frac{E_{\prime \prime}}{2} \sin \cdot \frac{E_{\prime \prime \prime}}{2}}{\sin \cdot \frac{E_{\prime \prime}}{2} + \frac{E_{\prime \prime \prime}}{2}} \right\} ... (15).$$

The sides and angles of the triangle are thus found, (the angles in 11,) in terms of the areas of the four triangles: and the equation of condition

also which subsists among these four triangles; and the equation of condition also which subsists among these four triangles is assigned in (10).

By (12) the values of the factors in N are found, and by (8) there is another trigonometrical function of the factors of n assigned. From this, those factors themselves may be assigned, but the process is troublesome and the result inelegant. We have obtained a simpler form, but even then neither the form nor the method is well suited to this place: The values of the inscribed and circumscribed radii is at the process with the dispensed in the Penselium and the process. terms of the excesses will be discussed in the Repository, and we shall conclude this section with assigning the connexion between the polar systems of associated triangles, in respect to the areas.

The sides of the primary fundamental triangle being a, b, c, we have

11

(a) and hence
$$\frac{\mathbf{E}'}{4}$$

$$\frac{b+c}{9} = \frac{r}{9} - \frac{a+b+c}{4}$$

Again, in the supplemental

In respect to A for instance,) we have

$$-b) + (\pi - \pi - c = \pi - a + b + c$$

$$-a + b + c$$

$$4$$

$$-a + b + c$$

$$2$$

the partiurming the same changes upon 28',,

and $\frac{E'_{m}}{4}$ and $\frac{E'_{m}}{4}$; the whole form of

$$\frac{\frac{E'}{4} = \cot \frac{1}{2}}{\frac{1}{4} = \tan \frac{5-4}{2}}$$

$$\tan \frac{E'_{H}}{\frac{4}{4}} = \tan \frac{4-b}{2}$$

$$\tan \frac{E'_{H}}{\frac{4}{4}} = \tan \frac{3-c}{2}$$

Char; then tan. $\frac{E'}{4}$ tan. $\frac{E'_{,,,}}{4}$ tan. $\frac{E'_{,,,}}{4}$ tan. $\frac{E'_{,,,,}}{4}$ tan. $\frac{E'_{,,,,,}}{4}$ tan. $\frac{s-c}{2}$. . . (16).

omparison of (2) and (16,) we find

$$\frac{E'_{'''}}{4}\tan \frac{E'_{''''}}{4} = \tan \frac{E}{4}\tan \frac{E}{4} \tan \frac{E_{''}}{4} \tan \frac{E_{'''}}{4} (17).$$

on of the component equations of table (16) with those shall get the value of the area of any triangle in terms of system which is polar to it. Thus,

$$\frac{E'}{4} = \tan \cdot \frac{E}{4} \cot \cdot \frac{E_{i'}}{4} \cot \cdot \frac{E_{i''}}{4} \cot \cdot \frac{E_{i''}}{4} = \cot \cdot \frac{E}{4} \tan \cdot \frac{E_{i'}}{4} \cot \cdot \frac{E_{i''}}{4} \cot \cdot \frac{E_{i''}}{4} = \cot \cdot \frac{E}{4} \cot \cdot \frac{E_{i''}}{4} \cot \cdot \frac{E_{i''}}{4} = \cot \cdot \frac{E}{4} \cot \cdot \frac{E_{i''}}{4} \cot \cdot \frac{E_{i''}}{4}$$
... (18)

recly, by interchanging the system of reference in the polar cented letters 8, 10, de, denote quantities in the polar triangles which are the primary by 1, 15, de.

triangles we have
$$\cot \frac{2}{4} = \tan \frac{E'}{4} \cot \frac{E'}{4} \cot \frac{E'_{,''}}{4} \cot \frac{E'_{,''}}{4} \cot \frac{E'_{,''}}{4}$$

$$\cot \frac{2}{4} = \cot \frac{E'_{,0}}{4} \tan \frac{E'}{4} \cot \frac{E'_{,,'}}{4} \cot \frac{E'_{,''}}{4} \cot \frac{E'_{,''}}$$

By multiplying either of these sets, we should also obtain the reciprocal of equa. (17). By means of (10) applied to both systems of associated triangles, we have E+E,+E,,+E,,+E',+E',+E',+E',+E',... $= 4\pi = \text{surface of the sphere} \dots (20).$

Taking the values of tan. $\frac{E}{4}$ tan. $\frac{E'}{4}$ &c. from (1) and (16), we get

$$\tan^{2}\frac{E}{4}\tan^{2}\frac{E'}{4} = \cot \frac{s}{2}\tan \frac{s-a}{2}\tan \frac{s-b}{2}\tan \frac{s-c}{2}$$

$$\tan^{2}\frac{E}{4}\tan^{2}\frac{E'}{4} = \cot \frac{s}{2}\tan \frac{s-a}{2}\tan \frac{s-b}{2}\tan \frac{s-c}{2}$$

$$\tan^{2}\frac{E'}{4}\tan^{2}\frac{E''}{4} = \cot \frac{s}{2}\tan \frac{s-a}{2}\tan \frac{s-b}{2}\tan \frac{s-c}{2}$$

$$\tan^{2}\frac{E''}{4}\tan^{2}\frac{E'''}{4} = \cot \frac{s}{2}\tan \frac{s-a}{2}\tan \frac{s-b}{2}\tan \frac{s-c}{2}$$

From the equality of the right sides of the last equations we find

$$\tan \frac{E}{4} \tan \frac{E'}{4} = \tan \frac{E'}{4} \tan \frac{E'}{4} = \tan \frac{E''}{4} \tan \frac{E''}{4}$$

$$= \tan \frac{E'''}{4} \tan \frac{E''''}{4} \dots (22).$$

When the geographical positions of the three angles of a spherical triangle are given to determine the area, we have the following expression, first given by the author of this Supplement, in the 12th volume of the Edinburgh Transactions, viz.

$$\cos \frac{E}{2} = \begin{cases}
1 + \cos a_{1} \cos a_{2} + \sin a_{1} \sin a_{2} \cos (\beta_{1} - \beta_{2}) \\
+ \cos a_{2} \cos a_{2} + \sin a_{2} \sin a_{2} \cos (\beta_{2} - \beta_{2}) \\
+ \cos a_{2} \cos a_{2} + \sin a_{2} \sin a_{2} \cos (\beta_{2} - \beta_{2}) \\
2(1 + \cos a_{2} \cos a_{2} + \sin a_{2} \sin a_{2} \cos \beta_{2} - \beta_{2}) \\
(1 + \cos a_{2} \cos a_{2} + \sin a_{2} \sin a_{2} \cos \beta_{2} - \beta_{2})
\end{cases}$$

where a_{ij}, β_{ij} ; a_{ij}, β_{ij} ; and a_{iji}, β_{ijj} , are the colatitudes and the longitudes of the vertices.

The spherical excess may also be very readily exhibited under another form by a direct investigation, but which, in my paper, in the Mathematical Repository now publishing, is obtained by inference from another property. Thus,

$$\frac{\tan \frac{\mathbf{E}}{2}}{\cos \frac{\mathbf{A}}{2}} = \frac{\sin \frac{\mathbf{A} + \mathbf{B} + \mathbf{C} - \mathbf{r}}{2}}{\cos \frac{\mathbf{A} + \mathbf{B} + \mathbf{C} - \mathbf{r}}{2}} = \frac{\cos \frac{\mathbf{A} + \mathbf{B} + \mathbf{C}}{2}}{\cos \frac{\mathbf{A} + \mathbf{B} + \mathbf{C}}{2}}$$

* by lest preceding equation (16)

Now, for these several functions of the angles, insert their values from (1, 2, page 49.) keeping in mind that for the $\frac{A}{8}$ cos. $\frac{C}{9}$ cos. $\frac{C}{9}$ + cos. $\frac{A}{9}$ sin. $\frac{B}{9}$ sin. $\frac{C}{9}$ + sin. $\frac{A}{9}$ cos. $\frac{B}{9}$ sin. $\frac{C}{9}$ sin. $\frac{B}{9}$ cos. $\frac{C}{9}$ - $\sin \frac{A}{3} \sin \frac{B}{3} \sin \frac{C}{3} + \sin \frac{A}{3} \cos \frac{B}{3} \cos \frac{C}{3} + \cos \frac{A}{3} \sin \frac{B}{3} \cos \frac{C}{3} + \cos \frac{A}{3} \sin \frac{C}{3}$ ğ

quantity there marked \$8 (half the sum), we have, in this supplement, written s; and, performing the same upon each of the saxes, we shall obtain $\frac{\cos c. s + \csc. (s - a) - \csc. (s - b) + \csc. (s - c)}{\sin. s + \sin. (s - a) - \sin. (s - b) + \sin. (s - b)} {\sin. (s - b) \sin. (s - b) \sin. (s - c)}$ $\frac{-\csc s + \csc (s-a) + \csc (s-b) + \csc (s-b)}{-\sin s + \sin (s-a) + \sin (s-b) + \sin (s-b)} \{\sin s \sin (s-a) \sin (s-b) \sin (s-c)\}$ $\frac{\csc s \cdot s + \csc (s - a) + \csc (s - b) + \csc (s - c)}{\sin s \cdot s + \sin (s - a) \sin (s - b) \sin (s - c)} \left\{ \sin s \sin (s - a) \sin (s - b) \sin (s - c) \right\}^{\frac{1}{2}}$ cosec. $s + \csc(s-a) + \csc(s-b) + \csc(s-c)$ sin. $(s-a)\sin(s-a)\sin(s-b)\sin(s-c)$ sin. $(s-a)\sin(s-b)\sin(s-c)$ cot. E... 1 0 m 원 | cs 턿 ğ

Again, if for s, s-a, s-b, s-c, we insert their values in terms of r, r,, r,..., from (5, p. 138,) we shall have the several areas of the associated triangles as functions of their inscribed radii.

$$\cot \frac{E}{3} = \frac{-\cot r + \cot r}{-\tan r} + \tan r, \frac{+}{+\tan r} + \frac{-\cot r}{r}, \frac{-\cot r}{+\tan r} + \tan r, \frac{-\cot r}{r} + \cot r, \frac{-\cot r}{r} +$$

We are also enabled, by means of the last set of equations, combined with (10), to ascertain the relation that subsists among the four radii, $\tau_{r_1}\tau_{r_2}\tau_{r_3}$ a relation which I believe has never before been assigned.

For we have
$$\frac{E + E_{,+} + E_{,,-}}{2} = 0 = \frac{\Sigma_{4}(t) - \Sigma_{4}(tt_{,-}t_{,-})^{\bullet}}{1 - \Sigma_{4}(tt_{,-}t_{,-})^{\bullet}}$$

$$\tan \frac{E+E_{,}+E_{,,,}+E_{,,,}}{2}=0=\frac{\sum_{i}(i)-\sum_{i}(i\,t_{,}\,t_{,,})^{\bullet}}{1-\sum_{i}(i\,t_{,})+\sum_{i}(i\,t_{,}\,t_{,,,})^{\bullet}}.$$

Now this may be fulfilled in two different ways, either making the denominator infinite, whilst the numerator is finite; or making the numerator zero, whilst the denominator is a real quantity, finite or infinite. It would exceed the confined limits of a work like the present to discuss the circumstances of this function, and I shall, therefore, assume (though I shall elsewhere prove it) that the only condition that obtains is the latter. We hence have $\Sigma_4(t) - \Sigma_4(t,t,n) = 0$; which may be written as follows:

(having previously divided it by tan. $\frac{E}{\Omega}$ tan. $\frac{E}{\Omega}$ tan. $\frac{E_{\parallel}}{\Omega}$ tan. $\frac{E_{\parallel}}{\Omega}$):

$$-\cot.\frac{E}{2} + \cot.\frac{E}{2} \cot.\frac{E}{2} \cot.\frac{E}{2} \cot.\frac{E}{2}$$

$$-\cot.\frac{E}{2} + \cot.\frac{E}{2} \cot.\frac{E}{2} \cot.\frac{E}{2}$$

$$-\cot.\frac{E''}{2} + \cot.\frac{E}{2} \cot.\frac{E}{2} \cot.\frac{E''}{2}$$

$$-\cot.\frac{E''}{2} + \cot.\frac{E}{2} \cot.\frac{E}{2} \cot.\frac{E'}{2}$$

$$-\cot.\frac{E'''}{2} + \cot.\frac{E}{2} \cot.\frac{E'}{2} \cot.\frac{E''}{2}$$

Insert for these cotangents their values, and reduce the expression to its simplest form. The work is somewhat laborious, but the result is comparatively simple; and hence I shall leave it as an exercise, for the student to perform alone. In another place I have given a different investigation of this formula, and several collateral topics are also combined with it, which will render it needless to enter into further detail upon this class of subjects, in the present necessarily very incomplete sketch. I trust, however, that enough is done to excite the interest of the mathematical student, whilst the extent of the subject itself will afford sufficient exercise for his ingenuity, and reward to his perse-

I am obliged to terminate these researches abruptly, on account of the space which they would occupy, if developed with any approach to completeness. I take the opportunity afforded me by reading the proofs, to state that my friend and neighbour, the Rev. Professor Logan, has also engaged in these and several collateral researches, and that the results to which both he and I may ultimately be found to have arrived, upon comparison of our MSS., will be published in a single dissertation to be considered as our joint production. These researches will extend to every other function of parts of the spherical triangle, as well as those which have been in this supplement discussed; and to a considerable extension of each of these. It will then be seen that Spherical Geometry offers one of the most ample fields of research that

[•] It is left for the student to prove, from the expression for the tanof the sum of two arcs, at p. 33, that the expression for the tan. of four arcs is that in the text, in which E (t) denotes the sum of the tangents of those arcs $E(u_i)$, the sum of their products taken two and two, and so on. The same may be generalized for any number of arcs.

has yet been discovered; and I hope I shall not be thought too sanguine in anticipating that the properties of figures, traced upon the surface of the sphere, will, in a very few years, become as familiar to English Geometers as the correlative figures in plane now are.*

Not only have Spherical Geometry and Spherical Trigonometry been greatly neglected in England, but also upon the Continent. The continental Geometers have, however, been truly assiduous in the cultivation of the Geometry of three divisions, and have imagined and discussed almost every variety of method for conducting their investigations in this branch of science: whilst, on the other hand, it will be difficult to point to any one British Geometer who ever added a single important theorem to our stock, much less devised a single original method of investigation. Of the causes of this humiliating fact, the present is not the place to speak. It may, however, be allowed me to mention what appears to be a barrier to our removing the discreditable charge. We have no work, expressly devoted to the subject, in which either the methods themselves are developed, or the spirit of them at all displayed. Mere illustrations, taken in a considerable degree at random from different works, in which they were originally very appropriately placed, when brought together without due regard to the principles themselves, and often without adapting the notation to any uniform standard—works like these, though they may be entitled treatises on the Geometry of Three Dimensions, can scarcely be called so without a complete perversion of the use of terms. He that renders a method of investigation intolligible, with whateve paucity of mere illustration, does more for the interests of science than he who collects all the illustrative examples of those methods that have ever been given into one single mass. Such cellections are, indeed, too commonly calculated to confuse the young mind and to repress all the ardour it might otherwise have felt.

Long ago, impressed with the importance of the subject, the author of this supplement formed the ambitious project of supplying this desideratum, and of furnishing a wear in which the spirit of the methods which have been employed by the continental Geometers should be the first object of his anxiet

branch of science in England.

He has been, however, led to think that a subsidiary elementary work on Descriptive
Geometry would not be unacceptable to British Geometers, before the other goes to press.

Even on this, the simplest of all the forms under which the Geometry of these dimensions presents itself, a merely graphic form—we have no treatise in England, nor yet a single chapter in any English course of Mathematics. There was indeed published it America, in 1821, a thin octavo, by M. Crozet, for the use of the Military College of the United States; but it would be scarcely less difficult to devise the methods originally than to acquire them from that treatise. Such a volume will therefore be sent to press with all convenient speed, the avant courier of the larger work.

NOTES.

NOTE A. p. 126.

THE following pretty theorems I have received from Mr. Lowry, since the first chapter on Spherical Geometry was in forms.

"Let ABC be a spherical triangle, D the middle of one of the sides, AC; and let AB = d. Then $\cos a + \cos c = 2 \cos \frac{1}{2} b \cos d$.

For
$$\frac{\cos a - \cos \frac{1}{b} \cos d}{\sin \frac{1}{b} \sin d} = \cos BDC$$

$$\frac{\cos c - \cos \frac{1}{b} b \cos d}{\sin \frac{1}{b} \sin d} = \cos BDA = -\cos BDC$$

Hence cos. $a \cos b \cos d = -\cos c + \cos b \cos d$, $\cos a + \cos c = 2 \cos b \cos d$.

Cor. 1. When the triangle is inscribed in a semi-circle, the diameter of which is b, $\cos a + \cos c = 2 \cos^2 b$, or $\cos a + \cos c = 1 +$

Cor. 2. And when a = c, we have $\cos a = \cos^2 -$

Cor. 3. Hence, in a spherical square, the cosine of the sides is equal to the square of the cosine of half the diagonal.

Cor. 4. The sine of half the area of the triangle ACB in the circle is $= \tan \frac{a}{2} \tan \frac{c}{2}.$ Vide form 20, Math. Repos. v. part 1. p. 7.

Cor. 5. Hence in a spherical rectangle, the sine of one fourth of the area is equal to the rectangle of the semi-tangents of the two sides, that is = tan. $\frac{a}{2}$ tan. $\frac{b}{2}$.

Cor. 6. And in the spherical square, the sine of $\frac{1}{2}$ area = tan.

Cor. 7. In a spherical parallelogram, I the sides of which are a, b, c, d and diagonals h, h', we shall have .

$$\cos a + \cos b + \cos c + \cos d = 4 \cos \frac{k}{2} \cos \frac{k'}{2}.$$

These properties are very simple, but neat, and might serve as exercises in an elementary treatise."

NOTE B. p. 133,

To account for some seeming discrepances, between the notes and text of this supplement, it is necessary to state that the text was drawn up in its present form from my manuscript, and the demonstration remodelled, (in many cases invented), to adapt it to the disolated state of the portions here given, during brief intervals stolen from other

* The figure may be easily sketched by the student.

† A spherical four sided figure, whose sides are all equal, and whose angles are also all equal.

‡ A our sided spherical figure, or whose angles are equal; or, perhaps, better adapted to the term, we may call it the figure in which great circles bisecting the pairs of opposite sides intersect each other at right angles.

T A figure whose opposite sides are equal.

These terms are adopted by analogy from Plane Geometry. Perhaps it may be found desirable ere long to modify our terminology considerably: but it does not appear to be the time. Perhaps it may be MOTES.

pursuits and occupations, having but little alliance with these subjects. The notes were added afterwards, in a letter to Mr. Young, and distributed by him so as not to interfere (where the interference would occasion much change in the text already partly in slips and partly in forms,) with the part already in the compositor's hands. Where addition could be worked into the text, and appeared more adapted to incorporation, it has been done; and where it did not coalesce with the text conveniently it has been put into foot notes. Some cases have, however, occurred where the addendum could not be properly made by either method, and it has therefore been altogether omitted. Still as these omissions are rather of a historical than a mathematical nature, no inconvenience can result from them, except the possibly erroneous distribution of the names of discoverers of particular theo-Should this be ultimately found to be the case, I trust the authors to whom they are erroneonsly attributed, as well as the authors to whom they are actually due, will excuse the undesigned mistake.

There is, however, one particular case to which I wish more especially to refer, since I had till just now considered a theorem upon which I set some value, (and which, indeed, was the origin of my researches upon these topics), to be original, when, in fact, it had been discovered more than a quarter of a century ago, by Professor Lowry. I have just received a note from that distinguished Geometer, containing, amongst other matters, a reference to the Mathematical Repo-

sitory, N.S. vol. 1. p. 157.

Upon turning to this volume I and an anticipation of this beautiful property of the polar triangles: but as my copy of the Repository had been lent to a friend during the whole of the time I had the subject before my mind, my own discovery was perfectly independent of his, though so long posterior to it. I am quite sure, indeed, that I had never read that passage, or so beautiful a property must have been inevitably laid up amongst my collections. I am happy, however, to be able to render back to Professor Lowry the credit of the priority or discovery in the same volume in which I had seemed to claim not only independence but priority.

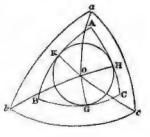
His demonstration (as was to be expected when the methods of spherical research in general at the two periods are compared) differs totally from mine; but his, as the geometrical often will have over the analytical, even when the latter is cultivated to its utmost perfection, has advantages over mine, which render it desirable to give it here. It is simple, and it proves more than mine proves, or perhaps can prove in moderate compass, viz. that the centres of the two circles, whose radii are complimentary, coalesce with one another. I will add, that to him alone we owe every important spherical theorem that can be set down to the credit of Englishmen during at least a century past, pro-

bably even longer.

Find the centre O of the inscribed circle in ABC, and from the points of contact G,H,K, draw the radii OG, OH, OK. Then these being perpendicular to the sides BC, CA, AB, respectively pass through the poles a, b, c, of those sides. Hence by polar triangles,

$$\mathbf{z}$$
OG = b OH = ϵ OK. = $\frac{\pi}{2}$. But

OG = OH = OK, and, therefore, Oa = Ob = Oc, or O is also the centre of b the circle about the polar triangle abc: that is, the centres of the primary in-



scribed, and the polar circumscribed circles are coincident. In the same manner the centres if polar inscribed and primary circumscribed are coincident. And it has been shown that these radii are complementary.

I may remark that the expression for the distance of the inscribed and circumscribed centres, in terms of the radii themselves, has not yet been given. In plane that distance was so assigned by Mr. Landes, and has been very elegantly investigated by Mr. Lovery, in the Mathematical Repository. The corresponding problem has been several times attempted, but other parts of the triangle have appeared in every result that has yet been published. The neatest form that I have seen is given anonymously in the Annales des Malamatiques, tom. vi. p. 223. viz.

cos. D =
$$\frac{\sin a + \sin b + \sin c}{\sqrt{\sin s \sin s - a \sin s - b \sin s - c}} \cdot \sin r \cos R.$$

THE END.

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MATHEMATICAL TABLES;

COMPREHENDING

THE LOGARITHMS OF ALL NUMBERS

FROM 1 TO 36,000;

ALSO

THE NATURAL AND LOGARITHMIC SINES AND TANGENTS:

COMPUTED TO SEVEN PLACES OF DECIMALS, AND ARRANGED ON AN IMPROVED PLAN;

WITH

SEVERAL OTHER TABLES,

UNEFUL IN

NAVIGATION AND NAUTICAL ASTRONOMY,

AND IN

OTHER DEPARTMENTS OF PRACTICAL MATHEMATICS

BY J. R. YOUNG,

. AUTHOR OF "ELEMENTS OF TRIGONOMETRY," &C.

REVISED AND CORRECTED BY

J. D. WILLIAMS,

AUTHOR OF "KEY TO HUTTON'S MATHEMATICS," &G.

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PREFACE TO THE TABLES.

THE following Tables are designed as well for the practical man as for the mathematical student. They comprehend, in a portable and cheap form, the principal information sought for in larger and more expensive collections.

The more important of these tables, viz. those immediately connected with trigonometrical and astronomical calculations, differ considerably both in form and arrangement from those in general use; and it is hoped that this departure from the usual plan, which has not been hastily made, will tend to increase the facility of reference.

In the table of the Logarithms of Numbers a new device has been adopted to mark the change of figure, and the several columns are so printed that, in seeking for the number corresponding to any proposed logarithm, the leading figures of the given logarithm may readily present them selves to the eye. Instead of omitting the several leading figures common to a number of successive logarithms, as is generally done, it has been recommended to preserve all the common figures, as at page 2 of these tables. This plan might perhaps facilitate, in a small measure, the writing out of a logarithm corresponding to a given number, but it would certainly render the detection of any given logarithm from among such a dense mass of figures much less easy.

In the table of logarithmic sines and tangents, the trigonometrical lines are inserted to every second, for the two first and two last degrees of the quadrant, and the old arrangement is followed; that is, the sines, cosines, &c. of the small arcs proceed in order from the top of the page to the bottom; and those of the large arcs, complements of the former, proceed in the reverse order, from the bottom to the top. The bulk of the table, however, is arranged differently;

1*

the sines and tangents proceeding onwards to the end, and the cosines and cotangents in the reverse direction. This is the arrangement recommended by Professor Airy, in his Trigonometry, but it was not originally my intention to adopt it. Its advantages, however, having been more clearly pointed out to me by some scientific friends, occupied in computing the Nautical Almanack, and in the continual use of trigonometrical tables, I have been induced to depart from my first design, and to adopt the improved form. I regret that I had not come to this determination earlier, before the table for the two first degrees had been printed.

The table of natural sines and tangents is arranged upon the same plan as the former. The remaining tables of the volume require no particular observations here: a more minute detail of particulars will be found in the introduc-

tory explanation prefixed.

As accuracy in mathematical tables is of far more consequence than arrangement, it may be proper to state here that the present collection have all undergone very careful and repeated examination. The proofs of the tables of numbers, and of sines and tangents, were each compared twice with the tables of Bagay, Hutton, and Babbage, and in some cases with those of Taylor also; and the impressions from the stereotyped plates were again all compared with Hutton and Babbage. Many errors in Bagay's Tables of numbers were thus detected, and one or two in the last edition of Hutton; in Mr. Babbage's table I could find no error, and I have no doubt they amply deserve the reputation for accuracy which they have obtained.

J. R. YOUNG.

Jan. 1, 1833.

EXPLANATION OF THE TABLES.

THE principal tables in this collection are the three following, 1st, a Table of the Common Logarithms of Numbers; 2d, a Table of the Logarithms of the Trigonometrical lines to radius 1010; and 3d, a Table of the natural nu-

merical values of the same lines to radius unity.

The explanation which we here propose to give of these tables must be understood to concern not the methods of computing them, but simply the manner of using them. The various methods of constructing a table of logarithms we have already discussed in a separate tract,* which will shortly be followed by a similar tract on the formation of a table of sines and tangents; our object here, therefore, will be to explain the use of tables already constructed.

TABLE I.

Of the Table of the Logarithms of Numbers.

The base of the system of Common Logarithms is 10; that is, every positive number is considered as some power, either whole or fractional, positive or negative, of the number 10, and it is the exponent of this power which is called the logarithm of the proposed number. If, therefore, we inquire what is the logarithm of any number, 60 for instance, we mean to ask what value the exponent x must have in order that 10° may be equal to 60; the proper value, as far at least as seven places of decimals, is 1.7781513; that is to say $10^{17781518} = 60$. The method of ascertaining the proper value of x, for any proposed number, is fully explained in our tract on logarithms above mentioned, but when the proposed number is any whole power of 10, whether positive or negative, it will be immediately seen to be such by mere inspection, and its logarithm will then be readily discovered. For example, the numbers.

1, 10, 100, 1000, 10000, &c.

[•] An Elementary Essay on the Computation of Logarithms.

are at once seen to be positive powers of 10, which powers are 10°, 10¹, 10², 10³, 10⁴, &c.

and the numbers

·1, ·01, ·001, ·0001, &c.

are as readily seen to be the following negative powers of 10, vis. 10^{-1} , 10^{-2} , 10^{-4} , 10^{-4} , &c.

Hence, of the series of numbers

 \dots , 10000, 1000, 100, 10, 1, ·1, ·01, ·001, ·0001, the logs. are

 \ldots , 4, 3, 2, 1, 0, -1, -2, -3, -4, \ldots

All this is very obvious; and it is further obvious that a number between any two terms of the first of these series will have its logarithm between the two corresponding terms of the second series. Thus the logarithm of a number between 10 and 100 will lie between 1 and 2; in other words, the *integral part* of the logarithm of any number, consisting of but two integral places of figures, however many decimals may follow, will always be 1.

In like manner, the logarithm of a number between 100 and 1000 will be between 2 and 3, of a number between 1000 and 10000 the logarithm will be between 3 and 4, and so on; that is, when the proposed number has three places of integers the integral part of its logarithm will be 2, when the number has four places of integers the integral part of its logarithm will be 4, and generally when the number has n places of integers, the integral part of its logarithm will be n-1; and this expresses the number of places which the highest denomination, or first figure in the proposed number, is from the unit's place. Thus if 24785.37 be the number proposed, then, seeing that its first figure 2 is four places from the unit's place, we know that its log. is 4 + a decimal. Upon the same principles the logarithm of any number between 1 and 1 is between — 1 and 0; that is, it is — 1+a decimal, the logarithm of any number between ·01 and ·1 is -2 + a decimal, and generally the logarithm of any number whose first significant figure is in the nth place of decimals is -n, and this expresses the number of places which the first significant figure in the proposed number is from the unit's place. Thus if 00000736 be the number proposed, we know that as the first significant figure 7 is six places from the unit's place, its logarithm must be - 6 + a

decimal. Seeing, therefore, that the integral part of a logarithm is so easily found from the proposed number, it is thought sufficient to insert in the table only the decimal part; accordingly, all the logarithms in a table of common logarithms must be understood to be decimals, although the decimal points may not appear.*

A valuable peculiarity of the common system of logarithms or that whose base is 10, is this, viz. that the logarithms of all numbers consisting of the same significant figures differ only in their characteristics. For example,

the log. of 16843 is		4.2264194
1684:3		3.2264194
168.43 .		2.2264194
16.843 .		1.2264194
1.6843 .		0.2264194
·16843		1.2264194
.016843		2.2264194
•0016843		3.2264194
	80.0	Arc.

That such must really be the case is very plain, for as

$$10^{42284194} = 16843 \therefore 10^{32284194} = \frac{16843}{10} = 1684\cdot3,$$

$$10^{92284194} = \frac{1684\cdot3}{10} = 168\cdot43, &c.$$

We may remark too, as a particular case of this property of the present system of logarithms, that the decimal part of the logarithm of a number consisting of any number of significant figures, either followed, or preceded, by ciphers, is always the same as if the ciphers were absent. Thus the decimal part of the logarithm of 358000 or of 00358 or of 3580, &c. is the same as the decimal part of the logarithm of 358, so that, in seeking for the decimal part of the logarithm of a proposed number in the table, we are to disregard the ciphers with which it may commence or terminate.

Having stated these preliminary notions, we shall now enter more particularly into the manner of using the table of logarithms following.

[•] In some few tables, however, the characteristics or integral parst of the logarithms are inserted, as well as the decimal parts.

PROBLEM I.

To find the logarithm of any number from 1 to 36000. If the proposed number either begin or end with ciphers these, as remarked above, are to be disregarded. The first significant figure to the right is to be considered as occupying the place of units, the preceding figures therefore will express so many tens. We must look for these leading figures in the column of tens in the table, and the horizontal row of logarithms against them will be that in which the sought logarithm occurs; it will be found under that figure, printed in the Egyptian character, which agrees with the figure in the unit's place of the proposed number. This being premised, we shall proceed at once to a few examples which will much better show the manner of using the table than any written direction.

EXAMPLE I.

Required the logarithm of 3265.

The leading figures 326 of this number I find in the column marked tens, at page 7; and carrying my eye along the horizontal row of logarithms, thus pointed out, I find in the vertical column headed 5 the logarithm sought, which (when the integral part 3 is supplied) is 3.5138832; for the 38832 is considered to be preceded by the 51 a little above it.

EXAMPLE II.

Required the logarithm of 3266.

The proper horizontal row of logarithms being found as before, I find that which is under the 6 to be 40162, which number is however considered to be preceded by the same figures as the number adjacent to it, or immediately before it, that is, by 51; hence supplying the index, or integral part, the required logarithm is 3:5140162.

EXAMPLE III.

Required the logarithm of 3236.

Having found the horizontal row which contains the logarithm, by means of the 323 in the tens column, I find the part under the 6 to be 00085 which I should proceed to

complete by prefixing, as in last example, the 50 belonging to the number immediately before it, were it not that the crooked mark f directs me to the 51 below, so that, supplying the index, the required logarithm is 3.5100085.

EXAMPLE IV.

Required the logarithm of 4680000.

Disregarding the terminating ciphers, I seek first for 46 in the *tens* column, and I find it in page 2 of the table; and in the same horizontal line with it, and under the s, I find the decimal 6702459; hence, supplying the index, the required logarithm is 6.6702459.

EXAMPLE V.

Required the logarithm of .002138.

Disregarding the ciphers, I seek first for 213 in the column of tens page 5, against which, and under the 8, I find the decimal 3300077; hence, prefixing the index, the required logarithm is 3.3300077.

PROBLEM II.

To determine the logarithm of a number beyond the limits of the table.

When the number proposed is beyond the limits of the table, that is, when it exceeds 30600. Enter the table with only the first five figures of the number, or indeed, with only the first four figures, should the five exceed the limits of the table, and find the corresponding logarithm. From the column marked dif. take out the number opposite to this logarithm, and multiply it by the remaining figures of the proposed number, reject from the product as many figures to the right as there are in the multiplier, and add the rest of the product to the logarithm already found: the sum will be the logarithm sought.

EXAMPLE I.

Required the logarithm of 843742.

I first seek the logarithm of 8437, the four first figures, the five first being beyond the limits of the table; this logarithm I find at page 16 to be, without the index, 9261880,

and opposite to it in the column dif. is 515; this multiplied by 42, the remaining figures of the proposed number, produces 21630, from which product the two right-hand figures 30 being rejected, there remains 216 to be added to 9261880, which gives 9262096 for the decimal part of the required logarithm; therefore, prefixing the index 5, the complete logarithm is 5.9262096.

EXAMPLE II.

Required the logarithm	of 1326927.	
Log. 132690	. 5·1228382 88	dif. 3277 27
Log. 1326927	. 5.1228470	2289 654
		88,29
EXAM	IPLE III.	
Required the logarithm	of 114·1285.	
	. 2·0573618 324	dif. 381 85
Log. 114·1285	. 2.0573942	1905 3048
		323.85.

It must be observed that as the column of differences does not commence till page 7 of the table, the preceding pages are never to be consulted for the logarithm of a number beyond the limits of the table.

PROBLEM III.

A logarithm being given, to find the corresponding number.

In this problem, too, as in the last, reference will be made to those pages only which contain the dif. column; among these we are to seek for the decimal part of the proposed logarithm, and we shall readily be guided to it, or else to a logarithm very near it, by means of the leading figures, which are separated in the table from the others, to attract the eye. If we find a logarithm exactly agreeing with that given, then the number, which the table shows us to

belong to the logarithm found, will be the required number. If, however, as is most likely, we do not find the proposed logarithm exactly, then we are to take out the number cor responding to the next less logarithm; this number will of course fall short of that required, but the deficiency may be supplied as follows. Divide the difference between the tabular logarithm and the given one by that number in the dif. column which is opposite to the tabular logarithm, and add the quotient to the number already taken from the table.

EXAMPLE I.

Required the number v	whose logarithm is	s 1·2335678.
Given lo	ogarithm .	. 2335678
Given le The next less in the tab	le is log. 17122	. 2335545
Add .	. 52 tab. dif	. 254)133·00 (·52
Required number .	17.12252	1270
		600
		508
		92

EXAMPLE II.

Required the number whose logarithm	n is 3·1241987.
Given logarithm	1241987
Next less log. 13309, .	. 1241454
163 Tab. dif.	326) 533·00 (1·63 326
Required number 1331·063	320
	2070
	1956
	1140

These examples will, no doubt, be found sufficient to examplify the manner of referring to the table when we are in search of a logarithm answering to a given number, or of a number answering to a given logarithm. We shall now give an example or two of the use of the table in facilitating arithmetical operations.

PROBLEM IV.

To multiply numbers together.

Add together the logarithms of the numbers, and the sum will be the logarithm of their product.

EXAMPLE L

Required the product of 26784	and	7.865.
log. 26784 .		4.4278754
log. 7.865 .	• `	·8956987
log. 210656·1 .	•	5.3235741.

EXAMPLE II.

Required the product of	3.	58	6, 2	1046	, ·8372, and ·0294
log. 3.586			•		.5546103
2.1046			•		.3231696
.8372				•	$\overline{1}$ -9228292
.0294	•				2 ·4683473
Product -1857618					1.2689564

PROBLEM V.

To divide one number by another.

Subtract the logarithm of the divisor from that of the dividend, and the remainder will be the logarithm of the quotient.

EXAMPLE I.

log. 28·654 127·34	1·4571853 2·1049648
Quotient ·2250197	<u>1</u> ·3522205.
EXAMPLE II.	
Divide ·06314 by ·007241.	
log. 06314	2.8003046
Quotient 007241	3.8597985
8.71979.	·9405061.

Divide 28:654 by 127:34.

PROBLEM VI.

To find the nth power of a given number.

The logarithm of the nth power will be equal to n times the logarithm of the given number.

EXAMPLE I.

Required the fourth power of .09163.

log. ·09163 . . 2·9620377

Power ·0000704938 . . . 5·8481508.

EXAMPLE II.

Required the tenth power of .64.

Power ·011529225

2·0618000

PROBLEM VII.

To find the nth root of a given number.

The logarithm of the nth root will be equal to the nth part of the logarithm of the given number.

EXAMPLE I.

Required the fourth root of .434296.

log. ·434296 . 1·6377858

 $\frac{1}{2}$ of it . . . $\frac{1}{2}$. $\frac{1}{2$

As the negative index $\overline{1}$, of the given logarithm, is not divisible by 4, it is increased by 3 to make it so, and the 3, thus borrowed. is afterwards restored, by being prefixed to the 6, making it 3.6; that is, the proposed logarithm is viewed under the form $\overline{4} + 3.6377858$, to which it is obviously equivalent.

EXAMPLE II.

Required the tenth root of 2.

EXAMPLE III.

Required the cube root of .00048.

log. ·00048 . 4·6812412

The negative index 4 not being divisible by 3, it is increased by 2 to make it so, and then the borrowed 2 restored by considering the positive part to commence with 26 instead of 6.

TABLE II.

Of the Table of Logarithmic Sines, Tangents, &c.

This second table consists of two parts: the first part containing the logarithmic sines, cosines, &c. of the first two and of the last two degrees of the quadrant, computed to every single second; and the other part of the table, containing the trigonometrical lines of the intermediate part of

the quadrant, for every minute only.

The first part of the table, or that computed to seconds, is arranged in the usual manner; that is, the sines, cosines, tangents, and cotangents of the small arcs proceed from the top of the page to the bottom, according to the magnitude of the arcs, of which the degrees and minutes stand at the head of the columns, and the seconds occupy the lefthand column of every page. The sines, cosines, &c. of the large arcs, or those which are near 90°, and are the complements of the former, proceed, on the contrary, from the bottom of the page to the top, according to the magnitude of the arcs, of which the degrees and minutes stand at the bottom, and the seconds occupy the right-hand column of every page. In entering this part of the table, therefore, with a small arc, the eye must be directed to the top of the page, but on entering it with a large arc we must look to the bottom of the page.

The arrangement of the remaining part of the table is different from that usually adopted; for here the sines and tangents all proceed regularly, in the order of their magnitudes, from the top to the bottom of the page; while the cosines

and cotangents all proceed in the contrary order, that is, from the bottom of the page to the top. This arrangement has considerable advantages over that of other trigonometrical tables, of which we may mention the following as in-Suppose we enter this table with an arc containing seconds, as well as degrees and minutes, then if we seek its sine or tangent, that is, if we proceed down the table, the proportional difference, due to the seconds, will always be, additive; but if we want the cosine or tangent, that is, if we proceed up the table, then, on the contrary, the proportional difference will always be *subtractive*. Again, suppose that we enter the table with a logarithmic line, in search of the corresponding arc. We may first find the nearest tabular value less than the proposed, note the corresponding degrees and minutes, and then proportion for the seconds, which will always be additive if we proceed down the table, that is, if the given line be a sign or tangent, and always subtractive if we proceed up the table, that is, if the given line be a cosine or cotangent; of course the contrary will have place if we transcribe the nearest greater instead of the nearest less tabular value. But perhaps the principal advantage of the present arrangement is this, viz. that every opening of the table presents us with a greater number of consecutive sines, cosines, &c. than it could do under any other arrangement; and this peculiarity will always facilitate those operations which involve the sines, or the cosines, &c. of several neighbouring arcs, (as in the bunar problem, for instance, where the true and apparent attitudes of the bodies differ but little from each other.) The arc also, corresponding to any given logarithmic line, will be more readily found than under the old arrangement.

We must remark here, that the secants and cosecants of arcs have not been inserted, because they may be immediately supplied from the cosine and sines. For, since

$$\cos$$
: rad.:: rad.: sec.
 \therefore sec. = $\frac{\text{rad.}^2}{\cos}$ \therefore log. sec. = 20 — log. cos.

and thus the log. secant of an arc is got by subtracting its log. consine from 20; and the log. consecant, by subtracting its log. sine from 20.

Having spoken of the arrange-

ment of this table, we shall now more particularly describe the manner of referring to it.

PROBLEM I.

To find the log. sine, &c. of a very small or of a very large arc, expressed in degrees, minutes, and seconds.

By a very small arc we mean one not exceeding two degrees; and to find its log. sine, we first search among the left-hand pages of the early part of the table, for that which presents the proposed degrees and minutes at the top; having found this, we shall have the vertical column in which the sine is; we must then pass the eye down the left-hand column, till we come to the number of seconds, then, in the same horizontal line with this number, and, in the vertical column before found, we shall find the sine required.

The tangent and cotangent are found in a similar man-

ner among the right-hand pages.

The same pages which contain the sines, cosines, &c. of arcs below 2°, contain also those of arcs above 88°. When such a large arc is given, we must seek for that page which presents the degrees and minutes of it at bottom, and we shall thus find the column in which the sought trigonometrical line is; the corresponding seconds column will be seen on the right of the page; we must pass the eye up this till we reach the given number of seconds, opposite to which, in the vertical column already found, we shall see the sought number.

To find the log. sine, log. cosine, &c. of an arc consisting of degrees and minutes only, and between 2° and 88°

Within these limits the trigonometrical lines are given for every minute only; but columns of differences are annexed, by means of which the proper correction for seconds

may be easily found.

In this part of the table the sines and tangents proceed throughout from the top to the bottom of the page; the cosines and cotangents from the bottom to the top. If we enter the table with degrees and minutes, and seek for a sine, we look for the given degrees at the top of one of the left-hand pages; if for a tangent, we look for the degrees a

the top of one of the right-hand pages: the minutes are to be found in the left-hand marginal column of the page: the number sought will be under the degrees at top, and in the same horizontal row as the minutes. But if we seek for a cosine or a cotangent, we look for the degrees at the bottom of the page instead of at the top, and for the minutes in the right-hand marginal column instead of in the left.

To find the log. sine, &c. when the arc consists of degrees, minutes, and seconds.

In this case we enter the table with the degrees and minutes as before, and take out the corresponding number: between this number and that which belongs to the succeeding minute we shall find, in the adjacent column, the proper difference. Multiply this difference by the number of seconds, divide the product by 60, and we shall have the correction to be applied to the tabular number: this correction will be additive if we proceed down the table, or seek for a sine or tangent, but it will be subtractive if we proceed up, or look for a cosine or cotangent. We shall give an example or two of this operation.

EXAMPLE I.

Required the log. sine of 35° 27' 24".

log. sin. 35° 27' = 9.7634222 + correction for <math>24'' = 7096 log. sin. 35° 27' 24'' = 9.7634932

EXAMPLE II.

Required the log. cosine of 48° 35′ 27".

The log. cosine of 48° 35' we find, at page 128, to be 9.8205496, therefore.

EXPLANATION OF THE TABLES.

X

log. cos. 48° 35′ =
$$9.8205496$$
 Dif. = $\frac{1433}{27}$ = $\frac{645}{9.8204851}$ = $\frac{10031}{2866}$ = $\frac{645}{645}$ = Cor.

EXAMPLE III.

EXAMPLE IV.

Required the log. cotangent of 41° 0′ 29″.

log. cot. 41° 0′ = 10.0608369 Dif. = 2551— correction for 29'' = 1233log. cot. 41° 0′ 29″ = 10.0607136 29 22959 5102 6,0)7397,9

EXAMPLE V.

1233 - Cor.

Required the log. secant of 13° 24′ 23′. log. sec.13°24′(=20 — log. cos.)=10·0119872. Dif.=301 + correction for 23″ = $\frac{110}{603}$ log. sec. 13° 24′ 23″ = $\frac{10}{10\cdot0119982}$ $\frac{23}{602}$ 6,0) $\frac{662}{662}$ 3 $\frac{110}{602}$

EXAMPLE VI.

Required the log. cosecant of
$$34^{\circ}$$
 52′ 43″.

log. cosec. 34° 52′ (= 20 — log. sin.) = 10° 2428556....Dif. = 1813 — correction for $43''$ = 1239 — 43

log. cosec. 34° 52′ 43″ = 10° 2427257 — 5436 — 7248

6,0)7791,6

1298 6 = Cor.

To find the arc corresponding to a given log. sine or log. tangent, &c.

Search in the table for that log. sine, or log. tangent, which is nearest to the proposed, but less than it, and take out the corresponding degrees and minutes. Find also the difference between this tabular number and the proposed, multiply it by 60 and divide by the tabular difference, the quotient will give the proper number of seconds.

EXAMPLE I.

Required the arc whose log. sine is 9.7634932.

To find the arc corresponding to a given log. cosine or log. cotangent.

Proceed, as in last problem, with this exception only, that instead of taking from the table the number next less, take the next greater; or if we take the next less, we must subtract the correction, not add it.

EXAMPLE.

Required the arc whose log. cosine is 9 8204851.

Given log. cosine . 9 8204851
log. cos. 28° 35′ . 9 8205496

27"

Req. arc = 28° 35′ 27"

60

1433)38700(27

2866

10040
10031

TABLE III.

Natural Sines, Tangents, &c.

This table is used like the former, but as the columns of differences are not inserted, when the difference between any two contiguous tabular numbers is required, for the purpose of correcting for seconds, this difference must be found by actual subtraction.

TABLE IV.

Traverse Table to every Quarter point of the Compass.

This table is useful in Navigation, showing, by inspection, the difference of latitude and departure due to any proposed course and distance. If the distance sailed be more than 120 miles it will exceed the limits of the table; but the difference of latitude and departure may still be determined from it by this simple operation: divide the given distance by any number that will give a quotient not exceeding 120; enter the table with this quotient, and multiply the corresponding dif. of lat. and dep. by the assumed divisor, and there will result the dif. of lat. and dep. due to the proposed distance.

The construction of the traverse table is obvious; the given distance and course being always the hypotenuse and adjacent angle from which the dif. of lat. and dep. tabulated

are computed.

TABLE V.

Workman's Table for correcting the Middle Latitude.

This table is useful for correcting what in Navigation is called the *middle latitude*. It is usual, in middle latitude sailing, to consider the departure which a ship makes in sailing upon an oblique rhomb from one parallel of latitude to another, to be equal to the distance between the meridians left and come to, measured on the middle parallel (see Trig. p. 74-5); but, as this is not strictly accurate, a correction becomes necessary. This correction is furnished by the present table; the given middle latitude is to be found in the first column to the left; in a horizontal line with which, and under the given difference of latitude, is inserted the proper correction to be *added* to the middle latitude to obtain the latitude in which the meridian distance is accurately equal to the departure. The formula for constructing this table is obtained as follows:

Let d = proper diff. of lat. D = meridional diff. of lat. m = middle latitude. M = m + correction. L = diff. of longitude.Then, (Trig. p. 75), tan. course $= \frac{\cos M \times L}{d}$ But, (Trig. p. 77), tan. course $= \frac{\text{rad.} \times L}{D}$ $\therefore \frac{\cos M \times L}{d} = \frac{\text{rad.} \times L}{D} \therefore \cos M = \frac{\text{rad. } d}{D}$ $\therefore \text{correction} = \cos -1(\frac{\text{rad. } d}{D} - m).$

TABLES VI., VII., VIII., IX., X., XI., AND XII.

These are all tables of corrections to be applied to the observed altitudes of the celestial bodies; the manner of using them must be sufficiently obvious from inspecting them, provided the object of the several corrections is clearly un derstood; and this is explained at length in the chapter on Nautical Astronomy in the Trigonometry, where several examples of the corrections are given.

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LOGARITHMS OF NUMBERS

FROM 1 TO 36,000.

Between $1 = \log^{-1} 0$, and $600 = \log^{-1} 2.7781513$.

Table 1.] LOGARITHMS OF NUMBERS FROM 1 TO 36,000.

Between $600 = \log^{-1} 2.7781513$, and $1200 = \log^{-1} 3.0791812$.

i			6		,		- 0			
tens.	1	2	1 3	4	5	G	1 7	8	9	1
60	7783745	95965		10369	7817554	24726	7831997	39036	7846173	1
61	7860412			81684	89751					
62)	7930916		7944990				72675		86506	
63	8000294	07171	8014037	20893	8027737	34571	8041394		8055009	
641	69590	75350	82110	88959	95597	/02325	5109043	15750	8122447	
651	8135810		8149132		8162413			82259	98954	ı .
66	8202015					34742		47765	8254261	ь.
				21681	8228216					
67	67225		80151	86599		99467	8305887	12297	3313638	1
68	8331471	37844	8344207	50561	8356906	63241	69567	75894	82192	
69	94780	01061	8407332	13595	8419348	26092	8432328	38554	8444772	
200										
70	9457180	£63371.	69553	75727		88047		00333	8506462	
71	8518696	24800	8530995	36982	8543060	49130	8555192	61244	67289	
72		95372	91383	97386	9603360	09366	8615344	21314	6627275	
73	8639174					68778		80564	86444	
74	0039114	90111	0401600				8733206	39016		
14	98185	,04039	8709838	15729	8721563					
75	8756399	62178	67950	73713	79470	85218			8802418	ı
76	9813847	19550	8325245	30934	3836614	42286	8847954	53612	E0263	
77	70544		81795	87410		98617		09796	8915375	
78					8948697			65262	70770	
	3926510		8937618							
79	81765	87252	92732	98205	9003671	09131	9014583	20029	9025468	
80	9036325	41744	9047155	52560	57050	63350	69725	74114	79485	
81								27533		
		95560	9100905		9111576					
82				59272	64539		75055	80303	85545	
83	96010	01233	19206450	11661	9216865	22063	9227255	32440	9237620	
84	9247960	63121	58276	63424	68567	73704		83959	89077	1
Bal			19309490				19329808		9339932	
86								85197		
	9350032			65137		75179			90198	
87	9400182		9410142			25041		34945	9439889	
88	49759	54686	59607	64523	69433	74337	79236	84130	89018	
89	98777	,03649	9503515	13375	9518230	23080	9527924	32763	9537597	
	00111	-								
90	9547248	52065		61684		71282		80856	85639	1
91	95184	99948	9604703	09462	9614211	18955	9623693	28427	9633155	
92	9642596	47309		56720		66110		75480	80157	ł .
93	89497				9703116				9726656	
							3111000	400000		1
94	9735896		9745117			58911		66083	72662	•
95	81805	66369			19800034	94579			9818186	1
96	9827234	31751	9836263	40770	45273	49771	54265	58754	63238	
97	72192	76663		85590		94496			9907827	ш.
98	9916690		9925535				9943172	47569	51963	
99	60737	65117	69492	73864	78231	82593	86952	91305	95655	
100	0004341	08677	0013009	17227	0021661	25000	0030295	34605	0038912	
		51805						77478		n .
101				60350		68937			81742	1
102	90257		98756	103000	0107239				0124154	
103	0132597	36797	0141003	45205	49403	53598	57788	61974	66155	
104	74507	78677		97005		95317	99467	/03613	0207755	
	0216027				0232525	36690	99467 0240750	44957	45060	
						PTC-D	01644	95714	Divings	
106			65333			77572		85713	89777	1
107		101948		10043		15123		26188		
108	0338257	42273	46285	50293	54297	58298	62295	66289	70279;	1
109	78248	82226	86202	90173	94141	98106	0402066	06023	0409977	
	0.0		12							1
110	0417873			29691	0433623		41476		49315	
111	57141	61048	64952	68852	72749	76642	80532	8441R	88301	
112			0503798				0519239	23091	0526939	1
113	0534626	38464		46131	49959	53793	57605	61423	65237	
114		76661		84260		91846	95634		0603200	
	0610753				0625820			37086	40934	
116	48322	52061	55797	59530	63259	66986	70709	74428	78145	
117	85569	89276	92980	96681				11453	0715138	
iis			0729847	33517		40947		48164	51819	
		62763	66404	70043				84568		
119					73679				88192	
	1	2	3	4	- 6	6	7	8	9	

Between 1800 = log. -1 3-2552725, and 2400 = log. -1 3-3802112.

	Between 1800 = log. ~1 3·2552725, and 2400 = log. ~1 3·3802112. 190 255937 57549 2559957 62365 2564772 67177 2569582 71994 2574385 1 79165 81592 83978 86373 88766 91155 93549 95939 98327 2 803099 05454 2607867 10248 2612629 15006 2617385 19762 2522137 3 26833 29255 31625 33993 36361 38727 41092 43455 45817 4 80538 52896 55253 57609 59964 62317 64669 67020 69369 5 174064 76410 78754 81097 83439 85780 88119 90457 92794										
-	me.	1. 1	2	3	4	ő	6	1 7	8	9	1
-	180	2555137	57549	2559957	62365	2564772	67177	2569582	71984	2574336	
-1	1	79155	81582	83978	86373	88766	91158	93549	95939	983271	1
-1	9	96000	90055	2007867	10248	2612629	1500F	2017385	19702	42017	1
-1	d	20083 BUS 20	59000	31023	53993	200001	60017	64660	43400 67090	49911	
ı	5	74064	76410	78754	81097	83439	85790	98119	90457	92794	1
1	6	041404	Acmes.	Carrier Co. A. A. A.	01140	ORDORADO.	0014.	CHELL LICE	5 15 W. 101	-Set 4 - Security	
	7	2720738	23058	25378	27696	30013	32328	34643	36956	~ 39268	
Ш	8	43883	46196	48503	60909	53114	55417	57719	60020	62320	
1	9	66915	69211	2702129 25378 48503 71506 94388 2817150 39793 62319 84728	73900	76092	78383	80673	82962	85250	
ı	190	69821	92105	94389	96669	98950	/01229	2803507	05784	2909059	1
ı	1	2812607	14879	2817150	19419	2821688	23955	26221	28486	39750	
ı	13	35274	37534	39793	42051	44307	46563	48817	51070	53322	
1	3	57823	60071	62319	64565	66810	69054	71296	73539	75778.	1
1		9000000	82492	84728	86963	89196	91428	93660	95800	98118	
ı	6	94776	26990	2907022	99246	2911408	15989	2915908	40251	AUWUGUT.	1
ı	71	46966	49069	51971	52471	55671	57900	60067			1
	8	68845	71037	73227	75417	77605	79792	81979	84164	96348	
	9	90713	92893	95073	97252	99429	.01605	3003781	05955	3009128	
20	0	3012471	14641	2907022 29203 51271 73227 95073 3016809 38438 59959 81374	19977	3091144	22200	25474	27637	29799	1
	11	34121	36280	38138	40595	49751	44905	47059	49212	61363	١
1	2	55663	57812	59959	62105	64250	66394	68537	70690	72820	
	3	77099	79237	81374	83509	85644	87779	89910	92042	94172	1
	41	98430	00557	59959 81374 3102694	04809	3106933	09056	3111173	13300	3115420	1
	6	3119657	21774	23689 44992 65993 86893	26004	28119 49201	30231	34343	34404	90009	1
	6	40780	42887	44992	47097	49201	91303	53405	55505 76455	57605	1
	7	61801	63898	65993	69088	70181	72273	74305	70455	78545	
	9 3	12125	04507	3207692	98977	91061	93144	993224	97305	99384	1
21		24261	26327		30457	32521	34584 55157 75633	36645	38706	40766 61310	1
1	2	44882	40939 67454	60500	51050	53104	55157	57209	59260	01310	1
-	3	85834	87879	69500 89909 3310222	91944	02070	06019	99045	100077	3302108	1
	į,	3306167	08195	3310222	12248	2314273	16297	3319320	20343	22364	ſ
- 1	51	26404	28423	30440	324571	34473	36498	38501	40514	42526	1
-	6	46548	48557	50565	52573	54579	565B5	58589	60593	62596	1
	7	66598	69598	70597	72595	74593	76589	78584	80579	92572	
	B),	96557	88547	90537	92526	94514	96502	98488	00473	3402458	
	9	3405424	08405	50565 70597 90537 3410386	12366	3414345	16323	3419301	20277	22252	
22	D	26200	28173	30145	32116	34086	36055	38023	39991	41957	
	Ц	45887	47851	49814	51776	53737	55699	57657	59615	61573	
-	2	65486	67441	69395	71348	73300	75252	77202	79152	81100	
	1	S4990 S604410	00994	30145 49814 69395 88887 3508293	10550	92775	14000	2616021	17069	19805	
	51	92755	25684	27612	20530	31465	14090	35316	37226	30162	1
i	6	43006	44926	46846	48764	50682	52500	54515	56431	58345	
-	7	62171	64093	65994	67905	69814	71723	73630	75537	77443	
	3	81253	83156	85059	86961	83962	90762	92662	94560	96458	
5	9	3600251	02146	46846 65994 85059 3604041	05934	3607327	09719	3611610	13500	3615390	ı
23	0	19166	21053	99030	0400E	96-00	ODEGO	ワロオアの	20200	2.1 (2.20)	1
	1	37999	39878	41756	43634	45510	47386	49260	51134	63007	1
	2	56751	58622	60492	62361	64230	66097	49260 67964 86587 3705131	69830	71695	1
4	3	75423	77235	79147	81009	82369	84728	86587	88445	90302	l
	41	94014	95869	97723	99576	3701428	03280	3705131	06931	3708830 27279;	
-	5	20060	22700	3/10/19	26475	19909	40143	41000	42917	45681	1
-	7	40316	51147	52977	64907	56624	59464	60202	621101	63944	1
9	7	67594	69418	71240	73063	74994	76704	79524	80343	82161	1
1	9	85796	87612	3716219 34637 52977 71240 89427	91241	93055	94868	96680	98492	3800302 9	
	1	1	2	3	4	5	6	7	H	9	1
-	_		_		-		-				_

Between $2400 = \log^{-1} 3.3802112$, and $3000 = \log^{-1} 3.4771213$.

tena.	1 1	12	3	4	- 5	6	7	8	9	
240	3903922		3807538		3911151	12956		16565		- 1
1	21972	23773	25573	27373	29171	30969	32767	34563	36359	
2	39948		43534	45326	47117	48908		52487	54275	
3	57850	59636	61421	63206	64990	66773	68555	70337	72119	
4	75678	77457	79235	81012	82789	84565	86340	88114	89888	
Б			96975		3900515		3904052			
6	3911116	12880		16407	18169	19931	21691	23452	25211 42765	
7	29727		32241	33997	35752	37506	39260	41013	60249	
8	46268		49767	51516		55011	56758 74185	59504° 75924	77663	
9	63737		67223	68964	10109	72446				
250		82873		86343	98077	89811		93275	95007	
1	98467	100196			4005380		4008832	10557	4012282	
2	4015728	17451	19173	20894		24333		27771	29488	
3	32921	34637	36352	38066		41492		44916	46627	
4		51755	53464	55171	56879	58584	60239		63698	
5		69807		72209		75608	77307	79005	80703	
6		85791	87486	89180	90974	92567		95950 12829	97641 4114513	
8	4101021 17880	02710 19562	4104398	06095 22925	4107772	09459	4111144 27964	29643	31321	
9		36350	21244 38025	39700	24605	26295	44719		48063	
-			1		41374					
260		53073	54742	56410	58077		61410		64741	
1)	69069		71394	73056	74717	76377	78037	79696	81355	
2	64670			89638	91293		94601		97906	1
3	4201208						4211101		4214394	l
4		19328	20972	22615	24257	25898		29180	30820	
5		35735	37372	39009		422BI	43916		47163	1
61	50449			55347		58601	60230 76484	78106	63486 79727	
8	66739 82968	9458S	69990 86207	71614 87825	73239	74861	92677	94293	95908	
9		00751	4302364		89443 4305588	91060	4308809	10419	4312029	
-	20101	100701								1
270	4315246	16853	18460	20067	21673	23278	24983	26497	28090	1
1 2	31295	32897 48881	34498	36098	37698	39299	40896 56851	59444	44092	
3	47285 63217	64907	50476 66396	52071 67985	53665		72748	74334	60035 75920	
4	79090		82268	93841	69573 85423	71161 67005	88567	90167	91747	1
5		96494	98062		4401216				4407517	
6	4410664	12237	4413909	15380	16951	18522	20092	21661	23230	1
7	26365		29499	31065	32630			37322	38885	1
B			45132	46692		49811	51370	52928	54485	1
9	57598		60709	62264	63918		66925	68477	70029	ı
280	73131	74661	76231	77780	79329	2	82424	83971	85517	
		90153	91697	93241	947P4		97968	99410	4500951	
1	4504031		4507109	08647	4510185	11722	4513258	14794	16329	1
2 3		20932	22466	23998		27062	28593		31654	
4	34712	36241	37769	30296	40823			45400	46924	
5	49972			54540	56061	57582	59102	60622	62142	
6	65179		69213	69730	71246	72762	74277	75791	77305	
7	90332		83356	84869	86378	97889		90908	92417	L
8	95433	96940	98446	99953	4601459		4604468	05972	4607475	
9	4610481	11983	4613484	14985		17986	19485	20984	22482	
290	95477	26974	28470	29966	31461	32956	34450	35944	37437	и
				44895		47875		50853	62341	ı.
1 2		56802		59774		62743	64227	65711	67194	1
3	70158		73121	74601	76081	77561	79039	80518	81996	1
4	84950	86427	87903	89378	90953	92327	93801	95275	96748	
5	99692	(01164)	4702634	04105	14705575		4709513			
6	4714384	15851	17317	18782	20247	21711	23175	24639	26102	
7	29027	30489		33410	34B70	36329	37788	39247	40705	
8		45076	46533				52352	53806	55259	ı
9		59616	61067			65418	66867	68316	69765	
	1	2	3	4	5	6	7	8	9	1
									-	

Table 1.] LOGARITHMS OF NUMBERS FROM 1 TO 36,000. Between $3000 = \log^{-1} 3.4771213$, and $3600 = \log^{-1} 3.5563025$.

tens.	L	2	3	4	5	6	7	8 1	9	dif.
300		74107		76999	477-445				4784222	1446
1	87108	89550	89991	91432		94313	95753	97192	98631	41
2	4301507		4604391	05818	4807254	08659	4810134	11559	4812993	36
3	15859	17292	18724	20156	21587	23019	24448	25878	27307	31
4	30164	31592	33020	34446	35873	372.19	33725	40150	41574	27
5	44422	45845		48690		51533		54375		
6	69633	60052	61470	62898	64305	65722	67138		69969	17
7	72798	74212	75626	77039	7-451	79863		82696	84097	12
8	86917	68326		91144	92552	93959		96773	98179	US
9	4900990				4906607	09010			4912216	04
-			*****							
310		16418		19217	20616	22015	23413		2,731.7	1399
1	29000	30396		33186		35974	37369		400174	5.5
2		44329	With P House	47110		49990	51279		54056	90
3		59218		60390	62375	63761	65143		67-113	8.5
4	70679	72062		74925	76;206	77587	78067	F0347	81707	81
5		85862		89617		91370				
6		99619	5000992	0.2365	5003737	05109				72
7	5011962	13332	14701	16069	17437	105	20172	21539	22005	68
8	25637	27002	25366	29731	31004	32458	33-21	351-3	36545	63
9	39268	40629	41989	43349	44709	46068	47426	147.43	50142	69
320	K9957	54213	55560	56925	ESSON	59635	coson	62344	63097	55
1		67755		70459		73160	74511	75-960	77:210	51
2		81255		83950		80044		893335	0.000	
3		94714		97400					5104109	43
4			paco		98743 5112147	10,105	14823			
	5106790			10908					17497	39
6		21505		24175		26844		29511		35
7		34840	BANK H F H	37502	38932	40162	41491			30
8		49133			52113	53439	54704		57114	26
		61386		64031	65354		67997	69318	70439	22
9	73279	74598	75917	77236	78554	79872	81189	82507	83853	18
330	86455	87771	89086	90400	91715	93028	94342	95655	96968	14
1	99592	(00903		03525		06145	5207455		5210073	10
2	5212689	13996		16610	17916	19222	20529		23138	06
2	25746	27050		29656	30958	32260	33562			02
4		40064		42663	43961	45259	4,6557	47854	49151	1298
51		53040		55631		53220			62100	
6		65977		69560	69851	71141	72431		75010	91
7	77538	78876		81451	82738	34024	85311	86596	87852	87
8	90452	91736		94304	95587	96970	9-152		5300716	83
9	5303278				5308395		5310955		13512	60
340		17343	18619	19896	21171	22446	23721	24996	26270	76
14	23817	30090		32635	33907	35179	36450	37721	39001	72
3	41531			45339	46606	47574	40141	50408	51675	68
3	64207	55473		58003	59267	60532		63059	64322	64
4	66847	69109		70631	71902	73153			76932	
5	79450	80708	81966	83223	84481	85737	86994	8R250	99506	
6	92016	93271	94525	95779	97032	99236	99538	/00791		
7	5404546		5407049	09299	5409548	10798	5412047	13296	14544	61
8	17040	18288	19535	20781	22023	23274	24519	25765	27010	47
9	29493	30742	31986	33229	34472	35714		38198	39439	43
	41921									
350				45641		48119		50596	51834	39
1		55545	56781	58018	59253	60489	61724		64193	35
2		67394	69126	70359	71591	72923	74055	75296	76517	32
3	78977	90207		82666	63894	85123	86351	87578	89306	29
41	91259	92486	93712	94937	96162	97327			5501060	25
51			5505952		5509306		5510839			22
6	15720	16939	18158	19377	20595	21813	23031	24249		18
7	27899	29115	30330	31545	32760	33975	35189	36403		15
8		41256	42469	43690	44992	46103	47314	48524	49735	12
9		63363	54572	55781	56989	58197	59404	60612	61881	08
	1	12	3	4	- 3	6	7	19	0	
-								-		-

9		LOGA	RITHMS	OF NU	UMBERS	FROM	1 то 36	,000.	[Tab	le 1.
Between $3600 = \log^{-1} 3.5563025$, and $4200 = \log^{-1} 3.6232493$.										
360 1 2 3 4 5 6 7 8	5600 1 2 12207 24118 35997 47644 59658 71440	01458 13399 25306 37183 49027 (0838 72617	5602654 14592 26497 38369 50209 62017 73793	03849 15784 21685 39655 61392 63196 74969	5605044 16975 25874 40740 52573 (4375 76144	06239 18167 30062 41925 53756 65553 77320	5607433 19358 31250 43109 54936 66731 78495	08627 20648 32437 44293 56117 67909 79669	5609821 21739 33624 45477 57298 69087 80843	1 1189 5 1 1178
370 1 2 3 4 5 6 7 8 9	64565 76067 87538	65717 77215 88683	66868 78363 89828	68019 79511 90973	87882 99588 5711263 22906 34518 46099 57650 69170 80659 92118	89054 /00757 12429 24069 35678 47256 58803 70320 81806 93262	90226 5701926 13594 25231 36837 46412 59956 71470 52953 94406	72620 84100 95550	73769 85246 96693	1 1148 5
380 1 2 3 4 5 6 7 8 9	78232	79353	5801263 12668 24043 35388 46704 57990 19247 80475	02405 13807 25179 36521 47834 59117 70371 81696 02769	5803547 14945 26314 37654 48963 60244 71495 82717	04688 16084 27450 38786 50093 61370 72618 83838 95028	5805829 17222 28585 39916 51222 62496 73742 84958	86078 97263	87198	1119
390 1 2 3 4 5 6 7 8 9	160 tars 17'	11005	19009	14081	15168	16256	17341	18428	5909532 20657 31753 42820 53860 64871 75856 86811 97739 6008640 19514	2 0 1107 4 1 1099 6 3 0 1087
400 1 2 3 4 5 6 7 8	21086 32527 43341 54128 64889 75622 86330 97011 6107666	22771 33609 44421 55205 65963 76694	23856 34692 45500 56282 67037 77766	24941 35774 46580 57359 69111 78837 89537 /00216 10857	26025 36855 47659 58435 69185 70909 90605 6101276	27109 37937 48738 59512 70259 80979	29193 39018 49816 60587 71332 62050 92742 6103407 14046 24660	29277 40099 50896 61663 72405 83120 93809 04472 15109 25720	30361 41180 51973 62739 73478 84191 94877 6105537 16171 26779	1079 6 4
410 1 2 3 4 5 6 7 8 9	28898 39478 50026 60552 71052 81527 91977 6202402	29957 40531 51060 61603 72101 82573 93021 03443	31015 41597 52133 62654 73149 83619 94064 6204484	32074 42643 53187 63705 74197 84665 95107 05524	33132 43698 54240 64755 75245 85710 96150 6206565	34189 44754 55292 65805 76293 86755 97193 07605	35247 45809 56345 66855 77340 97800 98235 6208645	36304 46863 57397 67905 78387 88845 99277 09684	37361 47918 58449 68954 79434 89889 6200319 10724	5 0 1048 5 3

Table 1.1 LOGARITHMS OF NUMBERS FROM 1 TO 36,000.

Between 4200 \pm log. $^{-1}$ 3-6232493, and 4800 \pm log. $^{-1}$ 3-6812412.

										-
tens. 420	6233527	34560	893350A	1 30627	8237660	10000	6239725	4073	6241730	dif. 1033
1 1		44334		46945		49006		51006	52095	0
2		55182	56211	57239	59267	69295	60322			
3		65457		67509		69560	70555	71.10	72634	5
4		75707		77754		79800		81345	825467	1 3
1 5		85,333		87975		90016		92057	93076	
6	95115	96134	97153	95172	90190.	00209	6391225	02244	6333361	1018
7	6305296	06312			6309361	10377		12409	13423	6
₽.		16467	17481	IB495	19508	20522		22548	23560	3
9:	25585	26597	27609	23620	20532	30343	31654	32664	33374	1
430	35694	36704	37713	33723		40740	41749	42757	4 3765	1009
1	45750	46738	47795	49301		50814		52926	5.3832	6
2		56848		58457		OUHG		62873	61570	4
3		6634	67337		696 11	70903		72895	73397	2
4	A to blue	76398		78398		80307		82405	93894	
5		811549		83334		90979		92972		
6		96857	97854	98347	99842	100037	Mu [332		64 13820	5 3
7 8	6405-03			09798		10773 20636		12758 22666	13749 23656	0
9	25634	16724 26623	17715 27512	16705 23601	2,1539	30677		32552	33540	988
								-		
440		3,1200	37497		39459	502%		42416	4810t 53340	6
1 2		46355		45323		60114		52257 62076	63057	1
3	59209	56187 65998		58151 67957		69915		71 73	72.51	979
4		75796	76763		78719	79695	90671	81648	82/124	7
5		86552		87502		89452		91401	923751	
6		95296	96269	97242	98215	90197	65001-10		6502104	3
7	3504047			06960	6507930	UP901	09971	10841	11911	0
8		14719	15687	16656	17624	18593	19561	20528	21496	968
9	23431	24397	25364	26331	27297	28263	29229	30195	31160	6
450	33090	34055	35019	35934	36949	37912	39876	39839	40802	4
1	42729			45616	49578	47539		49462	50423	2
2	52345	53306	54266	55226	56136	57145	58105	59064	60023.	0
3	61941	62339	63357	64-15	65773	66730		68645	69602	958
4		72471	73427	74393	75339	76294	77250		79159	6
5		82023	82977	83930		85937		87743		3
6		91553	92305	93456		95359		97261	98212	1
7	6600112		6002012		6603911	04360	6605809		6607706 17181	949
9		10551	11499		12393	14341	15237	16234 25690	26634	5
		20019		21910		23900				
460		20466	30410			33230		35125	36067	3
1		39993		40776	41717	42559 52056		44539	45490 54872	020
2		48299		50179	51117 (00497			53934 63307	642441	939
3 4		57686 67051	58623 67997	59500 69922	69957	70792	71727		73595	
5		76397	77331	78264	79197	90130		81995	82927	1 3
6		85723	86654	87595	84516	89447		91309	92239	ĩ
7		95028	95958	96887		98745		00602		929
B	6703386		6705242	06169		09023	6708950		10802	7
9	12654	13590	14506	15431	16356	17281	18206	19130	20054	5
470	21903	22826	23750	24673	25596	26519	27442	28365	29287	3
1		32053	32974		34817	35738		37579	38500	1
2		41260		43009	44019		45856	46775	47693	919
-3		50447		52283	53200	54117		55951	56967	7
4	59700	59515		61447	62362	63277		65107	66022	5
5		68764	69678	70592	71505	72415		74244		
6	76982	77304	78806	79718	90629	81540		63362	84273	1
7		87004		83824	89734	90643		92461	93370	909
8		96096		97912	98619	99727	6900634	10602	6802448	8
9			6906074	06980	6907886	08792 6	09097	8	11507	6
_	1	2	3	*	1 0	10		9	19	

10 Logarithms of numbers from 1 to 36,000. [$\hat{T}able$ I. Between 4800 = $\log^{-1} 3.6812412$, and 5400 = $\log^{-1} 3.7323938$.

-										_
tens.	1 1	120	3	4	5	6	1 7	8	9	dif.
480	6813317	14222		16030		17838		19645	6820548	904
1	22354	23256	24159	25061	25963	26865	27766	29668	29569	2
5	31371	32272	33173	34073	34973	35873	36773	37673	38572	0
3		41269	42168	4306G		44863	45761	46659	47556	898
4		50248	51145			53834	54730		56522	6
5				60998		62787	63681	64575	65469	6.
6	67256	68150	6:4043	69506	70828	71721	72613	73506	74308	3
7	76131	77073	77964			80637	81528	82418	83308	1
8	85088	85979	RoP-57	P7757	PP646	89535	90423	91312	92200	839
Į.	93977	94964	95752	96040	97527	98414	99301	,00188	6901074	7
490	6902847	03733	6904619	05505	6906390	07275	6908161	09046	09930	5
1	11639		13468	14352		16119		17885	18768	3
2	20534		22299			24944		26707	27588	2
2 3	29350		31111			33752	34631	35511	36390	.i
4	38149			40785	41663			44297	45175	879
5		47806		49560		51313		53065	53941	7
6	55692			68318	59193		60942	61816	62690	5
7		65311		67058		68804	69676	70549	71421	3
B	73165		74909	75780	76652	77523	78394	79264	80135	2
						86224			88831	0
9		62746		84495				87963		
500		91437	92305		94041	94908	95776	96643	97510	868
1		(00111	7000977	01843	7002709	03575	7004441		7006172	6
3	7007902			10496	11361	12225		13953	14816	5
3		17406	19269	19132	19995	20857	21720	22582	23444	3
4	25167	26028	26890	27751	28612	29472		31193	32054	1
5		34633	35493	36352	37212			39788	40647	0
6	42363	43221	44079		45794	46652	47509	48366	49223	P55
7		51792	52649		54360	55216	56072	56927	57782	6
8	59492		61201	62055	62910	63764	64617	65471	66325	5
9		69884	69737	70589	71442	72294	73146	73998	74850.	3
	76553		78256	79107	79957			82509	83359	1
510		85909	86758		89456	89305		91003	91851	815
1		94396	95244			97796		99460		013
2	7102020		7103713			06250	7107096		08786	1
3.	10476				13954	14698	15542	16385	17229	4
4	18915		12165 20601		22287	23129	23971	24813		3
5		29190		21444		31544	32385	33225	34065	1
6			29021	29862			32385 40782	41620	42459	Ö
7	35745		37425	38264		39943	49162	50000	50937	939
8	44136		45812			48325			59198	7
9	52510			65019	55856		57527			
520	60869			63373	64207		65876	66710	67544	5
1	69211	70044	70977	71710	72543	73376	74208	75041	75873	3
2	77537	78369	79200	80032	80963	81694	82525		84156	1
3	85847		87507	88337	89167		90826		92454	0
4	94142		95799	96627	97455	99293		99936		828
5	7202420					065541			090.2	6
6	10683			13159	13984	14809	15633	16458	172-2	Б
7	18930		20578	21401	22225	23048	23971	24694	25517	4
8	27162		28806	29628	30450		32093	32914	33736	2
9	35379			37839		39480	40300	41120	41939	1
530		44397		46035		47672	49491	49309	50127	819
	51763		53399	54216		55850	56667		58300	7
1 2				62380		64012	64827	65642	66457	6
2				70530	71344		72972	73786	74599	4
3	68087		69716 77852	70530				81914		3
4	76226		77852 85972		67595				90838	1
5		85161			95697	90507	97316		98934	809
6	92458		7302168	94888	7303785		7305400		7307015	8
7	7300552					12663	13470	14276	15082	6
B		09437	10244 19304		11957	20719		22329	23133	5
9		17499	19304	19109	19914	20719 G	21024	22329	23133	
V	1	74	3	1	(3)	19		E)7	0	

Tuble 1.] LOGARITHMS OF NUMBERS FROM 1 TO 36,000.

Between $5400 = \log_{10}^{-1} 3.7323938$, and $6000 = \log_{10}^{-1} 3.7781513$.

	-									
lens.	1	22	3	4	5	6	7	H	9	dif.
64.	7524742	25546	7326350				7329564	30367	7331170	804
1	32775	33578	34380	35183	35985	36787	37588	38390	39192	2
2		41595	42396	43197	43997	44798	45598	46398	47198	0
3	49798	49598	50397	51196		52794	53593	54392	55191	799
4	56787	57585	56383	59181		60776	61574	62371	63166	8
F	64762	65558	66355		67948		69540	70335	71131	7
6	72722	73517	74312	76107	75902	76696	77491	78285	79079	5
7	80667	81461	82254	83048	83841	84634	85427	86220	87013	4
8		89390		90974	91766	92558	93350	94141	94932	2
9	96514	97305	98096	99887	99677	00467	7401257	02047	7402837	0
550	7404416	05206	7405995	06784	7407573	09362	09151	09939	10728	789
. 1	F2304	13092	13880	14668	15455	16243	17030	17817	18604	8
2	20177	20964	21750	22537	23323	24109	24895	25680	26466	6
- 3	28037	28822	29607	30392	31176	31961	32745	33530	34314	5
4	36892	36665	37449	38232	39016	39799	40582	41365	42147	4
5	43712	44495	45277	46059	46841	47622	48404	49185	49967	2
6	51529	52310	53091	53871	54652	55432	56212	56992	57772	1
7	59332	60111	60890	61670	62449	63228	64006	64785	65564	779
B	67120	67898	68676	69454	70232	71009	71787	72564	73341	8
9	74895	75672	76449	77225	78001	78777	79553	80329	81105	7
560	82656	09421	P4906	84981	05750	86531	07200	88080	88854	5
1	90403	91177	91960			94271	95044	95317	96590	4
2		96908		00453			7502769		7504312	2
3	7505855				08939		10480	11251	12021	ĩ
4	13561	14331	15101	15870	16639	17409	18178	18947		ô
5	21263	22022		23558				26629	19716 27397	768
6	28932	29699		31232	31999		33532	34298	35066	7
7	36596	37362	38128	35893	39659	40424	41189	41954		6
9		45012	45777	46641		48069	48832	49596	42719	4
9		52649	53412	54175	47305				50359	3
					54937	55700		57224	57987	
570		60272		61795	62556		64079	64840	65600	2
1	67122	67882		69402	70162	70922	71682	72442	73201	
2	74719	75479		76996		78513	79272	80030	80799	769
3	82304		83819			86091	86848	87605	88362	7
4	89875	90632		92144	92900	93656	94412	95168	96923	6
Б	97434	98189	98944	99699			7601962	02717	7603471	4
6	7604979		7606486	07240	07993		09500	10263	11005	3
7	12511	13263	14016	14768	15520	16272	17024	17775	19527	2
8	20030	20781;	21532	22293	23034	23784	24535	25295	26035	1
9	27536	28286	20035	29785	30534	31284	32033	32782	33531	749
580	35029	35777	36526	37274	30022	39770	39518	40266	41014	8
1	42509	43256	44003	44750	45497	46244	46991	47737	48484	7
2	49976	50722	51468	52214	52959	53705	54450	55195	55941	6
3	57430	58175	58920	59664	60409	61153	61897	62641	63385	5
4	64872	65616	66359	67102	67845	6R588	69331	70074	70816	3
5	72301	73043	73785	74527	75269	76011	76752	77494	79235	2
6	79717	80458	81199	81940		83421	84161	84901	85641	0
7	87121	87860	88600	89339	90079	90918	91557	92296	93035	739
8	94512	95250	95988	96727	97465	96203	98940	99678	7700416	8
9	7701890	02627	7703364	04101	7704939	05575	7706311	07048	07794	7
590	09256	09992	10728	11463	12199	12934	13670	14405	15140	6
1	16610	17344	18079	18813	19547		21016	21750	22483	4
2	23951	24684	25417	26150	26884	27616	28349	29082	29815	3
3	31279	32011		33475	34207		35670	36402	37133	2
4		39326		40789	41519				44440	î
5	45900	46629				49547	60276	51005	51734	
6		53920		55376		66832		58288	59016	728
7	60471	61198	61925			64106	64833			7
7 8.	67738	68464	69190	69916	70642		72093			6
9	74993	75718		77167		79616				
2)	14993	2	3	4	5	6	79340	8	1)	10
	-		1 0	-		-0	1 .	C9	1 59	

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-		rh.			-	-				
660	8196097	96755	8197413	± 09071	8169799	00380	9200049	00700	9 8201358	dif.
	8202572		8203985					07268	07924	7
2		09892		11203		12514		13825	14480	. 6
3		16445	17100	17755		19064		20372	21027	5
41	22335			24296	24950	25603	26257	26910	27563	4
5		29522	30175	30828		32133				3
6		36046		37350	38002	38.53	39305		40607	2
8		42560		43862 50364		45163		46464	47114	1
9		49065 55559	49715	56857	51014	51664 58154		52963 59451	53612 60100	640
670	67872	62044 68519		63340 69813	63988			65931	66578	8
2		74985		76277		71107 77569	78214	72400 78860	73046 79505	6
3		81441		82731		84021		85310	85955	5
4		B7887		89176		90463		91751	92394	4
5		94324		95611		96896		98182		3
6	8300109	00752	8301394	02036	9302678				8305245	2
7		07139		08452	09093	09734	10375	11016	11656	1
8		13578	14218		15499	16139	16778	17418		0
9	19337	19977	20616	21255	21895	22534	23173	23812	24450	. 0
680		26366		27643	28281	28919	29558	30195	30833	639
1		32746		34021					37207	8
2		39117		40390		41663		42935		7
3		45479		46750		48021		49291	49926	6
4		51831 58174	52465	53100		54369		55638	56272	5
5 6		64507		59441 65773		60708 67038		61975 68303	62608 68936	3
7		70332		72095		73359		74622	75253	2
8		77147		78409	79039		80301		81562	ĩ
9		83453		84713		85973		87232	87861	0
690	89120	29750	90379	91008	91637	92256	92895	93523	94152	629
1		96037		97294		98550		99806		8
2		02316	8402943	03571				0.073	06706	7
3		08586		09838		11091	11717		12969	7
4		14846	15472			17348				6
5		21078		22347		23596		24844		5
6		27.340			29211	29835		31081	31705	4 3
7 8		33574 39798	34197	34819 41042	35442	30065 42286	39687	37310 43529	37932 44150	2
9		46014		47256	47877			49739	50360	î
										0
700		52221 58419		53461 59658		54701 60996		55941 62134	56561 62752	619
2		64608		65845		67081		68318	68935	919
3	70171					73258		74493	75110	7
4						79426		80659	81275	6
5			83739	84355	84970	85586			87432	5
6		89277		90507		91736	92351		93580	5
7		95423	93037			97878		99106	99719	4
9			8502172						8505850	3
9	07075	07687		09912	09524	10136	10748	11360	11972	2
710	20.0	13907		15030	15641	16252	16863	17474	1808	1
1	19307			21139		22359		23580	2/100	0
2 3	25410 31504	26020 32113	32722	27239 33331		28458 34549	29068 35157	29077 35768	36374	600 9
4		38198				40630		41845		8
5		44275		45489		46703		47917		7
6		50343		51556		52768		53980	54586	6
7	55797			57614		58924		60035		5
8		62454		63663	64268	64872	65476	66081	66685	5
9		68497		69704	70308	70912		72118	72722	4
	1	2	3	4	5	6	1 7	8	6 /	1
	6)									

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14									. [Ta	
									8920946	
tens.	1	2	3	4	10220010	15	1 7	8	9 8578750 84770 90782 96786 8602781 08768	dij
720	79955	74531 80557	8575134 91159	75737 81761	8576340 82363	76943	83567 83567	78148 84169	84770	2
2	85973	86575	87176	87777	98379	88980	89591	90191	90782	2
3	91994	92584	93185	93785	94385	94986	95586	96186	96786	1
5	18603979	04578	13605177	05776	06374	06973	07571	08170	08768 14747	1593
6 7	09964	10562	11160	11758	12356	12954	13552	14149	14747 20717	8
8	21910	22507	23103	23699	18330 24296	18927	19524 25488	20121	26680	77
9	8603979 09964 15941 21910 27871	28467	29062	29658	30253	18927 24392 30848	13552 19524 25488 31443	32039	26680 32634	6
730	33923	34418	35013 40956 46890	35608	36202	36797	37391	37985	39580 44517 50447 56369 62282	5
1	39768	40362	40956	41550	42143	42737	43331	43924	44517 50447	4 3
2 3	45704 51632 57552	52225	52817	53409	54001	54593	55185	55777	56369	2
4	57552	58144	52817 58735	59327	59918	60509	61100	61691	62282	1
5 6	69368	64055	70549	71138	71728	72317	67008 72907 78798 84681	73496	68188 74086	0
7	75264	69958 75853	76442	77031	77620	78200	78798	79387	79975	689
8 9	81152	81740	82329	82917	65827 71728 77620 83505 89382	84093	84681	85269 91143	85857 91730	8 7
740	02004	02/01	04077	04664	05304	05909	06423	07010	97596 97596 9703454 09304 15146 20980 26806 3262 3362 344238 50034	7
1	98763	99354	99940	00526	9701112	01697	8702283	02868	3703454	6
2	8704624	05210	8705795	06380	06965	07549	09134	08719	09304	5
3	16313	16897	17480	18064	12810	19230	13978	20397	20980	4 3
5	22146	22728	23311	23894	24476	25059	25641	26224	26806	2 2
6	27970	28552	29134	29716	30298	30980	31462	32043	3262#	2
8	39597	40177	40757	41338	41918	42498	43079	43658	44238	Ó
9	45398	45978	46557	47137	47716	43296	48875	49454	50034	579
750	51192 56978 62756	51771	52349	52928	53507 59290 65065 70833 76592	54086	54664 60446 66219 71985 77743	55243	55921 61601 67373 73137 79894	9 8 7 7
2	62756	63333	63911	64488	65065	65642	66219	66796	67373	8
3	68526 74289	69103	69680	70256	70833	71409	71985	7256L	73137	7
4	74289	74865	75441	76017	76592	77168	77743	78319	79894	6 5 4
6	85792	86357	86941	87515	83080	88663	89237	89811	94643 90385	4
7	91532	92106	92680	93253	93926	94400	94973	95546	96119	3
9	97205	03562	98411 8904134	04706	99550	05950	06421	06993	94643 90385 96119 8901846 07564	3 3 2
760	08707	09279	09850	10421	10992	11563	12134 17840 23537 29228 34911 40586 46255	12705	13276	ĩ
1	14417	1/093	15553	16129	16699	17269	17840	19410	13276 18980	0
2 3	20120 25815	20083	21259 26953	21829	22398	22968	23537	24107	24676 30365	
4	20120 25815 31502 37182 42855	32070	32639	33207	33775	34343	34911	35479	30365 36047	8 8 7
5 6	37182	37750	39317	39885	39452	40019	40586	41154	41721 47397	7 7
7	49520	49086	49652	50218				52481	53047	6
8	54178		55308	55874	56439	57004	57569	58134	53047 58699 64343	6 5
770		60393								
770 1	65471 71107		66599 72233					69417 75048		4
2	76736	77298	77860	79423	78985	79547	80109	50671	81233	3 2 2 1
3	82357	82918	83480	84042	84603	95165	85726	86287	86848	2
51	93577	941391	94698	95258	95819	963781	96938	97498	98058	. 0
5 6 7	99177	99736	8900296	00855	8901415	01974	8902533	03092	8903651	Õ
8	8904769 10354	10912	05887	12022	07004	07563	08121	08679	09238	550
8 9	15932	16489	17047	17604	18161	18718	19275	19832	75610 81223 86848 92457 98058 8903651 09238 14817 20389	7
	1 .	2	3	4		8	7	8	9	

Between $7800 = \log^{-1} 3.8920946$, and $8400 = \log^{-1} 3.9242793$.

between 1800 = 10g. · 3.8920340, and 8400 = 10g. · 3.9242133.										
780			8922616							
l i	27066		28178		29290		30401		31512	5
2 3	32623 39172		33733 39281	39836		35398 40944		36508 42053	370c3 42607	4
4		44268	44822		45929			47590	48143	4
5		49803	50356			52015		53120		3
6	54778		55883			57539		58644	59195	2
7	60299		61403			63057		64160	64711	2
8	65813	66364	66915	67466		68568	69118	69669	70220	1
9	71320	71871	72421	72971	73521	74071	74621	75171	75721	0
790	76821	77370	77920	78469	79019	79568	80117	80667	81216	0
1	82314	82863	83412	83960	84509	85058	85606	86155	86703	549
2		88348	88897			90541		91636	92184	8
3		93827	94375	94922	95469	96017	96564	97111	97658	7
4		99299	99846	00392	9000939	01486	9002032	02579	9003125	6
5 6		10222	9005310	11313	11050	06948 12403		08039 13493	08585 14038	5
7		15673		16762		17851		18940	19485	5
8	20573	21117	21661	22205		23293		24381	24924	4
ğ		26555		27641		28728		29814		4
900	31443			33071		34156		35241	35783	3
300	36867			38493		39577		40661	41202	2
$\hat{2}$		42827		43909		44992		46074	46615	ĩ
3		48237		49318		50399		51480		i
4		53641	54181			55800		56880	57419	0
5	58498	59038		60116		61195		62273		
6		64428		65505		66582		67659		9
7		69812		70887		71963				8
8		75188		76263		77337		78411		6
9		80559		81632		82705		83778		
810		85922		86994		88066		89137	89673	6
2		91279		92350		93420		94490		5
3		96630	9102508	97699		98768		99837		5 4
4		07311		08378		09444				3
		12642				14772				3 2 2
1 6		17966		19030		20094		21157		2
7	22752	23284		24346	24878	25409	25940	26471		1
8		28595		29656		30717		31778		1
; 9	33369	33899	34430	34960	35490	36019		37079	•	0
820	38668	39198	39727	40257	40786	41315		42373		
1		44489		45547		46604		47661		
3	49246	49775		50831		51887		52943		8 7
1 3		55054		56109		57163		58218		
1 4		60326		61380		62433 67697		63487 68749		6
. 6		65592 70852		66645 71903		72954		74005		5
		76105		77155		79205		79254		
		81352		82401		83449		84497		4
9		86593		87640		88687	89211	89734	90258	4
830	91304	91827	92350	92873	93396	93919	94442	94965	95488	
		97055		98100		99145			9200711	2
	9201755	02277	9202799	03321	9203842		9204886	05407	05929	2
		07493		08535		09577		10619		1
	12181			13743		14784		15824		
	17385			18945 24140		19984 25179		l 21024 3 26217		
	22582 7 27773			29330		30367		31404		
	7 27773 3 32958			34513				36584		
	38137			39690		40724		41759		
	1	2	3	4	5	6	7	8	9	

lens.	1	2	3	4	- 5	6	1 7	8	9	dif.
840.									9247444	
1		48993		50025		51057		52099	52605	6
2	53637	54152		55184	55699	56215	56730	57245	57761	6
3		59306		60336	60851	61366		62395	62910	5
4		64453	64968		65997	66511	67025	67539	68053	4
5		69595		70622		71650		72677	73190	4
6	74217 79347	74730	75243		76270	76783		77808	78321	3 2
8	84471	79959 84983	85495	80885		81909 87030		82934 88054	83446 88565	2
9		90100		91123		92145		93167	93678	î.
850	94700					-		-		- 4
830			95722 9300826	96233		97254		98275	98785 9303886	0
	9304906			06434		07453		08472	08981	0
3	09999	10508		11526	12035	12544	13053	13562	14070	509
4		15596		16612	17121	17629	18137	18645	19153	8
5		20677		21692		22708				B
6	25245	25752	26259	26767		27781	28288	28795	29301	7
7.		30855		31835		32848		33860	34367	7
8	35379		36391	36897		37909		38920	39426	6
9	40437	40943	41448	41953	42459	42964	43469	43974	44479	5
860		45994	46499	47004	47509	48013	48519	49023	49527	5
1		51040		52049	52553			54065	54569	4
2		56080	56584			58095		10169	69605	4
3		61114	61617			63126		64132	64635	3
4	65640		66645			68152	69656		69659	
5	70663 75680	71165	71667 76683	72169 77184	72671	73172			74677	2
6	80692	81193		82194	77686	78187		79189	79690	1
8	85698		86698		82695 87698		83696	94196 99198	84697 89698	ô
9	90697		91697		92696			94194	94693	0
870	95692	96191	96690							499
					97693 9402674			99194	99683 9404667	499
2	05663		06659		07654			09147	09645	8
3	10640			12132	12629	13126	13623	14120	14617	7
4	15611	16103	16605		17599	19095	18591	19088	19584	7
5	20577	21073	21569	22065		23058	23553	24049		6
6				27024	27519	28015	28510	29005	29501	6
7	30491	30986	31431	31,376:	32471	32966	33461	33956	34450	5
8	35440		36420	36923	37418	37912		38900	39395	5
9	40383	40677	41371	41365	42358	42852	43346	43840	44333	4
930	45320		46307	46800	47294	47787	48280	48773	49266	3
1		50745		51730		52716		53701	54193	3
2	55178			56655	57147	57639			59115	2
3	62014	65505	61092			62557		63540	64031	2
54		70414		71.05	66978	67469 72376	67960		68942	1
5	74827	75317	75807	76297	76787	77277	72966 77767	73357 78257	73847 78747	0
7	79726	80215	B0705	B1194		82173	82662	83151	83641	489
8		85108	85597			87063		88040	68529	9
9		89005	90423		111111111111111	91948		92924	93412	8
806	94389			95952	96339			97902	98290	
1		99752	3500233		9501213	01701			9503162	8 7
2	9504135			05596		06569		07542	08028	7
3		09497		10459				12404	12889	6
4	13861	14347	14832			16299		17260		6
5		19201		20171	20656	21141		22111		6
6		24049		25018	25503	25987		26956	27440	5 4
7		28893	29377	29861	30345	30828	31312		32280	
8	33247	33731	34214		35181	35664	36147	36631	37114	4
9	35050	38563		39529		40494		41460		3
		74	3.7	4	5	6	1 7	8	9	

		-						-		
1.9	1	2	3	4	5	6	7	8	9	dif.
			9543873				9545802		9546766	482
1	47730	48212		49176	49657	50139	50621	51102	51584	2
2	52547	53028	53510	53991	54472	54953		55916	56397	1
3	57358	57839		58801		59762		60723	61204	1
41	62165	62645		63606		64566		65526	66006	0
5		67445	67925	68405	68885	69364	69844	70323	70803	. 0
6	71761	72241	72720	73199	73678	74157		75115	75594	479
7	76552			77988	78466	78945		79902	80380	9
8	81337	81815	82293	82771	83249	83727	84205	84683	85161	8
9	86117	86594	87072	87549	89027	88505	88982	89459	89937	8
10	90891	91368	91845	92322	92800	93276	93753	94230	94707	7
1	95660	96137	96614	97090	97567		98520	98996	99472	7
2	9600425	10200	9601377	01853	9602329	02805	9603281	03756	9604232	6
3	05183	05659	06135	06610	07086	07561	08036	08512	08987	6
4	09937	10412	10887	11362	11637	12312	12787	13262	13736	5
13	14686	151f0	15635	16109	16583	17058	17532	18006	18481	5
€	19429	19903	20377	20251	21325	21799	22272	22746	23220	4
7	24167	24640	25114	25587	26061	26534	27007	27481	27954	4
В	28900	29373	29846	30319	30792	31264	31737	32210	32693	3
9	33628		34573			35990		36934	37406	2
	38350	38822	39294	39766		40710		41653	42125	1
9	43068		44011		44953			46367	46838	2
2	47780			49193	496C4	50135	80006		51546	ĩ
3	52488		53428			54339		55780	56250	0
4		57660		58599		59539		60478	60948	ő
5	61987			63296		64233		65172		
	66579	67048	67517	67985	68454			69860	70329	9
		71734	72203	72671	73139			74544	75012	8
	75948		76894	77351	77819			79222	79690	8
	80625			82027	82494			93895	84362	7
1							P.			
	85296		86230			87630		86564	88030	7
1	89963		90896	91362		92295	92761		93693	6
2	94625		95557	96023	96488	96954		97885	98351	6
3	99282		9700213	00678	9701143		9702074		9703004	5
	9703934			05328		06258	06722		07652	5
5	08591		09509	09974	10438	10902		11530	12294	4
G.		13686		14614	15078	15542	16005	16469	16932	4
7		18323	18786	19249	19713	20176	20639	21102	21565	3
8	22491	22954	23417	23980	24343	24805 29430	2526B	25731: 30354:	26193	3 2
9	27118			28506	10.000				30816	
G	31741	32202		33126		34050	34511		35435	2
1	36358	36819	37281	37742	38203	38664	39126	39587	40048	1
2	40970	41431	41892	42353		43274		44196	44056	1
3	45577	40039	46498	46959		47879		48900	49260	0
41	50180	50640		51560		52479		53399	53858	0
51	5477R		55697	56156		57075		57993		
6	59370		60588			61665		62582	63041	9
7	63958		64875	65334	65792	6F 25 L		67167	67625	8
8	68541	ecouc.	69458	69915	70373	70831	71289	71747	72204	8
9	73120	73577	74035	74492	74950	75407	75864	76322	76779	7
0	77693	78150	78607	79064	79521	79978	80435	80892	81348	7
1	82262	8271R	83175	83631	84088	84544	85001	85457	85913	6
2			67738	88194	88650	89106	89562	90017	90473	6
3	91395	91840		92751	93207	93662	94118	94573	95028	6
41	95939		96649	97304	97759	98214		99124	99579	5
					9802307				98041251	5
6	05033			06396		07304		08212	08066	4
7	09573		10481	10934	11388	11841	12295	12748	13202	4
8	14108		15015	15468	15921	16374	16827	17280	17733	3
9	18639			19997	20450			21807	22260	3
1	1	2	3	4	5	G	7	8	9	

Between $9600 = \log^{-1} 3.9822712$, and $10200 = \log^{-1} 4.0086002$.

tens.	k	14	3	+	- 5	6	7	8	9	dif.
960	9823165								9826782	452
1		26138			29493	29945	30396	30848		2
3		32654 37165		33556 35066	34007 38517	34459 38968	34910	35361 39869	35812 40320	1
4		41671		42572		43473		44373	44823	Ô
51		46173		47073		47973		48972		0
6		50670	51120			52468	52917		53816	449
7	54714	55163	55612		56510			57856	59305	9
8	59202			60548	60996			62341	62790	8
9	63686		7.	65030	1	65926		66822	67270	8
970		68613		69508		70403		71298	71745	8 7
1		73097		73991		74975		75769	76216	1
2 3		77556 82021	62467	78450		79343 83906		80236 84698	80682 85144	6
4	86035		86027		87818			83155	89601	6
51		90937		91828		92718		93608		5
6		95388	95833	96278	96722	97167	97612	93057	98501	5
7		99835			9901168					4
8	9903833		04721		05608			03940	07383	4
9	08271	09714	09158	02601	10044	10458		11374	11918	3
980	12704			14033		14919		15805	16247	3
1	17133	17575		13461	19 03		19798		20673	3
3		21399	22441			23768	24210		25093 29510	2 2
4	25977 30392	26419 30834	31275	27302	32157	28185 32598	33039	23068 33480	33921	ĩ
51		35244		36126		37007		37888	383291	i
6.		39650		40531	40971			42291	42731	0
7	43612	44051	44491		45371	45811	45251	46690		0
8		43443	46893		49767			51085	51524	439
9	52402	-	53230	53719	54159	54597	55933	55474	55913	9 ,
990		57229		58106	58545			59860	60298	8
1.		61613		62480		63365		64241	64679	8
2		65992		66868		67743		63619	69055)	8
3 4	69930	70367		71242		72116 76435		72300. 77358	73427	7
51	78667			79976		803491		81721	821571	6
6		83465				83209		86030	\$6516	6
7		87523	83259	93694	8.0129	89564	90000	90435	90370	5
6	91741		92611			93916		94785	95220	5
9	96000	96524	96959	97393	97523	98565	93697	99131	99556	4
1000			0001303				0003039			4
1		05208		06076		03943		07810	03244	3
2.		09544	09077			11277		12143	12576	3
3		13875 19202	14308	19067		15607 11932		16472 20706	15 105 21223	2
51		22525		23339		24253		25116		2
6				2770di		28569	20001	20432	21363	1
7		31157		32010		32392		33744	34174	1
8		35467		36323	3:5759	37190	37620	39051	33491	1
9	39342	39772	40203	40633	41063		41924	42354	42784	0
1010	43644	44074		44933	45363			46652	47032	0
1		46371		49229		50088		50 147		429
2		52663				54379		55237	55366	9
3		56952		57809. 62092		53666 62949		59523 63805	64233	8
4:		61236 65516		66372		67227		68032		8
6	69365	69792		70647		71501	71929	72355	72782	
7				74917	75344	75771	76194		77051	7
8	77904	78331		79134	79610	80037	80463	60989	81316	6
9		82594	83020	83446		84208	84724	85150	\$3576	6
	1	- 12	3	-1	- 5	-6	7	74	9	
-		-						_	-	

Table 1.] LOGARITHMS OF NUMBERS FROM 1 TO 36,000. Between $10200 = \log^{-1} 4.0086002$, and $10800 = \log^{-1} 4.0334238$.

-										
tens.	0000407	2	3	4	5	6	7	8	9	dif
1020	0096427 90683		0087279		92384	92809		89407		426
2	94934			91959 96208		97058	93234 97483	93659 97907	94084 98332	5
3			0100030							4
4	0103424	0.3646	04272			05544	05967		06815	4
51				03932			10204	10627	11050	4
6	11897	12320	12743	13160	13590	14013		14859	15282	2
7	16127	16550	16973	17396		18241		19086	19809	3
6	20354	20776	21198	21621	22043	22465	22887	23310	23732	2
9	24576	24998		25842		26685		27529	27951	3 2 2
1030	26704	29215	29637	30059	20150	30901	31323	91744	32165	2
1		33429	33850	34271	34692	35113		35955	36376	1
2		37639		38460	38901	39321		40162	40583	ì
3		41844		42685		43525		44365	44785	0
4		40045		46885		47725		48564	48984	ő
5		50243		51082		51920		52759		
6	54017		54855	55274		56112		56950	57369	8
7	58206	58625	59044	59462		60300		61137	61555	9
8	62392	62810	63229	63647	64065	64483	64901	65319	65737	8
9	66573	66991	67409	67827	68245	68663	69080	69498	69916	8
1040	70751	71168	71586	72003	72421	72838	73256	73673	74090	7
1	74924	75342	75759	76176	76593		77427	77844	78260	7
2		79511		80344	80761		81594		82427	7
3		83676	84092	84508		85341	85757	86173	86589	6
4	87421	87837	88253	88669	89084	89500	89916	90332	90747	6
5		91994		92825	93240		94071	94480	94902	
6		96147		96977	97392		98222		99052	5
7		/00296			0201540				0203198	5
8	0204027		04856	05270		06099	06513		07341	4
9	08169	U2680	08997	09411	09824	10238	10652	11066	11479	4
1050	12307	12720	13134	13547	13961	14374	14787	15201	15614	3
1		16854	17267	17680	18093	18506	18919	19332	19745	3 3 2
2		20983	21396	21808	22221	22634	23046	23459	23871	3
3		25109			26345	26758	27170		27994	2
4		29230		30054	30466	30878	31289		32113	2
5		33348		34171	34582	34994		35817		2
6 7		37462	37873	39284 42393	38695	39106	39517	39928 44036	40339	I
8	41161	41572	41982 46088	46498	42904	43214	47729		44446 48549	0
9	45267	45678. 497811		\$0000		47319 51419		48139 62239	52649	ő
1										_
1060		53878	54288	54697		55516		56335	56744	409
1		57972	58382	68791		59609	60018		60836	9
2		62063		62881 66967		63698 67783		64515	649241 69008	8
4		70233		71049		71865	72273			8
5		74312		75127	75535	75942		76767	77165	
6		78387		79201		80016		80830	81237	7
7	82061		82865	83272	83679	84086		84699		7
8	86119			87339	87745	88152		88964	89371	7
9		90590		91402		92214		93026	93432	6
1070		94649		95461		96272		97084	97489	6
1 1		98706		99516		00327				5
2	0302353				0303973			05188	05592	5
3		06807	07211	07616	08020		08830		09636	5
4	10447		11256	11660		12468	12872	13277	13681	4
5	14489		15296	15700		16509	16912	17315	17719	4
6	18526	18930		19737		20544	20947	21350	21754	4
7		22963		23770	24173	24576	24979	25382	25795	3.
8	26590		27396	27799	28201		29007		29812	3
9	30617		31422			32629		33433	33835	2
	1	2	3	4	5	6	1 7	8	9	
married State of		THE PERSON NAMED IN								_

LOGARITHMS OF NUMBERS FROM 1 TO 36,000. [Table 1. Between $10800 = \log^{-1} 4.0334236$, and $11400 = \log^{-1} 4.0569049$.

tens.	1 1	2	3	4	5	6	1 7	8	9	dif.
1080									0337855	402
1		39060		39864		40667		41470	41871	2
2		43075		43878		44680		45482	45884	1
3		47087		47888			49091	49491	49892	1
4		51094		51895		52696	53096	53497	53897	0
5		55098		55898		56698		57498		0
6		59098		59898	60297	60697	61097	61496	61896	
7		63094		63893		64692	65091		65890	399
8		67087		67895		68683		69481	69880 73867	9
9	10018	71076	71475	71874	72272	72671	73070	73468	4	
1090	74663	75062	75460	75858	76257	76655	77053	77451	77849	8
1		79044		79839		80635		61431		8
2		83022	83419			84612		R5407	85804	7
3		86996	67393			88585		89379	89776	7 7
4	90570		91364			92554	92951	93348	93745	7
5		94934		95727		96520		97313		6
6		98999		99090	0400086		0400978	01274	0401670	6
7			0403264			C4441		05232	05628	6
8		06914		07005		08396	08791		09582	5
9	10372	10767	11162	11557	11952	12347	12742	13137	13532	5
1100	14322	14716	15111	15506	15700	10295	16690	17084	17479	5
1	13268	18662	19956	19451	19845	20235	20633	21028	21422	4
2	22210	22(ii)4	22998	23392	23786	24180	24574	24968	25361	4
3	26149	25543	26936	27330	27723	28117	28510	29904	29297	4
4	300-4	3/1477	30871	31264	31657	32050	32444	32937	33230	3
51	34016	3440.9	34902	35195	35587	35980	36373	36766		3
6		38337		31122	39514	39907		40692	41084	3 2 2 2
7	41869			43045	43437	43825		44614	45006	2
8	45790		46573	411966	47357	47745	46140	48532	48924	2
9	49707	50099	1,0400	50852	51273	51664	52056	52447	52839	2
1110	53621	54012	54403	54795	55186	55577	5596R	56359	56750	1
1	57531	57922	58313	58704	59005	551435		60267	60657	1
2	61439	61329	62219	62610	63000	63391		64171	64561	0
3	65342	65732		66512		67292		68072	68462	0
4	69242	69632	70021		70901	71100	71580	71970	72351	- 0
5	73138	73528	73917	74306	74696	76085	75474	75864		
6	77031	77420	77809	78198	78567	7897)	79365	79754	80143	
7	Brust	81309	BLOBB	R2087	82475	829/14	83253	83641	84030	9
8	64900	85195	85583	85972	86360	86748	97136	87525	87913	8
9	83639	80077	89465	80853	90241	506/29	91017	91405	91792	8
1120	92569	92956	93343	93731	94119	94506	94894	95281	95669	8
1	90444			97606		98390		99154	99541	7
2			0501000				0502637			7
3		04571		05344	05731			06890	07277	8 7 7 7 6
4		03436		09208			10367	10753		
F	11911	12297		13069		13841		14612		6
6	15770	16155	16541	16926	17312	17697		19468	18954	6
7	19624	20010		20780		21551	21036	22321	2270	5
8	23476	23861	24246	24631	25016		25785	26170	26555	Б
9	27324	27709	29093	29478	289,72	29247	29631	30016	30400	· (5
1130	21169	31553	31937	32321	22706	33090	22474	33858	34242	4
1		35394		36162	36546				39681	4
2		39232		39999		40766		41532	41916	4
3		43066		43532		44598		45365	45748	3
1		46896		47662		49428		49193		3
51		60724		51489	61971	52254		53019		3
6		54548		55312		56077		56841	57223	2
7	57987	58369		59132		59896	60278		61041	2
8		62186		62949		63712		64475	64856	3 2 2 1
9		66000		66762		67524		68287	68668	i
	1 .	2	3	4	5	6	7	A	9	
-			-			-			-	

Between $11400 = \log^{-1} 4.0569049$, and $12000 = \log^{-1} 4.0791812$.

								- 0		
tens. 1140	0569429	- 2 69810	0570191	4 70572	0570953	(j 71334	7 0571714	72095	9 0572476	dif. 381
1	73237			74379	74759	75140	75520		76281	301
2		77422		78182	78562	78942	79322		80082	Ô
$\tilde{3}$		81222		81982		82741		83501	83891	ŏ
4										
		85019	85399			86537		87296	87676	0
5	88434	88813		89572		90330		91088		
t t	92225	92604	92983	93362	93741	94119	94498		95256	9
7	96013			97148		97905		98662	99041	9
8	99797				0601310		0602066		0602822	8
9	0603579	03956	04334	04712	05090	05468	05845	06223	06601	8
1150	07356	07734	08111	08489	08866	09244	09621	09999	10376	8 7 7 7 6 6
1	11131	11508		12262	12639	13017	13394	13771	14148	7
2		15279		16032	16409	16786	17163	17540	17916	7
3		19046		19799	20176	20552	20929	21305	21682	7
4	22434	22811	23187	23563	23939	24316	24692	25068	25444	6
5		26572		27324	27699	29075	28451	28827	29203	1 6
6		30330	30705	31081	31456				32958	6
6 7	33709		34460	34835		35585	35060	32583 36335	36711	50
8	37461					39335		40085	40460	, š
9	41209		41958			43082	43457		44205	5 5
- 1				***						
1160	44954		45703			46826	47200		47948	4
1	48696		49444		50192		50940		51688	4
2	52435		53182		53930			55050	55424	4
3	56171		56917		57664			58784	59157	3
4	59903	60276	60649	61022	61395	61768	62141		62886	3
5 6 7	63632	64005	64377	64750	65123	65495	65868	66241	66613	4 4 3 3 3 2 2 2 1
6	67358	67730	68103	68475	68847	69220	69592	69964	70336	2
7	71081	71453	71825	72197	72569	72941	73313	73685	74057	2
8	74800	75172	75544	75915	76287	76659	77030	77402	77774	2 ;
9	78517	78888	79259	79631	80002	80374	80745	81116	81487	1
1170	82230	99601	82972	03343	83714	04005	84456	04007	85198	
11.10	85940		86681		87423		88164		88906	1
ŗ			90388							Ô
2	89647 93350	03701	94091		91129 94831		91869 95571		92610	ő
3	97051			98160					96311	ő
						98900	99270		0700009 03704	
5										
6	04442		05181		05919		06658		07396	9
7	08134		08871		09609		10347		11084	9
8	11822		12559			13664	14033		14770.	9
9	15506	19849	16243		16979	17348	17716	18084	18452	
1180	19188	19556	19924		20660	21028	21396	21763	22131	8
1	22867	23234	23602	23970	24337	24705	25072	25440	25807	8 :
2	26542		27277	27644	28011		28746	29113	29490	7
3	30215		30949			32050		32783	33150	9877766
4.		34251	34617	34984	35351		36084	36450	36817	7
51	37550	37916	38283	386491	39016	393821	39749	40114	404811	6
6	41213	41579	41945	42311	42677	43043	43409	43775	44141	6
7	44873		45605	45970		46702	47068		47799	6
8	48530	48895	49261	4962v	49902	50357	50723	51088	51453	6 5 5
9	52184		52914		53644			54740	55105	5
1190	55835		£6564		57204			58388	59753	5
I	59482		60211		(0940			62034	62398	4
2	63127		63855		64584			65676	6€ 0 40	4
3	f 5768		67496		68224			69316	69680	4
4		70771			71852	72225	72589	72952	73316	4
6		74406		75133	75496	75859	76222	76585		3
6	77675			78764	79127	79490		80216	80579	3
7	81304		82030		82755			83843	84206	3
8	84931		85656		86330		87105	87467	87830	3 3 2 2
9	88554		89279	.89640	90003			91089	91451	2
	1	2	3	4	5	6	7	8	9	

[Table 1. Between $12000 = \log_{10}^{-1} 4.0791812$, and $12600 = \log_{10}^{-1} 4.1003705$.

	Betweer	1200	$0 = \log$	4·0	791812,	and 12	2600 = 10	og. Ti 4	1·1003705	Ď.
tens.	1	2	3	4	5	6	7	8	9 079 50 68	dif
[12 0 0]	0792174	92536	0792898	93260	0793622	93983	0794345	94707	0795068	362
1	95792	96153	96515	96876	97238	97599	97961	98322	98683	1
2	99406	99767	0800129	00490	0800851	01212	0801573	01934	0802295	1
3	0803017 06626	03378	03739 07347	04100	04461	04822 08429	05183	05543 09150	05904	1
4	06626	06986	07347	07707	09068	08429	08789	09150	09510	1.
5 6	10231	10591	10952	11312	11672	12032	12393	12753	13113	Ŏ
6		14193	14553	14913	15273	15633	15993		16713	0
7 8 9		17792	18152	18512	18871	19231	19591	19950	20310	0
8	21029	21388	21748	22107	22467	22826	23185	23545	23904 27495	359
9	24622	24981		25700		26418		27136	27495	9
210	28213	28571	28930	29289	29648	30007 33593	30365 33951	30724	31083	9
	31800	28571 32159	29517	22276	33234	33593	33951	34309	34668	9 8
2	35385	35743	36101 39682	36459	36817	37176	37534	37892	38250 41829	Ř
3	38966	39324	39682	40040	40398	40756	41114	41471	41829	8
1 2 3 4	42545	42902	43260	43618	36817 40398 43975	44333	44690	41471 45048	45405	8
		46478	46835	47192	47550	47907	48264	48621	48979	7
6	49693	50050	50407	50764	51121	51478	51835	52192	52549	7
7		53619	53976	54333	54690	55046	55403	55760	56116	7
5 6 7 8 9	56829	57196	57542	57899	58255	58612	58968	59324	59681	6
9		60750			61818	62174	62530	62886	63242	6
220		64310				65734		66445		-
	67510	67868	64666	00022	68935	60000	60646	70001	66801 70357	6 5 5
1 2 3	0/512	71423	68224 71778	08579	70400	72944	72100	73554	70357	0
2	74000	74075	71118	72133	76040	76205	76750	77104	73909	5
4	74020	74975	75330 79878	75085	70500	76395 79943	76750 80297	00000	77459 81006	0
2	78169	82070	13318	19233	02122	83488	00291	84196	01000	5
5		85613			00070	87030	07204	87738		4
2	00000	89153	85967	86321	00070	90569	00000	91276	01620	4
7 8				89801	02750		90923	04019	91630 95165	4
9		92691 96226				94105 97639		94812 98345		
-										3
230	99404	99757	0900110	00463	0900816	01169	0901522	01875	0902228	3
- 1	0902933	03286	03639 07164 10687	03991	04344	04697	05049			3
2	06460	06812	07164	07517	07869	08222	08574	08926	09279	2
	09983	10335	10687	11039	11392	11744	12096	12448	12800 16318	2
41	13504	13855	14207	14559	14911	08222 11744 15263	15614	15966	16318	3 2 2 2 2
5 6 7	17021	17373 20887	17724 21239	18076	18427 21941	18779	19130	19482	19833 23346	2
6	20536	20887	21239	21590	21941	22292	22644	22995	23346	1
	24048	24399	24750	25101	25452	25903	26154	26505	26856	1
8		27908		28609	28960	29311	29661	30012		1
9	31064	31414	31764	32115	32465	32816	33166	33516	33867	0
240	34567	34917	35267	35618	35968	36318	36668	37018	37368	0
	38068	38418	38768	39117	39467	39817	40167	40517	40866	ŏ
1 2 3 4	41566	41915	42265	42614	39467 42964	43313	43663	44012	44362	
3	45061	45410	45759	46109	46458	46807	47156	47506	47855	9
	48553	48902	49251	49600	49949	50298	50647	50996	51345	9
	52042	52391	52740	53089	53437	53786	54135			9
5 6 7	55529	55877	56226	56574	56923	57271	57620	57968	58316	8
	59013	59361	59709	60057	60406	60754		61450		Š
8		62842	63190	63538	63885	64233	64581	64929	65277	8
9	65972	66320	66667	67015	67363	67710	68058	68405	68753	8 8 8
1250		69795		70490		71184				
		73267	72614	70490	74200		75000	71879 75349	72226	
1			77004	77431	74309	74656	70471	70017	75696	4
2 3 4	70057	76737	00550	00007	01949	78124	01020	78817	79164	1 4
3	63300	80204 83668	00000	80897 84360	01243	81590 85053	81936	82283 85745	82629 86091	۱ ,
	05322	03008	07/7	07001	04/07	85053	85399	00/45	86091	Ď
5 6 7 8	00040	87129 90588	00004	87821	88167	88513 91971	00010	89205	89551	þ
7	02600	94044	90934	91279 94735	91625	919/1	92316	92662 96116	93007	9
6	93098	07402	07040	00107	95080	95425 98877	95771	20110	96461	5
. 0	9/152	97497	91642	98187	96532	98877	99222	99007	99912	ı 5

1000602 00947 1001292 01637 1001982 02327 1002671 03016 1003361 1 2 3 4 5 6 7 8 9

5

96461 99912

_										
tena.	1004050	2	3	4	1000 100	G	1000110	8	9	dif.
1260		04395		08528	1005429				1000806 10249	345
1 2		11282		11970	08873 12314	12658	13002	09905 13346	13590	4
3		14721	15065	15409	15752	16096	16440	16784	17127	4
4		18168	18501	18845	19188	19532	19875	20219		3
51	21249	21592		22278	22621	22965		23651	239941	3
6	24680	25023	25366	25709	26052	26395	26739		27423	3
7	28109	28452		29137	29490	29822	30165	30507	30850	3322
. 8	31535			32562	32905	33247		33932	34274	2
9	34959	35301	35643	35985	36327	36669	37011	37353	37695	2
1270	38379	38721	39063	39406	39747	46089	40430	40772	41114	2
1	41797			42822		43505	43847	44188	44530	
23		45554	45895		46578	46919	47260		479431	1
3		48966		49648	49089	50331		51012	51353	1
41		52376	52717	53058		53739	54050		54761	1 0
5 6	58847	557831		56464 59868		57145 60548		57526	58166 61569	0
7	62249	62589		63269		63049	64289	61229 64629	64969	ő
8	65648		66328		67007		67687	68026	09366	0
9	69045			70063	70403	70742	71082	71421	71760	339
1290	72439		73117			74135		74613	75152	
2.000		76169	76509			77525		78203	78541	9
2		79558		80235		80912		81590	81928	9
3	82605			83620		84297	84635	84974	85312	
4	85986	86327	86665	87003	87341	87679	88017	86365	68693	88887777
51	99369	897071		90883		91059		91734	92072	B
$\tilde{6}$	92747	93085		93760		94435	94773		95488	8
7	96123	96460	96798	97135	97472	97810	98147		98921	7
8	99496	99833	1100175		1100844		1101518		1102192	7
9	1102866	03203	03540	03877		04550	04987	05224	95560	7
1290	06234	06570	06907	07244	07590	07917	08253	08590	08926	7
1	09599	99935	10272	10608	10944	11280	11617	11953	12259	7
2	12961	13297	13633	13969	14306	14642	14977	15313	15649	6
3		16657	16993	17329	17664	18000	19336	19671	19007	6
4	19678	20014	20350	20685	21021	21356		22027	22362	6
ő		23368		24(139)		24709		25390	25715	5
6		26720		27390	27725	28060		28730	29065	5
7	29735	30069	30404		31074	3140F	31743		32412	5
8	33081 36426	33416 36760	33751	34065	34420	34754	35088		35757 39090	4
9	-			37429		38097		38765		4
1300		40102	50436	40770 44108	41104		41771	42105	42439	4
1 2		43441			44442			46443	45776	4
3	46443	50111		47444 50777	47777	841111 51444	48444 61777		49111 52443.	3
4		53442		54108		54774	55107	55439		3
5		5677L		57436		58101			590991	3 53 51 51 51 51 51
6	59764			60762		61427	61759		62424	2
7		63420		64085	64417	64749	650AL	65413	65745	2
S	66409		67073		67737	68069	68401	68733	69065	2
9	69728	70060	70392	70723	71055	71387	71718	72050	72381	2
1310	73044	73376	73707	74039	74370	74702	75033	75364	75696	1
1		76669	77021		77683	78014		78676	79007	1
20		80000	80331	80662	80993	81324		81986	82316	î
3	82978	83309		83970	84301	84631		85293	85623	1
4		86615		87276	87606	87936	88267		88927	0
5		89918				91239			92229	0
6		93219		93879	94209	94539		55198	95528	0
7		96517	96847	97177		97836		98495	98925	200
8:		99813			120/1901	01131	1201460	01789	1202119	329
9	1202777	03406	03430	03765 4	1 14014	04423	1 14/52	01081	05410	9
	1	*	.,	4	4.5	**	. 4	-	# FF	

Between $13200 = \log^{-1} 4 \cdot 1205739$, and $13800 = \log^{-1} 4 \cdot 1398791$.

	Between	13200	$J = \log$.	4.12	910 139, a	ng 136	500 = 10	5. 4	1999 191	
tena.	1	12	34	*	- 5	6	7	H	9	dif
	1206068	06397			1207384	07713	1208042	08371	1208699	355
1		09686		10343		11000	11329		11986	9
3		12972		13628		14285° 17568		14942 18224	15270 18552	8
4	15927 1920d	16255 19536		16911 20192	20520		21175	21503	21931	8
51	22487	22814		23470				24780		8
6	25763		26418	26745		27400		28055	28382	8 7 7
7	29036		29691	30018		30672	31000	31327	31654	7
8	32308	32635	32062	33259		33942		34596	34923	7
9	35577	35903	36230	36557	36883	37210	37537	37863	38190	
1330	39943	39169	39496	39822		40475		41128	41454	6
1	42107	42433		43086		43738		44390	44716	6
2		45694	46020			46998		47650	47976	6
3		48953		49605		50256	50582	54162	51233 54487	5
51		52209 55463		52960 56114		53511 56764	53837	574141	57739	5
6		58715	59040		59690		60339		60989	5
7		61964		62613		63263		63912	64237	5
8		65210		65859		66508	66833		67481	4
9		68454	68779		69427	69751	70076	70400	70724	4
1340	71372	71696	72020	72344	72668	72992	73316	73640	73964	4
1	74612	74935		75583	75907	76230		76878	77202	4
3	77849	78172	78496	78819		79466		80113	80437	4]
3	91083			82053		82700		93346	83670	3
41		84639	84962		85609		86254		B6900	3
6		87369		88614		89160	99483 92709	89805	90128 93354	3
7	90773 93998		91418	94965	95288	92386 95610		96255	96577	3 2 2
8	97221			98187		98832		99476	99798	2
9					1301729				1303016	2
1350	03659		04303		04946		05589		06232	2
1	06875			07839		08482	08803		09446	1
2		10409		11052		11694		12336	12657	1
3		13620	13941	14262		14903		15545	15866	1
41		16828		17469		18111	18431	18752	19072	1 9
5	19713		20354	20675		21316	21636	21956	22277	0
6.	22917	23237		23979		24518 27718	24838	25158 28358	25478 28678	0
8	26119 29317	29637	26758 29957	27078 30277		30916		31555	31975	0
9:	32514			33473		34112	34431		35070	
1360		36029	36347			37305		37943	38262	9
1300	38900			39857		40495		41133	41452	9
2		42409				43684		44321	44640	9
3.		45596		46233		46870		47507	47825	8
4	49462	48780	49099	49417	49735	50054		50690	51008	
5		51963		52599		53235		53371	54199	8
6	54825			55779		56414		57050°	57367	8
7	58003			59956	59273		59908	60226 63400	60543 63717	7
9	61178	64669	61913 64986			62765 65937		66572	66889	7
									70058	
1370	67523 70691	67840 71008	68157 71325	68473 71641	68790 71958		69424 72591	69741 72908	73225	7
2	73958			74807	75124		75756	76073	76389	6
3		77338		77970	79287	78603		79235	79551	6
4		80499			81447		82079	82395 -	82711	6
51	83343	83659		84290	84606	84922	85237		85869	6
6	86500	86816	87131	97447		88078	88393		89024	5
7		89970		90601	90916	91231	91547	91862	92177	5
8	92807			93753		94383 97532		95013 96161	95328 98476	5
9	95958	96272	96587 3	96902	9/21/	91532	97647	30101	98470	0
		4	43	-	13	43	-		4.5	1

	le 1.]				NUMBER					25		
•	Between 13800 = log1 4·1398791, and 14400 = log1 4·1583625. 18. 1											
tens.	1300106	200420	1300725	4	1400264	00670	1400002	01200	1401622	dif.		
1	1402251	02566	1402880	03195	03509	03823	04138	04452	04766	315		
2	05395	05709	06023	06337	06651	06966	07280	07594	07908	4		
3	08536	08850	09164	09478	09792	10106	10419	10733	11047	4		
5	11675	11988	12302	12616	12930	13243 16379	13557	13871	14184	4		
6		15125 18259		15752 18885	19199	19512	19825	17006 20138	17319 20451	3 3 3 3		
7	21078	21391	21704	22017	22330	22643	22956	23269	20451 23582 26710	3		
8	24208	24520	24833	25146 28273	25459	22643 25772	26084	23269 26397	26710	3		
9	27335	27648	27960	28273	28586	28898	29211	29523	29836			
1390	30460	30773	31085	31398 34520	31710	32022 35144 38264 41381 44497	32335	32647 35768	32959 36080	2 2 2 1		
1		33896	34208	34520	34832	35144	35456	35768	36080	2		
3		37016 40135	37328	37640	37952	38264	38576	38888	39199	2		
41	42939	43251	43562	40758 43874	44185	41381 44497	44868	45119	42316 45431 48543	ĩ		
5 6		46365	46676	46987	47298	47610	47921	48232	48543	ı i		
6	49165	49476	49787	46987 50098	50409	507201	51031	51342	51653	1		
7		52586	52897	53207	53518	53829	54140	E4450	54761	1		
8 9	55382	55693 58798	50004	56314 59419	56625	53829 56935 60039	67246	57550 60660	57867			
			99100	09419	09129	00039	00350	00000	60970			
1400		61901 65001	65211	65621	62831 65931 69029 72124 75217 78308 81397 84484 87569 90651	66241	60551	66661	64071 67170	0		
2	67790	68100	68409	68719	69029	60338	69648	69958	70267	0		
3	70886	71196	71505	71815	72124	72434	72743	73052	73362	309		
4	73990	74290	74599	74908	75217	75527	75836	76145	76454	9		
5 6 7	77072	77381	77690	77999	78308	78617	78826	79235	79544	9		
7	80162	80471	90780	81089	81397	81706	82015	82324	82632	9		
8	86335	83558	96052	97260	97560	94/93	89195	89403	88809	9		
: ğ		89726	90035	90343	90651	90959	91267	91575	70267 73362 76454 79544 82632 85716 88802 91883	8		
1410	02400	92207	93115	03423	02721	04030	04347	04655	0.4069	8		
1	96578	95886	96193	96501	96809	97116	97424	97732	98039	8		
2	98655	98962	99270	99577	99885	00192	1500499	00807	1501114	7		
3	1501729	02036	1502344	02651	96809 99885 1502958 06030	03265	03573	03880	04187	8 7 7 7 7 6		
5	04801	05108	00405	00702	00000	06337	00044	10019	102257	4		
6		08178 11246	11000	11859	12166	09406 12472	12770	13085	10326 13392	7		
6	14005	14311	14618	14924	15231	15537	15843	16150	16456	6		
8	17069	17375	17681	17987	18293	18600	18906	19212 22272	19518 22578	6		
9	20120	20136	20742	21048	15231 18293 21354	21660	21966					
1420	23189	23495 26552	23801	24107	24412	24718 27774 30828 33880 36929	25024	25329 28385	25635	6 5 5 5		
1			26858	27163	27469	27774	28080	28385	28691	6		
3		29607 32659	29912	30217	30523	30828	31133	31439 34490	31744	b		
4	35405	35710	36015	33270 36320	36625	33880 36929	37234	37539	34795 37844	5		
	38453	35710 38758	39063	39368	39672	39977 43022	40281	40586	40901	. 5 i		
6	41500	41804	42109	42413	42718	43022	43327	43631	43935	5		
7		44848	45153	45457	45761	46065 49106	46370	46674	43935 46978 50018	4		
8 9		47890 50930	48194	48498 51538	48802 51042	52145	52440	49714 52753	53057	4		
1					51042 54070	D2190	FEAGE			- 1		
1430		53968 57003	57207	54575 57610	57014	55182 58217 61249 64280 67308	58520	55789 58824	59127	1 3 1		
2	59733	60037	60340	57610 60643	60946	61249	61553	61856	62159	3		
3	62765	63068	63371	63674	63977	64280	64583	64886 67914	65189	3		
4	65794	63068 66097	66400	66703	67006	67308	67611	67914	68216	3		
1 5	68822	69124 72149	69427	69729	70032	70334	70637	70939	71242 74265	3		
2 3 4 5 6 7 8 9	71847	72149 75172	69427 72452 75474 78496 81513	75776	76070	67308 70334 73359 76381 79401 82418	76602	70939 73963 76985 80004 83022	74265 77287	2		
8	77891	78193	78496	78797	79099	79401	79702	80004	80306	2		
9	80910	78193 81 21 2	81513	81815	82117	82418	82720	83022	80306 83323	21		
]	1	2	3	4	5	6	7	8	9			

D

26		LOGAR	I'THMS (F NU	MBERS I	ROM 1	то 36,	000.	[Tab	le 1.
	Between	14400	$= \log$.	-1 4-15	58 3625 , 8	nd 15	000 = 10	g1 4	1760913	3.
tens.	1	2	3	4	5	6	7			
1440		4223	1584530	4831	1585133		1585736	6037	1586338	301
1 2	6941 9954	7243	7544 1590556	7845 0857	8146 1591158	8448	8749 1591760	9050 2061	9351 1 5 92362	1 1
3	1592964	3265	3566	3867	4168	4469	4770	5070	5371	î
4	5973	6273	6574	6875	7175	7476	7777	8077	8378	1
5	8979	9280	9580	9881			1600762		1601383	1 0
6	1601993	2284	1002584 5586	2884 5883	3184 6186	3485 6486	3785 6786	4085 7086	4385 7386	ŏ
9	498 5 7986	5286 8285	8585	8885	9185	9495	9785	0084		Ŏ
9	1610984	1283	1611583	1883	1612182		1612781	3081	3380	0
1450	3980	4279	4578	4878	5177	5477	5776	6075	6375	0
1	6973	7273	7572	7871	8170	8470	8769	9068	9367	299
2	9965	/ 0264			1621161	1460	1621759 4748	2058	1622357 5345	9
3	1622955 5943	3254 6241	3553 6540	3852 6839	4150 7137	4449 7436	7734	5047 8033	8331	9
5	8928	9227	6540 9525	9824	1630122		1630719	1017	1631315	. 8
6	1631912	2210	1632503	2807	3105	3403	3701	3999	4297	8
7	4894	5192	5490	5788	6086	6384	6682	6979	7277 1640255	8
8	7873 1640851	8171	8469 1 64 1446	8767 1743	9064 1642041	9362 2339	9660 1642636	9958 2934	3231	8
			4421		5016	5313	5610	5908	6205	7
1460	3926 6799	4123 7097	7394	4718 7691	7988	8285	8582	8880	9177	7
2	9771		1650365	0662		1256	1651553	1850	1652146	7
3	1652740	3037	3334	3631	3927	4224	4521	4817	5114	7
4	5707	6004	6301	6597	6894	7190	7487	7783	9090 1661043	7
5 6	8673 1661636	8969 1932	9265 1662228	9562 2525	9959 1662821	/3117	1660451 3413	3709	4005	6
7	4597	4893	5189	5185	5781	6077	6373	6669	6965	6
8	7556	7852	8148	8444	8740	9035	9331	9627	9922	6
9	1670514	0809	1671105	1400	1671696	1991	1672287	2582	1672878	6
1470	3469	3764	4060	4355	4650	4946	5241	5536	5831	5
1	6422	6717	7012	7308	7603	7998 0848	8193 1681143	8489 1438	8783 1681733	5
2 3	9373 1682322	9668 2617	9963 1682912	/ 0258 3207	1680553 3501	3796	4091	4386	4680	5
4	5269	5564	5859	6153	6448	6742	7037	7331	7626	5
5	8215	8509	8803	9098	9392	9686	9981		1690569	4
6	1691158	1452	1691746	2040	1692335	2629 5569	1692923		3511 6450	4
7 8	4099 7038	4393 7332	4687 7626	4981 7920	5275 8213	8507	5863 8801	6157 9094	9388	4
9	9975	0269	1700563	0856	1701150	1443	1701737	2030		4
1480	1702911		3497	3791	4084	4377	4671	4964	5257	3
1	5844	6137	6430	6723	7017	7310	7603	7896	8189	3
2	8775	9068	9361	9654	9947	, 0240		0826	1711119	3
3 4	1711704 4632	1997 4924	1712290 5217	2583 5509	1712876 5802	/ 3168 6095	3461 6387	3754 6690	4046 6972	3
5	7557	7849	8142	8434	8727	90191	9311	9604		
6	1720480	0773	1721065	1357	1721649	1941	1722233	2526	1722818	2
7	3402	3694	3986	4278	4570	4862	5154	5446	5737	2
8	6321	6613	6905	7197	7488	7780	8072	8364	8655	2
9	9239	9530	9822		1730405		1730988	1280	1731571	- 1
1490	1732154 5068	2446 5359	1732737 5650	/ 3028 5941	3320 6233	3611 6524	3903 6815	4194 7106	4485 7397	1
2	7979	8270	8561	8852	9143	9434	9725	.0016	1740307	i
3	1740889	1180	1741471	1761	1742052	2343	1742634	/ 2925	3215	1
4	3797	4097	4378	4669	4959	5250	5540	5831	6121	0
5 6	6702 9606	6993 9897	7283 1750187	7574 0477		8155 1057		8735		0
7	1752508	2798	3089	3378	3668	3958	4248	4538	1751928 4828	ŏ
8	5408	5698	5988	6278	6567	6957	7147	7437	7727	0
9	8306	8596	9885	9175	9465	9754	1760044	0333	1760623	0
	1 1	5	3	4	5	6	7	8	9	<u> </u>

Between $15000 = \log^{-1} 4.1760913$, and $15600 = \log^{-1} 4.1931246$.

_										
tens.	1 1	2	3	4	5	6	7	8	9	dif.
1500	1761202	1492		2071	1762360	2649	1762939	3228	1763518	289
1	4096	4386	4675	4964	5253	5543	5832	6121	6410	9
2	6988	7278	7567	7856	8145	8434	8723	9012	9301	9
3	9879	0168	1770457	0745		1323		1901	1772190	9
4	1772767	3056	3345	3633	3922	4211	4499	4788	5076	9
5		5942	6231	6519		7096	7386	7673		- 8
6	8538	8826	9115	9403	9691	9960	1780268	0556	1780844	В
7	1781421	1709	1781997	2285	1782573	2361	3149	3437	3725	8
8	4301	4589	4877	5165	5453	5741	6029	6317	6605	8
9	7180	7468	7756	8043	8331	8619	8907	9194	9482	8
1510:	1790057	0345	1790632	0920	1791207	1495	1791782	2070	1792357	
1	2932	3219	3507	3794	4082	4369	4656	4943	5231	8 7 7 7
2	5805	6092	6389	6667	6954	7241	7528	7815	8102	7
3	8676	8963	9250	9537	9824	/ 0111	1800398	0685	1800972	7
4	1801546	1832	1802119	2406	1802693	2980	3266	3553	3840	7
5	4413	4700	4986	5273		5846	6133	6419		7
6	7278	7565	7851	8138	8424	8711	8997	9283	9570	7 7 6
7	1810142	0428	1810715	1001	1811287	1573	1811859	2145	1812432	6
8	3004	3290	3576	3862	4148	4434	4720	5006	5292	6
9	5864	6150	6435	6721	7007	7293	7579	7864	8150	6
1520				-						
	8722	9007	9293	9579	9864	/0150	1820435	0721	1821007	6
1	1821578	1863	1822149	2434	1822720		3290	3576	3861	6
3	4432	4717	5002	5288	5573	5858	6143	6429	6714	5
	7284	7569	7854	8140	8425	8710	8995	9280	9565	5
4	1930135	0420	1830704	0989	1831274	1559	1831844	2129	1832414	
5	2983	3268	3553	3937	4122	4407	4691	4976		5
6	5830	6114	6399	6684.	6968	7253	7537	7822	8106	5
7 8	8675	8959	9244	9528	9812	/ 0096	1840381	0665	1840949	4
	1841519	1802	1842086	2370		2939	3223	3507	3791	4
9	4359	4643	4927	5211	5495	5779	6063	6347	6630	4
1530	7198	7482	7766	8050	8333	8617	8901	9186	9468	4
1	1850036	0319	1850603	0886	1851170	1454	1851737	2021	1852304	4
2	2871	3155	3438	3721	4005	4288	4572	4855	5138	3
3	5705	5988	6271	6555	6838	7121	7404	7687	7970	3
4	8537	8820	9103	9386	9669	9952	1860235	0518	1860801	333222
5	1861367		1861932	2215		2781	3064	3347	3629	3
6	4195	4478	4760	5043	5326	5608	5891	6174	6456	3
7	7021	7304	7586	7869	8151	8434	8716	8999	9291	2
8	9846	0128	1870410	0693		1257	1871540	1822	1872104	2
9	1972668	2951	3233	3515	3797	4079	4361	4643	4925	
11540	5489	5771	6053	6335	6617	6899	7181	7463	7745	2
1	8308	8590	8872	9154	9435	6717	9999	/ 0290	1880562	2
2	1831125	1407	1881689	1970	1882252	2533	1882815	3096	3378	2 2
3	3941	4222	4504	4785	5066	5348	5629	5910	6192	1
4	6754	7035	7317	7598	7879	9160	9441	8723	9004	1
51	9566	9847	1890128	0409	1890690	09711		1533		1
3	1892376	2657	2938	3218	3499	3780	4061	4342	4622	1
7	5184	5465	5745	6026	6307	6587	6868	7148	7429	1
В	7990	8271	8551	8832	9112	9393	9673	9953	1900234	0
9	1900795		1901355	1636	1901916	2196	1902476	2757	3037	0
1550	3597	3877		4439		4998		5558	5838	0
			4157	7238	4718		5278			0
1	6398	6678	6958	7238	7518	7799	8078	9357 1155	8637 1911435	0
2 3	9197	9477 2274	9757	2833	1910316	0596 3392	1910876		4231	0
4	1911994	5060	1912553 5348	5628	3113 5907	6187	3672 6466	3951 6745	7025	
	4790	78621		8421	8700	8979		9538		9
5	7583 1920375	0654	8142				1922049	2328	1922607	9
6 7		3444	1920933 3723	1212 4002	4281	1770 4559	4938	5117	5396	9
8	3165 5953	6232	6511	6789	7068	7347	7625	7904	8193	9
9	8740	9018	9297	9575	9854	10132	1930411	0689	1930968	9
2	1 8/40	2010	3	4	5004	6	1930411	B	1930900	3
			439	-	9	U		107	1	

Between $15600 = \log_{-1} 4.1931246$, and $16200 = \log_{-1} 4.2095150$.

tena.	1 1	2 1	3	4	5	6	7	8 1	9	dif.
1560	1931524		1932081		1932638		1933194		1933751	278
	4307	4585	4864	5142	5420	5698	5976	6254	6532	8
1 2	7088	7366	7644	7922	8200	8478	8756	9034	9312	8
3	9868			0701		1257	1941534	1812		8
4	1942645	2923	3200	3478	3756	4033	4311	4599	4966	8
5	5421	5698	5976	6253	6531	6808		7363	7640	7 7 7 7
6	8195	8472	8749	9027	9304 1952075	9581 2353	9858 1952630	/ 0136 2907	1950413 3184	2
7 8	1950967 3739	1244 4014	1951521 4291	1798 4568	1952075	5122	1952630	5676	5953	7
9	6506	6783	4291 7060	7336	7613	7890	8167	8443	8720	7
1570		9550			1.	0656	1960932	1209	1961485	
1570	9273 1962038	2315	9826 1962591	/ 0103 2867	1960379 3144	3420	3697	3973	4249	7
2	4802	5078	5354	5630	5907	6183	6459	6735	7011	6
3	7563	7839	8115	9391	8667	8943	9219	9495	9771	6
4	1970323	0599	1970875	1151	1971427	1702	1971978	2254	1972530	6
5	3081	3357	3633	3908	4184	4460	4735	5011	5287	6
6	5839	6113	6369	6664	6940	7215	7491	7766	8042	6
7	8592	8868	9143	9418	9694	9969		0520		5
8	1981345	1620	1981896	2171	1982446	2721	2996	3271	3546	5
9	4096	4371	4646	4921	5196	5471	5746	6021	6296	
1580	6846	7121	7395	7670	7945	8220	8495	8769	9044	5
1	9593	9869	1990143	0417	1990692	0967	1991241	1516	1991790 4535	4
3	1992339	2614	2888	3163	3437 6181	3712 6455	3986 6729	4260 7003		4
4	5083 7826	5358 8100	5632 9374	5906 8648	8922	9197	9471	9745	2000019	4
5	2000567	0841		1200	2001662	1936		2484	2758	1 4
6	3306	3679	3853	4127	4401	4674	4948	5222	5496	4
7	6043	6317	6590	6864	7137	7411	7684	7958	8231	4
8	8778	9052	9325		9872	, 0146	2010419	0692	2010966	3
9	2011512	1786	2012059	2332	2012605	/ 2979	3152	3425	3698	
1590	4244	4517	4791	5064	5337	5610	5883	6156	6429	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3
1	6975	7248	7521	7794	8066	8339	8612	8885	9158	3
2	9703	9976	2020249	0522	2020794	1067	2021340	1612	2021885	3
3	2022430	2703	2976	3248		3793		4338		3
4	5156	5428	5700	5973	6245	6518	6790	7062	7335	3
5	7879	8151	8424	8696	9969 2031689	9240	9512	9785 2505	2030057	9
6 7	2030601 3321	0873 3593	2031145	1417	2031689 4409	1961 4681	2032233 4952	5224	2777 5496	2
8	6040	6311	3865 6583	4137 6855	7126	7399	7670	7941	8213	2
9	8756	9028	9299	9571	9842	,0114	2040395	0657	2040929	2
1600	2041471	1743	2042014	2285	2042557	2828	3099	3371	3642	1
1000	4195	4456	4727	4998	5269	5541	5812	6083	6354	
2	6896	7167	7438	7709	7980	8251	8522	8793	9064	1
3	9606	9877	2050148	0419		0960	2051231	1502	2051773	1
4	2052314	2585	2856	3127	3397	3668	3939	4209	4480	1
5	5021	5292	5562	5833	6103	6374		6915		1
6	7726	7996	8267	8537	8807	9078	9348	9618	9899	0
7	2060429	0699	2060969	1240	2061510	1780		2320		0
8	3131	3401	3671	3941	4211	4481	4751	5021	5291	0
9	5830	6100	6370	6640	6910	7180	7449	7719	7989	0
1610	8529	8798	9068	9338	9607	9877	2070147	0416	2070686	0
1 2	2071225	1495	2071764	2034	2072303	2573 5267	2842 5536	3112 5805	3381 6074	269
3	3920 6613	4189 6882	4459 7151	4728 7421	4997 7690	7959	5536 8228	8497	8766	9
3 4	9304	9573	9842	.0111			2080918	1187		9
5	2081994	2263			3070	3338		3876		9
6	4682	4951	5220	5489	5757	6026	6294	6563	6832	9
7	7369	7637	7906	8174	8443	8711	8980	9248	9517	9
8	2090054	0322	2090590	0859		1395	2091664	1932	2092200	8
9	2737	3005	3273	3541	3810	4078	4346	4614	4882	8
	1_1_	2	3	4	5	6	7	8	9	

Between $16200 = \log_{\bullet} -1 4.2095150$, and $16800 = \log_{\bullet} -1 4.2253093$.

9			u = rog.		, 00100		900 = 10			
lens.	0005410	2	3	4 coon	5000,100	6	I T	8	9007500	dif.
1620 1	2095419 8098	8366	2095954 8634	8902	2096490 9170	6758 9437	2097026 9705		2097562 2100241	268
2	2100776	1044	2101312	1579	2101847	2115	2102382		2918	8
3	3453	3720	3988	4255	4523	4790	5058		5593	R
4	6129	6395	6662	6930	7197	7464	7732		8266	B 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
5	8801	9068	9335	9603		10137	2110404	0671		7
6	2111472	1740	2112007	2274	2112541	2808	3075		3609	7
7	4142	4409	4676	4943	5210	5477	5744		6277	7
8	6811	7078	7344	7611	7878	8144	8411	8678	8944	7
9	9477	9744	2120011	0277	2120544	0810	2121077	1343	2121610	
1630	2122142	2409	2675	2942	3209	3474	3741	4007	4273	6
1	4806	5072	5338	5605	5871	6137	6403	6669	6935	66666655555
2	7468	7734	8000	8266	8532	8798	9064	9330	9596	6
3	2130128	0394	2130660	0926	2131191	1457	2131723		2132255	6
4	2786	3052	3318	3584	3R49	4115	4381	4646	4912	6
5 6	5443	5709	5974	6240	6505	6771	7037	7302	7568	6
6	8098	8364	9629	8895	9160	9425	9691	9956	2140221	5
7	2140752	1017	2141293	1548	2141813	2078	2142343	2609	2874	5
8	3404	3669	3934	4199	4464	4730	4995	5260	5525	b
	6055	6319	6584	6849	7114	7379	7644		81743	
1640	8703	8668	9233	9498	9762		2150292	0556	2150821	5 4 4 4
1	2151350	1615	2151980	2144	2152409	2673	2938		3467	. 5
3	3996	4260	4525	4789	5054	5318	5583		6111	4
4	6640	6904	7169	7433	7697	7961	8226 2160867	6490 1131	8754 2161395	4
61	9282 2161923	9546 2187	2162421	/ 0075	2160339	0603		3771	4034	4
6	4562	4826	5090	2715 5354	2979 5617	3243 5881	6145		6672	4
7	7200	7463	7727	7991	8254	8518	8781	9045	9309	d
8	9836 /	0099	2170363	0626	2170890	1153	2171416	1680	2171943	3
9	2172470	2733	2997	3260	3523		4050	4313	4576	4 3 3
1650	5103	5366	5629	5892	6155		6682		7208	2
1	7734	7997	8260	8523	8786	9049	9312		9838	3
2	2180463	0626	2180889	1152	2181415	1677	2181940	2203	2182466	3
3	2991	3254	3517	3779	4042	4305	4567	4830	5092	3
41	5618	5890	6143	6405	6668	6930	7193	7455	7718	2
5	8242	8505	8767	9030	9292		9816		2190341	2
6	2190866	1128	2191390	1652	2191914	2177	2192439	2101	2963	2
7	3487	3749	4011	4273	4535	4797	5069	5351	5583	2
B	6107	6369	6631	6693	7155	7417	7679	7940	9202	2
9	8726	8987	9249	9511	9773	0034	2200296	0558		333322222222111111111111111111111111111
1660	2201342	1604	2201866	2127	2202389	2650	2912	3173	3435	2
1	3958	4219	4481	4742	5003	5265	5526	5788	€049	1
2	6571	6833	7094	7355	7617	7878	8139		9666 2211272	1
3	9184 2211794	9445 2055	9706 2212316	9967 2577	2210228 2838	0489 3099			3882	1
5	4403	4664	4925	5186	5446	5707	5968		6489	
6	7011	7271	7532	7793	8053	8314	8574	8835	9095	i
7	9617	9877	2220138	0398	2220658	0919	2221179	1440	2221700	ô
9	2222221	2481	2741	3002	3262	3522	3783		4303	0
9	4824	5084	5344	5604	5864		6384		6905	0
1670	7425	7685	7945	8205	8465	8725	8985	9245	9505	0
1010	2230024	0284	2230544	0904	2231064	1324	2231583	1843		ő
21	2622	2882	3142	3402	3661	3921	4181	4440	4700	Ö
3	5219	5479	5738	5998	6257	6517	6776		7295	0
4	7814	8073	8333	8592	8852		9370	9630		259
51	2240407	0667		1185	2241444	1704	2241963		2242481	P
6	2999	3258	3517	3777	4036	4295	4554	4813	5072	9
7	5590	5849	6107	6366	6625	6884	7143	7402	7661	9
8	8178	8437	8696	8955	9213		9731	9990	2250248	9 9
9.	2250766	1024	2251283	1541	2251800			2576	2834	9
	1	2	3	4	- 5	6	7	8	9	

							-	-		-
tens.	1	2	3	-	5	6	7	8	9	dif.
1680	2253351	3610	2253668	4127	2254385	4644	2254902	6160	2255419	258
1	6935	6194	6452	6710	6969	7227	7485	7743	8002	8
2	8518	8776	9034	9293	9551	9809	2260067	0325	2260583	8
3	2261099	1357	2261615	1873		2389	2647	2905	3163	8
4	3679	3937	4194	4452	4710	4968	5226	5484	5741	В
5	6257	6515	6772	7030	7288	7545	7803	8060	8318	8
6	8833	9091	9346	9606	9863	/0121	2270378	0636	2270893	8
7	2271408	1666	2271923	2180	2272438	2695	2953	3210	3467	8 7 7
8	3982	4239	4496	4753	5011	5268	5525	5782	6039	7
9	6554	6811	706B	7325	7582	7839	8096	8353	8610	7
1690							7		£	
	9124	9381	9638	9895	2280152	0409	2280666	0922	2281179	7 7 6
1	2261693	1950	2282206	2463	2720	2977	3233	3490	3747	7
2	4260	4517	4774	5030	5287	5543	5800	6057	6313	7
3	6826	7093	7339	7596	7852	8108	8365	8621	8878	
4	9390	9647	9903	/ 0159	2290416	0672	2290928	1185	2291441	6
5	2291953	2209		2722	2978	3234	3490	3746	4002	6
6	4515	4771	5027	5283	5539	5795.	6051	6307	6562	6
7	7074	7330	7586	7842	8098	8354	8609	8865	9121	6
8	9633	9888	2300144	0400	2300656	0911	2301167	1423	2301678	6
9	2302189	2445	2701	2956	3212	3467	3723	3978	4234	6
1700	4745	5000	5256	5511	5766	6022	6277	6532	6788	5
1700	7298	7554	7809	8064	8320	8575	8830	9085	9340	
2										5
	9851	/0106	2310361	0616		1126		1636	2311891	9
. 3	2312401	2656	2911	3166	3421	3676		4186	4441	5
4	4951	5206	5460	5715	5970	6225	6480	6734	6989	5
5	7499	7753	8008	8263	9517	8772		9281	9536	8
6	2320045	0299	2320554	0808	2321063	1317	2321572	1826	2322081	5
7	2590	2844	3098	3353	3607	3861	4116	4370	4624	4
8	5133	5387	5641	5896	6150	6404	6658	6912	7166	4
9	7675	7929	8183	8437	8691	8945	9199	9463	9707	4
1710	2330215	0469	2330723	0977	2331231	1495	2331739	1992	2332246	4
1	2754	3008	3262	3515	3769	4023	4277	4530	4784	4
2	5291	5545	5799	6052	6306	6559	6813	7067	7320	4
3	7827	8081	8334	8588	8841	9095	9349	9601	9855	72
4	2340362		2340868	1122	2341375	1629	2341681	2135	2342388	4555555
		0615		3664			4414		4920	3
5	2894	3148	3401		3907	4160		4667		d
6	5426	5679	5932	6185	6438	6691	6944	7197	7450	- 3
7	7956	8209	8462	8715	8967	9220	9473	9726	9979	3
8	2350484	0737	2350990	1243	2351495	1748	2352001	2253	2352506	3
9	3011	3264	3517	3769	4022	4274	4527	4779	5032	
1720	5537	5789	6042	6294	6547	6799	7052	7304	7556	2
1	8061	8313	8566	8818	9070	9323	9575	9827	2360079	2
2	2360594	0836	2361088	1340	2361592	1844	2362097	2349	2601	2
3	3105	3357	3609	3861	4113	4305	4617	4869	5121	2 2 2 2 2 2 2
4	5625	5876	6128	6380	6632	6884	7136	7387	7639	2
5	8143	8394	B646	9898	9160	9401	9653	99051		2
6	2370660	0911	2371163	1414	2371666	1917	2372169	2420	2672	2
7	3175	3426	3678	3929	4181	4432	4683	4935	5186	2
Ŕ	5689	5940	6191	6443	6694	6945	7196	7448	7699	1
9	8201		8703	8955			9708	9959	2380210	1
		8452			9206	9457				-
1730	2380712	0963	2391214	1465	2381716	1967	2382218	2469	2720	1
1	3222	3472	3723	3974	4225	4476	4727	4977	5228	1
2	5730	5980	6231	6482	6732	6983	7234	7484	7735	1
3	8236	8487	8737	8988	9239	9489	9739	9990	2390240	0
4	2390741	0992	2391242		2391743	1993	2392244	2494	2744	0
5	3245	3495	3746	3996	4246	4496	4747	4997	52471	0
6	5747	5998	6248	6498	6748	6998	7248	7498		Ö
7	8248	8498	8748	8998	9248	9498	9748	9998	2400248	0
8	2400748	0997	2401247	1497	2401747	1997	2402247	2496	2746	Ü
9	3246	3495	3745	3995	4244	4494	4744	4993	5243	0
. "	1	2	3	4	7.74	6	7	8	9	
-		-		-		-			12 1	

Between $17400 = \log^{-1} 4.2405492$, and $18000 = \log^{-1} 4.2552725$.

-										
tens.	1	2	1 3	4	6	6	1 7	8	9	dif
1740	2405742	5992	2406241	6491	2406740	6990	2407239	7489	2407738	250
1	8237	8487	8736	8985	9235	9484	9734	9963	2410232	249
2	2410731	0980	2411229	1479	2411728	1977	2412226	2476	2726	9
2	3223	3472	3721	3970	4220	4469	4718	4967	5216	9
4	5714	5963	6212	6461	6710	6959	7208	7457	7705	ğ
5	8203	8452		8950	9199	9447	9696		24201941	9
6	2420691	0940	2421189	1437	2421686	1935	2422183	2432	2680	9
7	3178	3426	3675	3923	4172	4420	4669	4917	5166	9
ŝ	5663	5911	6160	6408	6656	6905	7153	7401	7650	8
9	8146	8395	8643	8891	9139	9388	9636	9884	2430132	8
					0					
1750	2430629	0877	2431125	1373	2431621	1869	2432117	2365	2613	8
1	3109	3357	3605	3853	4101	4349	4597	4845	5093	B
2	5589	5837	6085	6332	6580	6828	7076	7324	7571	8
3	8067	8315	8562	8810	9058	9305	9553	9801	2440048	- 8
4	2440543	0791	2441039	1286	2441534	1781	2442029	2276	2524	8
5	3019	3266	3514	3761	4008	4256	4503	4750	4998	7
6	5492	5740	5987	6234	6483	6729	6976	7223	7470	
7	7965	8212	8459	8706	8953	9200	9448	9695	9942	7
81	2450436	0683	2450930	1177	2451424	1671	2451918	2165	2452411	7
9	2905	3152	3399	3646	3893	4140	4386	4633	4880	7
			r :							
1760	5373	5620	5867	6114	6360	6607	6854	7100	7347	7 7
1	7840	9087	8333	8580	8826	9073	9320	9566	9813	7
2	2460306	0552	2460798	1045	2461291	1539	2461784	2030	2462277	6
3	2769	3016	3262	3508	3755	4001	4247	4493	4740	6
4	5232	5478	5724	5970	6217	6463	6709	6955	7201	6
5	7693	7939	8185	8431	8677	8923	9169	9415	9661	6
6	2470153	0399		0891	2471136	1382	2471698	1874	2472120	6
71	2611	2857	- 3103	3349	3594	3840	4086	4331	4577	6
8	5068	5314	5559	5805	6051	6296	6542	6787	7033	6
9	7524	7769	8015	8260	8506	8751	8997	9242	9487	5
1770	9978	/0223	2490469	0714	2480959	1205	2481450	1695	2481940	5
1	2482431	2676	2921	3166	3412	3657	3902	4147		5
	4882	5127	6372	5617	5862	6107	6352	6597	4392 6842	5
3	7332	7577	7822		8312	8557	8802			0
4	9781	/ 0026		8067				9047	9291	5
51	2492228	2473	2490271	0515	2490760 3207	1005	2491249 3696	1494	2491739	5
6			2718	2962		3451		3941	4185	
7	4674	4919	5163	5408	5652	5897	6141		6630	4
	7119	7363	7607	7952	8096	8340	8585	8829	9073	4
8	9562	9906	2500050	0294	2500539	0783	2501027	1271	2501515	4
9	2502004	2248	2492	2736	2980	3224	3468	3712	3956	4
1790	-4444	4688	4932	5176	5420	5664	5908	6151	6395	4
1	6893	7127	7371	7614	7858	B102	8346	8590	8833	4
2	9321	9564	9808	/ 0052	2510295	0539	2510783	1026	2511270	4
3	2511757	2001	2512244	2488	2713	2975	3218	3462	3705	3
4	4192	4435	4679	4922	5166	5409	5652	5996	6139	3
51	6625	6869	7112	7355	7599	7842	8085	8329	8571	3
6	9058	9301	9544	9787	2520030	0273	2520516	0759	2521002	3
7	2521489	1732	2521975	2218	2461	2703	2946	3189	3432	3
В	3918	4161	4404	4647	4889	5132	5375	5618	5861	3
9	6346	6589	6832	7074	7317		7802			3
						7560		8045	8288	
1790	8773	9016	9258	9501	9743	9986	2530228	0471	2530713	3
11	2531198	1441	2531683	1926	2532168	2411	2653	2895	3138	2
2	3622	3865	4107	4349	4592	4834	5076	5318	5561	2
3	6045	6287	6529	6772	7014	7256	7498	7740	7982	2
41	9466	8709		9193	9435	9677	9919	/ 0161	2540403	222222221
5	2540886	112B	2541370	1612	2541854	2096		2580	2822	2
6	3305	3547	3789	4030	4272	4514	4756	4997	5239	2
7	5722	5964	6206	6447	6689	6931	7172	7414	7655	2
8	8138		8621	8863	9104	9346	9587	9629	2550070	2
9	2550553			1277	2551519	1760	2552001	2242	2484	ĩ
~	1	2	3	4	5	6	7	8	9	4
_				*		-		C)		

LOGARITHMS OF NUMBERS FROM I TO 36,000. [Table 1.] Between 18000 = log. - 4 2552725, and 18600 = log. - 4 2695129.

tens,	1	2	3	4	5	63	1 7	8	9	dif.
1800		3208		3690		4172	2554414	4655	2554896	241
1	5378	5619	5860	6102	6343	6584	6825	7066	7307	1
3	7789	8030 0439	8271	8512	8753	8994	9235	9475	9716	1
4	2560198 2606	2847	2560680 3087	0921 3329	2561161 3569	1402 3810	2561643 4050	1884 4291	2562125 4531	1
5	5013	5253		5734	5975	6215	6456	6696	6937	1
6	7418	7658	7899	8139	8380	8620	8866		9341	Û.
7	9922	0062	2570302	0543	2570783	1023	2571264	1504	2571744	0
8	2572224	2465	2705	2945	3105	3425	3665	3905	4146	
9	4626	4866	5106	5346	5586	5826	6066	6306	6546	0
1910	7026	7266	7506	7745	7985	8225	8465		8945	U
1	9424	9664	9904	70144	2580383	0623	2580863		2581342	(
2 3	2581822	2061	2582301	2541 4936	2780	3020	3259		3738	0
4	4218 6612	4457 6852	4697 7091	7330	5176 7570	5415 7809	5665 8048	5894 8288	6133	239
5	9006	9245		97231		0202	2590441	0680		9
6	2591398	1637	2591376	2115	2592354	2593	2832	3071	3310	9
7	3788	4027	4266	4505	4744	4983	5222		5700	9
8	6178	6417	6655	6894	7133	7372	7611	7849	8098	9 9
9	8566	8904	9043	9282	9521	9759	9998	/0237	2600475	
1820	2600952	1191	2601430	1668	2601907	2145	2002394	2622	2861	9
1	3338	3576	3815	4053	4292	4530	4769		5245	8
2	5722	5960	6199	6437	6675	6914	7152		7628	8
. 4	8105 2610486	9343 0725	\$591 2610963	8820 1201	9059 2611430	9296 1677	9534 3611915	9772 2153	2610010 2391	8
5	2867	3105		3580	3818	4056	4294	4532		0
6	5246	5483	5721	5959	6197	6435	6672	6910	7148	8
7	7623	7861	8099	8336	8574	8811	9049	9287	9524	3
8	9999	/0237	2620475	0712	2620950	1187	2621425	1662	2621900	8
9	2622374	2612	2849	3087	3324	3562	3799	4036	4274	7
1830	4748	4986	5223	5460	5697	5935	6172	6409	6646	900000000000000000000000000000000000000
1	7121	4359	7595	7832	8069	8306	8543	8761	9018	1
2	9492	9729	9966	/ 0203	2630440	0677	2630914	1151	2631388	17
3	2631862 4230	2098 4467	2632335 4704	2572 4940	2809	3046	3283 5651	3520 5897	3757 6124	7
5	6597	68341	7071	7307	5177 7544	5414 7780	8017	8254	84901	7
6	8963	9200	9436	9673	9909	/0146	2640382		2640855	6
7	2641328	1564	2641801	2037	2642273	2510	2746	2982	3219	6
8	3691	3928	4164	4400	4636	4973	5109	5345	5581	6
9	6053	6290	6526	6762	6993	7234	7470	7706	7944	
1840	8414	8650	8886	9122	9359	9594	9830	10066	2650302	6
1	2650774	1010	2651246	1481	2651717	1953	3652189	2425	2660	6
2 3	3132	3368	3604	3839	4075	4311	4546	4782	5018	6
4	5499 7845	5725 8090	5960 8316	6196) 8551	6431 8787	6667 9022	6903 9257	7138 9493	7374 9728	6
5	2660199	0434	2660670	0905		1376	2661611	1846		5
6	2552	2787	3023	3258	3493	3728	3963	4199	4434	5 5 5 5
7	4904	5139	5374	5609	5844	6080	6315	6550	6785	5
8	7255	7490	77:25	7960	8195	8429	8664	6899	9134	5
9	9604	9839	2670074	0305	2670543	0778	2671013	1248	2671483	5
1850	2671952	2197	2421	2656	2891	3126	3360	3595	3630	5
1	4299	4533	4768	5003	5237	5472	5706	5941	6175	5
2 3	6644	6879	7113	7349	7582	7817	8051	8285	8520	4
4	8969 2681332	9223 1566	9467 2691900	9692	9926 2682268	$\frac{10160}{2503}$	2680394 2737	0629 2971	2680863 3205	4
5	3673	3907	4141	4376		4844	5078	5313	5546	4
6	6014	6248	6492	6716	6950	7183	7417	7651	7885	4
7	8353	8587	8821	9054	9298	9522	9756	9990	2690223	4
8	2690691	0925		1392	2691626	1859	2692093	2327	2560	4
9	3028		3495	3728	3962	4195	4429		4896	4
	1 1	2	3	+	5	6	7	8	9	

Between $18600 = \log^{-1} 4.2695129$, and $19200 = \log^{-1} 4.2833012$.

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cns.	1	2	3	4	5	6	7	8	9	dif. 233
1860	2695363	5596	2695830	6063	2696297	6530	2696764	6997	2697230	233
1	7697	7930	8164	8397	8630	8864	9097	9330	9564	3
2	2700030	0263	2700496		2700963	1196	2701429	1662	2701895	3
2 3 4	2362 4692	2595 4925	2828 5158	3061 5391	3294 5624	3527 5857	3760 6090	3993 6323	4226 6555	3
4	7021	7254	7487	7720	7953	8185	8418	8651	8884	3
5	9349	9582	9815	. 0047	2710290	0513	2710745	0978	2711211	3
7	2711676	1908	2712141		2606	2839	3071	3304	3536	3
į	4001	4234	4466	4699	4931	5163	5396	5628	5861	2
9	6325	6558	6790	7022	7255	7487	7719	7952	8184	33333333
1870	8648	8881	9113	9345	9577	9809	2720041	0274	2720506	2
1	2720970	1202	2721434	1666	2721898	2130	2362	2594	2826	2 2 2 2 2 2 1 1 1
2	3290	3522	3754	3986	4218	4450	4682	4914	5146	2
3	5610	5841	6073	6305	6537	6769	7001	7232	7464	2
4	7928	8159	8391	8623	8854	9086	9318	9549	9781	2
5 6 7	2730244		273 0708	0939	2731171		2731634	1865		2
6	25 60	2791	3023	3254	3486	3717	3949	4180	4411	1
		510E	5337	5568	5799	6031	6262	6493	6725	1 1
8		7416	7650	7881	8112	8343	8574	8806	9037	1
_		9730	9961	/0192	2740423	0654	2740885	1116		
1880		2040	2742271	2502	2733	2964	3195	3426	3657	1 1 1 1
1	4119	4350	4581	4811	5012	5273	5504	5735		1
2		6658	6886 9195	7119	7350	7591	7811	8042		1
4		8964 1270	2751500	9426 1731	£656 2751961	9887	2750117	0348 2653	2750578 2883	Ö
5		3574	3805	4035	4235	2192 4496	2422 4726	4956		lő
6	5647	5877	6108	6338	6568	6798		7259		ŏ
7	7949	8179	£409	8640	8870	9100	9330	9560		0 0 0
ŕ		0480	2730710	0940	2761170	1400	2761630	1860		ŏ
9	2549	2779	3009	3239	3469	3699	3929	4158		0
1890	4843	5078	5307	5537	5767	5997	6226	6456	6686	0
1	7145	7375		7834	8063	8293	8523	8752		ŏ
2	9441	9670		/0129		0588		1047		Ŏ
3	2771736	1965		2424	2653	2882		3341	3570	229
4	4029	4258	4483	4717	4946	5175	5405	5634	5863	9
5 6 7	6321	6550		7009	7238	7467		7925	8154	9
6	8612	8841	9070	9299		9757	9986	,0215		9
7	2780902	1131	2781360	1589	2781818	2047	2782276	2504		9
9	3191	3420		3877	4106	4335		4792		9
	1	5707	1	6164		6622		7079		9999999888888888888
1900		7993		8450		8907	9136	9364		9
1	2790050	0278	2790506	0735		1192		1648		8
3	2333 4616	2562 4844		3018		3475		3931 6213		ğ
4	6898	7126	7354	5301 7582		5757 8038		8494		8
i		9406			12800090	0317		0773		. 8
ě	2801457	1685		2140		2596		3051		ă
1	3735	3962	4190	4418	4645	4873	5101	5328	5556	8
	6011	3962 6239	6467	6694		7149		7604		8
	8287	8514	9742	8969	9197	9424	9651	9879	2810106	7
1910	2810561	0788	2811016	1243	2811470	1698	2811925	2162	2380	7
	2834	3061	3299	3516	3743	3970	4197	4425	4652	
	5106				6014	6242		6696		7
	3 7377			8058	8285	8512		8966		7
	9646		2820100			0781	2821007	1234		7
1	5 282 1915 6 4182					3049		3502	3728 5995	4
	6 4182 7 6448					5315 7580		5768 8033	8260	4
	8 8712		9165			9844		0297		6
	9 2830976					2107		2560		6
	1	2	3	4	5	6	7	8	9	
										-

LOGARITHMS OF NUMBERS FROM 1 TO 36,000. [Table 1. Between 19200 = $\log^{-1} 4.2833012$, and $19800 = \log^{-1} 4.2965652$.

tens.	1	2	3	4	- 5	6	1 7	8	9	dif.
1920	2933238	3465		3917			2834595	4821	2835048	226
1	5500	5726	5952	6178	6404	6630	6856	7082	7308	6
2.	7760	7986	8212	8438	8663	8839	9115	9341	9567	6
3	2840019	0245	2840470	0696	2840922	1148	2841373	1599	2841825	6
4	2276	2502	2728	2953	3179	3405	3630	3856	4062	6655
6	4533 6789	4759 7014	4984 7239	5210	5435	5661	5896	6112	6337	6
7	9043	9268	9493	7465 9719	7690 9944	7916 70169	8141 2850394	8366 0620	8592	0
8	2851296	1521	2851746	1971	2852196	2422	2647	2872	2850945 3097	5
9	3547	3773	3998	4223	4448	4673	4898	5123	5348	6
1930	5798	6023	6248	6473	6698	6923	7148	7.0		
1	8048	8273	8497	8722	8947	9172	9397	7373 9622	7598 9846	6
2.	2860296	0521	2860746	0970	2861195	1420	2861644	1869	2862094	5
3	2343	2768	2993	3217	3442	3666	3891	4116	4340	5
4	4789	5014	5238	6463	5687	5912	6136	6361	6585	5
1	7034	7259	7493	7707	7932	8156		8605	8829	4
61.0	9:276	9502	9726	9951	2870175	0399	2870624	0848	2871072	4
1	2971520	1745	2871969	2193	2417	2641	2865	3090	3314	4
	3762	3986	4210	4434	4658	4882	5106	2330	5554	4
9	6002	6226	6450	6674	6398	7122	7346	7570	7793	4
1940	8241	8465	8689	8913	9136	9360	9594	9808	2880032	4
1	2980479	0703		1150	2681374	1596	2981821	2045	2269	4
3	2716	2939	3163	3397	3610	3934	4057	4261	4504	4
4	4952 7186	5175 7409	5399 7633	5622 7856	5845	6069	6292	6516	6739	3
. 5	9419	96431		/ 0039	9079 2990312	8303 0536	8526 3890759	9749 0982	8973 12891205	3
6	2891652	1875	2892098	2321	2544	2767	2990	3213	3436	3
6 7	3983	4106	4329	4552	4775	4998	5221	6444	5667	3
B	6112	63351	6558	6781	7004	7227	7450	7673	7896	3
9	8341	8564	. 9787	9010	9232	9455	9678	9901	2900123	44888888888
1950	2900569	0792	2901014	1237	2901460	1682	2901905	2127	2350	
1	2795	3018	3240	3463	3686	3908	4131	4353	4576	13 03 04 04 04 04 04 04 04 04 04 04 04 04 04
2	5021	5243	5466	5699	5910	6133	6355	6578	6800	2
3	7245	7467	7690	7912	8134	8356	8579	8801	9053	2
4	9468	9690	9912	/ 0135	2910357	0579		1023	2911245	2
5	2911690	1912		2356	2578	2900	3022	3244	3466	2
6 7	3911	4133	4355	4577	4799	5020	5242	5464	6686	2
8	6130 8349	6352 8570	6574 8792	6796 9014	7018 9236	7240 9458	7461	7683	7905	2
9	2920566	0788	2921009	1231	2921453	1674	9679 2921896	9901 2118	2920123 2339	2
										- 4
1960	2782 4997	3004 5219	3225 5440	3447 5662	3668	3890	4111	4333	4554	2
1 2	7211	7433	7654	7875	5883 8097	6105 6318	6326 8539	6547 8760	6769 8982	1
3	9424	9645	9867	/ 0088	2930309	0530	2930751	0973	2931194	1 1 1 1
4	2931636	1857	2932078	2299	2520	2741	2962	3193	3405	i
5	3847	40681	4289	4510	4730	4951	5172	5393		1
6	6056	6277	6498	6719	6940	7160	7381	7602	7823	1 1 1 1 1 1
7	8264	8435	8706	8927	9147	9368	9589	9810	2940030	ī
8	2940472	0692	2940913	1134	2941354	1575	2941795	2016	2237	1
9	2678	2898	3119	3339	3560	3780	4001	4221	4442	
1970	4983	-5103	5324	5544	5764	5985	6205	6426	6646	-0
1	7087	7307	7527	7749	7968	8188	9408	8629	8849	0
2	9299	9510	9730	9950	2950170	0390	2950610	0831	2951051	. 0
3	2951491	1711	2951931	2151	2371	2591	2811	3031	3251	0
4	3691 5891	3911 6111	4131 6331	4351 6550	4571	4791	5011	5231	5451	0
6	8089	8309	8529	8748	6770 8968	6990 9188	7210 9408	7430 9627	7650 9847	0
7	2960296	0506	2960726	0945	2961165	1385	2961604	1824	2962043	0
. 8	2482	2702	2922	3141	3361	3580	3800	4019	4238	219
1 9	4677	4897	5116	5336	5555	5774	5994	6213	6433	9
	1	2	3	4	3	41	7	B	9	"
	-			_		-				

Between $19800 = \log^{-1} 4.2966652$, and $20400 = \log^{-1} 4.3096302$.

В	etween .	13900	= 10g.	4.290	66652, ar	1d 204	UU == 10g		3096302.	
tens.	1	2	3 2967310	4	.5	6 1	7	8 1	2968626	tif.
1980	2966871	7091	2967310	7529	2967748	7968	2968187	8406	2968626	219
I	9064 2971256	92831	9502	9722	9941 2972132	/ 0160	2970379 2570 4760	0598	2970817	9
2 3	2971256 3446	1475 3665	2971694 3884	1913	2972132 ' 4322	4551 4541	4760	2789 4979	3008	a
41	3636	5854	6073	3103 6292	nhii	6730	6040	7168	5198 7386	9
	7824	80431	8261	8480	6511 8699 2980886	8918	6949 9136 2981323 3508	9355	95741	99999888
5 6 7	7824 2980011	9043 0230	2980448	8480 0667 2853	2980886	1104	2981323	1542	9574 2981760	9
71	2197	2416	2634	2853	3071	1104 3290	3508	3727	3945	8
8 9	4382	4601	4819	5038	5256	5474	5693 7876	5911	6129	8
	6566	6785	7003	7221	7439	7658	7876	8094	8313	
1990	8749	8967	9185 2991367	9404	9622	9840	2990058 2239	0276	2990494	8
1	2990931	1149	2991367	1585	2991203	2021	2239	2457	2675	8
2	3111 5291	3329	3547	3/65	3983 6162	42011	4419	4637	4855	8
2 3 4	7469	7607	7005	3765 5945 8123	6162 8340	6380 8558	6598 8776	6816 8994	7034 9211	Q
51	9647	98641	7905 3000082 2258 4433	0300	3000517	0735	20000053	1170	3001388	8
6	9647 3001823 3998 6172	2041	2258	2476	3000517 2693	2911	3000953 3128 5303 7476	3346	3001388 3563 5737 7911	8
7	3998	4216 6390	4433	4650	4868	5085	3128 5303 7476 9648	5520	5737	7
8	6172	6390	4433 6607 8780	4650 6824 8997	4868 7042 9214	7259	7476	7693	7911	7
24	8340,	8562	8780	8997	9214	9431	9048	9000	2010002	7
2000	3010517	0734	3010951	1168	3011386	1603	3011820 3990	2037 4207 6376	2254	7
11	2688	2905	3122	3339	3556	3773	3990	4207	4424	7
3	4858 7026	70/0	5291 7460	5508	5725	0110	6159	0376	6593 9760	7
4	0104	9411	5291 7460 9627 3021794 3959 6123	1017	5725 7893 3020061	0110	6159 8327 3020494	0711	3020927	7
51	3021360	1577	3021794	2010	2227	2443	2660	2876	30931	7
6	3526	3742	3959	2010 4175	4392	4608	4825	2876 5014	5257	6
7	3021360 3526 5690 7853	5906	6123 8286 3030448	6339	6556 8718 3030880	6772	4825 6988 9151 3031312	7204	5257 7421 9583 3031745	6
8	7853	8070	8286	8502	8718	8935	9151	9367	9583	6
9	3030016	0232	3030448	0664	3030880	1096	3031312	1528	3031745	8888888777 7777776666 66666655555 55555444444
2010	2177	2393	2609 4769 6927 9085 3041242	2825	3041 5200 7359 9516 3041673	3257	3473	3680	200%	6
1	4337 6496	4553	4769	4984	5200	5416 7575	5632 7790	5848	6064 8222 3040379	6
2	6496 8653 3040810	9960	0927	0201	0510	0720	0040	0160	3040270	6
4	3040810	1026	3041249	1457	3041672	1880	3042104	2310	2535	6
51	2966	3182	3397	3613	3828	4043	7790 9948 3042104 4259 6413	44741	4690	5
6	5121	E236	5559	3613 5767	5982	6198	6413	6628	6844	5
		7490	7705 9857 3052008	7920	8135	8351	8566 3050718 2869	0/01/	0990	5
8	9427	9642	9857	/ 0072	3050288	0503	3050718	0933	3051148 3299	5
	3051578	1/93	3032008	2224	2439	2054		3084	3299	6
2020		3944	4159 6308 8456 3060603 2749	4374	4589 6737	4803 6952	5018	5233	5448 7597 9744 3061891 4036	5
1 2	5878 8026	0093	0308	9671	0737	0100	7167 9315	0500	0744	Ď
3	3060174	0220	3060603	00/1	3061022	3100 1947	3061461	1676	3061901	K
4	8026 3060174 2320	2534	2749	2963	6737 8885 3061032 3178	3399	9315 3061461 3607	3821	4036	5
5	2320 4465 6609 8752 3070894	4679	4894	5108 7252	5322	5537	5751 7895 3070037 2178 4319	5966 8109	6180	4
6	6609	4679 6823	7037	7252	5322 7466	7680	7895	8109	6180 8323	4
7	8752	8966	9180	9394	9609	9823	3070037	0251	3070465	4
8 9	3070894	1108	3071322 3463	1536	3071750 3891	1964	2178	2392	2606 4746	4
9	3035	3249	1			4105	4319	4032		4
2030	5174	5388	5602	5816	6030	6244	6458	6672	6885	4
1 2	7313 9451	7527 9664	7741 9878	7954	8168	0512	3000722	8810 0947	9023 3081160	4
2 3 4	3081597	1201	9878 3082015 4150 6284 8418	1 2220	9449	2655	9960	3060	3081160 3296 5431 7564 9697	4
4	3081587 3723	3936	4150	4363	4577	4790	5004	5217	3296 5431	4
5	5858	6071	6284	6498	6711	6924	7138	7351	7564	3
6	7991	8204	8418	8631	8844	9057	9271	9484	9697	3
7	3090123	0337	3090550	0763	3090976	1189	3091402	1616	3091829 3969	3
5 6 7 8 9	2255 4385	8204 0337 2468 4598	2681 4811	2894 K094	3090976 3107 5237	3320	6458 8596 3080733 2869 5004 7138 9271 3091402 3533 8663	3746	3959 6089	44443333333
9	1 1	2	3	4	5	6	7	5876	9	3

Table 1.] LOGARITHMS OF NUMBERS FROM 1 TO 36,000. Between $21000 = \log_{10} 4.3222193$, and $21600 = \log_{10} 1.4.3344538$.

_	setween	21000			22193, ar		-		3344538	
21.00	3222400	2 2607	3222813	4	5 7000007	6	7	8	9	dif
1	4467	4674	4881	3020 5087	3223227 5294	3434	3223640	3847	3224054	207
2	6534	6740	6947	7153	7360	5501 7567	5707 7773	5914 7980	6121 8186	7 7
3	8599	8906	9012	9219	9425	9632	9838	0045	3230251	6
4.	3230664		3231077	1283		1696	3231902	2108	2315	6
5	2727	2934	3140	3346	3552	3759		4171	4377	1 6
6	4790	4996	5202	5408	5615	5821	6027	6233	6435	6
7	6R51	7058	7264	7470	7676	7982	8038	8294	8500	6
8	8912	9118	9324	9530	9736	9942	3240148	0354	3240560	6 6 6 6
9	3240972	1178		1589	3241795	2001	2207	2413	2615	
2110	3030	3236	3442	3648	3854	4059	4265	4471	4677	6
2	5088 7145	5294 7350	5499 7556	5705 7762	5911	6117	6322	6528	6734	6
3	9201	9406	9612	9017	7967 3250023	8173 0228	8378 3250433	8584 0639	8789 3250844	0
4	3251255	1461	3251666	1972	2077	2282	2498	2693	2838	B
51	3309	3514	3720	3925	4130	4336		4746	4951	665555555
6	5362	5567	5772	5978	6183	6398	6593	6798	700%	5
7	7414	7619	7824	8029	8234	8439	8644	8849	9055	5
8	9465	9670	9875	,0080	3260285	0490		0900	3261105	5
9	3261515	1719	3261924	2129	2334	2539	2744	2949	3154	5
2120	3563	3768	3973	4178	4393	4588	4792	4997	5202	5
1	5611	5816	6021	6226	6430	6635	6840	7044	7249	5
1 2 3	7658	7863	8068	8272	8477	8682	8886	9091	9295	5 5 5
3	9705	9909		0318	3270523	0727 2772 4915	3270932	1136	3271341	5
4	3271750	1954 3998	2158 4202	2363	2567	2772	2976	3181	3385	4
6	3794 5837	6041	6245	4407 6450	4611	4815	5020 7062	5224 7267	5428	4 4
7	7879	8083	8287	8492	6654 8696	6959 8900	9104	9308	7471 9512	4
B;	9920	,0124	3280328	0533	3280737	0941	3281145	1349	3281553	À
9	3281961	2165	2369	2572	2776	2980	3184	3388	3592	4
2130	4000	4204	4408	4612	4815	5019	5223	5427	5631	4
1	6038	6242	6446	3650	6853	7057	7261	7465	7668	4
2	8076	8279	8483	8687	8890	9094	9298	9501	9705	4
3	3290112	0316	3290519	0723	3290926	1130	3291334	1537	3291741	4
	2148	2351	2555	2758	2962	3165	3369	3572	3775	3
5	4182 6216	4396 6419	4589 6622	4792 6826		5199 7232	5402 7436	5606 7639	5809 7842	3
7	8248	8452	8655	8858	7029 9061	9264	9468	9671	9874	3
8	3300280	0483		0880	3301093	1296	3301499	1702	3301905	3
9	2311	2514	2717	2920	3123	3326	3529	3732	3935	3
2140	4341	4544	4747	4949	5162	5355	5558	5761	5964	444 4555555555555555555555555555555555
1	6370	6572		6979	7181	7384	7586	7789	7992	3
2	63 17	86C0	8903	9006	9208	9411	9614	9816	3310019	3
3	3310424	0627	3310430	1032	3311235	1437	3311640	1843	2045	3
	2450 4475	2653 4678	2855	3058	3261	3463	3666	3968	4070	2
5	6500	6702	4880 6904	5083 7107		5489 7511		5992	6095 8118	2
7	8523	8725	8927	9129	7309 9332	9534	7714 9736	7916 9938	3320141	2
8	3320545	0747	3320949	1151	3321354	1556	3321758	1960	2162	2
9	2566	2768	2970	3172	3374	3577	3779	3981	4183	2
2150	4587	4789	4991	5193	5304	5596	5798	6000	6202	3
1		6808	7010	7212	7414	7615	7817	8019	9221	3
	6606				9432	9633	9835	+0037	3330239	3
2	8624	8826		9230	110111111111	2000		& CALLES !		
2	8624 3330642	8826 0844	3331045	1247	3331449	1650	3331852	2054	2255	2
2 3 4	8624 3330642 2659	8826 0844 2860	3331U45 3062	1247 3263	3331449 3465	1650 3667	3331852 3868	2054 4070	2255 4271	1
3 4 5	8624 3330642 2659 4574	8926 0844 2860 4876	3331U45 3062 5077	1247 3263 5279	3331449 3465 5490	1650 3667 5682	3331852 3868 5883	2054 4070 6085	2255 4271 6286	3 3 2 1
23456	8624 3330642 2659 4574 6789	8926 0844 2860 4876 6890	3331045 3062 5077 7092	1247 3263 5279 7293	3331449 3465 5480 7495	1650 3667 5682 7696	3331852 3868 5883 7897	2054 4070 6085 8099	2255 4271 6286 8300	1 1 1
2 3 4 5 6	8624 3330642 2659 4574 6789 8703	9926 0844 2960 4876 6890 8004	3331045 3062 5077 7092 9106	1247 3263 5279 7293 9307	3331449 3465 5490 7495 9608	1650 3667 5682 7696 9709	3331852 3868 5883 7897 9911	2054 4070 6085 8099 0112	2255 4271 6286 8300 3340313	1 1 1 1 1
2 3 4 5	8624 3330642 2659 4574 6789	9926 0844 2960 4876 6890 8004	3331045 3062 5077 7092 9106 3341118	1247 3263 5279 7293	3331449 3465 5480 7495	1650 3667 5682 7696	3331852 3868 5883 7897	2054 4070 6085 8099	2255 4271 6286 8300	1 1 1 1 1 1 1

4

	Between	21600	= log.	4.33	14538, ar	rd 222	$200 = \log$	3, -14.	3463530	
tens.	3344739 6749	2	3	4	5	6	7	8	9	dif.
2160	3344739		3345141		3345543	5744	3345945	6146	3346347	201
	21 40	6950	7151	7351	7552	7763	7954	8155	9356	1
2	8758	8959	9159	9360	9561	9762 1770	9963 3351970	/0164 2171	3350364 2372	i
3	3350766	0967	3351168	1368 3375	3351569 3576	3777	3977	4178	4378	l il
	2773 4790	2974 4950	3175 5181	5381	5582	5782		6183		i
6	6785	6986	7186	7386	7587	7787	7988	8188	8389	200
7	8790	8990	9190	9391	9591	9791	9992	/0192	3360392	0
В	3360793	0993	3361194	1394	3361594	1795	3361995	2195	2395	0 3
9	2796	2996	3196	3396	3597	3797	3997	4197	4397	0
2170	4797	4998	5198	5398	5598	5798	5999	6198	6398	0
1	6798	6998	7198	7398	7598	7798	7998	8198	8398	0
2	8798	8998	9198	9398	9598	9798		/0198	3370397	0 :
3	3370797	0997	3371197	1397	3371596	1796	3371996	2196	2396	0 1
4	2795	2995	3195	3394	3594	3794	3994	4193	4393	0
5	4792	4992	5192	5391	5591	5791	5990	6190		0
6	6788	6989	7188	7387	7587	7786	7986	8185	8385	100
7	8784	8993	9183	9382	9592	9781	9981	/0180	3380379	199
8	3390778	0978	3391177	1376	3381576	1775	3381974	2174	2373 4366	9
9	2772	2971	3170	3369	3569	3768	3967	4166		
2180	4764	4963	5163	5362	5561	5760	5959	6158	6358	9
1	6756	6955	7154	7353	7552	7751	7950	8149	8348	9
2	B746	8946	9145	9344	9543	9742	9940	/0139	3390338 2327	9
3	3390736	0935	3391134	1333	3391532	1731 3719	3391930 3918	2129 4117	4316	9
4	2725	2924	3123	3322 5309	3520 5508	5707	5906	6104	6303	9
5	4713 6700	4912 6899	7098	7296	7495	7693	7892	8091	8289	9
7	8686	8685	9084	9282	9481	9679	9878		3400275	9
B	3400672	0870	3401069	1267	3401466	1664	3401862	2061	2259	198
9	2656	2854	3053	3251	3449	3648	3846	4045	4243	8
2190	4639	4838	5036	5234	5433	5631	5829	6027	6226	8
	6622	6920	7018	7217	7415	7613	7811	8009	8207	8
1 2	8604	►S802	9000	9198	9396	9594	9792	9990	3410188	8
3	3410584	0782		1178	3411376	1574	3411772	1970	2168	8
4	2564	2762	2960	3158	3356	3554	3752	3950	4147	8
5	4543	4741	4939	5137	5334	5532	5730	5928		8
6	6521	6719	6917	7114	7312	7510	7708	7905	8103	8
7	8498	8696	6894	9091	9289	9486	9684	9882	3420079	9
8	3420474	0672	3420870	1067	3421265	1462	3421660	1857	2055 4029	197
9	2450	2647	2545	3042	3240	3437	3635	3832		
2200	4424	4622.	4819	5016	5214	5411	5608	5806	6003	7
1	6399	6595	6792	6990	7187	7394	7581 9554	7779 9751	7976 9948	7
2	9370	8568	8765	9962	9159	9356 1328	3431525	1722	3431919	7
3	3430342 2313	0539 2510	3430736 2707	0933 2904		3298	3431525	3692	3889	7777777
5		4480	4677	4874		5268	5464	5661		7
6	6252	6449	6646	6842	7039	7236	7433	7630	7827	7
7	8220	9417	8614	8810	9007	9204	9401	9597	9794	7
8	3440187	0384	3440581	0777	3440974	1171	3441367	1564	3441761	7
9	2154	2350	2547	2743	2940	3137	3333	3530	3726	7
2210	4119	4316	4512	4709	4905	5102	5298	5495	5691	196
1 I	6084	6280	6477	6673	6869	7066	7262	7459	7655	6
2	8084	8244	8440	8636	6933	9029	9225	9422	9618	6
3	3450010	0207	3450403	0599	3450795	0991	3451188	1384	3451580	6
4	1972	2168	2365	2561	2757	2953	3149	3345	3541	
5	3933	4129		4522		4914	5110	5306	5502	6
6	5894	6090	6295	6481	6677	6873	7069	7265	7461	6
7	7853	8049	8245	8440	8636	8832	9028 3460986	9224 1182	9420 3461377	6
8	9811	/ 0007	3460203 2160	0399 2356	3460594 2551	0790 2747	2943	3138	3334	6
9	3461769	1964	3	4	5	6	7	8	9	
		~	-	•		**				-

Between $22200 = \log^{-1} 4.3463530$, and $22800 = \log^{-1} 4.3579348$.

lane.	-	-76		-	_					
2220	2400000	2	3	4	5	6	7	8	9	dif.
	3463725	3921	3464117	4312		4703	3464899	5094	3465290	196
1	5681	5877	6072	6268	6463	6659	6854	7050	7245	195
2	7636	7831	8027	8222	8418	8613	8908	9004	9199	- 5
3	9590	9785	9981	0176	3470371	0567	3470762	0957	3471153	5
4	3471543	1738	3471934	2129	2324	2519	2715	2910	3105	5
5	3495	3691	3886	4081	4276	4471	4666	4861	5056	5
6	6447	5642	5937	6032	6227	6422	6617	6812	7007	- 5
7	7397	7592	7787	7982	8177	8372	8567	8762	8967	5
8	9347	9542	9737	9931	3480126	0321	3480516	0711	3490906	5
9	3481296	1490	3481685	1880	2075	2270	2464	2659	2954	5
2230	3243	3438	3633	3929	4022	4217	77		1.0	
1	5190	5395	5590	5774			4412	4606	4801	5
2	7136				5969	6164	6358	6553	6747	8
3	9082	7331	7526	7720	7915	8109	8304	949B	8693	5
		9276	9471	9665	9860	00:4	3490248	0443	3490637	194
4	3491026	1220	3491415	1609	3491804	1998	2192	2387	2581	4
5	2970	3164		3552	3747	3941	4135	4330	4524	4
6	4912	5106	5301	5495	5689	5883	6077	6272	6466	4
7	6854	7048	7242	7436	7630	7825	8019	8213	8407	4
8	8795	8989	9183	9377	9571	9765	9959	0153	3500347	4
9	3500735	0929	3501123	1317	3501511	1705	3501898	2092	2286	4
2240	2674	2868	3062	3256	3449	3643	3937	4031	4225	4
1	4612	4806	5000	5194	5387	5581	5775	5969		4
2	6550	6743	6937	7131			7712		6162	
3	8486	8680	8974		7325	7518		7905	8099	4
4	3510422	0616	3510809	9067	9261	9454	9648	9841	3510035	4
5	2357	2550		1003	3511196	1390	3511593	1777	1970	193
6	4291		2744	2937	3131	3324		3711	3906	3
7		4484	4678	4871	5064	5258	5451	5644	5B37	3
	6224	6417	6611	6804	6997	7190	7383	7577	7770	3
8	8156	8349	8543	8736	8929	9122	9315	9508	9701.	3
9	3520098	0281	3520474	0667	3520860	1053	3521246	1439	3521632	30 m m m
2250	2018	2211	2404	2597	2790	2983	3176	3369	3562	3
1	3948	4141	4334	4527	4720	4912	5105	5208	5491	3
2	5877	6070	6262	6455	6648	6841	7034	7226	7419	9
3	7805	7997	8190	8383	8576	8768	8961	9154	9346	3
4	9732	9924	3530117	0310	3530502	0695	3530888	1080		3
5	3531658	1851	2043	2236	2428	2621	2913	3006	3531273	3
6	3583	3776	3969	4161						3
7	5508	6700	5893	6085	4353	4546	4739	4931	5123	192
8	7432	7624	7816	8009	6279	6470	6662	6855	7047	2
9					8201	8393	8586	8778	8970	2
-	9355	9547	9739	9931	3540123	0316	3540500	0700	3540892	2
2260	3541277	1469	3541661	1553	2045	2237	2429	2621	2814	2
1	3198	3390	3582	3774	3966	415R	4350	4542	4734	2
2	5118	5310	5502	5694	5886	6078	6270	6462	6654	9
3	7037	7229	7421	7613	7805	7997	8189	8381	8572	9
4	8956	9148	9340	9531	9723	9915	3550107	0299	3550490	9
5	13550874	1066	13551257	1449	3551641	1832	2024	2216	2407	22222222
6	2791	2982	3174	3366	3557	3749	3940	4132	4324	6
7	4707	4899	5090	5261	5473	5664	5856	6048	6239	2
8	6622	6813	7005	7196	7398	7579	7771	7962		
9	8536	8728	8919	9111	9302		9685		9154	191
						9493		9876	3560067	1
2270	3560450	0641	3560832	1024	3561215	1406	3561598	1789	19801	1
1	2363	2554	2745	2936	3127	3319	3510	3701	3892	1
2	4274	4466	4657	4848	5039	5230	5421	5612	5B03	1
3	6185	6376	6568	6759	6950	7141	7332	7523	7714	ī
4	8096	8287	8478	8668	8859	9050	9241	9432	9623	i
5	3570005	0196	3570397	0578		0959		1341	135715321	Î
6	1913	2104	2295	2486	2677	2867	3058	3249	3440	î
7	3821	4012	4202	4393	4584	4775		5156	5347	î
8	5728	5918		6300	6490	6691	6872	7062	7253	1
8	7634	7824	8015	8205	8396	8586	8777	8967	9158	1
- 0	1	2	3	4	75	G	0.11	8	9198	1
		-	,	-		U		-	29	

Between $22800 = \log^{-1} 4 \cdot 3579348$, and $23400 = \log^{-1} 4 \cdot 3692159$.											
tens.	1	2	- 3	4	- 5	6	7	8	9 1	dif.	
2280	3579539		3579920		3580301	0491	3580682	0872	3581062		
2	3531443	1634	3581824	2014	2205	2395 4298	2595 4488	2776	2966 4869	0	
3	3347 5249	3537 5440	3727 5630	3918 5820	4108 6010	6200	6391	4679 6591	6771	0	
4	7151	7341	7531	7722	7912	8102	8292	8482	8672	0	
6	9052	9242	9432	9622	9812	/0002	3690192	0382	3590572	0	
6	3590952	1142	3591332	1522	3591712	1902	2092	2282	2472	0	
7	2852	3041	3231	3421	3611	3801	3991	4181	4370	0	
8	4750	4940	5130 7027	5319 7217	5509 7406	5699 7596	5889 7786	6078 7976	6268 8165	0	
	6649	6837								0	
2290	8544	9734, 0630,	6924 3600920	9113	9303 3601199	9493 1388	9682 3601578	9872 1767	3600061 1957	0	
1 2	3600440 2336	2526	2715	2904	3093	3283	3472	3662	3851	189	
3	4230	4419	4609	4798	4987	5177	5366	5555	5745	9	
4	6123	6313	6502	6691	6891	7070	7259	7448	7638	9	
5	A016	8205	8395	8584	8773	9962	9151	9341	9530	9	
6 7	9908	/ 0097	3610286	0475	3610664	0854	3611043	1232	3611421 3311	9	
8	3611799 3689	1989	2177	2366 4256	2555 4445	2744 4634	2933 4823	3122 5012	5201	0	
9	5579	5768	5956	6145	6334	6523	6712	6901	7090	9	
2360	7467	7656	7845	8034	8222	8411	8600	8789	8977		
1	9355	9544	9732	9921	3620110	0298	3620487	0676	3620865	9	
2	3621242	1430	3621619	1808	1996	2185	2374	2562	2751	9	
3	3128	3317	3505	3694	3882	4071	4259	4448	4636		
4	5013	5202	5390	5579	6767	5956	6144	6332	6521	188	
5	6898	7086	7276	7463		7840	8028	8216	8405	8	
6	8781	8970	, 9158	9346	9535	9723	9911	/ 0099	3630288 2170	8	
7 8	3630664 2546	0852 2734	3631041 2923	1229 3111	3631417 3299	1605 3487	3631794 3675	1982 3863	4051	8	
9	4427	4615	4804	4992	5180	5368	5556	5744	5932	8	
2310	6308	6496	6684	6872	7060	7248	7436	7624	7312	8	
1	8197	8375	8563	8751	8939	9127	9315	9503	9650	80 00	
2	3640066	0254	3640442	0630	3640817	1005	3641193	1381	3641569	8	
3	1944	2132	2320	2507	2695	2883	3070	3258	3446	8	
4	3821	4009	4197	4384	4572	4759	4947	5135	5322	8	
6	5698 7573	5895) 7761	6073 7948	6260 8136	6448 8323	6635 8511	6823 8698	7010 8885	7198 9073	187	
7	9449	9636	9823	/0010	3650197	0385	3650572	0760	3650947		
ė	3651322	1509	3651696	1894	2071	2258	2446	2633	2820	7 7 7	
9	3195	3382	3569	3757	3944	4131	4318	4505	4693	7	
2320	5067	5254	5441	5629	5816	6003	6190	6377	6564	7	
1	6939	7126	7313	7500	7687	7874	8061	8248	B435	7	
2	8809	8996	5183	9370	9557	9744	9931	/0118	3660305	7	
3 4	3660679	0866 2735	3661053	1240	3661427	1614	3661801	1987	2174 4043	777777777777777777777777777777777777777	
5	2548 4416	4603		3109 4977	3296 5163	3492 5350	3669 5537	3856 5724	5910	7	
6	6284	6471	6657	6844	7031	7217	7404	7591	7777	7	
7	9150	8337	8524	8710	8697	9083	9270	9457	9643	7	
B	3670016	0203			3670762		3671135	1322	3671508		
9	1881	2068	2254	2441	2627	2814	3000	3186	3373	186	
2330	3746	3932	4113	4305	4491	4677	4864	5050	5236	6	
1	5609	5795	5982	6168	6354	6540	6727	6913	7099	6	
2	7472	7658	7844	8030	6217	8403	8589	8775	8961	6	
3	9334 3681195	9520	9706 3681567	9892 1753		0264 2125	3680450 2311	0636 2497	3680822 2683	6	
5		3241	3427	3613		3985	4171	4357	4542	6	
6	4914	5100	5286	5472	5658	5844	6030	6215	6401	6	
7	6773	6959	7145	7330	7516	7702	7838	8074	8259	6	
8	8631	8817	9002	9188	9374	9559		9931	3690117	6	
9	3690498	0674		1045		1416			1973	6	
	1	12	3	4	5	6	7	8	9		

Table 1.] LOGARITHMS OF NUMBERS FROM 1 TO 36,000.

Between $23400 = \log_{\bullet} - 14.3692159$, and $24000 = \log_{\bullet} - 14.3802112$.

										_
tens.	1	2	3	4	- 6	6	7	*	9	dif.
2340	3692344	2530	3692715	2901	3693086	3272		3643		186
1	4200	4385	4571	4756	4942	5127	5313	5498	5683	5
2	6054	6240	6425	6611	6796	6981	7167	7352	7538	5
4	7908	8094	8279	B464	8650	8835	5020	9205	9391	5
	9761	9947	3700132	0317	3700502	0688	3700873	1058	3701243	5
5	3701614	1790	1984	2169	2354	2540	2725	2910	3095	5
6	3456	3650	3635	4020	4206	4391	4576	4761	4946	5 5
6	5316	55U1	5686	5871	6056	6241	6426	6611	6796	0
9	7166	7351	7536	7721	7906	8091	8275	8460	8645	5
-	1015	92(4)	9385	9570	9754	9939	3710124	0309	3710494	
2350	3710863	1(4)	3711233	1418	3711603	1787	1972	2157	2342	5
1	2711	2896		3265	3450	3635	3819	4004	4189	5
2	4558	474%	4527	5112	5296	5481	5666	5850	6035	5
3	6404	6586	6773	6957	7142	7327	7511	7696	7880	5
4	8249	8434	8618	8802	8987	9171	9356	9540	9725	184
5	3720094	0275		0647		1015		1384		4
7	1937	2122	2306	2490	2674	2859	3043	3227	3412	4
9	3780	3904	4149	4333	4517	4701	4885	6070	5254	4
9	5622	5806	5991	6175	6359	6543	6727	6911	7095	4
	7464	7648	7832	8016	8200	8384	8563	8752	8936	4
360	9304	9488	9672	9856	3730040	0224	3730408	0592	3730776	4
I	3731144	1328	3731512	1696:	1879	2063	2247	2431	2615	4
2	2983	3167	3350	3534	3718	3902	4086	4270	4453	4
3	4821	5005	6189	5372	5556	6740	5924	6107	6291	4
4	6658	6842	7026	7210	7393	7577	7761	7944	\$128	4
5	8495	8679	8862	9046	9230	9413	9597	9780	9964	4
ti	3740331	0515	3740698	0882.	3741065	1249	3741432	1616	3741799	4
7	2166	2350	2533	2716	2900	3083	3267	34500	3634	183
8	4000	4184	4367	4551	4734	4917	5101	5284	5467	3
9	5834	6017	6201	6394	6567	6750	6934	7117	7300	
370	7667	7850	8033	8216	8400	8593	8766	8949	9132	33333333333
1	9409	9682	9865	0048	3750231	0414	3750599	0781	3750964	3
2	3751330	1513	3751696	1879	2062	2245	2428	2611	2794	3
3	3160	3343	3526	3709	3892	4075	4268	4441	4624	3
41	4990	5173	5356	5539	5722	5905	6088	6270	6453	3
5	6819	7002	7185	7367	7550	7733	7916	8099	8282	3
6	8647	8830	9013	9195	9378	9561	9744	9926	3760109	3
7	3700475	0667	3760840	1023	3761205	1388	3761571	1753	1936	3
8	2301	2434	2666	2849	3032	3214	3397	3579	3762	3
9	4127	4310	4492	4675	4857	5040	6222	5405	5587	3
380	5952	6135	6317	6499	6682	6864	7047	7229	7412	182
1	7776	7959	8141	8323	8506	8688	8871	9053	9235	2
2	9600	9782	9965	0147	3770329	0511	3770694	0876	377105R	5
3	3771423	1605	3771787	1969	2152	2334	2516	2698	2880	2222222222
4	3245	3427	3609	3791	3973	4155	4338	4520	4702	2
51	5066	5249	5430	56121	5794	5976	6158	6340	6522	2
6	6886	7068	7250	7432	7614	7796	7978	8160	8342	2
7	8706	8888	9070	9252	9434	9616	9798	9979	3780161	2
8	3780525	0707	3780889	1071	3781252	1434	3791616	1798	1980	2
9	2343	2525	2707	2889	3070	3252,	3434	3616	3797	
390	4161	4342	4524	4706	4887	5069	5251	5432	5614	2
1	5977	6159	6341	6522	6704	6885	7067	7249	7430	222
2	7793	7975	8156	9338	8519	8701	8882	9064	9245	2
3.	9609	9790	9971	0153	3790334	0516	3790697	0879	3791060	181
41	3791423	1604	3791796	1967	2148	2330	2511	2692	2974	i
51	3237	3418	3599	3730		4143		4596	4687	i
6	6049	5231	5412	5593	5774	5956	6137	6318	6499	i
7	6862	7043	7224	7405	7586	7767	7948	8130	8311	î
8	8673	8854	9035	9216	9397	9578	9759	555511	13800121	
7 8 9	8673 3800484	8854 0665	9035 3800846	9216 1027	9397 3801208	9578 1389	9759 3801570	9940 1750	3800121 1931	1

4*

3 3861600 1778 1957 2135 2314 2492 2670 2849 3027 178	حصم										
2400 3902293 2474 3902665 2236 2236 2366 23676 2236 24464 4646 4626 6007 6198 5368 55649 1											
1		Betw een	24000	$= \log.$	-1 4 ·38	02112, a	nd 240	$600 = \log$	1 4	3909351	•
1	tens.	1	2	3	4	8	6	7	8	9	dif.
3	2400	3802293 4102	2474 4283	3802655	2836 4645	3803017 4826	3198 5007	3803379 5188	3560 5368	3803741 5549	181
3	2	5911	6092	6272	6453	l 6634	6815	6995	7176	7357	i
6 3811331 1512 3811693 1873 2054 2234 2415 2595 2776 1			7899	8090	8261	8441	0428	3810600	8983	9164	
C		3811331	1512	3811693	1873	2054	2234	2415	2595	2776	l i
2410 3820351 0531 3820711 0891 3821071 1252 3821432 1612 3821792 0	((3317	3498	3678	3859	4039	4220	4400	4580	0
2410 3820351 0531 3820711 0891 3821071 1252 3821432 1612 3821792 0	8		6926	7106	7286	7467	7647	7827	8007	8198	ŏ
2 3953 4133 4493 4673 4853 5033 5213 5933 4		8548	8729	8909	9089	9269	9450	9630	9810	9990	
2 3953 4133 4493 4673 4853 5033 5213 5933 4	2410		0531	3820711	0891	3821071	1252	3821432	1612	3821792	0
6 3831149 1329 3831509 1688 1868 2048 2227 2407 2587 7 2946 3126 3306 3485 3665 3844 4024 4204 4383 68 4743 4922 5102 5281 5461 5640 5820 6000 6179 6179 7 7 7 7 7 7 7 7 7	2		4133	4313	4493	4673	4953	5033	5213	5393	ŏ
6 3831149 1329 3831509 1688 1868 2048 2227 2407 2587 7 2946 3126 3306 3485 3665 3844 4024 4204 4383 68 4743 4922 5102 5281 5461 5640 5820 6000 6179 6179 7 7 7 7 7 7 7 7 7	3	5753	5933	6113	6293	6473	6653	6833	7013	7193	0
6 3831149 1329 3831509 1688 1868 2048 2227 2407 2587 7 2946 3126 3306 3485 3665 3844 4024 4204 4383 68 4743 4922 5102 5281 5461 5640 5820 6000 6179 6179 7 7 7 7 7 7 7 7 7			9531	9711	uqui	202N170	0250	12020420	0610	3830790	i
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6	7682	7857	8033	8208	8393	8559	8734	8909	9085	5
7	9435	9611	9786	9961	3940137	0312	3940487	0662	3940838	5
8	3941198	1364	3941539	1714	1889	2064	2240	2415	2590	5
9	2940	3116	3291	3466	3641	3816.	3991	4167	4342	5
2490	4692	4867	5042	5217	5392	5567	5742	5918	6093	5
1	6443	6618	6793	6968	7143	7318	7493	7668	1 7843	5
2	8193	8368	8543	8718	8893	9068	9242	9417	9592	5
3	9942 3951691	/ 0117 1866	3950292	0467	3950642	0817	3950991	1166	3951341	5
51	3439	36131	2040 3788	2215	2390 4138	2565 4312	2740	2914	3089	5
6	5186	5361	5535	3963 5710	5885	6089	4497 6234	4662 6409	4837 6583	5
7	6932	7107	7282	7456	7631	7805	7980	8155	9329	5
8	8678	9853	9027	9202	9376	9551	9725	9900	3960074	5
9	3960423	0598	3960772	0947	3961121	1296	3961470	1645	1819	174
2490	2168	2342	2517	2691	2865	3040	3214	3389	3563	4
1	3912	4086	4260	4435	4609	4783	4959	5132	5306	4
2	5655	50,00	6003	6177	6352	6526	6700	6874	7049	4
3	7397	7571	7745	7920	8094	6268	8442	8616	6790	4
4	9139	9313	9487	9661	9835	0009	3970183	0357	3970531	4
5	3970830 2620		3971229	1402	3971576	7 1750	1924	2099	2272	4
6 7	4359	2794 4533	2968 4707	3142 4881	3316 5055	3490 5229	3664	3838 5577	4011	4.
8	6098	6272	6446	6620	6794	6967	7141	7315	5750 7489	4
9	7836	8010	8184	8358	8531	8705	8879	9053	9226	4
2500	9574	9748	9921	.0096	3980269	0442	3980616	0790	3980963	4
1	3981311	1434	3081659	/ 1831	2005	2179	2352	2526	2699	4
2	3047	3220	3394	3567	3741	3914	4098	4261	4435	4
3	4782	4956	5129	5302	5476	5649	5923	5996	6170	173
4	6517	6690	6864	7037	7210	7394	755 7	7731	7904	3
5	8251	8424		8771	8944	9117	9291	9464	9637	3
6	9984	0157	3990331	0504	3990677	0960	3991024	1197	3991370	3
7 8	3991717 3448	1890 3622	2063	2236	2409	2583	2756	2929	3102	3
9	5180	5353	3795 5526	3968 6699	4141 5872	4314 6045	4487 6218	4660 6391	4834	3
									6564	
2510	6910 8640	7083 8813	7256 8986	7429	7602 9332	7775	7948 9678	8121	8294	3
2	4000369	0542	4000715	9159 0888	4001061	9505 1234	9678 4001406	9851 1579	4000023 1752	3
3	2098	2271	2443	2616	2789	2962	3134	3307	3490	3
4	3825	3908		4344	4516	4689	4862	5035	5207	33333
5.		6725		6071	6243	6416		6761	6934	3
6	7279	7452	7624	7797	7969	8142	8314	8487	8660	3
7	9005	9177	9350	9522	9695	9867	4010040	0212	4010385	3
8	4010730	0902	4011075	1247	4011420	1592	1764	1937	2109	172
9	2454	2626	2799	2971	3144	3316	3488	3661	3833	2
	1	2	3	4	- 5	4	7	H	. 9	

44 LOGARITHMS OF NUMBERS FROM 1 TO 36,000. [Table 1. Between 25200 = $\log^{-1} 4.4014005$, and 25800 = $\log^{-1} 4.4116197$.

										-
tens. 2520	1 4014178	2 4350	4014522	4605	4014967	6	4015212	8 5384	9 4015556	dif. 172
2020	5901	6073	4014522 6245	4695 6417	4014867 6590	5039 6762	6934	7106	7279	1/2
2	7623	7795	7967	8140	8312	8484	8656	8828	9000	$\tilde{2}$
3	9345	9517	9689	9861		0205		0549		2
4	4021066	1238	4021410	1582	1754	1926	2098	2270	2442	2
5	2786	2958	3130	3302	3474	3646	3818	3990		2
6	4505	4677	4849	5021	5193	5365	5537	5709	5881	2
7	6224	6396	6568	6740	6912	7083	7255	7427	7599	2
8	7942	8114	8286	8458	8630	8801	8973	9145	9317	2 2 2 2 2 2 2
9	9660	9832	4030003	0175	4030347	0519	4030690	0862	4031034	
2530	4031377	1549	1720	1892	2063	2235	2407	2578	2750	2
1	3093	3265	3436	3608	3779	3951	4122	4294	4465	2 171
2 3	4809 6523	4980 6695	5152 6966	5323 7038	5495 7209	5666 7381	5838 7552	6009 7723	6190 7895	ľi
4	8237	8409	8580	8752	8923	9094	9266	9437	9608	li
51	9951		4040294		4040636	0807	14040979		4041321	lî
6	4041664		2006	2177	2349	2520	2691	2862	3033	i
7	3376	3547	3718	3889	4061	4232	4403	4574	4745	1
8	5087	5258	5429	5601	5772	5943	6114	6285	6456	1
9	6798	6969	7140	7311	7482	7653	7824	7995	8166	1
2540	8508	8679	8850	9021	9192	9363	9534	9705	9876	
1	4050218	0388	4050559	0730	4050901	1072	4051243	1414	4051585	1
2	1926	2097	2268	2439	2610	2780	2951	3122	3293	Ī
3	2634	3805	3976	4147	4317	4488		4830	5000	1
5	5342	5512	5683	5854	602 5 7731	6195 7902	6366 8072	6537 8243	6707 8413	
6	7049 8755	7219 8925	7390 9096	7560 9266	9437	9607	9778	9948		li
7	4060460	0630	4060801	0971	4061142	1312	4061483	1653		170
8	2165	2335	2506	2676	2846	3017	3187	3358		ő
9	3869	4039	4209	4380	4550	4721	4891	5061	5231	Ó
2550	5572	5742	5913	6083	6253	6424	6594	6764	6934	0
1	7275	7445	7615	7786	7956	8126	8296	8466		Ŏ
2	8977	9147	9317	9487	9659	9828	9998	/0168	4070338	0
3	1070678	0848	4071018	1189	4071359	1529	4071699	1869		
4	2379	2549	2719	2889	3059	3229	3399	3569	3739	0
5		4249		4589	4759	4929	5099	5269		0
6	5778	5948	6118	6288 7987	6458	6628 8326	6798 849 6	6968 8666	7137 8836	0
8	7477 9175	7647 9315	7817 9515	9684	9854	0024	4080194	0363		ŏ
9	4090873		4081212	1382	4081551	1721	1891	2060		ŏ
2560		2739	2909	3078	3248	3417	3587	3757	3926	ŏ
2500	2569 4265	4435	2909 4604	4774	4944	5113	5283	5452		169
2	5961	6130	6300	6469	6639	6808	6978	7147	7317	9
2 3	7656	7825	7994	8164	8333	8503	8672	8841	9011	9
4	9350	9519	9688	9858		0196	4090366	0535	4090704	9
5	4071043		4091382	1551	1720	1889		2228		9 9 9 9 9 9
. 6	2736	2905	3074	3243	3413	3582	3751	3920		9
7	4428	4597	4766	4935	5105	5274	5443	5612	5781	9
8	6119 7810	6288 797 9	6458 8148	6627 8317	6796 848 6	6965 8655	7134 8824	7303 8993	7472 9162	9
2570	9500	9669	9838	/ 0007	4100176	0345	4100514	0683		9 9 9
1 2	4101190 2878	1359 3047	4101527 3216	1696 3385	1865 3554	2034 3723	2203 3891	2372 4060	2541 4229	1 8
3	4567	4735	4904	5073	5242	5410	5579	5748	5917	. 9
4	6254	6423	6592	6760	6929	7098		7435	7604	1 9
51	7941	8110	8278	8447	8616	8784	8953	9121	9290	9
6	9627	9796	9964		4110301	0470	4110639	0807	4110976	9
7	4111313	1481	4111650	1818	1987	2155	2324	2492	2661	168
8	2998	3166	3334	3503	3671	3840	4008	4177	4345	8
9	4682	4850	5019	5187	5355	5524	5692	5860	6029	8
	1	2	3	4	5	6	1 7	8	9	

Between $25800 = \log^{-1} 4.4116197$, and $26400 = \log^{-1} 4.4216039$.

						-				
tens.	1	2	3	4	. 6	15	T	8	9	dif.
2580	4116365	6534	4116702	6870	4117039	7207	4117375	7544	4117712	168
1	8048	8217	8385	8553	8721	8890	9058	9226	9394	8
2	9731	9899	4120067	0235	4120403	0571	4120740	0908	4121076	8
3	4121412	1580	1748	1917	2085	2253	2421	2589	2757	В
4	3093	3261	3429	3597	3765	3933	4101	4269	4437	8
5		4941	6109	5277	5445	5613	5781	5949	6117	8
6	6453	6621	6789	6957	7125	7293	7461	7629	7796	8
	8132	6300	8468	8636	8804	8971	9139	9307	9475	B
8	9811	9978	4130146	0314	4130482	0649	4130617	0985	4131153	8
	4131488	1656	1824	1991	2159	2327	2495	2662	2830	8
2590	3165	3333	3501	3668	3836	4004	4171	4339	4507	8
1	4842	5009	5177	5346	5512	5680	5847	6015	6182	8
2	6518	6685	6863	7020	7188	7355	7523	7690	785B	8
3	8193	8360	8528	8695	8863	8030	9197	9365	9532	167
4	9867	/0035	4140202		4140537	0704	4140872	1039	4141206	7
5		1708		2043		2378		2712		7
6	3214	3381	3549	3716	3883	4051	4218	4385	4552	7
7	4887	5054	5221	5388	5556	5723	5890	6057	6224	7
8	6559	6726	6893	7060	7227	7394	7561	7729	7896	7
9	8230	8397	8564	8731	8898	9065	9232	9399	9566	
2600	9901	/ 0068	4150235	0402	4150569	0736	4150903	1070	4151237	7
1	4151570	1737	1904	2071	2238	2405	2572	2739	2906	7
2	3240	3407	3574	3741	3907	4074	4241	4408	4575	7777777
3	4909	5075	5242	5409	5576	5743	5909	6076	6243	7
4	6577	6743	6910	7077	7244	7410	7577	7744	7911	7
- 5	9244	8411	8577	8744	8911	9077	9244	9411	9577	7
6	9911	10077	4160244	0411	4160577	0744	4160911	1077	4161244	7
7	4161577	1743	1910	2077	2243	2410	2576	2743	2909	
8	3242	3409	3575	3742	3908	4075	4241	4408	4574	166
9	4907	5074	5240	5407	5573	5739	5906	6072	6239	6
2610	6571	6738	6904	7071	7237	7403	7570	7736	7902	6
1	9235	8401	B568	8734	6900	9067	9233	9399	9565	6
2	9898		4170231	0397	4170563	0729	4170895	1062	4171228	6
3	4171560	1726	1893	2059	2225	2391	2557	2724	2890	6
4	3222	3368	3554	3720	3886	4053	4219	4385	4551	6
5	4883	6049	5215	5318	5547	5713	5879	6045	6211	6
6	6543	6709	6975	7041	7207	7373	7539	7705	7971	6
7	8203	8369	8535	8701	8967	9033	9199	9365	9531	6
8	9862		4180194	0360	4180526	0692	4180857	1023	4181189	6
9	4181521	1687	1852	2018	2184	2350	2516	2681	2847	6
2620	3179	3344	3510	3676	3842	4007	4173	4339	4505	6
1	4836	5002	5167	5333	5499	5664	6830	5996	6161	6
2	6493	6658	6824	6989	7155	7321	7486	7652	7817	6
3	8148	8314	8480	8645	8811	8976	9142	9307	9473	6
4	9804	9969		0300	4190466		4190797	0962	4191129	165
5	4191459		1739	1955	2120	2296	2451	2616		5
6	3113		3443	3609	3774	3939	4105	4270	4435	5
7	4766		5097	5262	5427	5593	5758	5923	6088	5
8	6419		6749	6915	7090	7245	7410	7575	7741	5
9	8071	8236	8401	8567	8732	8897	9062	9227	9392	5
2630	9723	9899	4200053	0218	4200393	0548	4200713	0878	4201043	5
2030	4201374	1539	1704	1869	2034	2199		2529	2694	5
2			3354	3519	3684	3849		4179	4344	5
3			5003	5168	5333	5498	5663	5828	5993	5
4	6323		6652	6817	6982	7147		7477	7641	5
5			8301	8465		8795		9125	92891	5
6	9619		9949	/ 0113	4210278	0442	4210607	0772	4210937	5
7	4211266		4211595	1760	1925	2089		2419	2583	5555
B			3242	3406	3571	3736	3900	4065	4229	5
9	4558		4888	5052	5217	5381	5546	5710	5875	5
9	1	2	3	4	5	6	7	8	9	
				-		-		-	4	

46		LOGA	RITHMS	OF N	UMBERS	FROM	1 то 3	6,000	[Tab	le 1.
H	Between.	2 6400		1 4.42	16039, ar	id 270		5. TI 4.	4313638.	
tens.	4216204	8260	3 4216533	4 6607	4216862	4i 7026	4217191	7255	9 4217520	dif.
1	7849	8013	8177	0040	0500	8671				4
2	9493.	9657	9821	9986	4220150 1793 3436	0314	4220479	0643	9164 4220807 2450 4093 5734 7375 9016 4230656	4
3	4221136 2779	1300	4221465 3107	1629	1793	1957	2122 3764	2286	2450	4
	4421	4585	4749	4913	5078	5242	3764 5406 7047 8688 4230328 1967	5570	4093 6734	4
6	6063	6227	6391	6555	5078 6719	6883	7047	7211	7375	4
7	7703	7868	8032	2106	8360	8524	8688	8852	9016	4
8	9344 4 23 0984	9508	9672	9836	4230000 1639	0164	4230328	0492	4230656	4
			4231311	1475	1039	1803	1001	~ LUX	2200	-
2650 1	2623 4261	2786 4425	2950 4589	3114 4753	3278 4916				3933 5571	4 4
2	5899	6063	6226	6390	6554	5090 6718	6981	7045	7209	4
3	7536	7700	6226 7864	6390 8027	6554 8191 9827	8355	8518 4240154	5408 7045 8682	8846	4
4	9173	9336	9500	9664	9827	9991	4240154	0318	"424 0482"	4
5	4240809	0972 2608	4241136 2771	1300	4241463 3098	1627 3262	1790 3425	1954	2117 3752	162
7	4240809 2444 4079 5713	4242	4406	4569	4241463 3098 4733	4896	5060	1954 3589 5223	5386	3
8	5713	5877	6040	6203	6367	6530	6693	6857	7020	3
9	7347	7510	7673	7837	8000	8163	8327	8490	8653	3
26 50	8990 425 0612	9143	9306 4250938	9469	9633	9796	9959	/0122	4250286 1917	3
1	425 0612	0775	425 0938	1102	4251265	1428	4251591	1754	1917	3
2	2244 3975	2407	2570	2733	2896	3059	3222	3385	3549	3
2 5 4	5505	5668	5831	2733 4364 5994	2896 4527 6157	6320	6483	6646	3549 5179 6809	3
5	7135	7298	7461	7624	1181	7950	8113	8276	8439	3
6	8764	8927	9090	9253	9416	9579	3222 4853 6483 8113 9742 4261370	9904	4260067	3
7 8		0556	2570 4201 5831 7461 9090 4260719 2347	0881	9416 4261044 2672	1207 2835	4261370 2998	1533	1695	3
9	2021 3648	3911	3974	4137	4299	4462	4625	4787	1917 3549 5179 6809 4260067 1695 3323 4950	3
2670	5275	5438	5601				6251	6414	6576	3
1	6901	7064	7227	576 3 73 89	7552	7714	7977	80.30	8202	3
2	8527	8690	8852	9015	9177	9340	9502	9665	9827	3
3	8527 4270152 1776	0315	8852 4270477 2101	0639	9177 4270S02 2426	0964	4271127	1289	9827 4271452 3076	162
4	3400	3563	3725	2204	4050	4212	9502 4271127 2751 4374	2913	3076 4699	2
5 6 7	5023	5186	5348	5510	4050 5672 7295 8917 4280538	5835	5997	4536 6159 7781	6321	$\tilde{2}$
7	6646	6808	5348 6970 8592 4280213	7133	7295	7457	7619	7781	7944	2
8	8268	8430	8592	8754	8917	9079	9241	9403	9565	2
9	9989	/0051	4280213	0376	4280538	0700	4280862	1024	4281156	2
	4281510 3130	1672 3292	1834 3454	1996 3616 5235	2158 3778	2320 3940	2492	2644	2806	43333333333333333333333333333333333333
1 2	4750	4912	5073	5235	5397		5721	5883	6045	2
3 4	6369	6530	6692	6854 8472	7016 8634	7178	7340	7501	7663	$\tilde{2}$
4	6369 7987	6530 8149	6692 8311	8472	8634	8796	8958	9119	9281	2
5	9605	9766	9928 4291545	/ 0090	4290252	2020	4290575	0737	4290898	2
7	2838	3000	3169	3323	3495	3646	3808	3960	4131	2
8	9605 4291222 2838 4454 6070	3000 4616	3162 4777	3323 4939	3485 5100 6715	5262	7340 8958 4290575 2192 3808 5423 7038	5585	9565 4281186 2806 4426 6045 7663 9281 4290898 2515 4131 5747 7361	$\tilde{2}$
9	€070	t231	6393	6554	6715	687.7	7038	7200	7361	161

9776 1395

6

5

4300267

6716

4311546

3653

6877

3815

7038

4310258 1968

0428 4300589

9293

6 7

2686

5 110

9132 0741

2

7943

1063

3

ble I.] LOGARITHMS OF NUMBERS FROM 1 TO 36,000.

Between 27000 = log. -1 4.4313638, and 27600 = log. -1 4.4409091. Table 1.]

			-				,			
tens. 2700	1 1	2 3959	3	4	5	4000	1014760	8 ADD4	9	dif
1	4313798 5407	5567	4314120 5728	4281 5889	4314442 6050	4603 6210	4314763 6371	4924 6532	4315085 6693	161
2	7014	7175	7336	7496	7657	7818	7978	8139	8300	i
3	8621	8782	8942	9103	9264	9424	9585	9746	9906	î
4	4320227	038B	4320549	0709	4320870.	1030	4321191	1352	4321512	i
5	1833	1994	2154	2315	2475	2636	2796	2957	3117	ı î
6	3438	3599	3759	3920	4080	4241	4401	4662	4722	160
7	5043	5203	5364	5524	5685	5845	6005	6166	6326	0
8	6647	6907	6968	7128	7288	7449	7609	7769	7930	0
9	8250	8411	9571	8731	8892	9052	9212	9372	9533	0
2710	9853	/0013	4330174	0334	4330494	0654	4330815	0975	4331135	0
1	4341455	1616	1776	1936	2096	2256	2416	2577	2737	0
2	3057	3217	3377	3537	3697	3858	4018	4178	433B	0
3	4658	4818	4978	5138	5298	5458	5618	5778	5938	0
4	6259	6418	6578	6738	6898	7058	7218	7378	753B	0
5	7858	8018		8338	8498	8658	8818	8978	9138	0
6	9458	9617	9777	9937	4340097	0257	4340417	0577	4340737	0
7	4341056	1216	4341376	1536	1696	1855	2015	2175	2335	0
8	2654	2814	2974	3134	3293	3453	3613	3773	3932	0
9	4252	4412	4571	4731	4891	5050	5210	6370	5529	0
2720	5849	6008	6168	6328	6487	6647	6807	6966	7126	0
1	7445	7605	7764	7924	8083	8243	8403	8562	8722	0
2	9041	9200	9360	9519	9679	9838	9998	/ 0167	4350317	0
3	4350636	0795	4350955	1114	4351274	1433	4351593	1752	1912	0
4	. 2230	2390	2549	2709	2868	3028	3197	3346	3506	159
5	3824	3984	4143	4303	4462	4621	4781	4940	5099	9
7	5418	5577	5736	5896	6055	6214	6374	6533	6692	9
8	7011	7170	7329 8921	7488 9080	7648 9240	7807 9399	7966	8125	8284	9
9	8603 4360194	8762 0354	4360513	0672	4360831	0990	9558 4361149	9717 1308	9876 4361467	9
2730	1786	1945	2104	2263	2422	2581	2740	2899	3058	9
I	3376	3535	3694 5284	3853	4012 5602	4171	4330	4489	4648 6237	0
3	4966 6555	5125 6714	6873	5443 7032	7191	5761 7350	5920 7509	6078 7667	7826	9
4	8144	8303	8462	8620	8779	8938	9097	9256	9415	9999
5,	9732	9891		0208		0526		0843		9
6	4371320	1478	1637	1796	1955	2113	2272	2431	2589	9
7	2907	3065	3224	3383	3541	3700	3959	4017	4176	9
8	4493	4652	4810	4969	5127	5286	5445	5603	5762	9
9	6079	6237	6396	6555	6713	6872	7030	7189	7347	9
2740	7664	7823	7981	8140	8298	8457	8615	8773	8932	158
1	9249	9407	9566	9724	9883	/ 0041	4380199	035B	4380516	8
2	4380833	0991	4381150	1308	4381466	1625	1783	1941	2100	8
3	2416	2575	2733	2891	3050	3209	3366	3525	3683	8
4	3999	4158	4316	4474	4632	4791	4949	5107	5265	888
5	5582	5740		6056		6373	6531	6689	6847	8
6	7163	7322	7480	7638	7796	7954	8112	8270	8428	8
7	8745	8903	9061	9219	9377	9535	9693	9851	4390009	8
8	4390325	0483	4390641	0799	4390957	1115	4391273	1431	1589	8
9	1905	2063	2221	2379	2537	2695	2853	3011	3169	8
2750	3485	3643	3801	3959	4116	4274	4432	4590	4748	8
1	5064	5222	5379	5537	5695	5853	6011	6169	6326	8
2	6642	6800	6958	7115	7273	7431	7589	7747	7904	8
3	8220	8378	8535	8693	9851	9009	9166	9324	9482	8
4	9797	9955	4400112	0270	4400428	0586	4400743	0901	4401068	8
5	4401374	1531	1689	1347	2004	2162	2319	2477	2635	8
6	2950	3107	3265 4840	3422	3580	3738	3895	4053 5628	4210	157
7 8	4525 6100	4683 6258	6415	4998 6572	6155 6730	5313 6887	5470 7045	7202	5785 7360	7
9	7674	7832	7989	8147	9304	8461	8619	B776	8933	7
9	1014	2	3	4	5304	6	7	8	9	1
		146	,	-	,	40		.,	. 0	

48 LOGARITHMS OF NUMBERS FROM 1 TO 36,000. [Table 1. Between $27600 = \log^{-1} 4.4409091$, and $28200 = \log^{-1} 4.4502491$.

Lens. 1	0 7
114410821 0979 4411136 1293 4411480 1608 1765 1922 206 2 2394 2551 2708 2566 3023 3180 3337 3494 365 3 3066 4123 4280 4438 4595 4752 4909 5066 522 4 5538 5695 5852 6009 6166 6323 6480 6637 679 6 6679 8836 8993 9150 9307 9464 9621 9778 993 7 4420249 9045 4420562 0719 4420676 1033 4421190 1347 442150 9 3366 3543 3700 3857 4014 4171 4327 4484 464 2770 4954 5111 5268 5425 5582 5738 5895 6052 629 1 6522 6679 6835 6992 7149 7306	0 7
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61 7108 7265 7423 7580 9737 7894 8061 8208 836 6 6679 8336 8993 9150 9307 9464 9621 9778 9937 7 74420249 0405 4426662 0719 4420876 1033 421190 1347 442150 8 1818 1975 2132 2288 2445 2602 2759 2916 307 9 3386 3543 3700 3857 4014 4171 4327 4484 464 2770 4954 5111 5688 5625 5582 5738 5895 6052 6629 626 967 6835 6992 7149 7306 7462 7619 777 2 8089 8246 8402 8559 8716 8872 9029 9185 934 4313221 1378 4431534 1691 1947 2042 2160 2317 24430282	
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8 1818 1975 2132 2288 2445 2602 2759 2916 307 9 3386 3543 3700 3857 4014 4171 4327 4484 464 2770 4954 5111 5268 5425 5582 5738 5895 6652 6620 1407 7306 7462 7619 777 2 8089 8246 8402 8550 8716 8872 9029 9185 934 334 3691 9185 934 4430282 0438 4430585 0751 4430585 0751 4430585 0751 247 5 2786 2943 3099 3256 3412 3569 3725 3882 403 6 4351 4507 4664 4820 4977 5133 5290 5446 560 767 5915 6072 6228 6384 6641 6607 6853 7010 716 767 7515 6072 <t< td=""><td>1 7</td></t<>	1 7
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6 9967 0123 4450279 0425 4450590 0746 4420902 1058 445121 7 4451626 1681 1937 1993 2149 2305 2460 2616 277 8 3083 3239 3395 3561 3706 3862 4018 4174 432 9 4641 4797 4952 5108 5264 5419 5575 5731 588 2790 6198 6353 6509 6665 6820 6976 7132 7287 744 1 7754 7910 9065 8221 8376 8532 8687 8843 899	
7 4451626 1681 1937 1993 2149 2305 2460 2616 277 8 3083 3239 3395 3651 3706 3862 4018 4174 432 9 4641 4797 4952 5108 5264 5419 5575 5731 588 2790 6198 6353 6509 6665 6820 6976 7132 7287 744 1 7754 7910 9065 8221 8376 8532 8687 8843 899	
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3 4460865 1020 4461176 1331 4461487 1642 1798 1953 210 4 2419 2575 2730 2886 3041 3197 3352 3507 366	
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8 8632 8799 8.443 9098 9253 9408 9563 9719 987 9 4470184 9339 4470494 9659 4470805 9960 4471115 1270 447142	
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1 3286 3441 3596 3751 3906 4061 4216 4371 452	
2 4936 4991 5143 5301 5456 5611 5766 5921 607 3 6396 6541 6696 6351 7006 7161 7315 7470 762	
3 63% 6541 6696 6851 7006 7161 7315 7470 762 4 7935 8090 8245 8400 8554 8709 8964 9019 917	
51 9483 96381 9793 994814480103 025814480412 05671448072	
6 4481031 1186 4481341 1496 1650 1805 1960 2115 226 7 2579 2734 2883 3043 3198 3352 3507 3662 381	
8 4126 4280 4435 4590 4744 4899 5054 5206 536	
9 5672 5827 5981 6136 6290 6445 6600 6754 690	
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1 8763 8917 9072 9226 9381 9535 9690 9844 999 2 4490308 0462 420616 0771 4490925 1080 4491234 1389 449154	
3 1352 2006 2460 2315 2469 2624 2778 2932 308	
4 3395 3550 3704 3858 4013 4167 4521 4475 463	
51 4938 50931 5247 54011 5555 57101 5864 60191 617	
6 6481 6635 6789 6943 7098 7252 7406 7560 771	
7 8023 8177 8331 8485 8639 8793 8948 9102 928	
8 9564 9718 9872 / 0026 4500180 0334 45001 9 0643 450079	
9 4501105 1259 4501413 1567 1721 1875 2029 2183 233	
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2820	4502645 4185	2 2799 4339	3 4502953 4493	4 3107 4647	4503261 4801	G 3415 4954	4503569 5108	8 3723 5262	9 4503877 5416	di 15
3	5724 7263	5878 7416	6032 7570	6186 7724 9262	6340 7878	6493 8032	6647 8186	6601 6339	6955 8493	1
5	8801 4510338	8954 0492	9108 4510646	0799	9416 4510953	9570 1107	9723 4511261	1414	4510031 1568	
6 7 8 9	1975 3412 4949 6493	2029 3565 5101 6636	2183 3719 5255 6790	2336; 3873; 5408; 6943;	2490 4026 5562 7097	2644 4180 5715 7250	2797 4333 5869 7404	2951 4487 6022 7557	3104 4640 6176 7711	
2630 1	8018 9552 4521096	9171 9705 1239	8325 9859	8478 / 0012 1546	8632	6785 0319 1853	8938	9092 0626 2159	9245 4520779 2312	
34	2619 4152 5684	2772 4305 5837	2926 4458 5990	3079 4611 6143	3232 4765	3395 4918 6450	3539 5071	3692 5224 6756	3845 5377 6909	
6 7 8 9	7215 8746 4530277	7369 8900 0430	7522 9053 4530583	7675 9206 0736	7828 9359 4530889	7981 9512 1042	6603 5134 9665 4531195	8287 9818 1348	8440 9971 4 53 1501	
2840	1807 3336 4965	1960: 3469 5018	2113 3642 5171	2266 3795 5324	2419 3948 5477	2572 4101 5629	2725 4254 5782	2978 4407 5935	3030 4559 6088	
1 2 3 4	6394 7921 9449	6546 8074 9601	9754		7005 8532 4540059	8685 0212	7310 8R38 4540365	7463 8990 0517	7616 9143: 4540670	
5 6 7 8	4540975 2502 4027 5552	1128 2654 4180 5705	4541281 2807 4332 5857	1433 2959 4485 6010	1586 3112 4637 6162	1739 3264 4790 6315	1691 3417 4942 6467	2044 3570 5095 6620	2196 3722 5247 6772	15
9: 2950	7077 8601	7229 8753	7382 8906	7534 9058	7697 9210	7839 9363	7991 9515	8144 9668	8296 9820	
1 2 3	4550125 1647 3170	0277 1800 3322	4550429 1952 3474	0581 2104 3627	4550734 2257 3779	0886 2409 3931	4551038 2561 4093	1191 2713 4235	4551343 2865 4388	
5 6	4692 6213 7734	4844 6365 7886	4996	5149 6670 8190	6300 6822 8342	5453 6974 8494	5605 7126 8646	5757 7278 9798	5909 7430 8950	
7. B	9254 4560774 2293	9406 0926 2445	9558	9710 1230 2749	9862	.0014	4560166 1686 3205	0318 1838 3357		
2860 1 2 3	3812 5330 6848	3964 5482 7000	4116 5634 7152	4268 5786 7303	4420 5938 7455	4571 6089 7607	4723 6241 7758	4875 6393 7910	5027 6545 8062	
3 4 5 6	8365 9882 4571398 2913	8517 / 0033 1549 3065	8669 4570185 1701 3216	8820 0337 1863 3368	8972 4570498 2004 3519	9124 0640 2156 3671	9275 4570791 2307 3822	9427 0943 2459 3974	9578 4571095 2610	1 :
8 9	4428 5943 7457	4580 6094 7608	4731 6246 7760	48R3 6397 7911	5034 6549 8062	5196 6700 6214	5337 6851 9365	5489 7003 8516	4125 5640 7154 8668	15
2870	8970 4580483 1996	9122 0634 2147	9273 4590786 2298	9424 0937 2449	9576 4581098 2600	9727 1239 2752	9878 4591391 2903	0029	4580181 1693 3205	
3 4	3507 5019 6530	3659 5170	5321	3961 5472	4112 5623	4263 5774	4414 5925	4565 6076	4717 6227	
6	8040	6681 8191	8342	6983 8493	7134 8644	7295 8795	8946	75871 9097	7738 9248	
6 7 8 9	9550 4591059 2567	9701 1210 2718	9851 4591361 2869	/ 0002 1511 3020	4590153 1662 3171	0304 1813 3322	4590455 1964 3472	0606 2115 3623	4590757 2266 3774	
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Mr. a. S. Bland's and ...

tens. 2940	4683621	2	4603016	4064	4604219	4260	4694807	8 Aced	4604002	dif. 148
1	5098	5246	4683916 5393	5541	4694212 5689	5836	4694507 5984	6131	4684803 6279	148
2	6574	6722	6870	7017	7165	7312	7460	7607	7755	8
3	8050	8198	8345	8493	8640	8788		9083	9231	8
4	9526	9673	9821	9968	4690116	0263	4690411	0558	4690706	147
5	4691000	1148		1443	1590	1738	1885	2033	2180	7
6	2475	2622	2770	2917	3064	3212	3359	3507	3654	7
7	3949 5422	4096 5569	4243 5717	4391 5864	4539	4685 6159	4833 6306	4980 6453	5127 6600	7
9:	6895	7042	7190	7337	7454	7631	7778	7926	8073	7
2950	8367	8515		8809			9251	9398	9545	
1	9839	9986	8662 4700134	0281	8956 4700428	9103 0575	4700722	0869	4701016	7
2	4701311	1458	1605	1752	1899	2046	2193	2340	2487	7
3	2782	2929	3076	3223	3370	3517	3664	3811	3958	7 7 7
4	4252	4399	4546	4693	4840	4987	5134	5281	5428	
5	5722	5869	6016	6163		6457	6604	6750	6897	7
6	7191	7339	7485	7632	7779	7926	8073	8219	9366	7
7 8	8660 4710129	8807	8954	9101	9248	9394	9541	9688	9835	7
9	1596	0275 1743	4710422 1890	0569 2037	4710716 2183	0863 2330	4711009 2477	1156 2624	4711303 2770	7
2960	3064	3211	3357	3504	3651	3797	3944	4091	4237	7
1	4531	4677	4824	4971	5117	5264	5411	5557	5704	7
2	5997	6144	6290	6437	6584	6730	6877	7023	7170	7
3	7463	7610	7756	7903	8049	8196	8342	8480	8635	146
5	8929 4720393	9075	9222 4720686	9368	9515 4720979	9661	9908 4721272	9954	4720101 1565	6
6	1858	2004	2151	2297	2444	2590	2736	2983	3029	6
7	3322	3468	3615	3761	3907	4054	4200	4346	4493	6
8	4785	4932	5078	5224	5371	5517	5663	6809	5956	6
9	6248	6395	6541	6687	6833	6980	7126	7272	7418	6
2970	7711	7857	8003	8149	8296	8442	8588	8734	8880	6
2	9173	9319	9465	9611	9757	9903	4730050	0196	4730342	6
3	4730634 2095	$0780 \\ 2241$	4730926 2397	1073 2533	4731219 2679	1365 2825	1511 2972	$\frac{1657}{3118}$	1803 3264	6
4	3556	3702	3848	3994	4140	4286	4432	4678	4724	6
51	5016	5162		5454	5600	5746	5891	6037	6183	6
6	6475	6621	6767	6913	7059	7205	7351	7497	7642	6
7	7934	8080	8226	8372	8518	8664	8809	8955	9101	6
8	9393	9539	9684	9830	9976	/0122	4740268	0413	4740559	6
9	4740851	0997	4741142	1288	4741434	1580	1725	1871	2017	6
2980	2308	2454	2600	2746	2891	3037	3183	3328	3474	6
1 2	3765	3911	4057	4202	4348	4494	4639	4785	4931	6
3	5222 6678	5368 6824	5513 6969	5659 7115	5805 7260	5950 7406	6096 7552	6241 7697	6387 7843	6
4	8134	8279	8425	8570	8716	8861	9007	9152		
5		9734			4750171		4750462		4750753	5
6	4751043	1189	4751334	1480	1625	1771	1916	2061	2207	5
7	2498	2643	2788	2934	3079	3225	3370	3515	3661	5
8	3951	4097	4242	4387	4533	4676	4823	4969	5114	5
9	5404	5550	5695	5840	5986	6131	6276	6421	6567	5
2990	6857 8309	7002 8455	7148 8600	7293 8745	7438 8890	7583 9035	7729 9180	7874 9326	8019 9471	5 5
1 2	9761	9906	4760051	0196	4760342	0487	4760632	0777	4760922	5
3	4761212	1357	1502	1648	1793	1938	2083	2228	2373	5
4	2663	2808	2953	3098	3243	3388	3533	3678	3823	5
6	4113	4258		454B		4838		5128	5273	
6	5563	5708	5853	599R	6143	6288	6433	6578	6723	5
7	7012	7157	7302	7447	7592	7737	7882	8027	9171 press	5
2	8461	8606	8751	8896	9041	9185	9330	9475	9620	
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Between $30000 = \log^{-1} 4.4771213$, and $30600 = \log^{-1} 4.4857214$.

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tena.	1	2 1	3	4	- 5	6	7	8	9 1	4
3000	4771357	1502	4771647	1792	4771936	2081	4772226	2371	4772515	14
1	2905	2949	3094	3239	3393	3528	3673	3819	3962	1
2	4252	4396	4541	4686	4830	4975	5119	5264	# 4CD	5
3	5699	6843	5987	6132	6276	6421	6566	6710	6855	8
4	7144	7288	7433	7578	7722	7867	8011	8156	8300	141
5	8589	8734	9878	9023	9167	9312		9601	97451	144
6	4780034	0179	4760323	0468	4780612	0757	4780901	1045	4781190	1
7	1479	1623	1768	1912	2056	2201	2345	2490	2634	-ill
6 7 8	2923	3067	3211	3356	3500	3645	3789	3933	4079	11
9	4366		4655	4799	4943	5089	5232	5376	5521	ill
		4511								500 5
3010	5809	5954	6098	6242	6396	6531	6675	6319	6963	4
1	7252	739ú	7540	7694	7829	7973	8117	6261	8405	4.1
21	8394	8833	8083	9126	9271	9415	9559	9703	9847	4
3.	4790135	0230	4790424	0569	4790712	0856	4791000	1144	4791298	4
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8	7335	7480	7624	7768	7912	8056	8200	8343	8487	4
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1		0357		-		0932	4801076	1220	4801363	4
3020	4800213		4900501	0645	4900789				2801	4
1 2	1651	1795	1939	2082	2226	2370	2513	2657	4238	
2	3089	3232	3376	3519	3663	3807	3950	4094		4
3	4525	4669	4812	4956	5100	5243	5397	5531	5674	4
4 5	5961	6105	6249	6392	6535	6679	6923	6967	7110	4
5	7397	7541	7684	7823	7972	8115	8259	8402	9546	4
6 7 6	893.3	8976	9120	9263	9407	9550	9694	9837	9981	143
7	4810268	0411	4310555	0693	4810842	0935	4811128	1272	4811415	33
	1702	1946	1989	2132	2276	2419	2563	2706	2849	3
9	3136	3279	3423	3566	3710	3953	3996	4140	4283	3
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7	88-57	9010	9152	9295	9437	9580	9722	9865	4840007	3 142
8	4840232	0435	4840577	0720	4840862	1004	4941147	1299	1432	142
9	1717	1859	2002	2144	2285	2429	2571	2714	2856	2
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1 2	5988	6130	6272	6414	6557	6699	6841	6984	7126	2
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6	1676	1818	1960	2102	2244	2396	2528	2670	2912	9
6 7	3096	3239	3381	3523	3665	3807	3949	4091	4233	2
0	4517	4659	4801	4943	5085	5227	5369	5511	5653	9
9	5937	6079	6221	6363	6505	6647	6783	6930	7072	2222222222
	1	2	3	4	5	6	7	6	9	"
<u> </u>				-		-				-

Between $31800 = \log^{-1} 4.5024271$, and $32400 = \log^{-1} 4.5105450$.

1	.	Betweer	1 3180	$00 = \log$	⁻¹ 4·50)24271, 8	and 32	400 = 10	g. 1 4	5105450	
1											dif.
2	3180										137
3 8503 8639 8776 8912 9949 9185 9321 9468 9594 7 7 7 50319358 7 7 303958 7 7 303958 7 7 303958 7 303958 7 7 303958 7 303958 7 7 30397 4093 4229 4366 4502 4633 4774 4911 5047 7 8 5319 5456 5592 5728 5864 6000 6137 6273 6409 7 7 7 7 7 7 7 7 7	1	5773	5910	6046	6183	6319	6456	6592	6729	6865	7
6	2	7139			7548		7821		8093		7
6	3	8503	8639	8776	8912	9049	9185	9321	9458	9594	4
6					0276	5030413					7
8	e e										1 4
8					4366		4638	4774	4911	5047	7
1900 8043 8179 8315 8451 8587 8724 8860 8996 9132 7				5592	5728		6000		6273	6409	1 7
1900 9043 8179 8315 8451 8587 8724 8860 8996 9132 7	ğ			6954	7090		7362	7498	7635		7
1 9404 9540 9676 9812 9948 7095 5040721 0357 5040493 7											
3	1										7
4 3485 3621 3757 3893 4029 4166 4301 4437 4573*136 6 6204 6339 6475 6611 6747 6883 7019 7155 7291 6 7 7562 7698 7834 7970 8106 8241 8377 8513 8649 6 8 8920 9066 9192 3928 9464 5999 9735 5971 5050077 661 200 1635 1771 1907 2043 2178 2314 2450 2585 2721 6 1 2992 3128 3364 3399 3535 3671 3806 3942 4078 6 2 4349 4465 4620 4756 4891 5027 5163 5298 5434 6 3 5705 5841 5976 6112 6247 6383 6518 6654 6790 6	2	5040765	0901	5041037	1173	5041309	11445		1717		7
4 3485 3621 3757 3893 4029 4166 4301 4437 4573*136 6 6204 6339 6475 6611 6747 6883 7019 7155 7291 6 7 7562 7698 7834 7970 8106 8241 8377 8513 8649 6 8 8920 9066 9192 3928 9464 5999 9735 5971 5050077 661 200 1635 1771 1907 2043 2178 2314 2450 2585 2721 6 1 2992 3128 3364 3399 3535 3671 3806 3942 4078 6 2 4349 4465 4620 4756 4891 5027 5163 5298 5434 6 3 5705 5841 5976 6112 6247 6383 6518 6654 6790 6	3	2125	2261	2397	2533		2305		3077		7
5 4945 4980 5116 5252 5389 5524 5660 5796 5932 6 6 6204 6339 6475 6611 6747 6863 7019 7155 7291 6 8 8920 9056 9192 9328 9464 9599 9735 9871 5050007 6 2000 1635 1771 1907 2043 2178 2314 2450 2585 2721 6 2000 1635 1771 1907 2043 2178 2314 2450 2585 2721 6 24349 4485 4620 4756 4991 5027 5163 5298 5434 6 4 7061 7196 7332 7467 7603 7738 7874 8009 8145 6 5 8416 8551 8687 8922 8958 9093 9229 9364 9500 6	4	3485	3621	3757	3893	4029	4165	4301	4437	4573	
7 7562 7698 7834 7970 8106 8241 8377 8513 5050007 6 8 8920 9056 9192 9328 9464 9599 9735 9971 5050007 6 2000 1635 1771 1907 2043 2178 2314 2450 2585 2721 6 2 4349 4485 4620 4756 4891 5027 5163 5298 5434 6 3 5705 5841 5976 6112 6247 7603 7738 6518 5298 5434 6 4 7061 7196 7332 7467 7603 7738 7874 8009 8145 56 5 8416 8551 8687 8822 9859 9093 9229 9364 9509 6 6 9771 9906 506042 0177 5060312 0448 5060583 0719 506	5	4345	4980	5116	5252		5524	5660		5932	
8 8920 9056 9192 9328 9464 9599 5050093 1228 1364 6 2200 1635 1771 1907 2043 2178 2314 2450 2585 2721 6 1 2992 3128 3264 3399 3535 3671 3606 3942 4078 6 2 4349 4485 4620 4756 4891 6027 5163 5298 5434 6 4 7061 7196 7332 7467 7603 7738 7874 8009 8145 6 5 8416 8551 8687 8822 9959 9031 9229 9944 9500 6 6 9771 9906 506042 0177 5060312 0448 506683 0719 506084 6790 6 8 2479 2614 2750 2885 3020 3156 3291 3272 2073 </th <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>7019</th> <th></th> <th>7291</th> <th></th>								7019		7291	
1	7										
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1 2992 3128 3264 3399 3535 3671 3606 3942 4078 6 2 4349 4485 4620 4766 4891 5027 5163 5298 5434 6 3 5705 5841 5976 6112 6247 6383 618 6664 6790 6 4 7061 7196 8687 8822 8958 9938 7774 8009 8145 6 5 8416 8551 8687 8822 8958 9938 9229 9364 9500 6 6 9771 9906 5060042 0177 5060312 0448 5060583 0719 5060854 6 7 5061125 1260 1396 1531 1667 1802 1937 2073 2208 6 8 2479 2614 2750 2885 3020 3156 3291 3426 3562 6 9 3333 3968 4103 4238 4374 4509 4644 4780 4915 6 3210 5186 5321 5456 5591 5727 5662 5997 6133 6268 6 1 6539 6674 6809 6944 7079 7214 7350 7495 7620 6 2 7891 8026 8161 8296 8431 8567 8702 8837 8972 6 3 9242 9378 9513 9648 9783 9918 5070053 0188 5070324 6 4 5070594 0729 5070864 0999 5071134 1269 1405 1540 1676 6 6 3225 3430 3566 3701 3836 3971 4106 4241 4376 6 6 32395 3430 3566 3701 3836 3971 4106 4241 4376 6 7 4646 4781 4916 5051 5186 5321 5456 5590 5725 6 9 5396 6130 6265 6400 6535 6670 6805 6940 7075 6 9 5396 6130 6265 6400 6535 6670 6805 6940 7075 6 9 5996 6130 6265 6400 6535 6670 6805 6940 7075 6 9 5998 5998 5998 9233 9368 9503 9638 9772 135 1360 1384 1386 5 5 5 5 5 5 5 5 5											
2 4349 4485 4620 4756 4391 5027 5163 5298 5434 6 3 5705 5841 5976 6112 6247 6383 6518 6664 6790 6 5 9416 8551 8687 8822 8958 9093 9229 9364 9509 6 6 9771 9906 5060042 0177 5060312 0448 5060583 0719 5060984 6 8 2479 2614 2750 2885 3020 3156 3291 3426 3562 6 9 3333 3968 4103 4228 4374 4609 4644 4760 4916 6 2 7891 8026 8161 8296 8431 8667 8702 8837 8972 6 3 9242 9378 9513 9648 9773 9918 5070053 0188 5070324 6 </th <th></th>											
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6 8416 8551 8687 8922 8958 9093 9229 9364 9500 6 9771 9906 5060042 0177 5060312 0448 5060583 0719 5060854 6 7 5061125 1260 1336 1531 1667 1802 1937 2073 2208 6 9 3333 3968 4103 4238 4374 4509 4644 4780 4915 6 3210 5186 5321 5456 5591 5727 5862 5997 6133 6268 6 1 6533 6674 6809 6944 7079 7214 7350 7495 7620 6 2 7891 8026 8161 8296 8431 8567 8702 8837 8972 6 2 7891 95733 9648 9783 9918 5070053 0188 5070324 6 4 <th< th=""><th></th><th>7061</th><th>7100</th><th></th><th>7467</th><th></th><th>7720</th><th>7074</th><th>0004</th><th>0190</th><th>6</th></th<>		7061	7100		7467		7720	7074	0004	0190	6
6 9771 9906 5060042 0177 5060112 0448 5060583 0719 5060854 6 7 5061125 1260 1396 1531 1667 1802 1937 2073 2208 6 9 3833 3968 4103 4238 4374 4509 4644 4780 4915 6 3210 5186 5321 5456 5591 5727 5862 5997 6133 6268 6 1 6533 6674 6809 6944 7079 7214 7350 7455 7620 6 3 9242 9378 9513 9648 9783 9918 5070053 0188 5070324 6 4 5070594 0729 5070864 0999 5071134 1269 1405 1540 1675 6 3 3295 3430 3566 3701 3836 3971 4106 4241 4376	5				8822						1 6
7 5061125 1260 1396 1531 1667 1902 1937 2073 2208 6 8 2479 2614 2750 2885 3020 3156 3291 3426 3562 6 3201 3486 4103 4238 4374 4699 4644 4780 4915 6 3210 5186 5321 5456 5591 5727 5862 5997 6133 6268 6 2 7891 8026 8161 8296 8431 8567 8702 8972 6 2 8972 6 3 9242 9378 9513 9648 9783 9918 5070053 0188 5070324 6 4 5070594 0729 5070864 0999 5071134 1269 1405 1540 1676 6 5 1945 2080 3253 3430 3566 3701 3836 3971 4106 4241 <	6					5060312				5060854	6
8											6
9	8	2479									6
1	9	3833	3968								6
1	3210	5186	5321	5456	5591	5727	5862	5997	6133	6268	6
2 7691 8026 8161 8296 9431 8567 8702 8837 8972 6 3 9242 9378 9513 9648 9783 9918 5070053 0188 5070324 6 5 1945 2080 2215 2350 2485 2620 2755 2890 3025 6 6 3295 3430 3566 3701 3836 3971 4106 4241 4376 6 7 4646 4781 4916 5051 5186 5321 5456 5590 5725 6 8 5995 6130 6265 6400 6535 6670 6805 6940 7075 6 3220 8694 8828 8963 9098 9233 9368 9503 9683 59721 135 2 1390 1525 1660 1794 1929 2064 2199 2334 2463 5	1					7079					6
4 5070594 0729 5070864 0999 5071134 1269 1405 1540 1675 6 5			8026	8161	8296	8431			8837		
5 1945 2080 2215 2350 2485 2620 2755 2890 3025 6 6 3295 3430 3566 3701 3836 3971 4106 4241 4376 6 7 4646 4781 4916 5051 5186 5321 5456 5590 5725 6 8 5995 6130 6265 6400 6535 6670 6805 6940 7075 6 9 7345 7480 7614 7749 7884 8019 8154 8289 8424 6 3220 8694 8828 8963 9098 9233 9368 9503 6638 59772 135 2 1390 1525 1660 1794 1929 2064 2199 2334 2468 5 3 2738 2873 3007 3142 3277 3411 3546 3681 3316 5 <th></th> <th></th> <th></th> <th></th> <th>9648</th> <th>9783</th> <th></th> <th></th> <th></th> <th>5070324</th> <th>6</th>					9648	9783				5070324	6
6 3295 3430 3566 3701 3836 3971 4106 4241 4376 6 7 4646 4781 4916 5051 5186 5321 5436 5590 5725 6 8 5995 6130 6265 6400 6635 6670 6805 6940 7075 6 9 7345 7480 7614 7749 7884 8019 8154 8289 8424 6 3220 8694 8828 8963 9098 9233 9368 9503 9638 9772 135 1 5080042 1077 5090312 0447 5080581 0766 5090581 5081121 5 3 2738 2873 3007 3142 3277 3411 3546 3681 3316 5 4 4084 4220 4354 4489 4624 4758 4893 5028 5163 5 <t< th=""><th>и -</th><th></th><th></th><th></th><th>09991</th><th>5071134</th><th></th><th>1405</th><th></th><th></th><th></th></t<>	и -				09991	5071134		1405			
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8 5995 6130 6265 6400 6535 6670 6805 6940 7075 6 9 7345 7480 7614 7749 7884 8019 8154 8289 8424 6 3220 8694 8828 8963 9098 9233 9368 9503 9638 9772 135 2 1390 1525 1660 1794 1929 2064 2199 2334 2468 5 3 2738 2873 3007 3142 3277 3411 3546 3681 3516 5 4 4085 4220 4354 4489 4624 4758 4893 5028 5163 5 5 5432 5567 5701 5336 5970 6105 6240 6374 6501 5 6 6778 6913 7047 7182 7367 7451 7566 7720 7855 5	2	3295		3500		383b		4106		43/0	
9 7345 7480 7614 7749 7884 8019 8154 8289 8424 6 3220 8694 8828 8963 9098 9233 9368 9503 9633 9772 135 1 5080042 0177 5080312 0447 5080581 0716 5080981 0986 5081121 5 2 1390 1525 1660 1794 1929 2064 2199 2334 2468 5 3 2738 2873 3007 3142 3277 3411 3546 3681 3316 5 5 5432 5567 5701 5836 5970 6105 6240 6374 6601 5 6 6778 6913 7047 7182 7317 7451 7586 7720 7855 5 7 8124 8259 89393 8528 8663 8797 8932 9606 9201			6120	4910 6965		8535		6005			6
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3		1300		1660		1929		2199	2334		
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7 8124 8259 8393 8528 8663 8797 8932 9066 9201 5 9 5090815 0949 5091084 1218 1353 1487 1622 1766 5090546 5 3230 2160 2294 2429 2563 2697 2832 2966 3101 3235 5 1 3504 3638 3773 3907 4042 4176 4310 4445 4579 5 2 4848 4982 5117 5251 5355 5520 5654 5788 5923 5 3 6191 6326 6460 6594 6729 6863 6997 7132 7266 5 4 7534 7669 7803 7937 8072 8206 8340 8474 8609 5 5 8877 9011 9146 9280 9414 9548 9682 9917 951 5	6	6778	6913	7047	7182	7317	7451	7586	7720	7855	5
9 5090815 0949 5091084 1218 1353 1487 1622 1756 1891 5 3230 2160 2294 2429 2563 2697 2832 2966 3101 3235 5 4 3504 3638 3773 3907 4042 4176 4310 4445 4579 5 4 6191 6326 6460 6594 6729 6863 6997 7132 7266 5 5 8877 9011 9146 9280 9414 9548 9682 9817 9951 5 6 5100219 0354 5100488 0622 5100756 0890 5101024 1159 5101293 5 7 1561 1695 1829 1964 2098 2232 2366 2900 2600 2634 5 8 2903 3037 3171 3305 3439 3573 3707 3841 <	7	8124		8393	8528		8797	8932			5
3230 2160 2294 2429 2563 2697 2832 2966 3101 3235 5 1 3504 3639 3773 3907 4042 4176 4310 4445 4579 5 2 488 4982 5117 5251 535 5520 5654 5788 5923 5 3 6191 6326 6460 6594 6729 6863 6997 7132 7266 5 4 7534 7669 7803 7937 8072 8206 8340 8474 8609 5 5 8877 9011 9146 9280 9414 9548 9682 991 951 5 6 5100219 0354 5100488 6622 5100756 0890 5101024 1159 5101293 5 7 1561 1695 1829 1964 2098 2232 2366 2500 2634 5	8	9470		9739	9873		0142	5090277			5
1 3504 3638 3773 3907 4042 4176 4310 4445 4579 5 2 4948 4982 5117 5251 5335 5520 5654 5788 5923 5 3 6191 6326 6460 6594 6729 6863 6997 7132 7266 5 4 7534 7669 7803 7937 8072 8206 8340 8474 8609 5 5 8877 9011 9146 9280 9414 9548 9682 9817 9951 5 6 5100219 0354 5100488 0622 5100756 0890 5101024 1159 5101293 5 7 1561 1695 1829 1964 2098 2322 2366 2500 2634 5 8 2903 3037 3171 3305 3439 3573 3707 3841 3976 5 9 4244 4378 4512 4646 4780 4914 5048 5182 5316 134											
2 4848 4982 5117 5251 5335 5520 5654 5788 5923 5 4 7534 7669 7803 7937 8072 8206 8340 8474 8609 5 5 8877 9011 9146 9280 9414 9548 9682 9817 9951 5 6 5100219 0354 5100488 0622 5100756 0890 5101024 1159 5101293 5 7 1561 1695 1829 1964 2098 2322 2366 2500 2634 5 8 2903 3037 3171 3305 3439 3573 3707 3841 3976 5 9 4244 4378 4512 4646 4780 4914 5048 5182 5316 134		2160									5
3 6191 6326 6460 6594 6729 6863 6997 7132 7266 5 5 8877 9011 9146 9280 9414 9548 9682 9817 9951 5 6 5100219 0354 5100488 0622 5100756 0890 5101024 1159 5101293 5 7 1561 1695 1829 1964 2098 2232 2366 2500 2634 5 8 2903 3037 3171 3305 3439 3573 3707 3941 3975 5 9 4244 4378 4512 4646 4780 4914 5048 5182 5316 134	Ĭ	3504	3639	3773	3907	4042	4176	4310	4445	4579	5
6 5100219 0354 5100219 0354 5100219 5101024 5101	Z		4962	6460		6790	6060		7120	7966	5
6 5100219 0354 5100219 0354 5100219 5101024 5101	ار ا	7524	7660	7902		9079					5
6 5100219 0354 5100488 0622 5100756 0890 5101024 1159 5101293 5 7 1561 1695 1829 1964 2098 2232 2366 2500 2634 5 8 2903 3037 3171 3305 3439 3573 3707 3841 3975 5 9 4244 4378 4512 4646 4780 4914 5048 5182 5316 134	K.	9977		9146		9414		9689			5
9 4244 4378 4512 4646 4780 4914 5048 5182 5316 134	6	5100219		5100488	0622	5100756				5101293	5
9 4244 4378 4512 4646 4780 4914 5048 5182 5316 134	7	1561			1964	2098		2366			5
9 4244 4378 4512 4646 4780 4914 5048 5182 5316 134	8	2903		. 3171	3305	3439	3573	3707		3975	5
1 1 2 3 4 5 6 7 8 9 1	9					4780	4914	5048			134
	•	1	2	3	4	5	G	7	8	9	

_						-			 	_
56							то 36,0		[Tab	
							$000 = \log$			
tens.	1 5105584	2 5718	3 510 5 8 5 2	4 5986	5 5106120	6 254	5106388	8 6522	9 5106656	ďÝ:
1	6924	7058	7192	7326	7460	7594	7728	1002	1770	4
2 3	8264 9603	8398 9737	8532 9871	8666	8800 5110139	8934 0273	6110407	9202 0541	9336 5110675	4
4	5110942	1076	5111210	1244	14/0	1612	5110407 1745 3084	1879	2013	4
5 6	2281 3619	2415 3753	3887	2682 4020	2816 4154	2950 4288	44.77	3218 4555	3351 4689	4
8	4957 6294	5090	5224	5358	5492	5625	5759	5893 7230	6026 7363	4
9	7631	6428 7764	5224 6561 7898	6695 8032	\$ 8165	6962 8299	8433	8566	8700	4
3250	8967	9101	9234	9368	9502			9903	5120036	4
1 2	5120303 1639	0437	5120570 1906	0704 2040	5120838 2173	0971 2307	5121105 2440	1236 2574	1372 2707	4
3	2974	1772 3108	3241	3375	วรกฉ	3642	3775	3909	2707 4042 5377	4
5	4309 5643	4443 5777	4576 5910	4709 6044	4843 6177	4976 6310	5110 6444	5243 6577	5377 6711	4
6	5643 6977	7111	7244	7377	4843 6177 7511 8844 5130177	6310 7644	7778	7911	8044	4
8	8311 9644	8444 9777	9578 9911	8711 20044	5130177	8978 0311	9111 5130444	9244 0577	9377 51 30 710	4
9	5130977	1110	9911 5131243	1377	1910	1043	1776	1910	2043	4
3260	2309	2442 3774	2576	2709 4041	2842	2975 4307	3108 4440	3242 4573	3375 4706	4
2 3	3641 4973	5106	5239	5372	5505	5638	5771	5905 7235	6038	133
3	6304 7635	6437 7768	3908 5239 6570 7901 9231	6703 8034	6836	6969 8300	7102 8433	7235 8566	7368 8699	3
5	8965	9093	9231 5140561	9364	8167 9497	9630	9763	9896	5140029	3
6	5140295 1624	1757	5140561 1890	0694 2023	5140827 2156	0960 2289		1225 2555	1358 2688	3
8	2953	3086	3219	3352	3485	3618	3751	3883	4016	3
9	4282	4415	4548	4681	4813			5212	5345	3
3270 1	5610 6939	5743 7071	5876 7204	6009 7336	6142 7469 8797	6274 7602	6407 7735	6540 7867	6673 8000	3
2	6939 8266 9593	8398	8531 9858	8664	8797	8929	9062	9195	9327	3
3	5150919	9725 1052	5151185	1317	5150123 1450	1583	5150389 1715	1848	5150654 1980	3
5 6	2246 3571	2378 3704	2511 3837	2643 3969	2776	2909 4234	3041	3174 4499	3306 4632	3
7	4897	5029	5162	5294	5427	5560		5825	5957	3
8	6222 7547	6354 7679	6487 7811	6619 7944	5427 6752 8076	6984 8209	7017 8341	7149 8474	7282 8606	3
3280	8871	9003	9136	9268	9400	9533	9665	9798	9930	3
1	5160195	0327	5160459	0592	5160724	0856	5160989	1121	5161253	3
2 3	1518 2841	1650 2973	1783 3106	1915 3238	2047 3370	2180 3502	2312 3635	2444 3767	2577 3899	3
4	4164	2973 4296	4428	4560	4693	3502 4825	4957	5089	5222	3
5	5496 6808	5618 6940	5750 7072	5893 7204	6015 7336	6147 7469	6279 7601	6411 7733	6543 7865	132
7	8129	8261	8393	8526	8658	8790	8922	9054	9186	2 2
8	9450 5170771	9582 0903	9714 5171035	9846 11 6 7	9978 5171299	$\binom{0111}{1431}$		1695	5170507 1827	2
3290	2091	2223	2355	2487	2619 3939	2751	2883	3015	3147	2
1 2	3411 4730	3543 4862	3675 4994	3807 5126	3939 5258	4071 5390	4202	4334 5654	4466 5785	2 2
3	6049	6181	6313	6445	657 7	6709 8027	6840	6972 8291	7104	2
41 5	7368 868 6	7500 8818	7631 8950	7763 9081	7895 9213	93451	8159 9477	9608	8422 9740	2 2
6	5180004	0136	5180267	0399	5180531	0663	9477 5180794	0926	5181058	2
7 8	1321 2638	1453 2770	1585 2902	1716 3033	1848 3165	1980 3297	2111 3428	2243 3560	2375 3692	2 2 2
9	3955	4086	4218	4350	4481	4613	4745	4876	5008	2
(1	2	3	4	5	6	7	8	9	

Table 1.] LOGARITHMS OF NUMBERS FROM 1 TO 36,000. Between 33000 = $\log .^{-1} 4.5185139$, and 33600 = $\log .^{-1} 4.5263393$.

н

58	1	OGAR	ITHMS O	F NU	MBERS F	rom 1	то 36,0	00.	[Tab	le 1.
	Between	33600	$0 = \log .$	1 4.52	963393, a	nd 349	$200 = \log$	z. ⁻¹ 4	5340961	
tens.	1	2	3	4	. 8	6	7	8	9	dif.
3360	5263522		5263781		5264039		5264297		5264556	130
1	4814	4944	5073	5202		5460		5719		0
2	6106	6235	6365	6494		6752		7010		0
	7398	7527	7656	7785		8043		8302		0
4	8689	8818		9076		9334		9593		
5	9980		5270238		5270496		5270754		5271 012	
6	5271270	1399	1528	1657	1786	1915	2044	2173	2302	9
7	2560	2689	2818	2947	3076	3205		3463	3592	9
8	3850	3979	4108	4237		4494		4752	4881	9
9	5139	5268	5397	5526	5655	5783		6041	6170	9
3370	6428	6557	6686	6814	6943	7072		7330	7459	9
1	7716	7845	7974	8103		8360		961 8	8747	9
2	9004	9133	9262	9391	9520	9648			5280035	9
3	5280292		5280550		5280807		5281065	1193	1322	9
4	1579	1708		1966		2223		2480		9
5	2866	2995	3124	3252		3510		3767	3896	9
6	4153	4282	4410	4539		4796		5053	5182	9
7	5439	556 8	5696	5825	5954	6082	6211	6339	6468	9
8	6725	6854	6992	7111	7239	7368	7496	7625	7753	9
9	8010	8139	8267	8396	8525	8653	8782	8910	9039	9 1

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0916 5321044

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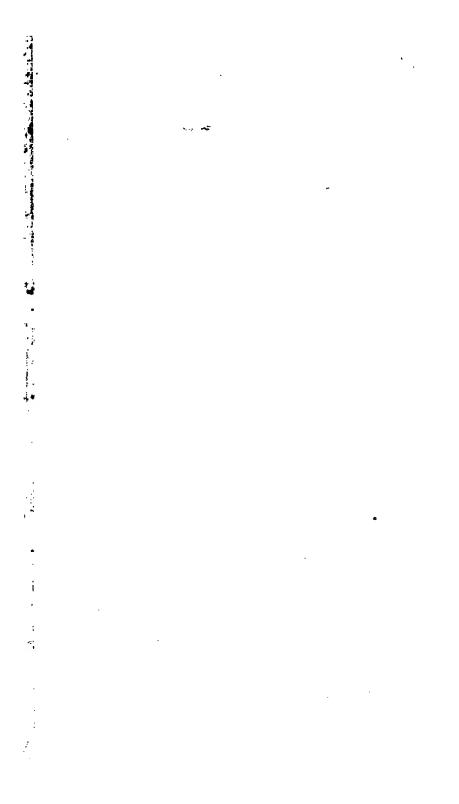
0661 5320789

9880

Between $34200 = \log^{-1} 4.5340261$, and $34800 = \log^{-1} 4.5415792$.

_	perween	13-1200	= 10g.	4 90	-	III OHIO	1,7		J-113 (3.6.	
3420	1 5340388	2 0515	3 5340642	0769	5 5340896	1022	5341150	1277	5341404	di f. 127
3420	1658	1785	1912	2039	2165	2292	2419	2546	2673	
2	2927	3054	3181	3308	3435	3561	3688	3815	3942	777777777777777777777777777777777777777
3	4196	4323	4450	4576	4703	4830	4957	5084	5211	7
4	5464	5591	5718	5845	5972	6099	6225	6352	6479	7
5		6859	6986	7113		7366	7493	7620	7747	1 7
6	8000	8127	8254	8381	8507	8634	8761	8888	9014	7
6	9268	9394	9521	9648	9775	1000	5350029	0155	5350281	7
8	5350535	0662	5350788	0915	5351042	1168	1295	14:12	1548	7
9	1802	1928	2055	2181	2308	2435	2561	2658	2815	7
3430	3068	3194	3321	3448	3574	3701	3827	3954	4081	7
1	4334	4460	4587	4713	4840	4967	5093	5220	5346	77777777777777
3	5599	5726	5852	5979	6105	6232	6359	6485	6612	7
3	6865	6991	7118	7244	7371	7497	7623	7750	7876	7
4	8129	8256	9382	6509	9635	8762	6888	9015	9141	7
5	9394	9520		9773		,0026			5360405	7
6		0784	5360911	1037	5361163	1290	1416	1543	1669	7
7	1922	2048	2174	2301	2427	2553	2680	2806	. 2932	7
8	3185	3311	3438	3564	3690	3817	3943	4069	4195	7
9	4449	4574	4701	4827	4953	5079	5206	5332	5458	
3440	5711	5637	5963	6089	6216	6342	6468	6594	6721	7 7 7
1	6973	7099	7225	7352	7478	7604	7730	7856	7982	7
2	8235	8361	8487	8613	6739	8866	8992	9118	9244	7
3	9496	9622	9749	9875	5370001	0127	5370253	0379		7
4	5370758	0884	5371010	1136	1262	1388	1514	1640	1766	7
5 6 7	2018	2144	2270	2396		2649	2775	2901	3027	7
0	3279	3405 4665	3531	3657	3783	3909	4035	4161	4287	7 126
9	4539 5799	5924	4791 6050	4917	5043	6169 6428	5295	5421 ccpo	5547	6
9	7058	7184	7310	6176 7436	6302 7561	7687	6554 7813	6680 7939	6806 8065	6
3450	6317	8443	8569	8694	8820	8946	9072	9198	9324	6
1	9575	6701	9827	9953	5380079	0205	5390330	0456	5380582	6
2	5390834 2092	0959 2217	5381085 2343	1211 2469	1337 2595	1463 2720	1588 2846	1714 2972	1940 3098	6
4	3349	3475	3601	3726	3852	3978	4103	4229	4355	6
		4732		4983	5109	5235	5360	5486	5612	
5 6 7	5863	5989	6114	6240	6366	6491	6617	6743	6868	6
7	7119	7245	7371	7496	7622	7747	7873	7999	8124	6
8	8375	8501	8627	8752	8879	9003	9129	9255	9380	6
9	9631	9757	9882	,0008	5390133	0259	5390384	0510	5390635	6
3460	5390887	1012	5391138	1263	1389	1514	1640	1765	1891	6
1	2141	2267	2392	2518	2643	2769	2894	3020	3145	6
2	3396	3522	3647	3772	3898	4023	4149	4274	4400	6
2	4650	4776	4901	5027	5152	5277	5403	5529	5653	6
4	5904	6030	6155	6280	6406	6531	6656	6782	6907	6
		7283		7534	7659	7784	7910	8035	8160	6
6	8411	8536	8661	8787	8912	9037	9163	9288	9413	125
7		9789	9914	0039	5400165	0290	5400415	0540	5400666	5
8	5400916	1041	5401167		1417	1542	1667	1793	1918	5
9	2168	2293	2419	2544	2669	2794	2919	3044	3170	- 5
3470	3420	3545	3670	3795	3920	4046	4171	4296	4421	5
1	4671	4796	4921	5047	5172	5297	5422	5547	5672	5 5
2	5922	6047	6172	6297	6423	6548	6673	6798	6923	- 5
3	7173	7298	7423	7548	7673	7798	7923	8048	8173	5
4		9548	8673	8798	8923	9048		9298	9423	- 5
5 6 7	9673	9798		,004B		0298		0548		5 5
6	5410923	1048	5411172	1297	1422	1547	1672	1797	1922	5
7	2172	2297	2422	2546	2671	2796	2921	3046	3171	5
8	3421	3546	3670	3795	3920	4045	4170	4295	4419	5
9	4669	4794	4919	5044	5168	5293	5418	5543	5668	5
	1	- 4	1 4	-	- 5	6	1	0	9	

	Betweer	3540	$0 = \log$.	1 4-54	90033, a		_	-	5563025	
tens.	1	2	3	4	5	6	# 400001	8	9 5491137	dif. 123
3540	5490155 1382	0278 1505	5490401 1627	1750	5490646 1872	1995	5490891 2118	1014 2240	2363	123
2	2608	2731	2853	2976	3099	3221	3344	3466	3589	ted test test test test test test test
2 3	3834	3957	4079	4202	4324	4447	4569	4692	4815	25
4	5060	5182		5427	5550	5672	5795	5917	6040	3
6	6285 7510	6407 7632	6530 7755	6652 7877	6775 8000	6897 8122	7020 8245	7142 8367	7265 8489	20
7	8734	8857	8979	9102	9224	9346	9469	9591	9714	3
B	9959	(0081	5500203	0326	5500448	0570	5500693	0915	5500938	. 3
9	5501182	1305	1427	1549	1672	1794	1917	2039	2161	3
3550	2406	2528	2651	2773	2895	3017	3140	3262	3384	03 03 03 03 03 03 03 03 03
1 2	3629	3751	3874 5096	3996 5219	4118 5341	4240 5463	4363 5585	4485 5708	4607 5830	5
3	4852 6074	4974 6197	6319	6441	6563	6685	6808	6930	7052	3
41	7296	7419	7541	7663	7785	7907	9030	8152	8274	1 3
5	8519	8640	8763	8885	9007	9129	9251	9373		1 3
7	9740	9862	9994 5511205	0106 1327	5510228 1449	0350 1571	5510472 1693	0594 1815	5510717 1937	(6
8	5510961 2181	1083 2304	2426	2548	2670	2792	2914	3036	3158	1
9	3402	3524	3646	3768	3990	4012	4134	4256	4378	1
3560	4622	4744	4866	4988	5110	5232	5354	5476	5598	122
1	5842	5964	6086	6209	6329	6451	6973	6695	6817	1 3
2	7061	7183	7305	7427	7549	7671	7793	7914	9255	
3	9280 9499	8402 9621	8524 9743	98646 9864	8768 9986	8890	9011 5520230	9133 0352	5520474	1
5	5520717		5520961		5521204	1326	1448	1570	1692	
6	1935	2057	2179	2301	2422	2544	2666	2788	2909	1
7	3153	3275	3396	3513	3640	3762	3883	4005	4127	
8	4370 5597	4492° 5709°	4614 5831	4735 5952	4857 6074	4979 6196	5100 6317	5222 6439	5344 6561	1
3570	6804	6925	7047	7169	7290	7412	7534	7655	7777	
1	8020	8142	8263	8385	8507	8628	8750	8871	8993	
2	9236	9358	9479	9601	9722	9844	9965	0087	5530209	1
3	5530452	0573	5530695	0916	5530938	1059	5531181	1302	1424 2639	
4	1667 2882	1789 3003		2032 3246	2153 3368	2275 3489	2396 3611	2517 3732	3854	1
5 6 7	4097	4218	4339	4461	4582	4704	4825	4947	5068	
7	5311	5432	5554	5675	5796	5918	6039	6161	6282	1 3
9	6525	6646	6767 7981	6889 8102	7010 8224	7132, 8345	7253 9466	7374 8588	7496 8709	
	7738	7860					9679	9801	9922	
3580 I	8952 5540164	9073 0286	9194 5540407	9315 0528	9437 5540650	9558 0771	5540892	1013	5541135	9
2	1377	1498	1620	1741	1862	1983	2104	2226	2347	24 64 64
3	2589	2710	2832	2953	3074	3195	3316	3438	3559	1
4	3801	3922		4165 5376	4286 5497	4407 5618	452S 5740	4649 5861	4770 5982	
6	5013 6224	5134 6345	6255 6466	6587	6708	6829	6951	7072	7193	121
7	7435	7556	7677	7798	7919	8040	9161	8282	8403	1
8	8645	8766	8987	9008	9130	9251	9372	9493	9614	1
9,	9856	9977	5550098	0219	5550340	0461	5550582	0703	5550924	1
3590	5551065	1196	1307	1428	1549	1670	1791	1912	2033 3242	1
1	2275 3484	2396 3605	2517 3726	2638 3847	2759 3968	2990 4099	3001 4210	3121 4330	3242 4451	
3 4	4693	4814	4935	5056	5176	5297	5418	5539	5660	1
	5902	6022	6143	6264	6385	6506	6627	6747	6868	
5	7110	7231	7351	7472	7593	7714	7835	7955	8076	
6	9318 9525	9646 9646	9559 9767	9680 9887	5560008	8921 0129	9042 5560249	9163 0370	9284 5560491	
7 8	5560732	0853		1094	1215	1336	1456	1577	1698	
9	1939	2060	2180	2301	2422	2542	2663	2784	2904	
+7	1	2	3	4	5	G	7	8	1 0	1



LOGARITHMS

OF

SINES, COSINES, TANGENTS, AND COTANGENTS.

6	4			LOG. B	INE Oo.			[Table II.
11	0'	1'	2"	3'	4'	5'	6'	7' "
0	- 00	64637261	6:7647561		7-0657860		7 2418771	7-3088239 60
1	4-6855749	709047	683602	432534	675918		30818	98567 59
2	9866049	779665	719347	456462	693901	55817	42832	7 2108870 58
3	5-1626961	849154	754800	480259	711810	70173	54813	19149 57 29404 56
4	2876349	917548	789965 824849	503926	729646	98745	66760 78675	39635 55
6	3845449 4637261	984882 4:5051188	859454	527465 550878	747408 765099		90557	49842 54
7	5306729	116497	893786	574164	782717	27131	7-2002407	60024 53
8	5886649	180838	927948	597327	800264	41254	14225	70183 52
9	6398174	244239	961645	620366	B17741	55332	26010	80318 51
10	6855749	306729	995182	643284	B35148	69364	37764	90430[50]
iii	7269676		6-029461	666082	862485	83351	49495	7 3200518 48
12	7647561	429074	061488	688760	869753	97293	61176	10583 48
13	7995182	488977	094265	711321	886953		72035	20624 47
14	8317029	54 ARIG	126796	733765	904085	25043	84462	30643 46
15	8616661	606361	159096	756094	921149	38953	96059	40638 45
16	8896948	663894	191137	778309	938147	52618	7-2607625	50610 44
17	9160238	720656	222954	800410	955079	66340	19160	60560 43
18	9408474	776695	254539	822400	971945	80018	30664	70497 41 80391 41
19	9643285	832019	285896	844279	988745	93654	42138	
20	9866049	886648	317029	866048			53582	00272 40
21	6.0077942	940599	347939	887709	22153		64996	7 3000131 39
22	0279975	993897	378632	909262	38760	34306	76300	09968 38 19783 37
23		6 6046529	409109	930708	55305	47772	8773-1	
24	0657861	098541	439373 469429	952050 973287	71787 88206	61197 74580	99058 7-2710353	29575 36 39345 35
25 26	0835,49 1005482	149939 200733	499277		7 1104564	87923	21619	49094 34
27	1169386	250941		7:0015451	20860		32856	58821 331
28	1327329	300575	558365	036381	37095	14485	44063	68525 32
29	1479729	349649	587611	057211	53270	27706	55242	76209 31
30	1626961	398174	616661	077941	69385	40886	66392	87870 30
31	1769366	446162	645519	098572	85440	54027	77514	97511 29
32	1907243	493627	674184		7-1201436	67128		7-3407130 28
33	. 2040888	54057B	702663	139544	17374	80189	99672	16727 27
34	2170539	587027	730955	159886	33253	93211	7:2810708	26304 26
35	2296429	632925	759065	180132		7 2106195	21717	35859 25
36	2418774	678461	786994	200285	64838	19140	32698	45394 24
37	2537766	723466	814745	220345	80545	32046	43651	54907 23
38	2653595	768009	842319	240313	96195	44914	54577	64400 22
39	2766395	812100	869719		7-1311789	57744	65475	73972 21
40	2876349	855748	R96948	279975	27328	70536	76346	83323 30
41	2983587	898962	924007	299671	42911	83290	97190	92754 19
42	3088242	941750	950898	319279	59239	96008		7-3502165 18
43	3190433	984121	977624	338796 358228	73612 88931	7-2208688 21331	19560	11555 17 20925 16
44 45	3290275		030589		7 1404196	33938	30296	30275 15
46	3397874 3483327	067641 108807	056829	396832	19408	46508	41006	39604 14
47	3576727	149595	092913	416006	34566	59041	51690	48914 13
48	3668161	189986	108841	435096	49672	71539	62347	58203 12
49	3757709	230013	134615	454103	64726	84001	72979	67473 [1]
50	3845449	269675	160237	473026	79727	96427	83584	76723 10
51	3931450	308978	185709	491868	94677		94164	B5954 9
52	4015782	347929	211033		7-1509676		7:3004718	95165 6
53	4098507	386533	236209	529307	24423	33494		7 3604356 7
54	4179686	424797	261241	547906	39221	45779	25749	13528 6
55	4259376	462727	286129	566426	53967	58030	36227	22681 5
36	4337629	500328	310975	584868	68664	70246	46679	31914 4
57	4414497	537607	335481	603231	83312	82429	57106	40929 3
58	4490029	574569	359948	621517	97910	94577	67509	50024 2
59	4564269	611218	384279	639727	7-1612459	7-2406691	77886 68239	59100 11 68157 0
60	4637261	647561 58'	408473 57'	657860 56'	26960 55'	18771 54'	53'	68157 0 52' "
	59'	36	37		SINE 890			J. 1
				LOG. CU	SINE OD			- 4

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T	able n.]			LOG. T	AN. 0°.			6	5
111	0'	1'	2'	3′	4'	5'	6'		"
0	— co		6.7647562			7.1626964			
1	4.6955749	709047	683603	432536	75921	41417	30825	98576	
11 21	9866049		719347	456464	93904	55821	42839	7 3108879	
	5-1626961	849154	754800	480261	7-0711813	70179 84488	54919 66767	19158 29413	
5	2876349 3845449	917549 984882	789966 824849	503928 527467	29649 47412	98760	78682	39644	
6		6-5051188	859455	550879		7:1712966	90564	49851	
7	5306729		893786	574166			7-2702414	60034	
8	5886649		927849		7-0600268	41259	14231	70193	
9	6398174		961646	620368	17744	55337	26017	80328	
10	6855749	306729	995183	643286	35151	69369	37771	90440	
111	7269676		6.6028462	666084	52488	83356	49492	7-3200528	
12	7647561	429074	061489	688762	69756	97298	61183	10592	
13	7995182	488977	094266	711323		7 1811195	72842	20634	
114	8317029	548066	126797		7 0904088		84469	30652	
15	8616661	606361	159087	756096			96066	40648	45
16	6896948	663985	191138	778311	38151		7 2607632	50620	
17	9160238	720656	222955	800412	55082		19167	60570	
18	9408474	776695	254540	822402	7194R		30672	70496	
19	9643285	832020	295897	844281	88749	93659	42146	80400	10.0
20	9866049	886649	317030	866050	7-1005484	7-1907252	53590	90282	
21	6.0077942	940599	347940	987711	22156	20802	65003		
22	0279975	993987	378633	909264	38764	34311	76367	09978	
23		6 6046530	409110	930710	55309		87741	19793	
.24	0657861	098542	439374	952052	71790		99066	29585	
25	0835149	149938	469429	973289	88210		7-2710361	39356	
.26	1005482	200733	499278		7-1104567	87928	21627	49104	
27	1169386	250941	528923			7-2001230	32863 44071	59831 69536	
28	1327329 1479729	300576 349649	558367	036383	37099 53274	14491 27711	55250	78219	
1000	100000000000000000000000000000000000000	4	597612	057213					
30	1626961	399174	616662	077943	69389		66400		30
31	1769366 1907249		645519	098575	85444	54032 67133	77521 88615	97521 7-3407140	
32	2040888	493627	674195		7-1201440		99679	16738	
34	2170538	540578 587027	702664 730957	139546 159889	17379 33257		7-2810716	26314	26
35	2296429		759066	180135	49079	7 2106201	21725	35870	
36	2418774	678461	786995	200288	64842		32706	45404	
37	2537766		914746	220348	80549		43659	54918	
138	2653595	768010	842330	240315			54585	64411	22
139	2766395	812101	869721	260191			65493	73883	21
40	2876349	855749	896949	279977	27332	70542	76354	83334	20
41	2983587	898963	924008	299673			87198	92765	19
42	3088242	941751	950900	319290	59242		98015	7-3502176	18
43	3190433		977626	338799	73616	7:2208694	7-2908805	11566	17
44	3290275	6-7026082	6.9004188	368231	88935		19668	20936	
45	3387874	067642	030589	377576			30304	30286	
46	3453327	108808	056830	396835	19412		41015	39615	14
47	3576727	149587	082914	416009	34570	59048	51698	48925	13
48	3669161	189987	108842	435099		71545	62356 72987	58215 67485	
49	3757709		134617	454105	64730	84007			
50	3945449		160239	473029			83593	76735	10
51	3931450		195711	491870		7-2709924	94173	85965	9
(52	4015792	347929	211034		7·1509580 24428		7·3004727 15255	95176 7:3604368	876
53	4098507	386534	236211	529310 547909		45786	25758	13540	É
55	4179686 4259376		261242 286130	566429	53972	58036	36235	22692	5
56	4337629		310976	584871	68669	40-0-0	46688	31926	4
57	4414497	537608	335482	603234	83316	82435	57115	40940	3
58	4490029		359950	621520	97914	94583	67517	50035	2
59	4564269		384290		7-1612464		77895	59112	2
190	4637261	647562	408475	657863	26964	19778	88248	68169	0
27	59'	58'	57'	56'	55'	54'	53'	52'	"
	-	-		Log. com	ran. 89°				

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66		**		Log. S	NE Oo.			Table n.
"	8'	9'	10'	11'	12'	13'	14'	15' "
0	7:3668157	74179681	74637255		7-5429065	7-5776694		7 6398160 00
1	77195	87716	44487	57756	35092	82249		7 6402933 59
1 2	86215	95737	51707	64321	41112	87806	08858	07800 58
3		74203742	61689	70876	47123	93356	14012	12612 57
4 5	7-3704198	11733	66112	77422	53125	98899	19161	17419 56
5	13162	19709	73296	83958	59120	7:5804435	24304	22221 55
6	22107	27670	80469	90483	65106	09964	29440	27017 54
7	31034	35617	87629	96999	71084	15485	34571	31808 53
8	39943	43549	94778	7-5103506	77053	21000	39695 44813	36593 52 41373 51
9	48832	51467	7-4701915	10002	83015	26506		
10	57705	59370	09041	16489	88968	32009	49926	46149 50
11	66559	67259	16154	22966	94913	37503	55032	50918 49
12	75396	75134	23257	29434	7.5500850	42990	60132	55683 48
13	84214	82995	30347	35892	06779	48470	65227	60442 47
14	93014	90841	37426	42340	12700	53943	70315	65196 46
	7-9801796	98673	44493	48779	18613	59409	75397	69945 45
16		7-4306491	51549	55208	24518	64869	80474 85544	74689 44
17	19308	14295	58594	61628	30414	70321		79428 43
18	28038	22085	65627	68038	36303	75767	90609	94161 43
19	36750	29861	72649	74439	42184	81206	95668	88389 41
20	45444	37624	79659	80830	48057	86638	7-6200721	93613 40
21	54122	45372	86658	87212	53921	92063	05768	98331 39
22	62782	53106	93646	93586	59778	97481		7-6-03043 30
23	71424	60827	7-4900623	99948		7.5902893	15844	07751 37
24	80050	68534		7.5206302	71469	08298	20873	12454 36
25	88658	76228	14542	12646	77302	13696	25897	17151 35
26	97249	63908	21485	19982	83127	19088	30915	21844 34
	7/3905824	91574	28417	25308	88945	24473	35927	26531 33
28	14381	99227	35338	31625	94755	29851	40933	31214 32
29	24342	7:4406866	42248	37933	7-5600557	35223	45934	35991 31
30	31446	14492	49147	44231	06352	40588	50928	40563 30
31	39953	22104	56035	50521	12138	45946	55917	45231 29
32	48444	29703	62913	56801	17917	51298	60901	49893 28
33	56918	37289	69779	63073	23689	56643	65878	54550 27
34	65375	44862	76634	69335	29452	61991	70850	59203 26
35	73916	52421	83479	75589	35208	67313	75816	63850 25
36	82241	59968	90313	81833	40957	72639	60777	69492 24
37	90650	67501	97136	88068	46698	77958	85732	73130 23
38	99042		7:4903949	94295	52431	83270	90681	77762 22
	7-4007418	82529	10750		58157	88576	95624	82390 21
40	15778	90023	17541	06721	63875		7 6300562	87012 20
41	24121	97504	24322	12920	69585	99169	05495	91630 19
42		7.4504973	31092	19111	75289		10421	96243 19
43	40761	12428	37851	25294	80984	09735	15342	7 6600850 17
44	49057	19971	44600	31467	86672	15009	20258	05453 16
45	57337	27302	51339	37631	92353	20277	25168	10052 1
46	65601	34719	58067	43787	98026	25538	30073	14645 14
47	73950	42124	64794	49934	7-5703692	30792	34971	19233 13
48	82083	49516	71492	56073	09351	36040	39865	23317 12
	90301	6 6896	78138	62202	15002	41292	44753	28395 11
50	98503	64263		68324	20646	46518	49635	32969 10
51	7.4106689	71618	91551	74436	26282	51747	54512	37533 9
52	14960	78960	98217	80540	31912	56970	59384	42103 8
53	23016	86290		96635	37533	62187	64250	46662 7
54	31156	93607	11519	92722	43148		69110	51217 6
55		7-4600912	19154	98800	49755	72602	73965	55767 6
56	47392	08205	-24790		54356	77800	78815	60312 4
57	55487	15496	31395		59949	82991	83659	64852 3
58	63567	22754	38000		65534	B8177	88498	69399 2
59	71631	30011	44595		71113	93356	93332	73919 1
60	79681	37255			766S4	98530	98160	79445 0
1	51'	50'	49'	1 48'	47	46'	45'	44' "
1				rog. co:	SINE 89			

T	able 11.]			LOG. T.	AN. 00.			67
11	8'	9'	10'	11'	12'	13'	14'	15' ["
	7-3668169	7-4179696		7:5061203				7-6398201 60
1	77207	87731	44506	57778	35119			7 6403024 59
2	86227	95752	51726	64343	41138	87837	08894	07842 58
3	95228	7-1203757	58934	70899	47149	93387	14049	12654 57
4 5	7-3704210	11748	66130		53152		19197	17461 56
6	13174 22119	19724 27685	73315 80487	63980 90506	69147 65133		24340 29477	22262 55 27059 54
2	31046	35632	87648	97022	71111	15517	34607	31850 63
7 8	39955	43564		7-5103528	77080	21032	39732	36635 52
9	48845		7-4701934	10025	83042	26540	44850	41416 51
10	57718 66572	59386 67275	09060 16173	16512	88995	32041	49963	46191 50
11 12	75408	75150	23276	22989 29457	94941 7-5200878	37535 43022	55069	50961 49 55725 48
13	84226	83010	30366		06807	48502	60169 65264	60485 47
44	93026	90857	37445	42363	12728	53975	70352	65239 46
	7-3801809	98689	44513	49802	18640	69441	75435	69988 45
16	10574	7 4306507	51569	55231	24545	64901	80511	74732 44
17	19321	14311	58613		30442	70353	85582	79471 43
18	28051	22101	65646	69061	36331	75799	90647	94204 42
19	36763	29877	72668	74462	42212	81238	95705	88933 41
20	45457	37640	79679	80854	48084	86670		93656 40
21	54134	45388	86678	87236	53949	92096	05805	98374 39
22	62794	53123	93666	93608	59806	97514		7-6503087 38
23	71437		74800642	99972	65656		15882	07795 37
24	80063	68551		7-5206326	71497	08331	20911	12497 36
25	88671	76244	14562	12670	77330	13730	25935	17195 35
26	97263	83924	21505	19006	83156	19121	30953	21888 34
27	7 3905837	91590	28437	25332	88974	24506	35965	26575 33
28	14395	99243	35359	31649	94784	29884	40972	31258 32
29	22935	7-4406882	42269	37957	7.5600586	35256	45972	35935 31
30	31459	14508	49168	44256	06380	40621	50967	40608 30
31	39967	22121	56056	50545	12167	45980	55956	45275 29
32	48457	29720	62933	56826	17946	51331	60939	49937 28
33	56931	37306	69799	63097	23719	56677	65917	54595 27
34	65389	44879	76655	69360	29481	62015	70889	59247 26
35	73830	52438	83500	75613	35239	67347	75855	63895 25
36	82255	59985	90334	91958	40986	72673	80816	68537 24
37	90663	67518	97167	88093	46727	77992	85771	73174 23
38	99055	76035 82546	7-4903969	94319	52460	83304	90720	77807 22
39	7-4007431	0.00		7-5300537	58186	88611	95664	82435 21
40	15791	90040	17562	06746	63904		7-6300602	87057 20
41	24135	97521	24343	12946	69615	99203	05534	91675 19
42		7-4504990	31113	19137	75318		10461	96288 18
43	40775 49071	12446	37872	25319	81014	09770		7-6600896 17
44	57351	19889 27319	44621 51360	31492	86702	15044	20298	05499 16
46	65616	34737	28088	37657	92383	20311	25208	10097 15
47	73964	42141	64806	43813	98056 7·5703722	25572 30827	30113 35012	14690 14 19279 13
48	82097	49534	71513	56098	09381	36075	39905	23863 12
49	90315	56913			15032		44793	28441 11
50	98517	64281	84897	68349	20676			
51	7-4106703	71635	91573	74462	26313		49676	33015 10
52	14875	78978	98239		31942	51782 57005	54553 59424	37535 9 42149 8
53	23030		7-5004895		37564	62222	64290	42149 8 46709 7
54	31171	93625	11541	92748	43179	67433	69151	51263 6
55	39296	7.4600930	18176		48786	72637	74006	55813 5
56	47406	08223		7-5404896	54386	77835	78856	60359 4
57	65501	15504	31417			83027	83700	64899 3
58	63581	22773			65565	88213	88539	69435 2
59 60	71646	30030		23055	71144	93392	93373	73966 1
60	79696	37273	51203		76715	98566	98201	78492 0
"	51'	50′	1 49'	1 48'	47'	46'	45"	44' "
1				LOG. CO	TAN. 89°	٠.		

6	8			LOG.	sine 0°.			[Table :	Π.
7	16'	1 17	18'	19'	20′	21'	22′	23′	77
0		7-6941733		7-7424775				7-8954507	
ļ	82967 87484	45988 50240	93986 99001	28583 32388	51154	62872	64747 68033	57653 60797	50 50
2 3	91996		7·7202013	36189	54769 58380	66315 69755	71317	63938	57
4	96503	58730	06021	39987	61989	73192	74599	67077	
5	7-6701006	62969	10026	43781	65594	76627	77878	70214	58
6	05504	67204	14027	47573	69197	80058	81154	73348	
8	09998 14486	71435 75662	18024 22017	51360 55145	72797 76393	83488 86914	84428 87699	76481 79611	53 52
9	18970	79884	26007	58926	79987	90337	90966	82738	
10	23450	84103	29993	62705	83577	93758	94235		50
11 12 13	27925 32395	98317 92528	33976 37955	66479 70251	97165 90750	97177 7·7900592	97499 7-8100761	88987	10
13	36861	96734	41930	74019	94332	04005	04020	92108 95227	
14	41322	7.7000936	45902	77784	97910	07415	07227	98343	
15	45779	05134	49869	81546	7.7701486	10823	10531	7-8001458	
16	50231	09328	53834	85304	05059 06629	14228	13783	04570	44
17 18	54678 59121	13518 17704	57794 61752	89059 92811	12196	17630 21029	17032 20279	07680 10787	43 42
19	63559	21886	65705	96560	15760	24426	23524	13893	
20	67993	26064	69655	7-7500306	19322	27820	26766		40
21 22	72422	30239	73601	04048	22890	31212	30006	20097	
22 23	76847	34407	77544	07787	26435	34601	33243	23195	
23	81267 85693	39573 42735	81483 85419	11523 15255	29988 33537	37987 41371	36478 39711		37 36
24 25	90094	46893	89351	13985	37084	44752	42941	32478	
26	94501	51047	93279	22711	40628	48130	46168	35568	
27	98904	55197	97204	26434	44169	51506	49394		33
28 29	7·6803302 07695	63485	7·7301125 05043	30154 33871	47707 51242	54879 58250	52617 55837		32 31
30	12084	67623	08957	37584	54774	61617	59055		30
31	16469	71757	12868	41294	58303	64983	62271		29
32	20849	75887	16776	45001	61830	68345	65494		28
33 34	25224	80014	20679	48705	65354	71705	68695	57136	27
34 35	29596 33963	84136 88254	24579 28476	52406 56104	68874 72392	75063 78418	71904 75110		26 25
36	38325	92369	32369	59798	75907	81770	78314		24
37	42683	96490	36259	63490	79420	85120	81516	69413	23
38	47037	7100586	40145	67178	82929	88467	84715		22
39	51397	04689 08788	44028 47908	70863	86436	91811	97912		21
40 41	55732 60072	12883	51783	74545 78224	89939 93440	95153 98493	91106 94298	78598 81655	20 19
42	64409	16975	55656	81900		7.8001830	97488	84710	18
43	68741	21062	59525	85572	7.7800434		7-8200676	87763	17
44	73069	25146	63390	89242	03926	08496	03861	90814	10
$\frac{45}{46}$	77392 81711	29225 33301	67252 71111	92908 96572	07416 10903	11825 15151	07043 10224	93863 96909	15 14
47	86026	37373		7.7600232	14387	18475	13402	99954	
48	90337	41442	79818	03889	17968	21797	16578	7.8402996	12
49	94643	45506	82666	07543	21347	25116	19751	06036	11
50 51	98945 7·6903243	49567 53624	86511 90353	11194 14842	24822	28432 31746	22922 26091	09074	10
51 52	07536	57677	94191	18487	28295 31765	35058	29258	12110 15144	2,0
53	11826	61726	98026	22129	35233	38367	32422	18176	7
54	16111		7-7401857	25768	38697	41673	35584	21205	6
55	20392	69814	05685	29403	42159	44977	38743	24233	5
56 57	24668 28941	73852 77886	09510 13331	33036 36666	45618 49075	48278 51577	41901 45056	27258 30281	4
58	33209	81917	17149	40292	52528	54873	48209	33302	2
59	37473	85943	20964	43916	55979	58167	51359	36321	ī
60	41733	89966	24775	47537	59427	61458	54507	39338	6543210X
["]	43′	42	41'	40′	39' NE 89°.	38′ I	37′	36′	
1				LOG. COS	ME OD.				- 1

T	able 11.]				an. 0°.			6	_ 1
["	16'	17' 7 6941786	18′	19′ 7•7424841	20 ′ 7·7647610	21′ 7·7859508	22′ 7:8061547	23′ 7 82 54604	~
0	83014	46042	94045	28649	51228	62954	64836	57750	59
2	87531	50293	98061	32454	54843	66396	68123	60894	
3 4	92043 96551	54541 58784	7·7202073 06081	36255 40053	58454 62063	69836 73274	71407 74688	64036 67175	
5	7-6701053	63023	10086	43848	65669	76708	77967	70312	55
6	05552 10045	67258 71489	14087 18084	47640 51428	69271 72871	80140 83569	81244 84518	73446 76579	
8	14534	75716	22078	55212	76469	86996	87789	79709	
9	19018	79938	26068	58994	80061	90420	91059	82837	- 11
10	23498	84157	30054	62772	83652	93841	94325	85962	
11 12	27973 32443	88371 92582	34037 38016	66547 70319	97240 90825	97259 7·7900675	97590 7-8100851	89086 92207	49 48
13	36909	96788	41991	74087	94407	04088	04111	95326	47
14	41371	7.7000990	45963	77952	97986	07498	07368		46
15 16	45827 50279	05189 09383	49931 53895	81614 85372	7·7701562 05135	10906 14311	10622 13874	7·8301557 04669	
17	54727	13573	57856	89128	08705	17713	17124	07779	43
18	59170	17759	61813 65767	92880	12272 15836	21113	20371 23615	10887 13992	47
19 20	63608 68042	21941 26119	69717	96629 7·7500374	19398	24510 27904	26858		40
21	72471	30293	73663	04117	22956	31296	30098	20197	39
22	76896	34463	77606	07856	26512	34685	33335		38
23 24	81317 85733	38629 42791	81545 85481	11592 15325	30064 33614	38071 41455	36570 39803		37 36
25	90144	46949	89413	19054	37161	44836	43033	32579	35
26	94551	51103	93342	22780	40705	48215	46261	35669	34 33
27 28	98953 7 -6 803351	55253 59399	97267 7· 7 301188	26504 30224	44246 47784	51590 54964	49486 52709	38757 41843	$\frac{33}{32}$
29	07745	63541	05106	33940	51319	58334	55930	44926	31
30	12134	67679	09020	37654	54851	61702	59148	48007	30
31 32	16519 20899	71813 75944	12931 16839	41364 45072	58381 61907	65068 68431	62364 65578	51087 54163	ž
33	25275	80070	20742	48776	65431	71791	68789	57238	27
34	29646	84193	24643	52477	68952	75148	71998	60311	26 25
35 36	34013 38376	98311 92426	28540 32433	56174 59869	72470 75985	78503 81856	75204 78408		24 24
37	42734	96537	36323	63560	79498	85206	81610	69515	23
38 39	47088 51438	7·7100643 04746	40209 44092	67249 70934	93007 96514	88653	84809 88006	72580 75641	$\frac{22}{21}$
40	55783	08846	47972	74616	90018	91898 95240	91201	78701	
41	60124	12941	51848	78295	93519	98579	94393	81758	19
42	64460	17032	55720	81971	97017	7-9001916	97583	84813	18
43 44	68792 73120	21120 25203	59589 63455	85644 89313	7·78 0 0513 04 005	05251 08582	7-8200770 03956	97867 90918	16
45	77444	29283	67317	92980	07495	11912	07139	93966	15
46	81763	33359	71176	96643	10982	15238	10319	97013	14
47	96078 90389	37432 41500	75031 79883	7·7600304 03961	14466 17948	18563 21884	13497	7·8400058 03100	
49	94695		82731	07615	21426	25203	19847	06140	11
50	98997	49625	86577	11266	24902	28520	23018	09179	10
51 52	7 -690 3295 07589		90418 94257	14915 18560	28375 31845	31834 35146	26187 29354	12215 15249	9
53	11878	61785	98091	22202	35313	38455	32518	18280	7
54	16163		7-7401923	25840	38778	41761	35680	21310	109876543210
55 56	20444 24721	69873 73911	05751 09576	29476 33109	42240 45699	45065 48366	38840 41997	24338 27363	4
57	28993	77945	13397	36739	49155	51665	45153	30387	3
58 59	33262 37526		17215 21030	40366 43989	52609 56060	54962 58256	48305 51456	33408 36427	1
60	41786	90026	24841	47610	59508	61547	54604	39444	Ô
"	43'	42	41'	40'	39′	38′	37	36′	"
<u> </u>				LOG. CO	TAN. 890	•			

70)			Log. 8	INE Oo.			Table :
1	24'	25'	. 26'	27'	1 28'	1 29'	30'	31'
0/3	748439338	7.8616623	7.8786953	7 8950854	7-9108793	7-9261190		7-9650819
1	42353	19517	89736	53534	11378		10831	53153
2	45366			56212	13960		13241	55486
3	48377	25300		58889	16542		15651	57818
4	51385		98075	61564	19121	71162	18059	60149
5	54392		7-8:00850	64237	21699		20465	62478
2	57396		03625	66909	24276		22871	64806
7	€0398		06397	69579	26851	78626	25275	
	63399		09167	72249	29425	81111		67133
	66397	42602	11936	74914	31997		27677	69458
						83595	30079	71782
H	69393	45479	14703	77580	34567	66077	32479	74105
	72387	48354	17469	80243	37136	P8558	34877	76427
1	75379	51228	20232	82905	39704	91037	37275	78747
	78369	54099	22994	65565	42269	93516	39671	81067
L	81357	56968	25754	88224	44834	95992	42066	83385
ı	84343	59836	28512	90881	47397	98467	44459	B5702 4
l	97326	62702	31269	93536	49958	7:9000941	46851	98017
ı	90308	65565	34023	96190	52518	03414	49242	90331
1	93238	68427	36776	98842	55076	05885	51631	92645 4
	96265	71287		7-9001493	57633	08354	54019	949564
					-			
	99241	74145	42277	04141	60189	10823	56406	97267
7	8502215	77001	45025	06789	62743	13289	58792	99576
	05186	79856	47771	09434	65295	15755	61176	7-9601885
	08156	82708	50515	12078	67846	18219	63559	041925
	11123	85559	53258	14721	70395	20682	65940	06497 3
	14088	88409	55999	17362	72943	23143	68321	08802 3
	17052	91254	58738	20001	75489	25603	70700	11105 3
	20013	94099	61475	22639	78034	28061	73077	13407 3
	22973	96942	64211	25275	80578	30518	75454	15708 3
1	259300	99784	66945	27909	83120	32974	77829	1800813
l								
Į.		7.8702623	69677	30542	85660	35428	80203	20306 3
	31839	05461	72407	33173	88199	37881	82575	22603 2
	34790	08296	75136	35803	90736	40332	84946	24899 2
	37739	11130	77863	38431,	93272	42783	87316	271942
	40687	13962	80589	41057	95807	45231	89685	29487 2
	43632	16792	93312	43662	98340	47679	92052	31780 2
	46575	19621	86034	46305	7.9200871	50125	94418	34071 2
	49517	22447	88754	48927	03401	52569	96783	36361 2
	52456	25272	91473	51547	05930	55012	99146	38649 2
	55393	28095	94190	54166	08457		7-9601508	40937 2
	58329	30916	96905	56763	10983	59895	03869	43223 2
	61262	33735	99618	59398	13507	62334	06229	45508 1
	64193	36552	7.8902330	62012	16030	64772	08587	47792 1
	67123	39367	05040	64624	18551	67208	10944	50075 1
	70050	42181	07749	67235	21071	69643	13300	52356 1
	72976	44993	10455	69844	23589	72077	15654	54637 1
	75899	47803	13160	72451	26106	74509	18008	569161
	78821	50611	15864	75057	28621	76940	20360	591941
	81740	53417	18565	77662	31135	79369	22710	61470 1
	6465B	56222	21265	80265	33648	81798	25060	63746 1
	87574	59025	23963	82866	36159	84224	27408	66020 1
	90487	61826	26660	85466	38668	86650	29755	68293
	93399	64625	29355	88064	41177	89074	32100	70565
	96309	67422	32048	90660	43683	91497	34444	72836
	99217	70218	34740	93256	46188	93918	36787	75106
7	8602123	73011	37430	95849	48692	96338	39129	77374
	05027	75B03	40118	98441	51195	98757	41470	79641
	07929	78594		7.9101031		7-9401175	43809	81907
	10829	81382	45489	03620	56195	03591	46147	64172
	13727	84168	48173	06208	58693	06005	48484	86436
	16623	86953	50854 33'	08793	61190	08419 30'	39'	88698 28'
	35′ (34'	33	32'	31'	90	23	25

Tal	ble n.]			LOG.	TAN 0°				71
1/2	24'	25'	26'	27'	28'	29'	30'	31'	18
		7.8016739							
1 2 3	42459	19632 22526	29861 92642	53668 56347	7 9111522 4105	6333	7-94 0996 3407	3330 5663	
2	45472 48483	25415	95422	59023	6686	8826		7995	
4	51492	28304	98199	61699		7-9271317		7-9560326	
5	54498	31191	7.8800975		7.9121844	3807	7:9420632	2655	55
6	57503	34076	03750	67044		6295	3037	4984	
7	60505	36958	06522	69714	6996	6782	5441	7310	
S 9	63506 66504	39839 42719	09293 12062	72383	7-9132142	7-9291267	7944	9636 7-9571961	
10		45596		77715		6233			
11	69500 72494	48471	14829 17594	60379			5045		
12	75487	51344	20358	83041		7-9291194	7442		
13	78477	54216	23120		7-9142416	3672		7.9581246	47
14	81465	57085	25880	88360	4980		7-9412233		
15	64451	59953	28639	91017	7543			5881 8197	
16 17	87435 90416	62819 65663	31395 34150	93673	7-9150105 2665	7-9301099 3571		7-9590511	
18	93396		36903	98979		6043	7-9451800	2825	
19	96374			7-9:01630					
20	99350	74263	42404	04279	7-9160336	7-9310991	6575	7447	40
	7.8502323		45152	06926		3448	8961	9757	39
22	05295	79974	47899	09572				7-9602065	
23	08265	82827	50643	12216	7994	8378		4373 6678	
24 25	11232	25677	53386			7·9·120840 3302	6110 8491	8983	
26	14198 17161	88526 91373	56127 58866	17500 20139	3091 5638			7-9611287	
27	20123		61604	22777		8220		3589	
28	23083	97062	64339	25413	7-91807:27	7 9330678	5624	5890	
29	26040	99903	67074	28048	3269	3133	8000	8190	31
30		7/8702743	69806	30691	5809			7-9620488	
31	31949	05580	72537 75266	33312		9041	2746		29
32	34900		75266			7·9340493 2943	5118 7488		
34	37850 40797	11250 14082	77993 80718	38570 41197	3422 5957	5392			
35	43743			43822	8490			7-9631963	
36	46686	19741	86164			7 9360286	4590	4254	24
37	49628		88885	49067	3552	2730	6955	6544	
38	52567	25393	91603	51687	6081	5174		8833	
39	56505	28215	94320	54306	8608			7-9641121	
40	58440 61374		97036	56923 59539	7-9211134 3658	7:9:60057 2496	4042 6402	3408 5693	
42	64305		99749 7-8902461	62153		4934	8760		
43	67235		05171	64765	8702			7 9650260	
44	70163	42303	07890		7-9221222	9805	3474	2541	16
45	73088		10587	69985				4822	
46	76012	47925	13292	72593	6258	4672	8182	7101	
48	78934 91853	50733 53540	15995 18697	75199	8774 7-9231288		7-9520534	9379 7-9661656	
49	84771	56344	21397	80407		7-9361961	5234	3932	
50	87687	59147	24096	83008		4388	7582		
51	90601	61949	26792	85609		6814	9929	8480	9
52	93513	64748	29487		7 9241330	9238	7.0532275	7-9670752	8
53	96423	67545	32181	90803		7-9391661	4620	3023	
54	99331	70341	34873	93399			6963	5293	6
55	7-8602237 05141	73135 75927	37563 40251	95992	9846 7-9251349	6503 8922	9305 7 9541646	7561 9829	4
57	08043	79717		7 9101175	3850			7-9682095	3
58	10943	81506	45623	03764	6349	3756	6323	4360	2
59	13841	84293	49306	06352	8847	6170	8660	6624	1
60	16738	87077	50998		7-9261344		7 9500996	8886	0
1	35′	34	33′	32'	31'	30'	29'	28'	
				TOE CO.	TAN. 89°	4			_

72				LQG. 8	SINE.			[Table	U
111	32	33'	34'	35'	36'	37'	38'	39'	1
0	7-9688698	7-9622334	7-9951980	8-0077867	B-0200207	8-0319195	8-0435009	8-0547814	6
1	7-9690960	4527	4108	9934	2217	8-0321150	6913	9670	5
2	3220	6718	6235	8.0092001	4226	3105	8816	8-0551524	16
3	5479	8909		4066	6234	5059	8-0440719	3378	15
4	7736	7-9831098		6131	8242	7012	2621	5231	8
6	9993	3287	2611	8194		8965	4522	7084	į
6	7-9702248	5474		8 0090257	2253	8-0330916	6422	8935	ľ
	4503	7660			4258	2866	8321	8-0560786	H
7 8	6756	9845		4379	6261		80 450 220	2636	
9	9008	7-9842029		6439		6765	2117	4485	
-								6333	н
0	7-9711258	4212	3216	8497		8713	4014		
1	3508	6394	5334			8-0340660	5910	8181	
2	5756	8574	7451	2612		2606	7905		
13		7-9850754	9566	4668		4551	9700	1874	
4	7-9720250	2933		6722			8-0461593	3719	ł
5	2495	5110		8776	8-0230261	8439	3486	5563	Ŷ
6	4739	7286	5908	8-0110829	2257		5378	7407	
7	6981	9461	9020	2881	4252	2323	7269	9250	
B	9222	7-9861636	7-9990130	4932	6247	4264	9159	3 0581092	١
9	7-9731463	3809		6982	8240	6204	8-0471048	2933	H
20		5981		9031	3	8143	2937	4774	d
	3702		4349				4825	6614	
1	5940	8151	6456			2019	6712	9453	
2	8177	7-9870321	8663					8-0590291	
3	7-9740412	2490				3956		2129	
14	2647	4658					8-0480483		
Б	4890	6824	4877	9261		7926	2368	3965	
G	7113	8989			2169	9760	4251	5901	
27	9344	7-9881154	9091	3347	4155	8-0371693	6134	7636	
28	7-9751574	3317		5388		3626	8016	9470	
29	3802	5479	3281	7428	8125	5657	9897	B-0601304	V
SU	6030	7641	5379	9468	8-0260108	7488	8-0491778	3137	ł
11	8257	9801	7477			9417	3657	4969	
12		7-9891960					5536	6800	d
13	2706	4117		5580			7414	8630	
14	4929	6274				5201		8-0410460	
35	7151						8-0501167	2289	1
		8430	5856			9053	3043	4117	
6	9372	7 9900585			1990	8-0300979	4918	5944	ľ
7	7-9771592	2738		3716					
B	3810	4891	2131	5748		2901	6792	7771	я
19	6028	7043	4220	7779	7919	4824	8665	9597	
0	8244	9193	6309	9808	9893	6746	8-0610537	8-0621422	1
n	7-9780459	7-9911342	8396	8-0161937	6-0281867	8667	2408	3246	i
	2673	3491			3839		4279	5070	H
3	4886	5638				2507	6149	6892	
4	7098	7784	4652			4426	8018	8714	
5	9309	9929	6735	9943		6343	9886		
Ĝ	7-9791518	7-9922073		W. F. A 10		8260		2356	
ř	3726	4216		3991	3689		3620	4176	
B	5934	6358		6013		2092	5486	5995	
9	8140	8499			7623	4006	7351	7813	
-									з
0		7-9930639			9588	5920	9216	9630	
1	2549	2778				7832		8 064 1447	
2	4752	4915		4093		9744	2942	3263	
3	6953	7052	3366			9 0421655	4803	5078	
54	9154	9188	5441	8127	7441	3565	6665	6893	ij
5	7-9811353	7-9941322			9403	5475	8525	8706	ı
6	3552	3456		2157	9 031 1363	7383		8-0650519	N
57	5749	5588		4171	3322	9291	2243	2331	
18	7945	7720		6184		8-0431198	4101	4143	
59	7-9820140	9850				3104	5958	5953	
30	2334	7-9951980	7867	8 0200207	9195	5009	7814	7763	
11	27	26'	25	24	23/	22'	21	20	۱
	40.5	20	1601.7	A APR	440	400	- AL	100	ø

T	able 11.]				. TAN. 0				73
10	32′	33′	34'	35′	36'	37	38	39	100
G	7-9658886	7-9822534		9.0078092			9-0435274		
	7.9691148	4727		8-0080159	2455		7179	9949	
2	3408	6919			4465	3357	9062		
3	5667	9110		4292	6473		3.0440985	3668	
4	7925		7-9960700	6357	8491	7265	2887 4789	5512	
5	7-9700182	3488		8420		9217	6689	7364 9216	D
6	2438 4692	5675	4947 7070	8 0090483 2545	2493 4498	3120		2-0561007	2
7		7862		4006		5069	3-0450487	3-0561067 2917	0
	6946	7-9840047	9191 7-9971311	6666	6501 6504	7018	2385	4767	JO.
9	9198	2231			01111				
	7.9711449	4414	3430		9 0220506	8967	4282	6615	
미	3698	6596		8 0100783		3:0914	6178	8463	
2	6947	6777	7666	2840		2860		8-0570310	
3	8194	7 9860957	9782	4896	6507	4806	9968	2156	
	7.9720441	3135		6951	6505	6750	8-0461962	4002	
5	2686	5313			3-001.0502	8694	3755	5846	
6	4930	7490	6124	3-0111058	2499		5647	7690	
7	7173	9665	8236	3110	4494	2579	7539	9634	
8		7-9861839		6161	6489	4520	9429		
	7-9731655	4013		7211	8483		8-0471318	3217	
0	3894	6185	4565		9.0240475	8400	3207	5058	
Ш	6132	8356	6673	8-0121308	2467	9-0360338	5095	6898	
2	8369	7-9870526	8780	3356	4458	2276	6982	6737	
23	7-9740605	2695	8-0000586	5402	6148	4213	8869		
24	2840	4862	2991	7447	8437	6149		2414	
25	6073	7029			8-024.0426	8084	2639	4250	
26	7306	9195		8.0131535	2413	40370018	4523	6087	
17	9637	7:9881359	9299	3578	4399	1951	6406	7922	
	7-9751767	3523	B-00:1400	5619	6385	3884	8288	9756	
29	3996	5685	3499	7660	8369	5815	8-0490169		
30	6224	7847	5598	9699	8-0260353	7746	2050	3423	3
31	8451	7-9890007	7696	8-0141438	2336	9676	3930	5255	2
32	7-9760676	2166	9792	3775	4318	8-0381605	5509	7087	
33	2901	4324	8-0021888	5812	6299	3533	7687	8918	
34	5124	6491	3983	7848	8279	5461		8 0610748	
35	7346	8637	6076	9883	1-0270259		8-0501441	2577	
36	9567	7-9900792	8169	8-0151916	2236	9313	3317	4405	
17	7-9771787	2946	6 0030260	3949	4213		6192	6233	
18	4006	5099	2351	5981	6190	3162	7066	8060	
39	6224	7251	4441	8012	9918	5065	8939	9886	2
10	8440	9401	6529	8.0160042	9-02:0140	7007	9-05:0812	8-0621711	2
-	7-9780655	7-9911551	8617	2071	2114	8928	2683	3536	
12	2870		8 0040703	4099		8-0400849	4554	5359	
13	6083	5847	2789	6127	6059	2768	6424	7182	
14	7295	7993		8153		4687	8294	9005	
15		7-9920138		80170178			8 0520 162		
16	7-9791715	2283		2203		8522	2030	2647	1
7	3924	4426		4226	3938		3897	4467	1
18	6131	6568	3202	6248	5905	2354	5763	6286	1
19	8338	8709	5282	8270	7872	4269	7628	8104	1
50	7-9800543	7-9930849	7360		9838	6193	9493	9922	1
51	2747	2988			8 3001802		8-0531356		
2	4950		9 0061514	4329	3766		3219	3555	
3	7152	7263		6347	5729	1919	5081	5371	
4	9353	9399	5665	8364	7692	3829	6943	7185	
	7-9811552	7-9941534		8-0190379	9653	5739	8803	8999	
6	3751	7-9941534 3667	9911	2394			8-0640663		
7		5800		4408		9555	2522	2625	
18	6948 8145	7932		6422	5531		4380	4436	
		7·9950062		8434	7489			6247	
10	2534	2192		R-0200445	9446	5274	8094	8057	
"	277	26'	25	24'	23	22/	21'	20	1
	21	200	40		TAN. 89				

ŧ

74				LOG. SI	NE 0°.			[Table n
. "	40'	41'	42'	43′	44'	45'	46'	47' 1"
0	81 657763		81769646	₹1971832		8-1169262	1.1264710	8·1358104 6 9644 5
1 2	9572 8 76 61381	6762 8526	* 871369 3091	3515 5198	3314 4958	3-1170870	6283 7856	
1 3	3188	90770290		6879	6601	2478 4085	9428	8·1361183'56 2722:5
4	4995	2052		\$560	8244	5691	8-1270999	4260 5
5	6801	3815	F254	3-1950240	9886	7297	2570	5797 5
6	8606 84 670411	5576 7337		1920		8902	4140	7334:5
á	2215	9097	3411	3599 5277	3169 4909	8·1180507 2111	5710 7279	8871'5 8-1370407'5
9		3-0780856	5128	. 6955	6449	3714	8848	1942.5
10	5820	2614	6845	8632	8088	5317	8 1290416	3477 5
īi	7622	4372	8561	8 0990309	9726	6919	1983	50114
12	9423	6129		1994	8-1091364	8520	3550	6545 4
13 14	8(681223 3022	7886 9641	1991 3706	3659 5334	3001 4639	8·1190121 1722	5117	6078 41 9610 4
15	4821			7008	6274	3322	8248	961044 8·138114344
16	6619	3151	7132	8681	7909	4921	9812	26744
17	8416	4904	8844		9544		8-1291376	42054
18	8 0690212		819(0555	2025				
19	2008	8409		3697	2912			
20 21	3503 5597	8-0≈ 0161 1912	3976 5685	5367 7037	4445 6077	8·1201312 2908	6065	8795 40 8-1390324 3
22	7390	3662		8706	7709		9188	
23	9183	5411		8-10:0375	9340	6099	8-1300749	33903
24	8 (7) 0975		8.010810		8-1110970	7693	2309	4907 3
25	2766	8908		3710	2600	9267	3869	
26 27	4557 6346	8 0810655 2401	4222 5928	5377 7043	5858	9·1210881 2474	5428 6986	
28	8135	4147	7632	8709	7486			8-14010113
29	9923	5892			9113		8-1310101	2535 31
30	8-0711711	7637	8-0921040	2038	8-1120740	7248	1658	4059 30
31	3498	9380	2743	3701	2366	8839	3215	5583 2
32		80921123	4445	5364		8-1220429	4770	7105 2
33 34	7069 8854	2866 4607	6146 7847	7027 8688	5617 7241	2018 3607	6325 7990	8628 21 8-1410150 20
35	8 0720637	6348	9547	8-10-0349	8865	5195	9434	1671 2
36	2421	8088	8 0931246	2010	8.1130488	6782	8.1320987	3192 24
37	4203	9828	2945	3669	2110	8369	2540	4712 23
38 39	5985 7765	8-0831567 3305	4643 6340	5328 6987	3732	9956 8·1231541	4093 5644	6232 22 7751 21
1								
40 41	9546 8-0731325	5042 6779	9037	8645 8·1040302	6974 8595	3127 4711	7196 8746	9270 20 8·1420788 19
42	3104		80941428		8-1140214		8 1330296	2306 18
43	4882	84840251	3123	3615	1833	7879	1846	3823 17
44	6659	1985	4817	5270	3451	9462	3395	5339 16
45 46	8436 8-0740211	3719 5452	6510 8203	6925 8579	5069 6686	8·1241044 2626	4943 6491	6855 18 8371 14
47	1986	7185		8-1050232	8302	4207	8039	988613
48	3761	8917	8-0951587	1885	9918	5787		8-1431400 12
49	5534	8-0850648	3277	3537	8-1151534	7367	8-1341132	2914 11
50	7307	2379	4968	5188	3148	8947	2678	4427 10
51	9090	4109	6657	6839		8-1250526	4223	5940 9
52 53	8 07 50851 2622	5838 7566	8346 8-0960034	8490 8-1060139	6376 7989	2104 3682	576 7 7311	7453 8 8964 7
54	4392	9294	1721	1788	9001	5052 5259		8·1440476 6
55	6161	8 086 1021	3408	3437	8-1161213	6836	8-1350398	1987 5
56	7930	2747	5094	5085	2824	8412	1940	3497 4
57	9698	4473	6780	6732	4434	9987	3482	5006 3 6516 2
58 59	8 0761 4651 32 31	6198 7922	8465 8-0970149	8379 8-1070024	6044 7654	3·1261562 3136	5023 6564	6516 2 8024 1
60	4997	9646	1832	1669	9262	4710	8104	9532 0
"	19	18'	17	16	15'	14'	13'	12"
				LOG. COS				•

7	able II.]			100 7	AN NO			==	75
<u>,,</u>		• •••	40.		an. 0°.				13
	40	41'	42′	43′	44'	45'	46′	2.1250510	CO
0				8-0972172				3 1060050	
Ĭ	9866		8.0871693	3855		8-1171243			
2			3416	5539	5314	2851	8245	1590	
3		8-0770599	5138	7220	6958	4458	9817	3129	57
4	5290		6859	8901	,8601		9.1271399	4667	56
5				8-0980592		7670	2960	6205	55
6		5886	8.0880299	2261	1885	9276	4531	7742	
7	8-0670707	7647	2018	3941	3526	8-1180681	6101	9279	
8	2511	9407	3737	5619	5167	2485	7670	8-1370815	52
9		8-0781167	5455	7297	6907	4088	9239	2350	51
10	6117	2926	7172	8975	8446	EC01	8-1280807	3886	ral
								5420	40
11	7919			3 0990651		7294	2375		
12	9720	6441	R-0890604	2327	1723	8896	3942	6954	
13	8-0681520		2319	4003		3.1190497	5509	8488	
14	3320		4033	5677	4998		7075	8.1380020	
15		8 0791709	5747	7351	6634	3698	8641	1553	
16	6917	3464	7460	9025	8269		8-1290206	3085	
17	8714			8.1000698	9904	6896	1770	4616	
18		6971			8-1101539		3334	6147	42
19	2306	6723	2595	4041		8-1200092	4897	7677	
								1	
20		8 0 8 0 0 4 7 5	4305	5712	4806		6460	9207	40
21	5896	2226	6015	7382	6438			8-1390736	
22	7690	3976	7724	9052	8070	4892	9583	2264	
23	9483	5726	9432	3.10:0721	9702	6477	8-1301144	3792	37
24	8-0701275	7475	8 0911140		8-1111332		2705	3792 5320	36
25	3066	9223	2847	4057	2962		4265	6847	35
26		8.0810970	4553	5724		8-1211260		8373	
27	6647	2717	6259	7390	6221			9899	
$\tilde{28}$	8436	4463	7964			4446	0041	8-1401425	
2 9				9056	7849			2949	34
		6208	9668	9-1020721	9477		8-1310498	1	
30	2012	7953	8.0921372	2386	8-1121104	7629	2056	4474	30
31	3799	9697	3075	4049	2730	9219	3612	5997	29
32	5586	8-0821440	4777	5713		3-1220810	5168	7521	28
33	7371	3183	6479	7375	5081	2399	6723		
34	9156	4925	8180	9037	7606	3988		8-1410566	
35	80720940	6666	9880		9230	5577	9933	2087	
$\widetilde{36}$	2723		8-0931579		8-11:0853		8-1321386	3608	24
30 37	4506				2476	8752	2940	5129	22
			3278	4019					
38	6288	1885	4977	5678		8-1230338	4492	6649	
39	8069	3624	6674	7337	5720	1924	6044	8168	21
40	9850	5361	8371	8995	7341	3510	7596	9687	20
41	80731629		8-0940068		8961	5095		8-1421206	
42	3408	8935	1763		8-1140581		8.1330697	2724	
12 43	5186		3458	3966	2200	8263		4241	
44				5621	3819		3796	5758	
	6964	2305	5153						
45	8741	4039	6846	7276		8-1241429	5345	7274	
46		5773	8539	8931	7054	3011	6893	8790	
47	2292		8 0950232		8671	4592		8-1430305	
48	4067	9238	1923		8.1150287	6173		1820	
49	5841	8-0850969	3614	3890	1903	7753	8·1341535	3334	[11]
50	7614	2700	5305	5542	3518	9333	3081	4848	10
Бĭ	9386	4430	6994	7193		8-1250912	4626		9
52	3-0751158	6160	8683	8843	6746	2491	6171	7874	8
53	2929		8-0960372	≈1060493	8359	4069	7715		7
рэ 54	4699			2142		5646	9259		6
		9616	2060		9972			. 1440097	
55		8-0861344	3747		8-1161584	7223		208	5
56	8238	3070	5433	5439	3195	8799	2345	2919	4
57	9-0760006	4796	7119	7087	4806	R-1260375	3887	5429	3
58	1773	6522	8804	8733	6416	1950	5429	6938	2
59	3540	8246		R-1070380	8025	3525	6970	8447	1
50	5306	9970	2172	2025	9634	5099	8510	9956	0
10	19'	18'	17'	16'	15'	14'	13'	12	"

76				LOG. S	INE Oo.			[Table II.
17	48'	49'	50'	51'	52'	53'	54'	55' "
	8-1449532	8-1539075	8-1626908			8-1879848	8-1961020	
1	0.1451040	3-1540552	8255	4223	8521		2360	2019 59
2	2547	2028	9702	5641	9912	2578 3943	3700 5039	3334 58 4649 57
3	4054	3504		7059 * 8477	8·1801303 2693	5307	6378	5963156
5	5560 7065	4979 6454	2594 4040	9894	4083	6670	7717	7277 55
6	9570	7928	5485		6472	B034	9055	8591 54
7	8-1460075	9402	6929	2726	6861	9397		9905 53
8	1579	9.1550876	8373	4142		8-1890769	1729	
9	3082	2348	9817	5557	9638	2121	3066	2530 51
10	4595	3821	8-1641259	6972	8-1811025	3482	4403	3842 50
11	6087	5293	2702	6386	2413	4843	5739	5154 49
12	7589	6764	4144	9800	3799	6204	7074	6465 48
13	9091	8235	5586		5186	7564	8409	7776 47
	8-1470591	9705	7027	2627	6571	8924	9744	9087 46
15	2092	8-1761175	8467	4039	7957	8-1900284		8-2060397 45
16	3592	2644	9907	5451	9342	1643	2412	1707 44
17	5091		8.1651347		8-1820726	3001	3746	3016 43
18	6590	5582	2786	8274	2111	4359	5079	4325 42
19	8088	7049	4225	9694	3494	5717	6412	5634 41
20	9586	8517	5663		4877	7074	7744	6942 40
21	8-1481083	9984	7101	2504	6260	6431	9076	8250 39
22		8-1571450	8538	3913	7643	9788		9557 38
23	4076	2916	9975	5322	9024	8-1911144		B-2070964 37
24	5571	4381	9-1661411	6731	8 1830406	2499	3069	2171 36
25	7066	5846	2847	8138	1787	3854	4399	3477 35
26	9561	7310	4282	9646	3167	5209	5729	4783 34 6088 33
27	8-1490055	8774 8-1580238		8-1750953 2359	4548 5927	6563 7917	7058 8387	7393 32
28	1549 3042	1701	7151 8585	3765	7307	9271	9716	8698 31
¢ .								
30	4534	3163		5171	8685		8.2001044	6/2080002 30 1306 29
31	6027	4625	1452		6-1840064	1976 3329	2372 3699	2610 28
32	7518 9009	6086 7547	2884	7981 9385	1442 2819	4680	5026	3913 27
33	8-1500500	9009	4316 5749		4196	6032	6353	5216 26
35		8-1590468	7179	2192	5573	7383	7679	6518 25
36	3479	1927	8610	3595	6949	8733	9005	7820 24
37	4968	m 20 7		4998	8325			9121 23
38	6457	4845	1469	6400	9700	1433	1655	8-2090422 22
39	7945	6303	2999	7801	8-1851075	2782	2980	1723 21
40	9432	7760	4327	9202	2450	4131	4304	3024 20
41	8-1610919	9217	5756		3824	5479	5628	4324 19
42		8-1600674	7183	2003	5197	6827	6951	5623 18
43	3891	2130	8611	3403	6570	8175	8274	6922 17
44	5377	3585	8.1690038	4902	7943	9522	9597	6221 16
45	6862	5040	1464	6201	9315	8-1940369		9520 15
46	8346	6495	2890	7599	8-1860687	2215	2241	8 2100818 14
47	9830	7949	4315	8997	2059	3561	3562	2115 13
48	8-1521314	9403			3430	4907	4883	3412 12
49		8-1610856	7165	1791	4800	6252	6203	4709 11
50	4279	2308	8589	3188	6170	7596	7523	6006 10
51	5761	3761	8-1700012	4584	7540	8941	8843	7302 9
52	7242	5212	1435	5980	8909		8-2000163	8598 8
53	8723	6663	2858		8-1870278	1628	1481	9893 7
54	CHOR	8114	4280	8770	1646	2971	2800	
55	1683	9564	5702		3014	4313	4118	Manage 4
56 57	3163 4641	8·1621014 2463	7123 8544	1558, 2951	4382 5749	5656 6997	5436 6753	3777 4 5070 3
58	6120	3912	9964	4344	7116	8339	8070	6364 2
59	7598		5-1711384	5737	8482	9680		7657 1
60	9075	6808	2804	7129				8949 0
00	11'	10'	9'	8	7'	6'	5'	4' "
					COSINE.		-	-
				40000	Section 4			

Te	ble 11.]			LOG. TA	N. 00.			7	77
4"	48'	49'	50'	51'	52'	53'	54'	55"	1"
10		8 1539516			8-1797626			9-2041259	
1		8-1540993		4701	9018	1730	2896	2575	
2	2971 4478	2470 3946			8-1800409 1800	3095	4236	3890	
3	5984	5422	1609 3055	7538 8956	3191	4460 5924	5576 6915	5206 6521	
5	7490			8-1720373		7188	6254	7835	
6	8995	8371	5946	1790		8552	9592	9149	
7	3-1460500	9846	7391	3207	7360			8 2950463	
8		8-1561319	8835	4623		8-1891278	2268	1776	
9	3508	2792	3-1640279	6038	8-1810137	2640	3605	3069	51
10	5011	4265	1722	7453	1525	4002	4942	4401	50
83	6514	5737	3165	8868	2913				
13	8016	7209		8.1730292			7614		
13	9518	8680	6049	1696			8949		
14		8-1560151	7490	3109			9 1980294		
15 16	2520 4020	1621 3090	8931 -1650372	4522 5934		9·1900805 2164	2953	H-2060958 2268	
17	5519	4559	1812		9:1821229			3578	43
19	7018			B757	2613	4881	5621	4887	42
19	8517	7496		8-1740168	3997			6196	
20	9 1480015	8964	6128	1579	5381	7597	B286	7505	40
21	1512	8-1570431	7566	2989			9619	8813	
22	3009	1898		4396		₹1910311		8.2070120	38
53	4506			5807			2282		37
24	6002		1978		3-1830910			2735	36
25 26	. 7497 8992	6295	3314	8624	2292		4943 6273		35
	8-1490487	7759 9224	6185	9·1750032 1439	3673 5053			6653	33
28		8-1580687	7619	2846			8933		
29	3474	2151	9054	4252			3-2000262		
30	4967	3613	8-1670487	5658		8-1921150	1598	8 2080568	30
31	6459		1921		9-1840571				
32	7951	6537	3353	6469			4246	3176	28
33	9442	7999	4786	9873		5207	5573		27
	8-1500933	9459		8-1761278		6559	6900		26
35	3913	8·1590920 2379	7649	2681 4084	7458	7910 9261		7096 8388	
37	5402	3839	9080 3-1680510	5487		8-1930611		9690	-23
38	6891	5297	1940		8-1850209	1961	2204	3-2090991	22
39	8380		3370	8291	1585		3529		21
40	9867	8213	4799	9693	2959	4660	4853		
	8-1511355	9671		3.1771094			6177		
42		3-1601129	7656	2494			7501		
43	4328		9083	3894	7081	8705	B924		
44	5813	4040		5294		F-1940053		8792	
45	7299 8783		1937	6693		1400 2746		8-2100091	
	8 1520267	6950. 8404	3363 4789	8091 9490			2792 4113		
48	1751	9958		8-1790887	3942				
49		8-1611312		2285	5313		6756	5282	
50	4717	2765	9064	3682			8076	6579	10
51	6199		9.1700487	5078	8053		9396	7875	
52	7681	5669	1911	6474		3-1950819	3-2030716	9171	8
53	9162	7121	3334	7870			2035		7
	8-1530643	8572	4756	9265	2161	3505	3354	1762	
55	3603	3-1620022	6178	3-1790659	3529			3057	
56 57	5082	1472 2922	7600 9021	2054 3447	4897 6264			4351 5646	
58	6560		3-1710442	4841	7631		8625	6939	
59	8038			6233	8998	3-1960215			
60	9516	7267	3292	7626		1556	8:2041259	9526	0
11	11'	10'	9'	8'	7'	6'	5'	4'	111
1				LOG. COT	ran. 890				

		100. 8	INE Oo.		L	OG. SINE	10.	[Table 11.
"	56'	57'	58'	59'	0'	1'	2'	3' "
	9 2118949	9-2195811	3-227 [335	9 2345569		3-2490332		8-2630424-60
	9-2120242	7080	2583	6795	9759	1518	2120 3277	1572 59 2721 58
2 3	1533	8349	3930	8021	8 2420965	2704 3890	4443	3869.57
4	2825 4116	9618 9-2200887	5077 6324	9247 8 2350472	2170 3376	5075	6609	5016,55
5	5407	2155	7570	1697	4580	6260	6775	6164 65
6	6697	3423	9816	2922	5785	7445	7941	7311 54
7	7987		8-2280061	4147	6989	8629	9106	8458 53
8	9277	5957	1306	5371	8192	9813	8-2570271	9604 52
9	3-2130566	7223	2551	6594	. 9396	9-2500997	1436	8-2640750 51
10	1854	9490	3796	7818	9-2430599	2180	2600	1896 50
11	3143	9756	5040	9041	1902	3363	3764	3042 49
12	4431	9-22/1021	6284	3-2300264	3004	4546	4928	4187 48
13	5719	2286	7527	1496	4206	5728	6091	5332 47
14	7006	3551	8770	2708	5408	6911	7255	6477 46
15	2293	4815		3930	6609	8092		7621 45
16 17	9579	6079 7343	1255	5151	7810	9274	9580 9:2580742	990943
18	3·2140865	7393 8606	2497 3739	6372 7593	9011 3-2440212	1636		8 2651053 42
19	3436	9869	4980	- 8813	1412	2816	3065	2196 41
20	4721	8 2221132	6221	3-2370033	2611	3996	4227	3339 40
21	6006	2394	7461	1253	3811	5176	5388	4482 39
22	7290	3636	8701	2472	5010	6356	6548	5624 39
23	8574	4917	9941	3691	6209	7535	7709	6766 37
24	9857	6178		4910	7407	8714	8869	7908 36
25	32151140	7439	2420	6128	8605,	9893	3·2590028	9049 35
26	2423	8699	3659	7346	9803			8-2660190 34
27	3705	9959	4897	8563	3-24510000	2249	2347	1331 33
28		8 2231219	6135	9781	2198	3426	3505	2471 32
29	6269	2478	7373	8-2380997	3394	4604	4664	3612 31
30	7550	3737	8610	2214	4591	5781	5922	4751 30
31	8931	4996	9847	3430	5787	6957	6980	5891 29
	3-2160111	6254	3-2011084	4646	6983	8134	8137	7030 28
33	1391 2671	7512, 8769	2320 3556	5862 7077	8179 9373	9310 8 2530485	9295	9308 26
35	3950		4792	8292	3-246056B	1661	1608	8-2670446 25
36	5229	1283	6027	9500	1762	2836	2764	1595.24
37	6509	2539		8-2390720	2957	4011	3920	2722 23
38	7786	3796	8496	1934	4150	5185	5076	3860 22
39	9064	5051	9731	3148	5344	6359	6232	4997 21
40	3-2170341	6306	3/2020965	4361	6537	7533	7387	6134 20
41	1618	7561	2198	5574	7730	8706	8541	7271 19
42	2896	8815	3431	6786	8922	9980	9696	8407 19
43	4171	8:2250070	4664	7998	9-2470115		9 2610850	9543 17
44	5447	1323	5896	9210	1306	2225		8 2680679 16
45	6723	2577	7128		2499	3397	3157	1814 15
46	7998	3930	8360	1633	3699	4569	4311	2949 14
	9273 3-2180547	5083	9592 8-2330923	2844	4990	6741	5463	4084 13
49	1921	7587	2053	4054 5264	6071 7261	6912 8083	6616 7768	5219 12 6353 11
50				-				
51	3095 4368	8639; 8-2260090	3284 4514	6474 7683	9451 9640	9254 6:2550424	5920 52620072	7487 to 8620 9
52	5641	1341	5743	7683 8392	9040 92450829	1594	1223	9754 8
53	6913	2591		8-2410101	2018	2764		9-2690887 7
54	8186	3841	8202	1310	3207	3933	3525	2020 6
55	9457	5091	9430	2518	4395	5102	4676	3152 5
	3.2190729	6341	9 2340(559	3725	5583	6271	5826	4284 4
57	2000	7590	1896	4933	6771	7439	6976	5416 3
58	3270	8839	3114	6140	7969	8607	8125	6548 2
59		8-2270067	4341	7347	9145	9775.	9275	7679 1
60	5811	1335	5568	8550	1-249(1332)			8810 0
t	-	_	1/	0'	59*	587	57	56' "
	L	og. costi	NE 28.			Log. CO	SINE 88	

Ta	ble n.]	LOG.	TAN. 0°		-	LOG. TA	N. 01.		79
111	56'	57'	58'	59'	0'	1'	2'	3'	11
0.8	9-2119526	1-21964UB	9-2271953	9-2346203	8-2419215	8 2491015	3-2561649	8-2631153	60
1	82120818	7678	3201		9-2420421	2202	2817	2302	59
	2110	6947	4449	8661		3388	3994	3451	58
23	3402	8-2200216	5696	9887	2833	4574	5151	4599	57
4	4694	1485		8-2351113	4038	5700	6317	5747	
5	5985	2754	8190	2339		6946	7484	6895	
6	7275	4022	9436	3564	6448	8131	8650		
7	8566	5289	3-2280682	4789		9315	9815		
8	9955	6557	1927	6013		9-2500500			
9	82131145	7824	3173	7237	3-2430061	1684	2146		
10	2434	9090	4417	8461	1264	2868	3310		
11	3723	5-2210356	5662	9684	2467	4051	4475		
12	5011	1622		5-2360909			5639		
13	6299		8150	2130			6803		
14	7587	4153	9393	3353		7600	7966		
15	8874		3-2290636	4575		8782	9129		45
	2140161	6682	1979	5796		9964	1-25F0292	9501	
17	1447	7946	3121	7018				8 2650645	
18	2733		4363	8239		2326	2617	1789	
19	4019	3-2220473	5605	9460		3507	3779		
20	5304	1736		0.2370690	3280	4688	4941		
21	6589		8087	1900		5868	6102		
22	7874	4260	9327	3120		7048	7263		
23	9158		3-2300568	4339		8227	8424	7504	37
	3-2150442	6784	1807	5558		9407	9584		
25	1725	8045	3047	6776	9276	4-2020586	8-2590744	9788	
26	3008		4286	7995		1764		8-2600929	
27		9-2330566	5525	9213		2943	3063		
28	5573	1826	6763	3-2350430	2869 4066	4121	4223 5381		
29	6855	3085	8001	1648		5298			
30	8137	4345	9239	2865		6476	6540	5492	30
31	9418		3.2310476	4081	6460	7653	7698		
	+2160699	6862	1713	5297	7656	8829	8856	7772	28
33	1979	8120	2950	6513		8-2530006	5-2000014	8911 8-2670051	96
34	3259		4186	7729	1242	1182 2358	2328		25
35	5918	8·2240635 1892	5422 6658	6944 6-2390159		3533	3485	2328	24
36	7097	3149	7893	1373		4708	4641		
38	8375	4405	9128	2588			5797		22
39	9653		9-2320363	3802		7058	6953		21
						1.00	8108	1	
	3-2170931	6917	1597	5015		8232	9263		
41	2209		2931	6228	8407	9406 #-2540579		9153	10
42	3456	9427 8-2250682	4064	7441			1479	8-2690289	
44	6038		5297 6530	8654 9866		2925	2727		
45	7314	3190	7763	3·2401078			3981		
46	8590		8995	2289					
47	9865		3-2330227	3500			6189		
	3-2161140		1458	4711		7614	7341		
149	2414		2689	5922			8493		
50	3698		3920	7132		9956	9646		
51		8-2260705	5150	8342		8-2551127	8-2620798		
52	6235	1956	63B0	9551	1510			8.2690503	
53	7508	3207	7610	8-2410760			3101		7
54	8780		9839	1969			4252		
55	8-2190053		9·234006B	3177	400	5806	5403		
56	1324		1297	4386			6554	5035	4
57	2596		2525	5593			7704		
58	3867	9456	3753	6801	-1000	9313	8854		
59		8-2270705	4980	8008			8-2630004		1
60	6408	1953	6208	9215	8-2491015	1649	1153		
11	3′	2'	1'	0'	59'	58'	57'	56"	"
1		1.0G. CC	TAN. 89	0	i	OG. COT	N. 880.		
1		manage and		-					_

80				LOG. SIN	E. 10.			[Tab	ı.
11	4'	5'	6'	7'	8'	9'	10′	II'	1"
	8-269PR10		8-2-32434		8-2962067	6.3025460		8-3149536	
$\frac{1}{2}$	9941 84701071	7249 9362	3530 4626	8814 9894	3131 4196	6509	8975	8-3150555 1574	
3	2201	9475		8-2900974	5259	9606	1042	2593	
4	3331		6818	2053	6322	9654	2075	3611	
5	4461	1700	7913	3132	7385	8-3030702	3109	4630	
6	5590	2811	9008	4211	8448	1749	4140	5649	
?	6719		8-2940103	6289	9511	2796	5173	6665	
8	7847	5034	1197	6367	8-2970573	3843	6205	7683	
9	8976	6145	2292	7445	1635	4890	7237	8700	
10	8-2710104	7256	3386	8523	2697	5937	9268	9717	
11	1232	8367	4479	9600	3759	6983		8-3160734	
12	2359	9477	5573 6666	8-291()677 1754	4820 5881	9029 9075	8-3100330 1361	1751 2767	
13	3486 4613	8-2780587 1696	7759	2831	6942		2392	3783	
15	5740	2806	8851	3907	8002	1165	3422	4799	
16	6866	3915	9943	4983	9063	2210	4452	5815	
17	7992	5023	8.2851035		9-2980123	3265	5482	6830	
18	9118	6132	2127	7134	1183	4299	6512	7845	
19	8-2720243	7240	3219	8210	2242	5344	7541	8860	
20	1368	8348	4310	9285	3301	6388	8570	9875	
21	2493	9456	5401		4360	7431	9599	8-3170889	
22 23	3618 4742	8-2790563 1670	6491 7582	1434 2508	5419 6477	8475 9518	8-3f10628 1656	1903 2917	
24	5866	2777	B672	3582			2684	3931	
25	6990	3993	9762	4656	8594	1604	3712	4945	
26	8113		8-2860651	5729	9651	2646	4740	5958	
27	9236	6095	1941		8-2990709	3688	5767	6971	
28	9-2730359	7201	3030	7875	1766	4730	6794	7984	
29	1481	9306	4118	8948	2823	5772	7821	8996	
30	2604	9411	5207	8-2930020	3679	6813			
31	3725		6295	1092	4936	7855	9874	1021	
32	4847	1621	7383	2164 3235	5992	B896		2032 3044	28
34	5968 7089	2725 3829	947 L 9558	4306	7048 8104	9936. 5-3060977	1927 2952	4055	
35	8210	4933	8-2970645	5378	9159	2017	3978	5067	25
36	9331	6036	1732	6448		3057	5003	6077	24
37	H-2740451	7139	2813	7519	1269	4097	602B	7088	23
38	1571	8242	3905	8589	2324	5136	7053	8098	22
39	2690	9345	4991	9659	3378	6175	8077	9109	
40	3810			8-2940729	4432	7214	9101	9-3190119	20
41	4929	1549	7162	1798	5486		8-3130126	1129	
42	6049	2650	8247	2867 3936	6539 7593	9291 8-3070330	1149		
44	7166 8284	3752 4853	9332 3-2880417	5005	9646	1368	2173 3196	4156	
45	9402	5954	1501	6073	9699	2405	4219		
46	-2750520	7055	2585	7141	9:3010751	3443	5242	6173	14
47	1637	8155	3669	8209	1804	4480	6264	7182	13
49	2754	9255	4752	9277	2856	5517	7287	8190	
49	3871	9-2920355		8-2950344	3907	6554	8309		1
50	4987	1454	6919	1411	4959	7590	9331		
51 52	6103	2553	6002	2478 3544	6010 7061	8626 9662	9°3140352 1374	1213 2220	
53	7219 9335	3652 4751	9084 5:2890166	4611	7061 8112		2395	3227	
54	9450	5849	1248	5677	9163	1734	3416		
	8-2700565	6947	2330	6742	6-3020213	2769	4436	5240	5
56	1680	8046	3411	7808	1263	3804	6457	6246	4
57	2794	9143	4492	8873	2313	4839	6477	7252	
58	3909		5573	993B	3362	5873	7497	8258	
59	5022	1337		8:2961003	4411	6907	8516	9263 8 3210269	
60	6136 55'	2434 54'	7734 53′	2067 52*	5460 51'	7941 50'	49'	48'	77
1	99.	94		og. cosm		13/1	99	40	1
			L	oc. Custo	E GO.				

7	able 11.]				AN. 10.				81
111	4'	5'	6'	7'	8'	9'	10'	11	"
0	8-2609563		6-2833234					8.3150462	
	8-2700694	8026	4331	9640	3981	7395	9876	1482	
2	1825	9139	5428	8-2900720	5046		8-3090910	2501	
20.00	2955	3-2770253		1800	6110	9482	1944	3520	
4	4065	1365		2879		8-3030531	2977	4539	
5	5215	2478		3959	8237	1579	4010	555B	
6	6345	3590	9811	6038	9300	2627	5043	6576	54
7	7474		8-2840906	6117	8-2970363	3674	6076	7595 8613	53
16	8603	5814	2001	7195	1426	4722	7109		
9	9732	6925	3096	8274	2489	5769	8141	9630	51
10	8-2710860	8036	4190	9352	3551	6816	9173	9-3160648	50
11	1989	9147	5284		4613	7862	3-3100205	1665	491
12		9-278025B		1507	5675	8909	1236	2682	48
13	4244	1368		251 4	6736	9955	2267	3699	
14	5371	2478	8565	360-1	7797	3-3041001	3295	4715	46
15	6498	3588	9658	4735	8858	2046	4329	5732	45
16	7625		8-2850750	5815	9919	3092	5360	6748	
17	6751	5806	1843	6891	8-2990980	4137	6390	7764	
lie.	9877	6915		7967	2040	5182	7420	8779	
	8.2721003	8024	4027	9042	3100		8450	9795	
100	2129			8-2920118		-	9479		
20		9132			4159		9479 8-3110508	1825	
21	3254 4379	8-2790240 1348		1193 2268	5219		1538	2839	
22					6278			3854	
23	5504	2455		3342		8-3050403	2566	4868	
24	6628	3563	9482	4417	8395	1446	3595		
.25	7752		8-2860572	5491	9454		4623	5882	
26	8876	5776	1662		8-2990512		5651	6895	
27	9999	6892	2752	7638	1570		6679	7909	
12B	9-2731122	7988	3841	8711	2627	6617	7707	8922	
(29)	2245	9094	4931	9784	3686	6659	8734	9935	
30	3369	\$-2800200	6019	3-2930857	4742		9761	9:3180949	
31	4490	1305	7108	1930	5799	8743	8-3120788	1960	29
32	5612	2410	6196	3602	6855		1815	2973	28
3.3	6734	3515	9284	4074	7911	8-3000825	2941	3985	
34	7856	4619	8-2870372	5145	8967	1866	3867	4997	26
35	8977	5723	1460	6217	9-3000023	2967	4893	6008	25
30	3-2740099	6927	2547	7289	1079	3947	5919	7019	24
37	1219	7930	3634	8359	2134	4987	6944	8031	23
18	2338	9034	4720	9429	3169		7969	9041	22
39	3459	8.2810136	5807	8 2940500	4244	7067	8994	8 3190052	21
40	4578	1239	6893	1570	5298	8106	8-3130019	1062	
41	5698	2342		2640	6353		1043	2073	
42	6817	3444	9065	3709		8-3070184	2068	3083	
6	7936		8-2880150	4779	8460		3092	4092	
No.	9054	5647	1235	5848	9514	2261	4115	5102	
145	3-2750173	6748		6916		3299		6111	
44	1291	7849		7985	1620		6162	7120	
47	2409	8950		9053	2673		7185	9129	
48	3526	9-2920051		8-2950121	3725		8208	9137	12
	4643	1151	6656	1189	4778		9230		11
50		2251	7740	2256	5930		8-3140253		10
51	5760 6876	3350		3324	688t	9523	1275	2161	9
52	7992	4450	990G	4391		8-3090559	2296	3169	8
53	9108	5549		5457	8984	1596	3318	4176	7
54	910F 9-2760224	6647	2071		8-3020035	2631	4339	5193	6
155	1340	7746	3156	7590	1096	3667	5360	6190	5
50		8844		9656	2136	4703	6391	7197	4
57	2455	9942	4235 5316	9721	3186	5739	7402	8203	3
58	3570 4684	9942			4236	6773	8422	9210	2
		2137		8·2960797 1952	5236	7807		8-3210215	î
35	5798 6912	3234	7478 8559	2917	6335		8-3150462	1221	0
Y C	55'	54'	53	52'	51'	501	497	48'	11
1	33.	94	99				10	40]	
_				reg. co	TAN. 889	•			

K

82				LOG. SI	NE. 10.			[Table 1
21	12'	13'	14'	15'	16'	17'	18'	19' 1'
(let	3210269	v3270163	9-3329243	+3387529	9-3445043			8-3613150
	1274	1155	3-3330221	8494	5095	2745	8762	4066
	2278	2146	1199	9459	6947	3685	9690	4982
3	3293	3137	2176	1-3390423	7899		8-3560617	5897
1	4287	4127	3153	1387	8951	5563	1544	6813
5	6292	6118	4130	2351	9802	6502	2471	7728
	6295	6108	5107	3315	8-3450753	7441	3398	8643
6	7299	7098	6064	4279	1704	8379	4324	9558
7			7060	5242	2655	9318		9-36204721
9	8303	8087					5251	
9	9306	9077	8036	6205	3605	3510256	6177	1387
1 30	3230309	3-3280066	9012	7168	4555	1194	7103	2301
i	1311	1055	9988	8131.	5505	2132	8029	3215
2	2314	2044	3:3340963	9093	6455	3069	8954	4129
3	3316	3032	1938	33400056	7405	4006	9880	5042
1	4318	4021	2913	1018	8354	4944		5956
5	5320	5009	3888	1979	9304	5891	1730	6869
g l	6322	5997	4863		8-3460253	6917	2654	7782
7	7323	6984	6837	3902	1201	7754	3579	8695
8	8324	7972	6811	4864	2150	8690	4503	9608
9	9325	8959	7785	5825	3098	9626	5427	9:3630520
	320326	9946	8759	6785	4047	3520562	6351	1433
1	1326	3-3290933	9732	7746	4995	1498	7275	2345
2	2326	1919	3-3350706	8706	5942	2433	8199	3257
3	3326	2906	1679	9666	6690	3369	9122	4169
4	4326	3892	2651	3:3410626	7837	4304	8.3580045	5080
5	5325	4878	3624	1586	8784	6239	0968	5991
6	6325	5863	4597	2546	9731	6173	1991	6903
7	7324	6849	5569	3505	8-3470678	7108	2814	7814
	8322	7834	6541	4464	1625	8042	3736	B724
9	9321	8819	7512	5423		8976	4658	9635
			8484			9910		3.3640545
	3240319	9804		6332	3517			
1		8-3300799	9455	7340	4463		6502	1456
2	2315	1773		B299	5409	1778	7424	2366
3	3313	2757	1397	9256	6354	2711	9345	3275
4	4310	3740	2368	3-3420214	7300	3644	9206	4185
5	5308	4724	3338	1172	8245	4577	9-3590187	5095
(5	6305	5708	4309	2129	9189	5510	1108	6004
7	73111	6691	5279	3036	9:3490134	6442	2029	6913
8	829B	7674	6248	4043	1079	7374	2949	7822
9	9294	8656	7218	5000	2023	8306	3870	8730
08	3250290	9639	8187	5957	2967	9239	4790	9639
1		3-3310621	9156	6913	3911	9-3540170	5709	
2	2282	1603	8-3370125	7869	4954	1102	6629	1455
3	3277	2585	1094	9825	5798	2033	7549	2363
4	4272	3567	2063	9781	6741	2064	8468	3271
5	5267	4548	3031	9:3430736	7694	3895	9387	4179
5	6262	6529	3999		8627	4826		
7	7256			1691		5756		5086
		6510	4967	2646	9570	6686	1225 2143	5993
8	8250	7491	5934		3-3490512			6900
9	9244	9472	6902	4556	1454	7617	3061	7807
0 3	3260239	9452	7869	5510	2396	6546	3979	8713
1	1232	4-3320432	8836	6465	3338	9476	4897	9620
2	2225	1412	9803	7419	4230	9-3550406		8-0660526
3	3218	2392	9:3360769	8372	5221	1335	6733	1432
1	4211	3371	1736	9326	6162	2264	7650	2338
5	5204	4350		8-3440279	7103	3193	8567	3244
G	6196	5329	3668	1233	8044	4122	9484	4149
7	7188	6308	4633	2186	8985	5050	6.3610401	
								5054
8	8180	7287	5599	3139	9925	6979	1317	5959
	9172	8265	6564		3-3500965	6907	2234	6964
0139	3270163	9243	7529	6043	1805	7935	3150	7769
	47'	46'	45'	44'	43'	42'	41'	40'

T	able 11.]			LOG. T	AN. 1°.			83
11	12'	13'	14'	15'	16'	17'	18'	19' "
. 0	8-3211221	8-327 143		3/33/8663	9-3446105		8.9558953	8-3614297 60
1	2227	2134	1229	9528	7075	3835	9881	5213 59
3	3232	3126	2206		8010	4775	3-3560809	
3	4237	4117	3184	145B	8962	5715	1737	7045 57
4	5242	5108	4161	2423	9914	6655	2664	7961 56
6	6246	6099	5139	3387	9-3450866	7594	3592	8877 55
6	7251 8255	7090 8080	6116	4351	1917	9533	4519	9793 54 8-3620708 53
8	9259	9070	7093 8070	5316 6279	2769	9472 8 3510411		1623.62
9	8-3220262		9046	7243	4671	1350	6373 7299	
1								
10	1266	1050		8206	5621	2288	8226	
11	2269	2039 3028	0999	9169	6572	3226	9152	4367 49
12	3272 4274	4017	1975	8.3400132	7522	4164	3-3570078	5281 49
14	5277	5006	2950 3926	1095 2058	8472 9422	5102 6040	1004 1929	6196 47 7110 46
15	6279	5995	4901	3020		6977	2855	8023 45
16	7281	6983	5876	3992	1321	7914	3780	8937 44
17	8283	7971	6851	4944	2271	8851	4705	
19	9285	8959	7826	5906	3220			8-5630763 42
19	9-3220286	9947	8800	6867	4169		6555	1676 41
20	1297	3-3290934			5117			2589 40
21	2288	1921	9774 8:3360748	7828 8789	6066	1661 2597	7479 9403	3502 39
22	3288	2908	1722	9750	7014	3533	9327	4414 38
23	4289	3895	2695	8-3410711	7962		8 8580251	5327 37
24	5289	4882	3669	1671	8910	5405	1175	6239 36
25	6289	5868	4642	2631	9857	6340	2098	
26	7289	6854	5615		9-3470805	7275	3022	8062 34
27	8288	7840	6587	4551	1752	8210	3945	8974 33
28	9287	8826	7560	5511	2699		4868	9685 32
29	5-3240286	9811	8532	6470	3646	8:3530080		8-3640796 31
30	1285	9-3300796	9504	7429	4592	1014	6713	1707 30
31	2284	1791	9:3360476	8388	5539	1948	7635	2617 29
32	3282	2766	1447	9347	6485	2882	8557	3528 28
33	4280	3751		9 3420305	7431	3816	9479	4438 27
34	5278	4735	3390	1263	6377		8.3590401	5348 26
35	6276	6719	4361	2221	9322	5683	1322	6258 25
36	7273	6703	5331		3/3/180268	6616	2243	7168 24
37	8270	7687	6302	4137	1213		3165	8078 23
38	9267 1-8260264	9653	7272 8242	5094	2158	8482	4086	8987 22 9896 21
40				6052	3103		5006	1 - 1
41	1260 2257	9.3310636	9212	7009	4047		5927	
42	3253	2601	8-3370181	7965 8922	4991 5936	1279 2211	6847	1714 19 2623 18
43	4249	3584	2120	9876	6979		7767 8687	3531 17
44	5214	4566		8-3430835	7823		9607	4439 16
45	6240	5548	4058	1791	8767	5006		5347 15
46	7235	6529	5026	2746	9710	5937	1446	
47	8230	7511	5994	3702		6968	2365	
48	9224	8492	6963	4657	1596	7799	3284	8070 12
49	9-3960219	9473	7930	5612	2539	8729	4203	
50		9 3320454	8898	6567	3481	9660	5121	
51	2207	1434	9866	7522		8-3550590		8-3660792 9
52	3201		6.3380833	8476	5365	1520	6958	
53	4194	3395	1800	9431	6307	2450	7876	
54	5188	4375	2767	9 3440385	7249		8794	3511 6
55	6181	5354	3733	1339	8191	4309	9711	4417 5
56	7173	6334	4700	2292	9132		8-3610629	5323 4
57 58	9166 9158	7313 8292	5666	3246	8.3500073	6167	1546	6229 3
	8-2270151	9271	6632 7597	4199	1014 1954	7096 8024	2463 3380	
60		6-3330249	8563	6105	2895	8953	4297	8945 0
11	47	46'	45'	44	43′	42	41'	40' "
1	**	. 10			AN. 88°.		34	700
-				100. COT	A. O.O.			

84				LOG. S	INE 10,			[Table II.
"	201	21'	22'	23'	24'	25'	26'	27' 1"
0	8:3667769	8-3721710	8-3774989			9-3031006	94981793	8 4031990 60
1	8674	2603	5870		8 3880483	1859	2634	2822 59
2	9578	3496	6753		1345	2710	3475	3653 58
3	9-36704612	4389		8-3830235	2206	3561	4316	4485 57
4	1386	5282	8517	1106	3067	4412	5157	6316 56
5	2290	6174	9398	1978	3927	5263	5998	6147 55
6	3193	7067	5-3750280	2948	4788	6113	. 6839	6978 54
7	4097	7969	1161	3719	5648	6964	7679	7909 53
8	5000	8851	2042	4590	6509	7814	8519	8639 52
9	5903	6743	2924	5460	7369	8664	9359	9470 51
10	6806	9-3730635	3804	6330	8229	9513	9-3990199	3 4040300 50
11	7708	1526	4685	7201	9088		1039	1130 49
12	9611	2418	5566					
13	9513	3309	6446	8070	9948	1213 2062	1879	1960 49
14	8-3680415	4200	7326		8-3690607		2718	2790 47
15	1317	5091		9910 8:3840679	1666	2911	3557	3620 46
16	2219	5981	9086		2626	3760	4397	4449 45
17	3120	6872	9965	1548	3394	4609	5236	5279 44
18	4022	7762		2417 3296	4243	5457	6074	6108 43
19	4923	8652			5102	6306	6913	6937 42
	***		1724	4155	5960	7154	7751	7766 41
20	5824	9542	2603	5023	6818	8002	8590	8594 40
21		8-3740431	3462	5992	7676	8860		9423 39
22	7625	1321	4361	6760	8534	9698	8.4000266	3-4050251 38
23	8526	2210	5239	7628	9392	8-3950646	1104	1080 37
24	9426	3099	6117	8496	9 3900249	1393	1941	1909 36
25	8-3690326	3988	6996	9363	1107	2240	2779	2736 35
26	1226	4977	7874	8-3850231	1964	3088	3616	3563 34
27	2125	5766	8751	1098	2821	3935	4453	4391 33
28	3025	6654	9629	1965	3678	4781	5290	5219 32
29	3924	7542	9:3800507	2832	4534	5628	6127	6046 31
30	4823	8430	1394	3699	5391	6475	6964	6873 30
31	5722	9318	2261	4565	6247	7321	7801	7700 29
32		6/3750206	3139	5432	7103	8167	8637	B\$27 28
33	7519	1094	4015	6298	7959	9013	9473	9353 27
34	9418	1981	4891	7164	9815	9859		9:4060190/26
35	9316	2868	5768	8030	9671	8-3960705	1143	1006 25
36	8-3700214	3755	6644	8896	8-0010526	1550	1981	1932 24
37	1111	4642	7520	9761	1362	2395	2816	2658 23
38	2009	5528		9-3860627	2237	3241	3652	3484 22
39	2907	6415	9271	1492	3092	4086	4487	4310 21
40						,		
41	3904 4701	7301		2357	3947	4930	5322	5135 20
42		8187	1022	3222	4901	5775	6157	5961 19
43	5598 6494	9073	1897	4087	5656	6620	6992	6786 18
44	7391	9959 8-3760944	2772	4951	6510	7464	7826	7611 17
45			3647	5816	7364	8308		8436 16
46	9287 9183	1729 2615	4522	6680	8215	9152	9465	9261 15
47	9163 8:3710079		5396	7544	9072		8-4020329	9-4070085 14
48	8/3710079 0975	3500 4384	6271	8408		8-3970940	1163	0910 13
49	1870		7145	9271	8:3920779	1683	1997	1734 12
-		5269		8-3870135	1633	2527	2631	2558 11
50	2766	6153	8892	0998	2486	3370	3664	3382 10
51	3661	7038	9766	1861	3339	4213		4206 9
52	4556		9.3820639	2724	4191	5056	5331	5030 8
53	5451	8400	1513	3587	5044	5898	6164	5863 7
54	6346	9 189	2396	4450	5897	6741	6996	6677 6
55	7240	8-3770573	325R	5312	6749	7583	7829	7500 5
56	8134	1456	4131	6174	7601	8425		S323 4
57	902B	2339	5004	7037	8453	9268		9146 3
68	9922	3222	5876	7898	9305	8 3980 [09	B4030326	9969, 2
59	8-3720816	4105	6748		8:3930156	0951		8:4080791 1
	1710	498B	7620	9622	1008	1793		1614 0
60								
GU	39'	38'	37'	36'	35'	34	33′	32' "

T	able II.]			LOG. T	AN. 10.			-	85
11	20	21'	22'	23'	24'	25'	26'	27'	1"
0	8-3663945	8-3722915	3.3776223	8-3829886	83880918			8-1033381	
1	9850	3809	7106	9758		3187	3994	4213	
	8:3670755	4703		3/3830631	2642	4039	4835	5045	
3	1660	5596	8972	1503		4891	5677	5877	
4	2564	6489	9754	2374		5742	6519	6709	
Б	3468		+3780636	3246		6593	7360	7541	
6.	4372	8275	1519	4117	6088	7444	8201	9372	
7	6276	9168	2400	4989		8295	9042	9203	
8	6180	-3730061	3282	5860		9145		8 4040035	
9	7093	0953	4164	6731	8670	9996	\$ 3990723	0866	
10	7987	1845	5045	7601	9530	8-3940846	1564	1696	50
11	8890	2737	6926	8472	6 3890391	1696	2404	2527	45
12	9793	3629	6807	9342	1251	2546	3244	3358	
13	8 3680696	4521	7688	4-3840213		3396	4084	4188	
14	1598	5412	8569	1083	2970	4246	4924	5018	46
15	2501	6304	9449	1953	3830	5095	5764	5848	46
16	3403	7195	4:3790329	2823	4689	5945	6603	6678	
17	4305	8086	1209	3692		6794	7442	7508	43
18	5207	8976	2089	4561	6408	7643			
19	6108	9867	2969	5430	7266	8492	9121	9167	4
20		A:3740757	3949	6299	8125	9340	9959	9996	40
21	7911	1647	4728	7168				8-4050825	
22	8812	2538	5607	8037	9842	1037	1637	1654	
23	9713	3427	6486		8-3900700	1895	2475		
24	8-2690614	4317	7365	9774	1558	2733	3313	3311	
25	1514	5206	8244	8 3850642		3581	4151	4140	
26	2414	6096	9122	1510	3274	4429	4980	4968	
27	3315	6995		2378	4131	5276	5827	5796	
28	4215	7874	0679	3245		6124	6664	6624	
29	5114	8762	1757	4113		6971	7502	7452	3
								8280	1
30	6014	9651	2634	4930	6703	7818	8339	9107	
31		9.3750539	3512	5847	7560	9665	9176	9935	
32	7812	1428	4390	6714	8417		8-4010013	8 4060762	
33	8711	2316	5267	7581	9273	3-3560358	1686	1589	
34	9610	3203	6144		8-3910120	1204 2050	2523	2416	
35	8-3700509	4091	7021	9314	0986	2897	3359	3242	
36	1407	4979	7898	8-3860180		3742	4195	4069	
37	2306	5866	8774	1046		4588	5031	4896	
38	3204	6753	9650	1912	3553			5723	
39	4102		8-3810527	2778	4409	5434	6867		1.
40	4999	8527	1403	3643		6279	6702	6548	
41	5897	9413	2278	4509			7538	7374	
42	6794	3:3760:290	3154	5374	6974	7969	8373	8199	
43	7692	1186	4030	6239		8814	9208	9025	
44	8589	2072	4905	7104		9659		9850	
45	9485	2958	5780	7969			0878		
46	3-3710382	3843	6655		8-0920393	1348	1713	1501	
47	1278	4729	7530	9698		2192	2547	2326	
48	2175	5614	8404	8/3870562		3036	3381	3151	
49	3071	6499	9279	1426	2955	3980	4216	3975	L
50	3967	7384	8-3820153	2290	3808	4724	5050	4800	l
51	4862	8269	1027	3153		5567	5884	5624	
52	5758	9153	1901	4017		6411	6717	6449	
53	6653		2775	4380		7254	7551	7273	
54	7548	0922	3648	5743		8097	8384	8097	
55	8443	1906	3645 4522	6606		8940	9217	8920	
				7469		9792		9744	
56	9338	2690	5396	8332		s-3980625		S-4080567	
57	6.3720232	3574	6268			1467	1716	1391	
58	1127	4457	7141		8-3930631	2310	2549	2214	
	2021	5340		9-3880056		3152	3381	3037	
59	Christian at								
60	2915 39'	6223 38'	8886 37'	0919 36'	2336 35'	34	33,	32'	1

86				LOG.				[Table II.
"	28,	29'	30′	31′	32′	33′	34′	35′ ″
0	8·4081614 2436	8·4130676 1489	8·4179190 9994	8·4227168 7963	8·4274621 5408	8·4321561 2339	8·4367999 8768	8·4413944 60 4706 59
3	3258	2302		8758	6194	3117	9538	5468 58
3	4080	3115	1602	9553	6990	3895		6229 57
4	4902 5723	3927 4740	2405 3209	8·4230348 1142	7766 8552	4672 5450	1077 1846	699056 775155
6	6545	5552	4012	1937	9338	6227	2615	8512 54
7	7366	6364	4815	2731	8.4280124	7004	3384	9273 53
8	8187	7176	5618	3525	0909	7781	4153	
9	9008	7988	6421	4319	1694	8558	4921	0795 51
10	9829	8800	7223	5113	2480	9335	5690	1555 50
11 12	8·4090650	9611 8·4140422	8026 8828	5907 6700	3265 4050	84330112 0888	6458 7227	2315 49 3076 48
13	2291	1234	9630	7494	4835	1665	7995	3836 47
14	3111		8.4190432	8287	5619	2441	8763	4596 46
15	3931	2856	1234	9090	6404	3217	9531	5855 45
16 17	4751 5571	3666 4477	2036 2838	9873 94240666	7188 7972	3993 4769	8·4380298 1066	611544 687543
18	6391	5287	3639	1458	8756	5544	1833	7634 42
19	7210	6098	4441	2251	9540	6220	2601	8393 41
20	8029	6908	5242	3043	8.4290324	7095	3368	9152 40
21	8849	7718	6043	3836	1108	7871	4135	9911 39
22	9668 8 4100486	8528	6844 7644	4628 5420	1891	8646 9421	4902	8-4430670 38 1429 37
23 24		9337 8 4150147	8445	6211	2675 3458	8.4340196	5669 6435	2187 36
25	2124	0956	9245	7003	4241	0970	7202	2946 35
26	2942	1765	8.4200046	7795	5024	1745	7968	3704 34
27	3760	2575	0846	8586	5807	2519	8734	4462 33
28 29	4578 5396	3383 4192	1646	9377 8·4250168	6590 7372	3294 4068	9501 8·4390266	5221 32 5978 31
30	6214	5001	3245	0959	8154	4842	1032	6736 30
31	7032	5809	4045	1750	8937	5616	1798	7494 29
32	7849	6618	4844	2541	9719	6389	2564	8251 28
33	8667	7426	5644	3331	8.4300501	7163	3329	9009 27
34 35	9484 8:4110301	8234 9042	6443 7242	4122 4912	1283 2064	7937 8710	4094 4859	9766 26 8 4440523 25
36	1118	9850	8040	5702	2846	9493	5624	1280 24
37	1934	8.4160657	8839	6492	3627	8.4350256	6389	2037 23
38	2751	1465	9638	7282	4409	1029	7154	2794 22
39	3567		8.4210436	8071	5190	1802	7919	3551 21
40	4383	3079	1234 2032	8861	5971	2574 3347	9683 9447	4307 20 5063 19
41 42	5200 6015	3886 4693	2830	9650 8·4260439	6751 7532	4119		5820 18
43	6831	5499	3628	1229	8313	4892	0976	6576 17
44	7647	6306	4426	2018	9093	5664	1740	7332 16
45	8462	7112	5223	2806	9873	6436	2503 3267	9097 15 9843 14
46 47	9278 8·4120093	7919 9725	6020 6818	3595 4393	8·4310654 1434	7207 7979	3267 4031	9599 13
48	0908	9531	7615	5172	2213	8751	4794	8.4450354 12
49		8.4170336	8412	5960	2993	9522	5557	1109 11
50	2537	1142	9208	6748	3773	8 4360293	6321	1965 10
51	3352		8.4220005	7536	4552	1064	7083	2620 9 3375 8
52 53	4166 4981	2753 3558	0801 1598	8324 9111	5332 6111	1835 2606	7846 8609	3375 8 4129 7
54	5795	4363	2394	9899	6890	3377	9372	4884 6
55	6609	5168	3190	8.4270686	7669	4148	8.4410134	5638 5
56	7422	5973	3986	1474	8447	4918	0996	6393 4
57 58	8236 9050	6777 7582	4782 5577	2261 3048	9226 8·4320004	5688 6459	1659 2421	7147 3 7901 2
59	9863	8386	6373	3834	0783	7229	3183	8655 1
60	8.4130676	9190	7168	4621	1561	7999	3944	9409 0
"	31′	30′	29′	28′	27′	26′	25′	24′ ″
				LOG. CO	SINE 889	·		

T	able 11.]			LOG. T	AN. 10.			87
50	28′	29'	30′	31'	32'	33'	34'	35' "
0		84132132		9.4228690			84309622	
1	3959	2945	1483	9485	6963		B-4370393	6365 59
23	4682	3759	2288		7750	4707	1163	7127 38
3	5505	4572	3092	1076	8537	5486	1933	7889 57
4	6327	5395	3896	1972	9324	6264	2703	8651 56
5	7149	6198	4700	2667	9-4280110	7042	3473	9413 55
6	7971	7011	5504	3462 4257	0897	7820	4242	
7 8	8793	7823 8636	6307		1683 2469	8598	5012	0936 53
9	9615 8-4000436	9448	7111 7914	5051 5846		9375 8:4300153	5781	1697 52
		p		-			6550	2458 51
10		8-4140261	8717	6640	4041	0930	7320	3219 50
11	2079	1073	9520	7434	4826	1707	8089	3980 49
12	2900		8-4190323	8229	5612	2484	8857	4741 48
13	3721 4542	2696	1126	9023	6397	3261	9626	5502 47
14	5362	3508	1929	9816	7182		8-4380395	6262 46
15	6193	4319	2731 3533	3-4240610	7968	4815	1163	7023 45
16	7003	5131 5942	4336	1404 2197	8752	5591 6368	1931	7793 44
19	7923	6753			9537 8-4290322	7144	2700 3468	8543 43
19	8643	7564	513H 5940	3783	1106	7920	3468 4235	9303 42 84430063 41
	-							
460	9463	8374	6741	4576	1891	8696	5003	0822 40
21	34100283	9185	7543	5369	2675	9472	5771	1582 39
23	1103	9995	8344	6162		8 4340248	6538	2341 38
24	2741	84150905	9146 9947	6954	4243	1023	7306	3101 37
25	3560	1616	8-4200748	7747 8539	5027	1799 2574	8073	3860126
25	4379	3235	1549	9331	5811 6594	3349	8840	4n19765 . 5375, 34
27	5198	4045	2349		7377		9607 8:4390374	613: 13
28	6017	4854	3150	0915	8161	4899	1140	687532
29	6835	5664	3950	1706	8944	5674	1907	7654 31
	-							
30	7653 8472	6473 7292	4750	2498	9727	6449	2673	6412 30
32	9290	8091	5550	3289	8-4300510 1292	7223	3440	9171 29
33	8-4110107	8900	6350 7150	4080 4872	2075	7997 8771	4206	9929 28 8 4440697 27
34	0925	9708	7950	5662	2857	9545	5738	1444 26
35		8-4160517	8749	6453		8-4350319	6503	2202 25
36	2560	1325	9549	7244	4422	1093	7269	2960 24
37	3377		8-4210348	8034	5204	1867	8034	3717 23
38	4194	2941	1147	8825	6985	2640	8800	4475 22
39	5011	3749	1946	9615	6767	3413	9565	5232 21
40	5828	4556	2745	8-4260405	7549		8-4400330	5989 20
41	6645	5364	3543	1195	B330	4960	1095	6746 19
42	7461	6171	4342	1985	9111	5733	1960	7503 19
43	8278	6979	5140	2774	9892	6506	2624	825917
44	9094	7786	5938		8-4310673	7278	3389	9016 16
45	9910	8593	6736	4353	1454	8051	4153	9772 15
46	34120726	9399	7534	5142	2235	8823	4918	
47	1541	9-4170206	8332	5932	3016	9598	5682	1285 13
48	2357	1012	9130	6720	3796	8:4360367	6446	2041 12
49	3172	1819	9927	7509	4576	1139	7209	2797 11
50	3989	2625	9-4220725	8298	5356	1911	7973	3552 10
51	4803	3431	1522	9086	6136	2683	8737	4308 9
52	561B	4237	2319	9875	6916	3455	9500	5063 8
53	6432	5043		8-4270663	7696	4226	8-4410263	5819 7
54	7247	5849	3912	1451	8476	4997	1027	6574 6
55	8062	6654	4709	2239	9255	5768	1790	7329 5
56	6876	7459	6505	3027	8-4320034	6540	2553	8084 4
57	9690	8264	6302	3814	0814	7310	3315	8839 3
58	8 4130504	9069	7098	4602	1593	8081	4078	9594 2
59	1318	9874	7894	5399	2372	8862	4841	84460348 1
60		84180679	8690	6176	3150	9622	5603	1103 0
"	31'	30'	29'	28'	27'	26'	25'	24' '"
				LOG. COT	ran, 88°			
-								

88				Log. St	NE 10.			[Table	II.
11	36'	37'	38'	39'	40'	41'	49'	43'	11
D	8-4459409	8.4504402				64679860		8 4764984	60
	8-4460163	5148	9672	3744	7372	8:4680567	3335	5686	59
2	0916	5894	8 4550410	4474	8096	1283	4044	6388	58
23	1670	6640		5205	8819		4753	7091	57
4	2423	7385	1686	5936	9542	2715	5462	7793	
5	3176	6131	2624	6666	8:4640265	3431	6171	6495	
6	3929	8876	3362	7396	0988	4147	6880	9197	
7	4682	9621	4099	8126	1711	4862	* 7589	9899	
8	5435	8-4510366	4837	8856	2434	5579	6297	84770600	
9	6188	1111	5574	9586	3156	6293	9006	1302	51
10	6940	1856	6311	84600316	3679	7009	9714	2003	
11	7693	2601	7048	1046	4601	7724		2705	49
12	8445	3345	- 7765	1775	5323	8439	1130	3406	
13	9197	4090	8622	2505	6046	9154	1838	4107	
14	9949	4834	9259	3234	- 6768	9869	2546	4808	
15	3-4470701	5578	9996	3963		8-4600584	3254	5509	
16	1453	6322		4692	8211	1298	3962	6210	
17	2205	7066	146B	5421	6933	2013	4669	6910	
18	2956	7810	2205	6150	9654	2727	5377	7611	
19	3707	9553	2941	6878	44600376	3441	6084	8311	41
20	4469	9297	3677	7607	1097	4156	6791	9012	40
21		+4520040	4412	8335	1818	4970	7498	9712	39
22	5961	0784	5148	9064	2539		8205	8-4780412	38
23	6712	1527	5884	9792	3260	6297	8912	1112	37
24	7462	2270	6619	8:4610520	3981	7011	9618	1612	36
25	6213	3013	7354	1248	4702		84740325	2511	
26	6963	3755	8090	1975	5422	8438	1032	3211	34
27	9714	4498	8825	2703	6143	9151	1738	3911	33
	6-4480464	5240	9560	3431	6963	9865	2444	4610	32
29	1214	5983	34570295	4158	7583	8 4700578	3150	5309	31
30	1964	6725	1029	4886	8303	1291	3956	6009	30
31	2714	7467	1764	5613	9023	2003	4562	6706	29
32	3463	8209	2499	6340	9743	2716	5268	7407	28
33	4213	8951	-3233	7067	3.4660463		5974	8105	
34	4962	9693	3967	7794	1182	4141	6679	8804	
35	5712	9.4530434	4701	8520	1902	4854	7385	9503	
36	6461	1176	5435	9247	2621	5566	8090	54790201	24
37	7210	1917	6169	9973	3340		8795	0900	
38	7959			94620700	4059		9500	1598	
39	8708	3400	7636	1426	4778	7702		2296	
40	9456	4141	8369	2152	5497	8414	0910	2994	
41	8-4490205	4881	9103	2878	6216	9126	1615	3692	19
42	0953	5622		3604	6935		2320	4390	
43	1701	6363	8.4580569	4330	7653		3024	5088	
44	2450	7103	1302	5055	8372	1260	3729	5785	
45	3198	7844	2036	5791	9090		4433	6483	
46	3945	8584	2769	6506	9808	2682	5137	7190	
47	4693	9324	3500		8-4670526	3393	5841	7878	
48	5441	84540064	4233	7957	1244	4104	6545	8575	
49	6188	0804	4965	6662	1962	4815	7249	9272	11
50	. 6936	1543	5697	9406	2680	5526	7953	9969	10
51	7683	2283	6429	34630131	3397	6236	8656	84800666	
62	8430	3023	7161	0856	4115	6947	9360	1362	8
63	9177	3762	7893	1580	4832	7657	84760063	2069	7
54	9924	4501	8626	2305	5549	8367	0766	2755	6
	5.4500671	5240		3029	6266	9077	1470	3452	
56	1417		8.4590088	3753	6983	9787	2173	4148	
67	2164	6718	0819	4477		94720497	2976	4844	3
58	2910	7457	1551	5201	8417	1207	3578	5540	2
59	3656	8195	2282	5925	9134	1916	4281	6236	
60	4402	8934	3013	€649	9850	2626	4984	6932	0
"	23'	22'	21'	20'	19'	18'	17'	16'	100
				T 00 000	INE 890.				

T	ible II.]			Log. T.	AN. 1°.			89
17	36'	37'	38'	39'	40'	41'	42'	43' "
			8-4550699					8 4766933 60
1	1857		1438	5545		2442	5248	
2	2611		2176	6277	9935	3169	5957	8339 68
3	3365		2915		8-4640659	3875		
4	4119		3654	7739		4592	7377	
5	4873		4392	8470		5309		8-4770448 56
6		8.4510609	5130	9201	2830	6025	8796	
8	6380 7133		5868	9932 8-4600662		6741	9505 84730214	1853 53 2555 53
9	7897	2846	7344	1393		9174		
-								1
10	8640		8082	2123		8890		
11	9393	4336	9820	2853		9005		4661 49
	3-4470146	5081	9558	3584	7168		3050	5363 48
13	0899			4314	7891	1037	3758	
14	1651	6571	1032	5043		1752	4467	6766 46
15	2404		1769	5773		2468		7468 48
16	3156		2506 3243	7232	84630059	3193 3898		8169 44 8871 43
17	3908	8805		7232	0781		6592 7300	
18	4660		3980	962 8691	1503 2225	4613 5328		9572 45 84780273 41
		8-4520294	4717					
20	6164	1038	5453	9420	2947	6043		0974 40
21	6916	1782		0.4610149		6757	9423	1675 39
22	7667	2526	6926	0878	4390		3-4740131	2375 38
23	8419		7662	1607	5112	8186	0838	
24	9170		8399	2336	5833	8900	1545	3776 36
25	9921	4757	9134	3064	6555	9615	2253	
	3-1480672		9870	3792		8-4700329	2960	5877 33
27	1423		8-4570606	4521	7997	1043	3667	6577 32
28 29	2174 2925		1341 2077	5249 5977	9718 9439	1756 2470	4374 5060	
30	3675		2912		8-4660159	3184	5787	7977 30
31	4426		3547	7433	0880	3897	6494	8677 29
32	5176		4282	8160	1600	4611	7200	9376.28
33		8 4530700	5017	588B		5324	7906	8-4790076 27 0775 26
34	6676		5752	9615	3041	6037 6750	8612	1475 25
36	7426 8176		6487 7221	8-4620343 1070	3761 4481		9319	2174 24
37			7956	1797	5201	8176	0730	2873 23
38	8925 9675		8690	2524	5921	8888		3572 25
	3-4490424		9424	3251	6640	9601	2142	4271 21
40	1173		3-468015B	3978		8-4710313	2847	4969 20
41	1923		0892	4704	8079	1026	3553	
42	2672		1626	5431	8798	1738		
43	3420		2360	6157	9517	2450 3162		7065 17 7763 16
45	4169		3094 3627	7609	8-4670236 0965	3162	5666 6373	
46	4918	9599 3:4540340	3527 4560	8335		4586	7078	
47		1081	5293	9061	2393		7783	
48	6415 7163	1822	6027	9787	3111	6009		8-4800555 12
49	7911	2562		9767			9192	
-								1
50	9659		7492	1239			9896	
51	9407	4043	8225	1963			5:4760600	2648 9 3345 8
	3 4500154	4793	8958	26B9		8853	1304 2008	
63	0902		9690 8-4590422	3414		9564 84720275	2008	
54	1649			4139 4864		0986	3416	
55 56	2397	7002	1155 1887	4504 5588	8138	1696	4120	
57	3144	7742 8481	2619	6313		2407	4823	6830 3
	3891		3351		84680290	3117	5527	7527 2
					IN TRUBATION	3111		
56	4638					2097	6920	9999 1
58 59	4638 5395	9960	4082	7762	1008	3827 4538	6230	9223 1 8920 0
56	4638 5395				1008	3827 4538 18'	6230 6933 17'	

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£.

90				LOG. S	INE 1º.			[Table II.
11	44'	45'	46'	47'	48'	1 49	50'	51' "
0	3-4506932	9:4846479	64689632	84930398	8 4970794	8-5010798	8:5050447	8-5089736 60
1	7628	9168	±4890314	1074	1454	1462		8 8090388 59
2	8323	9857	0997	1750	2124	2126	1762	1040 58
3		3-4850546	1679	2426		2790	2420	1691 57
4	9714	1235	2361	3102			3077	2343 56
8	14810410	1923		3778	4133		3735	2994 55
-6	1105	2612	3726	4453	4802	4780	4392	3646 54
7	1800	3300		5129		5443	5049	4297 53
5	2495	3989		5804	6141	6106	5706i	4948 52
9	3190	4677	5771	6480	6810	6769	6363	5599 51
IC	3884	5365	6453	7155		7432	7020	6250 50
11	45.79	6053		7830		8095	7677	6901 49
12	5273	6741	7816	8605	8817	8757	8333	7552 48
13	5968	7429		9180		9420	8990	8202 47
14	6662	8116	9178		8 4980154		9646	8853 46
18	7356	£804	9859	34940530	0823		3-5060303	9503 45
16	8050		8 4000540	1204	1491	1407	0959	
17		9-4960179	1221	1879		2069		0804 43
18	9438	0866	1902	2553		2731	2271	1454 42
19	34820132	1553		3223	3495	3393	2927	2104 41
20	0825	2240	3263	3902	4163	4055	3593	2754 40
21	1519	2927	3943	4576		4717	4239	
22	2212	3614	4624	5250				
23	2905	4300		5924	6167	6040		
24	3599	4987	5984	6597	6834	6701	6205	
25	4292	5673	6664	7271	7502		6861	6002]35
26	4986	6360		7945	8169	8024	7516	
27	5677	7046		8618			8171	7301 33
28	6370	7732		9292			8826	
29	7063	8418	, , , , , ,	9965			9481	6599 31
30	7755.		84910063		0838		8-5070136	9248 30
31	8448	9790		1311	1504	1329		9897 29
3.7		8.4870476		1964	2171	1989		8-5110546 28
33	9832	1161	2100	2667	2838	2650	2100	
	9.4830524	1847	2779	3330	1	3310	2755	
35	1216	2532		4002	4171	3971	3409	
36	1908° 2600	3217	4137	4675 5347		4631	4063 4717	
38	3291	3903 4588		6020	5503 6169	5291 5951	5371	3789 23
39	3983	5273	5495 6173	6692	6836	6611	6025	4437 22 5085 21
40	4674	5957	6852	7364	7501	7271	6679	
41	5365	6642		8036	8167	7931	7333	6381 19
42	6057 6749	, 7327	8208	9708 9380	8833		7987	7029 18
44	7439	8011 8696	8886	8-4960051	9499 3-5000164	9250	B640	
45	B129		9564 94920242	0723		9909 8-5040569	9294 9947	8324 16 8972 15
46	8820		0920	1394	1495	1228		8972 15 9619 14
47	9511	0748		2066	2160	1887	1254	8-5120266 13
48	₹4840201	1432		2737	2825	2546	1907	0914 12
49	0892	2116		3408	3490	3205	2560	1561 11
50	1582	2800						
51	2272	3494	3630 4307	4079 4750	4155 4820	3964	3213	2208 10
52	2962	4167	4984	5421	5485	4523 5181	3866	2955 9
53	3652	4851	5661	6092	6149	5840	4518 5171	3502 8 4148 7
54	4342	5534	6338	6763	6814	6498	5823	
55	5032	6217	7015	7433	7478	7157	6476	4795 6 5442 5
56	5721	6900		8104	8142	7815	7128	6088 4
57	6411	7583		8774	8806	8473	7780	6735 3
58	7100		9045	9444	9471	9131	8432	7381 2
59	7790	8949	9721		9:5010135	9789	9084	8027 1
60	8479	9632		0784	0798		9736	8673 0
11	15'	14'	13'	12'	11'	10'	9,00	8' "
					OSINE 88			- 1
				Mente L	DESCRIPTION S.P.			

T	able n.]			LOG	TAN. 1	0,		9	1
11	44'	45'	46'	47'	48'	49'	50′	51'	11
0	9-4809920		3-4891696	64932502			5.5052671	9.5092001	
1	9616		2380	3179	3598		3329	2653	
2	84810312		3063	3855	4269	4311	3987	3306	
3	1008		3746	4532	4939	4975	4646	3958	
4 5	1704 2400		4429 5112	5208 5885	5610 6230	5639 6303		4610 5 5262	
6	3096		5794	6561	6950		5962 6620	5914	
7	3792		6477	7237	. 7620		7277	6566	
7 8	4487	6020	7159	7914	8290		7935	7218	
9	5183			9590	8959		8593	7870	
	6978		8524	9266	9629	1	9250	8521	
10 11	6574	8086	9206	9941			9908	9173	
12	7269			3 4940617	0968		9.5060666	9824	
12 13	7964		9.4900570	1293	1638		1222	8 5100475	
14	8659	8.4860151	1252	1968	2307	2275	1879	1127	46
15	9353	0839	1934	2643	2976	2938	2536	1778	
16	8.4820048	1528	2615	3319	3645	3601	3193	2429	
17	0743	2216	3297	3994	4314	4264	3850	3090	
18	1437	2903	3978	4669			4507	3731	
19	2131	3591	4660	5344	5652		5164	4381	
20	2826	4279	5341	6019	6320		5820	5032	40
21	3520	4966	6022	6694	6939		6477	5683	39
22 23	4214	5654	6703	7369		7576	7133	6333	38
24	4908	6341	7384	8043			7789	6983	31
25	5602 6295	7028 7716	8065 8745	9717 9392	8994		8445		92
26	6989	8403	9426		9662	9563 95000225	9101 9757	8284 8934	34
27	7682	9089		0740	0998		8-5070413		
28	8376	9776	0797	1414	1666			8-5110234	32
29		6.4870463	1467	2038			1724	0883	31
30	9762	1149	2147	2762	3001	2871	2380		
	8-4830455	1936	2927	3435	3668			2183	20
32	1149		3507	4109	4336		3691	2832	28
33	1841	3209	4187	4783	5003		4346	2.127	27 1
34	2533	3895	4866	5456	5670		5001	4131 4780	26
35	3226	4581	5546	6129	6337	6178	5656	4780	25
36	3919	5267	6226	6802	7004			54291	24
37	4611	5952	6905	7476	7671	7499		6078	23
38	5303	6638	7594	8148	8338		7621	6727	22
39	5995	7324	8263	8921	9005		8275		
40	6687	8009	8942	9494	9671	9481	8930	8025	
41	7379	8695	9621	8-4960167		8-5040142	9584	9673	19
43	8071	9380		0889 1512	1004		5-5080239	9322	18
44	9454	8·4880065 0750	0979 1658	2194	1671 2337	1462 2122	0893 1547	9970	16
	84840146	1435	2336	2856	3003		2201	9-5120618	15
46	0837	2120	3015	3529	3669			1267 1915	14
47	1528	2805	3693	4201	4335		3509	2563	13
48	2220	3489	4371	4873	5000		4163		12
49	2911	4174	5049	5544	5666		4817	3859	11
50	3602	4958	5727	6216	6332		5470		10
51	4292	5543	6405	6989	6997	6740	6124	5154	9
52	4983	6227	7083	7559	7663	7400	6777	5801	8
53	5674	6911	7761	8231	8328	8059	7430	6449	7
54	6364	7595	8438	8902	8993	8718	8084	7096	6
55	7055	8279	9116	9573	9658	9377	8737	7743	5
56	7745	8962	9793		9-5010323		9390	8391	4
57 58	8435		9-4930471	0915	0988		8 5090042	9038	3
59		84890330	1148	1596 2257	1653	1353	0695	9685	2
	9915 5:4810505	1013 1696	1825 2502	2257	2317 2982		1348 2001	8-5130332	0
7.0	15'	14'	13'	12'	11'	10'		0978	11
,	10	, 47			AN. 880			0 1	-
2				THOUGH CONT	CONTAIL CASE	4			

92				LOG. S	INE 1º.			[Table 1	п
77	52'	53'	54'	551	56'	57'	58'	59′ 1	*
0		8-5167264	8-5205514	8-6243430	8-5281017		8-5355228	8-5391863	N
1	9319	7904	6148	4059	1641	8900	5842	2471	
2	9965	8544	6783	4698	2264	9518	6455	3079	
	8 5130611	9184	7417	5317		8-5320136	706B	3687	
4	1256	9624	8052	5946	3511	0754	7680	4295	
5		8-5170464	8686		4135	1372	B293	4902	
	2548			6574					
6		1104	9320	7203	4758	1990	8906	5510	
7	3193	1743	9954	7833	5381	2608	9518	6117	
B	3838		8-5210588	8460	6004	3226	8.5360131	6725	
9	4484	3023	1222	9088	6627	3944	0743	7332	5
10	5129	3662	1856	9717	7250	4461	1356	7939	5
1	5774	4301		8-6250345	7873	5079	1968	8546	
2	6419	4941	3123	0973	8495	5696	2580	9153	
3	7064	5580	3757	1601	9118	6313	3192	9760	
	7708								
14		6219	4390	2229	9741	6931		B-5400367	
15	8353	6858	5024	2857	8-5290363		4416	0974	
6	8997	7497	5657	3485	0985	8165	5028	1581	
17	9642	9135	6290	4112	1608	8782	5640	2187	
18	8-5140286	8774	6923	4740	2230	9399	6251	2794	
9	0931	9413	7556		2852	8-0330015	6863	3400	4
0	1575	8-5180051	8189	5995	3474	0632	7474	4007	
1	2219	0689	8822		4096	1249	8086	4613	
				6622					
2	2863	1328	9455	7249	4718	1865	8697	5219	
13	3507		8.5220087	7877	5339		9308	5825	
14	4150	2604	0720	8504	5961	3098		6431	
5	4794	3242	1352	9131	6583	3714	9.5370531	7037	É
26	5438	3860	1985	9757	7204	4330	1142	7643	H
27	6081	4518	2617		7826	4946	1752	8249	13
28	6725	5156	3249		8447	5562	2363	8854	13
29	7368	5793	3681	1637	9068	6178	2974	9460	
-	7.44						1		п
30	9011	6431	4513	2264	9689	6794		8-5410066	
31	8654	7068	6145	2890	8.5300310	7410	4195	0671	
32	9297	7706	5777	3517	0931	8026	4806	1276	
33	9940	8343	6408	4143	1552	8641	5416	1982	
34	8.5150583	8980	7040	4769	2173	9257	6026	2487	
35	1226	9617	7672	5395	2793	9872	6636		
16	1869	8-5190254	8303	6021	3414	8-5340457	7247	3697	12
37	2511	0891	8934	6647	4034	1103	7857	4302	1
8	3154	1528	9566	7273	4655	1718	8466		
39	3796		8-5230197	7898	5275	2333	9076		
-									
Û	4438	2801	0828		5895	2948		6116	
11	5080	3438	1459	9149	6516		8-5380296		
12	5722	4074	2090	9775	7136	4177	0905	7325	
13	6364	4710	2720	8-5270400	7756	4792	1515	7929	
4	7006	5347	3351	1025	8375	5407	2124	8534	
5	7649	5983	3982		8995		2734	9138	
6	8290	6619	4612	2276	9615	6636	3343		
7	9931	7255	5243		8-5310235	7250		8-5420346	
18	9573	7891	5873		0854	7864	4561	0950	li
	8.5160214	9526	6503		1473		5170	1554	f
-							1		Э.
50	0856	9162	7133		2093		5779	2158	
51	1497	9798	7763		2712		6388	2762	
2	2138	8.5200433	8393	6024	3331	8-5350320	6997	3365	
3	2779	1069	9023		3950		7605	3969	
4	3420	1704	9653		4569	1548		4572	
55	4061		8-5240283		5188	2161	6822		
							9431		
66	4701	2974	0912		5807	2775		5779	
57	5342	3609	1542		6426		8-5390039	6362	
68	5983	4244	2171		7044			6986	
59	6623	4879		8-5280393	7663		1255		
60	7264	5514	3430	1017	8281	5228	1963	8192	
יטכ					3'	2/	1'		

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Tab	de 11.}			LOG. T	AN. 1°.				93
"	52'	53′	54'	55'	56'	57'	58'	59'	111
-			8-5207902				8-5397787	3-5394466	
1	1628 2272	9.5170251 0892	8537 9173	6490 7120	4114 4739	1416 2035	9401 9015	5075 5683	
2	2918	1533	9808	7749	5363		9629	6292	575
3	3564		8-5210443	8379			8.5360242	6900	56
5	4211	2814	1078	9008	6611	3892	0856	7509	
61	4857	3455	1713	9638	7235	4510	1469	8117	54
7 8	5503	4095		8-5250267	7859	5129	2082	8725	
8	6149	4735	2982	.0896	8483	5747	2696	9333	
9	6795	5375	3617	1525	9106	6366	3309	9941	
10	7441 8087	6016 6656	4251	2154	9730	6984 7602	3922 4535	8-5400549 1157	
11	8732	7296	4886 5520	3412	6-5290353 0977	8220	5148	1765	
13	9378	7935	6154	4041	1600	8836	5761	2372	
	5140023	8575	6789	4669	2223	9456	6373	2980	46
15	0668	9215	7423	5298		8-5330074	6986	3587	
16	1314	9854	8057	5926	3470	0692	7599		
17	1959 2604	8-5180494 1133	8690	6555	4093	1310	8211 8823	4802 5409	
18	3249	1772	9324 9958	7183 7811	4716 5339	1927 2545	9436		
	3894		8-6220591				3.5370048	6624	
20	4539	3051	1225	9439 9067	5961 6584	3779	0660	7231	
22	5183	3690	1858	9695	7206	4397	1272	7838	38
23	5828	4329		8.5260323	7829	5014	1884	8445	
24	6472	4967	3125	0951	8451	5631	2496	1809	
25	7117	5606	3758	1579			3108		
26	7761	6245 6883	4391	2206	9696	6865 7482	3719 4331	8:5410264 0871	
27	9049	7522	5024 5657	3461	8-630031B 0940	8098	4942	1477	
29	9693	B160	6290	4088	1562		5554	2084	
	6150337	8798	6922	4716	2183	9331	6165	2690	
31	0981	9436	7555	5343		9948	6777	3296	
32		8-5190074	8187	5970		8 5340564	7398		
33	2263	0712	8820	6597	4048	1191	7999	4508	
34	2912	1350	9452	7223		1797	9610 9221	5114 5720	
35	3555 4199	1988 2626	8-5230084 0717	7850 8477	5291 5912	*2413 3029	9832	6326	
37	4942	3263	1349	9103	6534		8-5390442	6931	
38	5485	3901	1980	9730	7155	4261	1053	7537	22
39	6128	4538	2612	8 5270356	7776	4876	1664	8142	21
40	6771	5175	3244	0983	8397	5492	2274	8748	
41	7414	5813	3876	1609		6108	2884	9353	
42	8057	6450	4507	2235		6723	3495	9958	
43	8699	7087 7724	5139 5770	3487	8:5310259 0880	7339 7954	4105 4715	6-5420563 1168	
44	9342 9984	8361	6401	4113	1500	8569	5325	1773	
	6160627	8997	7033	4739		9184	5935	2378	
47	1269	9634	7664	5364	2741	9799	6545	2983	
48		8-5200271	8295	5990		8.5350414	7155	3588	
49	2553	0907	8926	6615	3991	1029	7765	4193	1
50	3195	1543	9557	7241	4601	1644	8374	4797	10
51	3637	2190	3.5240197	7866	5221 5841	2259 2873	6984 9593	5402 6006	98
52 53	4479 5121	2816 3452	0818 1449	8491 9116	6461	3469	9-5390:203	6610	7
54	5762	4088	2079	9741	7081	4102	0812	7214	6
55	6404	4724	2709	8 5280366	7700	4717	1421	7819	5
56	7045	5360	3340	0991	8320	5331	2030		4
57	7697	5995	3970	1616		5945	2639	9027	3
58	8328 8969	6631 7267	4600 5230	2241	9559 95220178	6559 7173	3248 3857		1
59 60	9610	7267		3490		7787	4466		Ô
00	7	6'	5'	4'	3,	2'	1'	0'	81
				og. cor	AN. 880				

9	4				Log. si	NE.			[T	able II.
1	20	diff.	1 30	diff.	1 40	diff.	50	diff.	60	diff.
0	6 5428192	36096	5.51000000		SLOSCICIO	18029	8-9402960	14416	9-0192346	12002 60
1	64218	25730				17060	17375	14967	2.000A34A	11071 59
9	99949	25479	1919-11-11-11	121277E	F & COMP.	17000	31743	14320	10278	11038 00
3	8-6635390	25 (50)	DO FAIL	1772152152		17005	40000	14272	23494	11903 57
4	70536	7496C	53300	12125 146	8-8507512 25245	19200		14226		
5	±5605404 39994	34550		43337	49005	17660	88739	14178	20065	11838 55
7	74310	34316	20005	admit d	2175 41019	17568	3-9503871	14132		THE STATE OF THE S
8	8-6708357	24041	76675	737.40	200010	TIBLI	16957	14086		7772000
9	42139	33792	100001		DE LET	11441	20006	14039	00169	11740 52 11708 51
10	75660	33521	0-7472590	24000	a-set 9022	17376	44001	13995		111100
	8-5808923	33263	45260	22774	30139	17306	600.10	13949		11677 50 11645 49
12	41933	33010	69015	22538	1 11010		72843	13905 13660	34212	11645 48
13	74694	29518				17109	86703	13814	-000	11582 47
	0.6907209	22274	3-7512973 34979	22305	81646	17034	86703 8-9600617	13771		
15	39483	22024	35278	22191	98680	16966	14288	13726	68958	11519 95
16	71517 9-6003317	21000	70646	22077	88715646	16900	25014	13683	C.O. 31. I	1 1 4 5 4 5 1 1 1 1 1 1
18	34996	31569 31340	-7601512	21966	98680 98680 88715646 32546 49381 66150	16835	41097	13640	91966 9 0103424	11459 43
19	66226		23366	21954	66150	16769	68934	12001	14852	11428
20	97341	orrio	45111	21745	Done 4	16704	82487	13553	00040	11001
	8-6128235	30894	0.0747	21636	99493	16639	95999	13512	Participal Control	11202
3.3	68910	20019	89275	21528	8-8816069	TODA (D	9-970946B	13469	40054	A L WILL SHAW
23			3.7709697	21422	32581	16512	22805	13427	60961	CT DOLL I'M
24					40021	16450 16397	36280	13385 13344	71538	11277 30 11246 36
35	49003	20221		21108	65418	16325	49624	13302	82786	11914 33
26				21006	C12 1 213	16264	62926	13262	94005	11180 54
27	8-6309111	29426	94340 94344 97815244 26048	20904	\$1000 F	16939	76188	13220	1,000 U. 134	11160 33
29	6776A	29426 2 9 227	3,919544	20804	9-8914209	16142	8940B 9-9802 5 SD	13151	16354	11131 32
40.00	01101	DESCRIPTION OF REPORT OF R	JUUTIO	20705	30351	16082		13140	27485	11103 31
30	90790 8-6425634	28839	77950	20606	46433	16022	15729 28829	13100	38588 49661	11073 30
31	54282	1286119	11000	20508	62455 78418	15963	415/00	13060	60706	11048 06
133	82742	28460	p-701 P979	20411	043555	15904	54010	13051	71723	1101712
3.1	+6511016			20316	94322 3-9010169	15846	67891	12981	D-2711	10088
\$50	39107	28091	58814	20127	25955	15787 15730	000034	12943	00079	10061 25 10932 24
115	67017	27910 27731	78941	20033	9.1955	15673	39191	12865	S. OOO TURNO	10.100 49
37	84140	107555	98974	19941	D1358	15617	2 2300007	12827	15509	10072 60
133				19849	72975	15560	15434	12788	26386	10040 22
,39	49084	27381 27209	35764	19759	88535	15504	32217	12751	37235	10822 21
40	L Gallerina	92090	0.00000	19669	8-9104039	15448	44968	12713	48057	10795 20
41	8:6703932			19580	23907	15394	67081	12675	900024	10767
13	57510	26972 26706	97772 8:8117264	19492	2435]	15338		12636	03018	10741
14	84052	20544	26860	19404	65504	15295	05505	12601	DIOTE	10714
45	8-6810433	20384	65005	19317	00794	15230	9 0008160	12565,	91074	10687
16	36654	20004	75217	19232 19146			Section Comments	T-MATERIAL E	12421	TODOOLITY
17	62718		94363	10869		15071	33179	12492	23055	10634 13
AR.	83625	25754	0.0519459	18979	26105	15012	45634	12419	33663	10581
19	9.6014379	25601	34904	19395	ATT From	14966	58053	12383	44244	10555
50	39980	105 (51	51299	18813	56099	14014	70436	12348	54799	10530 10
51	65431	25303	10112	13732	71003	14989	62/94	12312	00329	10503
52	90734	25155	85844			14812	500000	12278	10000	10479
53 54	3:7015989 40900				8-9300678 15439	14761	aniotata	19949	00310	10452 6
55	65766	$\begin{array}{c} 25010 \\ 24367 \\ 24724 \end{array}$	44557	18491	20150	14711		12207		10427
56	0.0400	441.64	£9066	18412	44911	145004			17590	113401
57	3·7115075	24585	B1304	10000		14611	56135			10376 3
58	1 0000	DOMESTICAL	W. C. C. C.		73993	14501	68239	12104	38317	
59	63829		8-8417741	12120				12070 12037	48643	$10326 \ 10302 \ 0$
60				T-D T-G-T	8-9402960	24.00	92346		00340	
1	870	diff.	860	diff.		diff.	840	diff.	830	diff.
1_					LOG. COS	BINE.	25 - 55			

7	able 11.]				LOG. T	AN.				ç	5
7	20	diff.	3n	diff.	40	diff.	50	diff.	60	diff.	-
0	8·5430839 66909		9:7193958 9:7213063	24105	9:3446437 64554	19117	8·9419518 34044	14520	9-0216202 28338	12136	
1 2	8-6502683	30114	42035	23972	82597	18043	48523	14475	40441	12103	59
3	38166	304978	65977	23942	9-8500566	17969	62954	14431	52510	12069	57
4	73362		SHO SH	23712 23585	18461	17895 17822	77338	14384 14338	6454B	1203F 12004	56
5	8 5608276	24626	3.7313174	23457	36283	17751	91676	[4291	76552	11972	56
6	42912	194969	36631	23333	54034	17679	3·9505967 20211	14244	89524 9-0300464	1.1046	154
8	77275 9:5711368	34093	59964 83172	23208	71713 89321	17608	34410	14190	12373	11909	52
9	45197	33829	3.7406258	23086	4-8606859	17538	48564	14154	24249	11876	51
10	78766	33569	29222	22964	24327	17468	62672	14108	36093	11844	en.
11	9-5812077	33311	52067	22845	41725	17398	76735	14063	47906	11813	140
12	45136	33059	74792	22725	59055	17330	90754	14019	5968B	11782	48
13	77945		97400	22608 22492	76317	17262 17194	3-96047:28	13974	71439	11720	47
14	8-5910509	30303	37519892	22377	93511	17127	18659	13986	83159	11689	40
15	42832	32085	42269	22262	8-8710638	17061	32545	13943	94848	11658	45
16	74917 8-6006767	31850	64531 86681	22150	27699 44694	16995	46398 60188	13900	9 0406506 18134	11628	
18	38386	31619	3-7608719	22038	61623	16929	73944	13756	29731	11597	49
19	63777	31391	30647	21929	78487	16864	87658	13714	41299	11568	41
20	8.6100943	31166	52465	21818	95286	16799	8-9701330	13672	52836	11537	40
21	31889	30946	74175	21710	3-8812022	16736	14959	13629	64343	11507	20
2.2	62616	30141	95777	21602	28694	16672	28547	13588	75821	11478	20
23	93127	30511 30300	37717274	$\frac{21497}{21391}$	45303	16609 16547	42092	13545 13505	87270		
	8 6223427	30001	38665	21237	61850	16484	55597	13463	98689	11389	36
25	53518	9.1024	59952	21184	79334	16423	69060	13423	a and LADA U	11961	30
26	83402	20391	81136	21082	94757	16362	82483 95866	13382	21439 32771	11332	34
27	8-6313063 42663	2040U	3-780221B 23199	20991	3-8911119 27420	16301	1.9409206	13341	44074	11303	33
29	71845	43434	44079	20880	43660	16240	22507	13301	55349	11275	31
30	3-6400931	20086	64961	20782	59842	16182	35769	13262	66595	11246	30
31	29825	28394	85544	20663	75963	16121	48991	13222	77813	11218	1311
32	58528	28703	9-7906130	20586	92026	16063	62173	13182	89002	11189	-30
33	87044	28516 28331	26620	20490 20394	3-9008030	16004 15947	75317	13144	990000164	11162	27
34	8 65 15 375	-20147	47014	20299	23977	15889	88421	13066	11297	1 2 1 500	411
35	43522	97040	67313	20206	39966	15831	5 9901487	13027	22403	11079	40
36	71490 99279	37700	87519	20113	55697 71472	15775	14514 27503	12989	33482 44533	11051	24
37	8-6626891	27612	\$9007632 27653	20021	87190	15718	40454	12951	55556	11023	23 22
39	54331	27440	47583	19930	8-9102853	15663	53367	12913	66553	10997	21
40	81598	27267	67422	19839	18460	15607	66243	12376	77522	10969	20
111	8-6709697	27099	87172	19750	34012	15552	79081	12838	88465	10943	10
12	35629	26931	*8106934	19662	49509	15497	91983	12903	99381	10916	10
43	62393	20100	26407	19573 19487	64952	15443 15389	9-0004647	12764 12728	9.0710270		3.7
44	88996	O 14 4 1	45894	19400	80340	15335	17375	12691	21133	10000	10
145	8-6815437	94909	65294	19314	95675	15282	30066 42721	12655	31969	10010	15
46	41719 67844	00105	\$4609 \$-8203938	19230	8·9210957 26186	15229	55340	12619	42779 53563	10784	14
相用	93813	25969	22984	19146	41363	15177	67924	12584	64321	10758	10
49	8-6919629	ZaH Lu	42046	19062	56487	15124	80471	12547	75053	10732	11
50	45292	29003	61026	18980	71560	15073	92984	12513	85760	10707	10
51	70806	120011	79924	18998	86581	15021	9 9105461	12477	06441	10681	9
52	96172	[25300	09741	18817	8.9301552	14971	17903	$\frac{12442}{12407}$	9-0807096	10655	8
53	8-7021390	25218	#8317478	18737 18656	16471	14919 14869	30310	12372	17726	10605	8 7 6
54	46465	14096	36134	19579	91930	14820	42682	12339	28331	10580	6
55		24700	54712	18499	46160	14769	55021	12304	38911	10555	5
56		94640	13311	12499	60929 75650	14721	67325 79594	12269	49466 59996	10530	4
57		24511	91633 3:8409977	10944	0//201	140/1	01831	12237	70501	10505	3 2
159		24314	20245	10405	8-9404944	14623	9-0504033	12202	190091	10490	î
60			46437	18192	19518	14574	16202	12169	91438	10457	0
1	870	diff.	86°	diff.	850	diff.	840	diff.	830	diff.	1
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	96				LOG. SIN:	Ε.			[Ta	ble u.
1	7	diff.	Ho	diff.	90	diff.	1 10°	diff.	110	diff.
0	9-0958945	10276	9.1435553	2070	9-1943324	70/10	9-2396702	7159	9.2805998	640× 60
1	69221	10252	44532	12061	51293	7054	9-2403861	7146		
2	79473	10227	53493	P049	59247 67186	7939	11007	7134	18967	6474 58
4	89700 99903	10203	62435 71359	70140	75110		18141	7123	25441 31905	6464 54
6	9-0910082	10179	80262	H; rua	83019	1300	25264 32374	7110	38359	6454
6	20237	10155	89148	HAMI	90913	1 COM	39472	unas	44803	0444 54
7	30367	10130	99015	8867 8949	98793	7880 7865	46558	7086 7074	51237	
8	40474	CHOKHI	9.1506864	3830	9.2006659	7851	D3032	7063	57661	
9	50556	10059	15694	A913	14303	7836	60696	7051	64076	
10	60615	10036	24507	8794	22345	7822	677/6		70490	6395 50
11	70651 80562	10011	33301 42076	ロフブロ	30167 37974	7807	74754 81811	10 44	76875 83260	0.335
13	80051	9989	50834	4194	45766	1135	88627	7016	B9636	03/0/42
14	9.1000616	9965	59574	9740	53545	7779	06930	7003	06001	0.105 Ac
15	10558	9942	68296	8722 9704	61309	7764 7750	9.2502822	8081	9.2902357	6356 45
16	20477	9896	77000	9686	69059	77'360	Uamna	6969	08704	6336 43
17	30373	0273	85686	R068	76795	7721	10//2	6057	15040	
19	40246 50096	SHOP	94354 9-1603005	9651	84516 92224	7708		0340	21367 27685	6318
20		9828		8634	99917	7693	37609	6934	33993	0303
21	69729	9805	11639 20254	8615	9.2107597	7680	A4520	0943		6298 39
22		9783	28853	פפפה	15263	7666	51444	03179	4 Charles	11259
23		9760 9738	37434	1245	22914	1691	59344			200
24	99010	9716	45998		30552	7694	09433	GRIT	59129	8261 3h
25	9-1108726	9694	54544	0220	38170	2611	/2110	6867	65390	6951 50
26 27		9672	63074	9519	43/3/	7597	78977	COSS	71641	6242 34
29	28092 37742	9650	71586 80081	6495	53384 60967	7593		0044		6233^{+33}_{-32}
29	47370	9628	98359	8478	60526	7569	00500	0999	90339	0223 21
30	1	9607	97021	0402	70009	1990	การเกรรรก	0941	ogeen	0214
31	66562	9585	0.1705.005	8444	20/325	7543	19141	DOLL	0.0000000	1 2 2 2
32	76125	9563 9542	19219	(54/25)	0.1164	7529	19941	6700	0.00	D 1959
33		0591	22305 30699	B 504	98680			6778	08953 15140	6177 27
34		0500	30699	8378	9.2206132	7489	33507	6767		
35		544 4 54	39077 47439	3362	13671 21147	7476		6756		
37		9457	55704	15.513	99000	7462	59775	0140		
38			64112 72425	F378	36059		60509	0134		
39	42477	9395	72425	12313	43495	7423	67232	6723		6123 21
40		9374	80721	8280	50918		73945	6709	E0106	C114 20
41		0354	80001	[82]9] [99.14		7307	D0.0-31	6691	.64303	6104 19
42		1,020.1	97265	8247	65725	7295	6112526	GGR1	70407	2000 13
43		31.51.5	19714	8232	73110	7771		6670	70503	6007 11
45	0	9202				7359	07349	-0003	99869	0018
16			30160	BEZOO	05125	1340	13007	0049	04797	0009 14
47	17064		39344	10 1 Mg	9:2300518	7320	20635	0035	9.3100798	6061 13
19	April Congress	0919	46512	8153	0993B	7907	41403	6617	06849	GD42/14
49	140,50 414	9193	59005	8137	17145	7295	33880	6607	12892	6034
50			E COCO		134440	1900	40497	6596	13926	6005 10
51 52		9153	780:20	8106	31722	7270	47000	RECR	24901	10017 9
3.1		9133	87120	8091	46249	7257	53003	6576	30968	600R
54		9114			b3494			Coppo	4907E	D/1/1/26 *
55	90370	0075	9.1903254	SHAR	60726	7990	73366	0000	48965	5000 6
55		9050	11299	180120	67946			Prince of A		5024 4
57		0038	19328 27342	9014	75153	23 Det	00440	65.05	00921	coca 3
58 59		3101	35341	7999	B0539	7193	00494	6614	79241	5956
.i0			43324		96702		9:2805988		78789	5949 0
1	820	diff.		diff.		diff.	790	diff.		diff.
					LOG. COS			20		
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10	ble 11.]				LOG. TA	N.				97	7
1	70	diff.		diff.	90	diff.	100	diff.	110	diff.	,
	0591438	10431	9.1478025		9.1997125	8169	9.2463188	7381	9-2886523	6740	60
1 2	12277	10408	871821 96321	9139	9·2005294 13449	8155	70569 77939	7370	93263 99993		
3	22660	10363	0-1505441	9120.	21588	8139	95907	7358			58 57
4	33020	Luadu	14543	9102	29714	B126	92643	7346	9-2506713 13424	6711	56
5	43355	10336	22627	9094	37825	8111	99978	7336	20126	6702	
6	53667	10312	32692	9065	45922	8097	9.2507301	1343	26817	DOST	54
7	63955	10288 10264	41739	9047 9030	54004	8092	14612	7311	93800	0063	53
8	74219	10204	50769	9011	62072	2 2 2 2 7	21912	7300 7286	40172		52
9	84460	10218	59780	8993	70126	0034	29200	7277	46836	6653	61
10	94678		68773		78166	marian	36477		53489		50
	9.1004872	10194	77748	8975	86191 94203	10019	43743	7260 7264			49
12	15044	10172 10148	86706	9959 8940	94203	7997	50997	7243	66769	6696	48
13	25192	10195	96646	8923	9-2102200	7984	58240	7990	19930	6616	47
14	35317	10103	9-1604569	8904	10184	7969	05472	7000	COULT	CCOM!	46
15	45420	10080	13473	8888	18153	7956	72692	7209	86618	6598	45
16	55500	10057	22361	8870	26109	7942	19901	7100	93216	BEER!	44
17	65557	10034	31231	8852	34051	7020	87099	7186			
16	75591 85604	10013	40083 48919	GOOM	41980	7914	94265	7176	9.3006383	SST1	43
1		9990		8818	49894	1 9 9 9 8	9-2601461	7164	12964	6560	41
20	95594	9968	57737 00130	8501	57795		08625	7154	19514		40
21	9.1105562	9946	66538	OTOA	65683	9	15779	7149	26066	6543	38
	15508	9923	75322	9767	73556 81417	7961	22941		32609		
23	25431 35333	9902	94069 92839	8750	81417 89264	7847	30053 37173	1150	39143 45667	6524	37 36
25	45213	9880	9-1701572	8733	97097	1833	44009	3 1 7 7 7	52183	0910	35
26	55072	7859	10289	8/11	9.2204917	11820	51382	1099	58689	051/0	34
27	64909	9837	18989	8700	12724	1 MUT	50470	1000	65187	0490	33
28	74724	9815	27672	9049	20518	1129	66647	1011	71675	0900	32
29	B4518	9794	3633B	5000	28298	1100	72613	7066	78155	6480	31
36	94291	9773	44489	8650	36068	7767	79669	7056	84626		30
	9-1204043	9752	A3697	19034	43819	1/04	86714	7045	91088	0402	24
32	13773	9730	69930	8011	51561	1142	027/0	1029	02531	6403	28
:33	23482	9709	70840	DON	50990	11120	0.0500779	11123	0.2102006	0.144	43.7
34	33171	9689 9668		8586 8568	67004	7715 7102		7019	10421	0420	26
35	42839	0647	61,583	Oct 2	74706	7000	2 2 2 2 2 2 2 2	6倍4500%		6310	25
36	52486	0626	90540	OE'M	0.4300	7676	21760	6609	23266		
37	62112	0606	a. 19non95	QK90	9007	7664	28702	0.071	29675	6403	33
38	71718		13602		97738	7651	35733		36076	6209	22
39	81363	9565	22100	10400		7638		unan		6383	21
40	90868	9545	30595		13024	1 15 3513	49644	TID SINGUL	48851	6375	20
43	9.1300413	9524	39000	9450	20666	me 2 3 60	26554	6930		6366	15
42	$\begin{array}{c} 09937 \\ 19442 \end{array}$	0505	4/025	8441	28262	2601		6920	67070	6358	18
43	28926	DADA			35862 43451	7588	77743	TO THE	67950 74299	6349	1
49 4E	38391	9465	79909	8410	51026	7575	24949	logari.		PRID A F	10.0
40	47835	5 444	81196	83314	ECEDI	1009	01131	0920		Chra	HT 4
47	- 57260	142	RUSTS	9015	00104	14900	parinc	10010	89908	0343	113
18	66665	1.4136	97939	5246	79/77	01539	M. 900 4070	1000s	0.00011	(3)310	13
19	70051	9380	9-1906287		01000	10.40	11796		0-220-010		i i i
30	85417	9366	14621	0000	00717	1514	1858	CC42	19916	0236	110
51	94764	9347	99034	18310	06916	abul	05/499	1,2130	10506	0.250	1
52	9-1404092	9328	31941	9207	9.2403708	14:10	29951	0845	94799	0252	1
53	13406	9308	39529	0200	1118/	1911	20020	02.12	21061	02/3	
54	22689	9289	41002		18600	7455	90010			6266	1
56	31959		50055	9943	26103	7440	D20//	6790	49999	6249	1
56	41210	0000	64302	19999	33543	7.196	00966	6770	45927	6941	1 9
57	60442	0213	72530	8913	40977	7817	00.448	6760	\$66019	6999	
58	59656	9194	00/43	12102	40000	7405	131114	Retain	04300	6994	
59	58949	0.176	88941	DIDA	55794	7794	19115	6756	08525	6216	
	75025		97126		63188	1	000340	1	74745	1	1
60	820	diff.	810	diff.	80°	diff.	790	diff.	780	diff.	1 6

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	98				LOG. SI	NE.			[]	able	n.
7	12,	diff.	130	diff.	140	diff.	15°	diff.		diff.	Ľ
0	9·3178789 84728	5939	9·3520880 26349	5469	9·3836752 41815	5063	9·4129962 34674	4712		4403	
2	90659	5931 5922	31810	5461 5454	46873	5058 5051	39381		12182	1398	58
3	96581 9:3202495	5914	37264	5446	51924	5045	44082	Acoc	16576	1200	
5	08400	5905	42710 43150	5440	56969 62008	5039	48778 52468	4690	20965 25349	4384	55
16	14297	5897 5989	53582	5432 5425	67040	5032 5027	58152	4684 4680	29728	4379	54
7 8	20186 26066	5880	59007 64426	5419	72067	5020	62832	4674	34103 38472	14369	100
9	31938	5872	69836	5410	77087 82101	5014	67506 72174	4668	42837	L DOO	51
10	37802	0004	75240	5404	87109	5008	76837	4663	47197	4500	EN
11	43657	5855 5848	80637	5397 5390	92111	5002 4995	81495	4658 4653	51553	4350	143
12 13	49505 55344	5839	86027 91409	5382	97106 9·3902096	4990	86148 90795	1647	55904 60250	1494C	48 47
14	61174	5830	96785	5376	07079	4983	95436	4641	64591	4341	46
15	00997	5823 5814	9.3602154	5369 5361	12057	4978 4971	9.4200073	4637 4631	68927	4336 4332	40
l6 17	79617	5806	07515 12870	5355	17028 21993	1965	04704 09330	4626	73259 77586	4327	12
18	84416	5799	18217	5347	26952	4959	13950	4620	81909	4323	49
19	90206	5790 5782	23558	5341 5334	31905	4953 4947	18566	4616 4610	86227	4313	41
20	95988	5773	28892	5327	36852	4942	23176	4604	90540	4000	40
21 22	9·3301761 07527	5766	34219 · 39539	5320	41794 46729	4935	27780 32380	4600	94849 99153	4304	39 38
23 24	13285	5758	44852	5313	51658	4929	36974	4594 4589	9·4503452 07747	4299	37
24	19035	5750 5742	50158 55458	5306 5300	56531 61499	4923 4918	41563	4584	07747	4295 4290	36
26 26	30511	5734	607/50	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			40147 #0796	4579	12037 16322	4285	35 34
25 26 27 28 29	36237	5726 5718	66036	5286	71215	4905 4900	55200	4573 4568	12037 16322 20603	4281	33
28	41000	5710	11919	5279 5272	10215	4894	69867	4563	22013	4272	32
	41000	5703	70367	5266	91109	4987	64430	4558	29151	4267	31
30 31		5694	81853 87111	5258	95996 90878	4882	68988 73541	4553	33418 37691	4203	30 29
32	64740	5687 5679	92363	5252	05754	4876 4871	70000	4548 4542	41939	4258	28
33	70428 76099	5671	97608 97608 9°3702847				82031	4538	40192	4249	27 26
34 35	81767	.,			05489 10348 15201	4959		4532		4245	25 25
36	87418	5656 5647	13304	5225 5219	15201	4853	96228	4527 4522	58926	4240	24
37	93005	5641	18523	5212	15201 20049 24889	4841	9.4300750	4517	67202	4231	23 22
		5632	23735 28940	5205	29724	-000	05267 09779	4512	67392 71618	4226	$\frac{22}{21}$
10	00003	5625	34139	5199	34554	4830	14286	4507	75040	4222	20
11	15580	5617 5610	39331	5192 5186	39378	4924 4818	18788	4502 4497	80058		19
12 13	21190 26792	5602		5179	44196	4913	23285 27777	4492	99400	4209	18 17
1.1		5594	54368	5172	43009	4007	32264	4487	02604	4204	16
15	37973	5587 5579	60034	5166 5160	53617	4801 4796	36746	4482 4477	96884	4200 4195	15
16 17	43552 49124	5572	70347	5153	63413 68203	4790	41223 45694	4471	9·4601079 05270	4191	14
18	54689	5564	75493	5146	72987	4784 4779	50161	4467 4462	09456	4196	12
19	00245	5557 5549	80633	5140 5134	77766	4773	54623	4457	13638	4182 4178	11
5(1	65794	5542	85767	5127	82539	4767	59080	4452	17816	1172	10
51 52	71336 76870	5534	90894 96015	5121	87306 9 2 068	4762	63532 67980	4448	21989 26158 30323		3
53	82397	5527	9:3801129	5114	96824	4756	72422	4442 4437	30323 34483	4165	7
54	87917	5520 5512	06237	5108 5102	9.4101575	4751 4745	76859	4433	34493	4156	6
55 56	93429 98934	5505	11339 16434	5095	06320 11059	4739	81292 85719	4427	38639 42790	4151	1 2
57	9:3504432	5498 5490	21523	5089 5082	15793	4734 4729	90142	4423 4418	46938	4140	3
38	09922	5483	26605	5077	20522	4723	94560	1112	51081	4120	
59 60	15405 20880	5475	31682 36752	5070	25245 29962	4717	989 7 3 9·4403381	4408		1124	0
1	770	diff.	760	diff.		diff.		diff.		diff.	
		-			LOG. COS	INE.				-	

T	able 11.]				LOG. T	AN.					99
1	129	diff.	130	diff.	140	diff.	15°	diff.	160	diff.	*
0	9-3274745	6208	9.3633641	5760	9.3967711	5378	9.4280525	5050	9.4574964	4766	60
1	80963	6200	39401	5754	73069 78463	5374	\$5575 90621	504t	79730	4761	59
2 3	87153 93345	6192	45155 50901	5746	83830	5367	95661	5041.	84491	4767	58
4	99528	6183	56641	5740	89191	5361	9-4300697	503t	89248 94001	4753	57
	9:3305704	6176	62374	5733 5726	94547	5356 5349	05727	5030 5036	98749	4748	55
6	11872	6169 6159	68100	5710	99896	5344	10753	5020	9.4603492	4743 4740	
7	18031	6152	43519	5713	9-4005240	5338	15773	501t	08232	オヤワた	DO 1
8	24183 30327	6144	79532 85238	5706	10576 15910	5332	20789 25799	5010	12967	47211	1 43 thm
9		6136		5699		5327		5005	17697	4726	01
.10	36463 42591	6128	90937 96629	5692	21237 26558	5321	30804 35805	500)	22423	44000	DU.
11	40197.9.3	6120	9'3702315	5686	31973	5315	40800	499£	27145 31863	A PER LINE	(200.0)
13	54823	6112	07994	5679	37182	5300	45791	4991	36576	4112	47
14	60927	0.504	m day on others	5673	42496	5304	50776	4985	41285		
15	67024	6097 6089	13667	5650	47784	529F 5292	55757	4970	45990	4700	40
116	73113	6081	24992	5653	53076	5287	60733	4971	50090	AGOG	44
17	79194 85267	6073	30645 36291	5646	58363 63644	5291	65704 70670	496t.	65386 60076	4692	43
18	91333	6066	41930	5639	68919	5278	75631	4961	64765	4687	41
20	97391	6058	47563	5633	74189	5270	80587	4956	69448	4683	40
21	9.3403441	6050	53190	5627	79453	5264	85538	4951	74127	4679	39
22	09484	6043	FODIO	5620	84712	0.259	90485	4947	78802	4675	38
23.	15519	$6036 \\ 6027$	64423	5013	89965		95426	4941	83473	4671 4666	37
24	21546	6020	70030	5601	95212	5242	9.4400363	3020	88139	4602	36
25	27566	6012	75631 81225	5594	9-4100454	5236	05298	40.27	92801	4658	35
26 27	33578 39583	6006	B6813	4588	05690 10921	5231	10222 15146	4923	97459 9·4702112	4653	34
38	45580	5997	92394	5581	16146	5225	20062	4917	00762	4650	32
29	51570	5990	97969	5576	21366	5220	24975	4913	11407	4645	31
30	57552	5982	9.3803537	5568	26581	5215	29863	4905	10048	4641	30
31	63527	5975	09100	5563	31789	5208	34786	4903	20685	4637	29
32	69494	5967 5960	14655	5555 5550	36993	5204 5198	39685	4899 4894	25318	4633 4629	ALC:
33	76454	5953	20205	5543	42191	5192	44579 49463	4889	29947	4625	4.1
34	81407	5945	25748 31295	5537	47383 52570	5187	49468	4984	34572	4620	26 25
36	93290 93290	5934	36816	5531.	PART IN	5182	54352 59232	4.380	39192 43808	4616	24
37	99220	5930	42340	5524	6292B	5176	64107	4978	45421		
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39	11059	5905	53370	5506	73265	5166 5160	73843	4861	57633	4600	21
40	16968	5901	58876	senn	78425	6155	78704	4857	62233	4596	20
41	22869	5894	64376	2.409	83590		83561	4851	66829	4592	19
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43	34650 40530	5890	75356 80837	5491	93674 99013	5139	93260 98102	4842	76009 60592	4999	16
45	46402	5872	96312	5475	9.4204146	5133	9.4502940	4838	85172	4000	15
46	52267	5965	91781	5469	09275	5129 5109	07774	4834	89748	4571	14
47	58126	5859 5851	97244	5463 5456	14900		12602	4828	94319	4568	13
48	63977	5844	9-3902700	5451	19515	5112	17427	4819	98887	4564	12
49	69921	6837	08151	5444	24628	5107	22246	4815	0.4803491	4560	11
50	75658	5820	13595	5439	29735	5103	27061	4811	08011 12566	4555	10
51 52	91487 87310	5823	19034 24466	5432	34838 39935	5097	31972 36678	4806	12566 17118	4652	8
53	93126	5816	29893	5427	45026	5091	41479	4801	21666		7
54	98935	5809	35313	5420	50113	5087	46276	4797	26210	4540	6
155	9.3604736	5801 5795	40727	5414 5409	55194		51069		90190	4536	5
56	10531	5788	46136	5402	60271	E621	65857	4784	35286	4532	3
57	16319 22100	5781	51538 56935	5397	65342 70408	50G6	60641 65420	4779	39818 44346	19520	
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4	75848	dita	15345	3B74	41067	3657	54375	3400	56433	2701	57 56
5	79960	4112	19216	3871 3867	44721	3654 3650	K7000		59711	1.632	55
6	84069	41114	23083	3963	48371	3646	01280	3451	62987	2979	54
7 8	98173 92273	ALCO	26946	3860	52017	3643	64737	2447	66259	2270	53
9	96369	411110	30800 34661	3855	55660 59300	3640	08184 71629	13440	69529 72796	3201	52
10	5 4700461	40:72	39513	3852	69096	19090	75070	3491		3204	51
ii	04548	4097	42361	3848	66569 70198	3633	78508	3438	76060 79321	3401	50 49
12	09631	4033	46205	3844	70198	$\frac{3.29}{3626}$	81943	3435	82579	3258	48
13	12710	4079	50046	3847 3837	73824	3623	85375		85835		47
14	16785	4071	53983	3833	77447	3619	88804	12/4/200	89088	3250s	46
15 16	20856 24922	4000	57716 61545	3329	81066 84682	3614	92230		92338 95585	39.17	45
17	28985	4063	65370	3925	83296	3613	95653 99073	3420	98829		44
18	33043	4058 4054	69192	3922	91904	3 (09 3606	9-5402499 05903	3416	9.5602071	3343	42
19	37097	4049	73010	3818. 3814.	95510	3602	05903	3411	05310		41
20	41146	1046	76824	3911	99112	3599	09314		08546	3233	40
21	45192	1040	80635	3/307)	FE202711	1596	12721	2406	11779	3233	39
22 23	49234 53271	4037	Hands	3803	06307	3592	16126	19401	15010	3227	39
24	57304	4033	98245 92045	3 400	09999 13486	1589	19527 22926	3.53	19237 21462	Jan Sant	37
25	61334	4030	95840	3795	17074	35B0	26391	3.395	24685	9449	36
26	65359	$\frac{4025}{4021}$	00699	$\frac{3793}{3788}$	20656	3592 357!	29713	3392	27504	1.52 1.91	34
27	6938u	4016	9.900.9121	3795	24235	3570	OOLOB	12.359	31121	3214	33
28	7339C	1013	07206	3781	27811	3572	36489		34335	3211	32
29	77409	4009	10987	3777	31393	3570	39873	3380	37546	3208	31
30	81419 85423	4005	14764	3774	34953	3565	13453	2277	40754		30
32	F9423	4000	1953° 22308	3771	3°51° 42081	1565	46630 50005	2215	43960	3303	29 28
33	93420	3997	26075	3767	45641.	3559	53376	3311	47163 50363	3410	27
34	97415	3992 3989	29838	3763 3759.	49190	3554. 3553	56745		53561		26
.35):480[40]	3984	33597	3750	52749	3545	60110	3362	56756	3199	25
36	05395	3981	37353 41105	3752	56298 69844	3540	63472 66832	3366	59948	2190	24
39	13.342	3976	44853	3748	63337	3543	70189	3357	63137 66324	3101	23 22
39	17315	3973	48598	3745	66927	3540	73542	3353	69508	31091	21
40	21293	396F	52339	3741	70463	3530	76893	3351	72689	9101	20
41	25249	3965 3950	E6077	3738 3734	73997	3534 352!	80240	3347 3345	75868		19
42	2.120-3	3957	9:3H11	3731	77526	3527	93595	3342	79044		18
43	33165	3952	63542	3727	81053	3524	86927	3339	P2217	3170	17
44	37117 41066	3949	67269 70992	3723	84577 85097	3520	90266 93602	3330	95387 99555	aton.	16
46	45010	3944	74712	3720	91614	3517	96935	3333	91721	3100	15 14
47	48051	3941 3937	78428	$\frac{3716}{3713}$	95128	3514 3510) 5500265	3330	94883		13
48	5288	3932	B2141	3709	98,335	350H	03592	3324	98043		12
49	56820	3920	85850	3705	F5302146	3504	06916	3321) 5701200	3155	11
50	60749	3925	89556	3702	05650	3501	10237	3319	04355		10
51 52	64674 68595	3921	93258 96956	3698	09151 12649	3496	13556 16871	3315	07506 10656	3150	9.6
53	72512	3917	0.5100351	3695	16143	3494	20184	3313	13862	3146	7
54	76426	3914 3909	04343	$3692 \\ 3688$	19635	3490	23494	3310	16946	3144	6
55	20335	2005	08031	3685	23123	3488 3488	26801	3307 3304	20087	3141	5
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57	88142 92040	3898	15397 19074	3677	30090 33569	3479	33406 36704	3298	26362 29495	3133	32
59	96034	3394	22749	3675	37044	3475	39999	3295	32626	3131	i
60	99824	3300	26419	3670	40517	3473	43292	3293	35754	3128	0
1	720	diff.		diff.	70°	diff.	690	diff.	680	diff.	1
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7	170	diff.		diff.		diff.	200	diff.	210	diff.	10
0	9·4853390 57907	4517	9·5117760 22057	4297	9-5369719 73821	4102	9.5610659	3929	9.6841774	3775	60
	62419	4512	26351	4294	77920	4099	14588 18515	3927	45549 49321	3172	59 58
3	66928	4505 4505	30641	4290 4286	62017	4097 4093	2243	3924	53091	3770	57
4	71433	4501	34927	4283	86110	40000	26364	3921 3918	56859	3768 3765	ili
6	75933 80430	1497	39210 43490	4280	90200	4087	30278	391t	60624	3762	55
7	84924	1494	47766	4276	94587 98371	1084	34114 38107	3915	643% 0/14%	3761	54
7 8	89413	4480 4485	52039	4273 4270	9.5402453	4081	42016	3911	71.00	J757	53
9	93898	4482	563U9	4266	06531	4078 4075	4592	35 07 35 06	7561.6	3756 3753	51
10	99380	4478	60575	4263	10606	4072	40031		79413		50
11	9.4902858	4474	64838	4259	14678	4069	53793		53163	2744	49
12	07332 11802	4470	69097 73353	4256	18747	4060	57633	3897	86912	2746	48
13 14	16269	4467	77606	4253	22913 26877	4064	61530 65424	3894	90657, 94401	(3144)	47
15	20731	4469	81855	4249 4246	30937	4060	69316	333	98142	3741	46
16	25190	4450	86101	$\frac{4243}{4243}$	34994	$\frac{4057}{4054}$	7,320,5	346	9-5901881	3739 3736	
17	29646	4451	00344	4239	39048	4052	77091	1954	05017		
18	34097 39545	4448	9458a 9821:	4236	43100 47148	4048	80071 84950	3881	09351	1.54.511	30
	42988	4443	9.5203052	4233		4045		3879	13082	3730	44
20 21	47429	4441	07281	4230	511: 3 £6236	4013	88735 92511	3876	16812 20539	3727	40 39
22	5186£	4436	11306	4226	69276	4040	Dudga	3873	24263	3724	38
23	56296	$\frac{4433}{4429}$	15730	$\frac{4222}{4220}$	63312) 5700355	3871 3868	27985		1377
24	60727	4425	19950	4216	67346	4031	04223	3865	31705	2719	36
25 26	65152	4422	24166 28379	4213	71 177 75405	4028	06088 11951	3963	35423	3715	35
27	73991	4417	32586	4210	79430	4025	15811	3960	39138 42851	3713	34
28	7840h	4416	36795	4206 4204	83452	4032	19669	3868	46561	3710	Eich
20	82816	4407	40999	4200	67471	4019	23524	3853	50269	3708 3706	21
30	67223	4403	45199	4196	91427		27377	3950	53975		30
31	51626	4400	49395	4194	955(4)	4013	31227	3947	57679		29
32 33	96026 9:5000422	4.500	53589 57779	4190	99511 9°5503519	470000	35074 38919	3945	61380	2600	28
34	04914	4392	61966	4187	07523	4004	42761	3842	65079 68776	3697	27 26
35	09203	4380	66150	4181	11525	4002	46601	3840	72470	3054	10E
36	13588	4381	70331	4177	15524	3999 3997	50438	3837	76162	3692 3690	34
37 38	17969 22347	4378	7450F 78692	4174	19521 23514	3993	5427:	3832	79850	3688	23
39	26721	4374	S2563	4171	27504	3990	68104 61934	3330	83540 97225	3685	22 21
40	31092	1371	87021	4168	31492	3988	65761	3827	90908	3683	20
41	35459	4367 4363	91170	4165	35477	3 95	69595	3824	94588	3690	10
42	39822	4360	95347	$\frac{4161}{4158}$	3 1450	3982	73407	3822 3819	08967	3679 3676	10
43	44182 48538	4356	9950:	4156	43439	3 77	77226	3817	0.0001542	3674	11
44	69901	4353	9·5303661 07813	1152	47115 51385	3973	81045 84858	3815	05G17 09289	9679	16
46	67240	4349	11961	414F	55359	3971	68669	3811	12958	3669	15
47	61586	4346 4343	16107	414L 4143	59327	3965 3965	02475	3810 3807	18625	3007	13
48	00928	4339	20250	4139	(13202	3963	9628	3804	20290		12
49	70267	4335	24389	4137	67255	3959	9-5800090	3802	23953	3660	11
50 51	74602	4331	28526	4133	71214	3957	03892	3799	27613	3656	10
52	78933 83261	4323	32659 36789	4130	75171 79125	3954	07691 11488	3797	31271 34927	3656	9
53	97596	4325	40916	4127	83077	3952	15292	3794	38581	3654	7
54	91907	$\frac{4321}{4317}$	45040	$\frac{4124}{4121}$	87025	3948 3940	19074	3792 3790	42233	3652 3649	6
55	96224	4315	49161	4117	90971	3943	22864	3787	46882	3647	5
56 57		4310	53278 57393	4115	94914 98354	3940	26651 30435	3784	49529	3645	4 3
58	00156	4307	61505	4112	9.5602792	3938	34217	3792	53174 56817	3643	2
59	13460	4304 4300	65613	4109 4106	<. 06727	3935	37997	3780	60457	3640	1
60	11100		69719		10659	3932	41774	3777	64096	3639	0
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1	1940	diff.	230	diff.	240	diff.	250	diff.	26° 9-6418420 9-6421009 3596 6182 9-6431347 3926 6504 9080 9-6441654 4226 6796	diff.
0	9.5735754	1 2F	9.5918780	2078	9.6093133	2830	9-6259483	2708	9.6418420	2599 60
1	8980	3125	9.5921755	2973	6969	2834	9.6262191	2706	9.6421009	2587 59
2	9.5742003	3120	4729	2970	8803	2832	4897	2704	3596	2586 68
3	0144	3117	0.5000000	296B	9.6101635	2830	7001	2702	0182	2583 57
5	0-5751256	3116	3631	2965	7909	2826	2003	2700	0-6431347	2582
6	4468	3112	6594	2963	9-6110118	2626	5703	2698	3926	2579
7	7679	3110	9555	2961.	2941	2823	8397	2696	6504	2579 5
8	9.5760696	2101	3.5942513	2019F	5762	9010	9-6281090	9609	9080	2574 5
9	3790	3100	5469	4990	8580	2017	3762	2600	9-6441654	2572 6
10	6892	DOOR	8422	2000	9.6121397	9014	3762 6472 9160 9-6291845 4529 7211 98.4	neces	9-6441654 4226 6796 9365 9-6451931 4496	5
111	9991	SUND	9.5951373	2597	4211	P182	9160	2002	6796	2570 4 2569 4
114	9.5773088	3003	4322	2046	7023	2014	0.0331949	PEGRA!	9300	9566
13	6183	3095	7265	2944	9833	2805	4529	2682	9-6451931 4496 7058 9619	2565
14	9275	3089	0.5900515	2942	0.6132641	2907	7211	2679	4496	2562
Iti	9.5782364	3080	3154	2039	0960	2804	P. ADDOS OF	2678	0610	2561
17	8535	3088	(30):30	2937	0.6141051	2801	5943	2675	9.6462179	2559
	9.6791616	3031	5469 8422 9:5951373 4322 7264 0:5960212 3154 6093 9034) 5971967	2.135	3950	2711	7917	2674	4735	2557
19	4695	3079	4897	2034	6047	2704	3.6310555	2072	7290	2555 4
20	7772	3077	7827 9-5380754 3675 660 2	anot.	9441	T199	3255	2002	9-6462179 9-6462179 9-6462179 9-6462179 9-6472395 4-946 7492 9-6480036 2582 5124 7665 9-6490203 2740 5274 7807 9-6500339 9-6510444 2966 5496 8004	2554
21	9-5800P45	3073	9-5980754	2927	9.6152234	2793	592	2008	9.6472395	2551 3
22	3917	3072	3675	2925	5024	1275H	8591	2000	4946	2550 3
23	6986	2009	6602	2021	7812	2701	3.6321255	2004	7492	2547 3 2546 3
24	9.2910025	3064	952:	2019	9.6160399	2793	391€	2660	9-6480036	2544
25	3116	3061	9-5992441	2910	3382	2783	6576	2657	2582	2542
26 27	6177 9236	3059	5357	2913	6164	2790	9233	2656	7005	2541 3
28	9-5822292	3056	0.6001101	2911	0-6171791	2777	4549	2653	0-6400303	2538 3
25	5345	3053	409K	2909	4496	2775	7194	2652	2740	2537 3
30	8397	3052	6007	2997	2020	2774	0044	2650	5974	2534
31	9.5931445	3048	9997	2904	0.6180041	2771	0.6040401	2647	7907	2533
32	4491	3046	9.6012803	2902	2909	2768	5137	2646	9.6500338	2531
33	7535	3044	5703	2900	5576	2767	7780	2643	2867	2530 2
34	9.5840576	2020	8600	2000	8341	2763	0.6350422	3094 ocan	5395	2527 2 2525 5
3.	3615	3038	0.6021495	2999	9.6191103	9761	3062	9627	7920	2524 2
30	6651	3034	4390	2590	32/4	2759	5699	2636	9-6510444	2522 2
37	9685	3031	0.0020101	2888	6022	2756	5335	2634	2966	2520 2
36	9-5852716 5745	3029	9.0030100	2R\$\(6\)	0-6909129	2754	9.0300508	2632	0004	2518 2
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41	0-5001705	3024	5930	2881	4894	2750	6231	2628	9.6520521	2514
4	9.3901139	3021	0.604 1606	2879	0-6910399	3748	5-697142A	2625	3035 E540	2513
3	7835	3019	4579	2877	3197	2745	4109	2624	0045 S056	2511
44	9-5970851	3016	7449	2975	6971	2744	6731	2623	9-6530568	2509
45	3865	3014	9.6050320	0000	8613	3741	9351	2620	3075	2507
46	6R76	3000	3190	29117	9.6221351	2727	9-6381969	2016	6581	2506 1 2503
17	9895	3007	6067	2966	4088	2736	4585	2614	8084	2503
48	9.5882802	3004	9928	2863	6824	2733	7199	2613	9.6540586	2500
112	5890	3001	9 6061786	2961	9557	2730	9813	2610	3086	2498
50	R997	3000	4647	2359	9.6232297	2720	9.6392422	2608	5584	2497
(5)	9.5891897	2990	7500	2956	5016	2727	5030	2607	8081	2494
10	4892	2998	3.0040305	2854	0.694040	2725	0.640094	2604	90050575	2493
1	19-8900990	2992	6068	2852	3 0540409	2722	904	2603	5550	2491
5.5	3861	5988	8918	2950	5911	2721	544	2601	8048	2489
56	6856	2987	9-6081766	2547	8629	2718	804	2599	9.6560536	2488
5	9841	2988	4611	2840	9.6251346	2717	9.6410640	2590	3021	2485
58	9.5912923	3000	7454	9940	4060	2710	323	250	5508	2484 2482
5	5803	297	9.6090294	3830	6772	2711	5828	259	7987	2481
10	8780	3:11	3133	23.7	948	11.00	8420	3.00	9.6570468	2451
1	670	aiff	1 600	arff.	650	arff	A 64°	laif.	5496 8004 9-6520521 5545 9059 9-6530565 8084 9-6540566 8081 9-6550577 9-6560537 9-6560537 9-6560537 9-6560537	diff.
L					LOG. CO	SINE				

7	able II.]				LOG. T	AN.				10)3
7	3 50	diff.	230	di∬.	210	diff.	25° 9·6696725 9·669023 3319 6613 9906 9 6703197 6486 9774 9·6713060 6345	diff.	260	diff.	7
0	9·6064096 7732	3636	9.6278519	3512	9.6485831	3399	0.6600022	3298	9.6881818	3205	6U
2	9.6071366	3634	554()	3509	9.6492628	3398	3319	3296	8227	3204	58
3	4997	3631	9048	3508	6023	3395	6613	3294	9.6891430	3203	57
4	8627	3627	9 6292553	3504	9417	3399	9906	3293	4631	3∻01. 3200	56
	9.6082254	3626	6057	3501	9.6502909	3390	9 6703157	3239	7831	3199	55
6	5880	3623	9:6303058	3500	0199	3388	0480	3288	9 0901030	3196	54
8	9-6093124	3621	6556	3498	9.6612974	3387	9.6713060	3286	7422	3196	50
ğ	6742	3618	9·6303058 6556 9·6310062 3545	3496	6359	3385	6345	3285	9.6910616	3194 3193	51
10	9.6100359	3017	3545	3493	9742	3303	9629	3403	3809	3193	50
11	3973	3614	7037	3492	9.6523123	3381	9.6722910	3282	7000	3191	49
12	7586	3013	9.6320527	3490	6503	3370	6190	3250	9.6920189	3139	49
	9.6111196	3608	4015	3486	9981	3376	9468	3277	3378	3197	47
14 15	4804 8409	3605	7501	3484	9'0533257	3374	9.6732745	3275	0565	3185	46
15 16	9·6122013	3604	3 0330985 AAGQ	3483	9-6540004	3373	0020	3274	0.6055051	3184	45: 44!
17	5615	3602	7948	3480	3375	3371	9.6742566	3272	6117	3183	43
110	9214	3500	9.6341426	3478	6744	3369	5836	3270	9298	3181	42
19	9.6132812	3505	4903	3475	9.6550112	3362	9105	3209	9.6942478	3170	41
121	6407	2502	8378	2470	3477	2264	6345 9628 9-6722910 9468 9-6732745 6020 9294 9-6742566 5336 9105 9-6752372 5638 9-903 9-6762165 5426 5426 9-6771644 5201 5201 9-6781709 4961 9-211	2000	5656	0170	40
21	9.6140000	3593	9.6351850	3412	6841	3304	5638	3200	8833	3177	39
22	3591	3539	5321	3469	9.6560204	3360	8903	3262	9.6952009	3174	38
23	7180	3586	8790	3467	3564	3359	9.6762165	3261	5193	3172	37
24 25	9·6150766 4351	3585	9.0302257	3465	0.6570220	3357	9696	3260	0.6061597	3172	36 35
26	7934	3583	0122	3463	3636	3356	9.6771644	3258	4607	3170	34
	9.6161514	3580	9.6372646	3461	6989	3353	5201	3257	7865	3168	33
28	5093	3579	6106	3460	9.6580341	3352	8456	3255	9.6971032	3167	32
29	8669	3574	9563	3457	3692	23201	9.6781709	3253	4198	3100	31
30	9.6172243	2570	9.6393019	2454	7041	2246	4961	2050	7363 9·6980526	3100	30
31	5815	3570	6473	3459	9.6590387	3340	8211	3250	9.6980526	3163	29
32	9385	3568	9925	3450	3733	3343	9.6791460	3248	3687	3160	28
33 34	9.6182953	3566	9.6393375	3448	7076	3342	4708	3245	0.600000	3159	27
34 35	9·6190083	3564	0.6400260	3446	3758	3340	9.6801198	3245	3164	3158	251
36	3645	3562	3714	3445	7097	3339	4440	3242	6320	3156	24
37	7205	3560	7156	3442	9.6610434	3337	7682	3242	9474	3154	23
	9.6200762	3556	9.6410597	3430	3769	3334	9.6810921	3239	9.7002628	3152	22
39	4318	3554	4036	3437	7103	3331	4160	3236	5780	3150	21
40	7872	3451	7473	3435	9.6620434	3331	7396	3236	8930	3150	20
41 42	9.6211423	3550	9.6420908	3434	3765	3328	9.6820632	3233	9.7012080	3147	19
12	4973	3547	4342	3431	7093	3327	3805	3233	5227	3147	191
43 44 45	9· 622 2066	3546	0.6431203	3430	3 0030420 374K	3325	9·6781709 4961 9211 9·6791460 4708 7953 9·6801198 4440 7682 9·6810921 4160 7396 9·6820632 3865 7098 9·6830328 3557 6785 9·6840011 3236 6459 9681 9·6852901 6120	3230	5227 8374 9·7021519 4663	3145	16
45	5609	3543	4631	3428	7069	3324	3557	3229	4663	3144 3142	15
46	9150	3541	8057	3426	9.6640391	3322	6785	3228	7805 9·7030946	3142	
47	9 6232690	3537	9.6441491	3422	3711	3310	9.6840011	3225	9.7030946	3141	13
48	6227	3536	4903	3421	7030	3316	3236	3223	4086	3139	
49	9763	3533	8324	3419	9.0050346	3316	6459	3222	7225	3137	11
50	9.6243296	3531	9.6451743	3417	3662	3313	9681	3220	9.7040362	3135	10
51 52	6827 9· 62503 56	3529	5160 0575	3415	0975	3313	g 6852901	3219	3497	3135	9
52 53	3884	3528	9-6461999	3413	3599	3310	0338	3218	9765	3133	7
53 54	7409	3525	5400	3412	6907	3309	9.6862553	3215	9.7052897	3132	6
55	9.6260932	3523	8810	3410	9.6670214	3307	5768	3215	6027	3130	5
56	4454	3510	9.6472217	3407	3519	3304	8981	3213	9156	3129 3128	4
57 58	7973	3519	5624	3404	6823	3303	9.6872192	3210	9.7062284	3126	3
58	9-6271491	3515	9028	3403	9.6680126	3300	5402	3209	5410	3125 3124	2
59 60	5006 8519	3513	9·6451743 5160 8575 9·6461988 5400 8810 9·6472217 5624 9028 9·6482431 5831	3400	6792	3299	9·6852901 6120 9338 9·6862553 5768 8981 9·6872192 8611 9·6881818	3207	0.70716E0	3124	10
Γ,	670	diff.	660	diff.	650	diff	640	diff.	630	diff.	
Į	. •.	· <i>y</i> ·	, 00	· ~	LOG. CO	-		·		· (L	١ إ
<u> </u>					200.00						1

10)4				LOG. SI	re			T.	ble n.
		2: A.	000	1: a.	290		30°	2:4.		
0	9:6570465	aij.	28° 9·671 609 3 846F 9·6720841	aij.	9.6855712	diff.	IQ-6020700	diff.	0.7119303	diff.
ĭ	2940	2478	9.6720841 3215 5583	2375 2373	7991	2279 2276	9·6989700 9·6991987 4073 6258 9441 9·7000622 2802 4981 7158 9334 9·7011504	2187	9.7120495	2102 50 2101 59
	E423	2475	9 6720841	2372	9.6860267	2275	4073	2185	2596	2099 58
3	9.6580371	2473	5583	2370	4816	2274	8441	2183	6792	2097 56
6	2812	2471	7952	2369	7688	2272	9.7000622	2181	8889	2097 55 2094 55
6	5312	2468	9 6730319	2365	9359	2269	2802	2179	9.7130983	2094 54
1 %	773 9·6590246	2466	2084 5047	2 363	3802	2267	7150	2177	5160	2092 52
9	2710	2464	7409	2362	6161	2266	9334	2176	7260	2091 51
10	1173	2403	9769	2300	8425	2204	9.7011508	21/4	9349	2089 50
11	7633	2460	9.6742128	2359	9 6880688	2203	3681	21/3	9.7141437	2087 49
12	9.6600093	2457	4485	2355	2949	2260	5852	2170	3524	2085 48
13 14	2550 E005	2455	9194	2354	7467	2258	9.7020190	2168	7693	2084
15	7459	2454	9.6751546	2352	9723	2256	2357	2167	9776	2083 45
16	9911 9 ·66123 61	2450	3896	2349	9.6891678	2254	4523	2104	9.7151857	2080 44
17	9.6612361	2449	6245	2347	4232	2252	6687	2162	3937	2078
18 19	7257	2447	4592 9-6760927	2345	1.484 9794	2250	9334 9:7011508: 3681: 5852: 6022: 9:7020190: 4523: 6687; 8849: 9:7031011: 3170: 5329: 7486: 9:641: 9:7041795: 3947: 6099: 8248: 9:7050397: 2543: 4689: 6833: 8976: 9:7061116:	2162	8002	2077 41
20	0.05	2445	3201	2344	0.60000003	2249	3170	2159	0.7160160	2076
21	9.6622145	2443	5623	2342	3231	2248	5329	2159	2243	2075 39
22	4586	2441	7963	2340	5476	2245	7486	2157	4316	2071 38
23 24	7026	2438	9.6770302	2332	7721	2243	9641	2154	6387	2071 37
25	0.6621000	2436	4075	2335	9904 0-601990#	2241	9.1041190	2152	0.7170596	2068
26	4335	2435	7309	2334	4445	2240	6099	2152	2594	2068 34
27	6718	2433	9642	2333	6683	2238	8248	2149	4610	2000 33
28	9199	2429	9.6781972	2329	8919	2236	9.7050397	2146	6725	$2064 \frac{32}{31}$
29	9.6641628	2428	4301	2328	9.6921155	2233	2543	2146	8789	2062 31
30	4056	2426	6629	2326	3358	2232	6022	2144	9.7180851	2061 30
32	890 :	2424	9.6791279	2324	7851	2231	8975 9·7061116	2142	4971	2059 28
33	9.6651329	2423	3602	2323	9.6930080	2229	9.7061116	2141	7030	$2059 _{27}^{20}$
34	3749	2419	2023	4.341	5,5(18)	2220	3256	2170	OCOG	2000
35	6168	2418	0.6000560	2317	4534	2224	7531	2137	9.7191142	2054 24
37	9.6661001	2415	2877	2317	8981	2223	9667	2136	5249	2053 23 2051 23
38	3415	2414	5191	2314	9.6941203	2222	9.7071801	2134	7300	2050 22
:39	5828	2410	7504	2312	3423	2219	3933	2131	9350	2049 21
40	8238	2409	4301 6629 8955 9-6791279 3602 5923 8243 9-6800560 2877 5191 7504 9816 9-6812126 4434 6741 9046 9-6821349	2310	5642	2217	6064	2130	9.7201399	2048 20
41	9.0070047	2407	9.0212126	2308	7859 4-60404-0	2215	9.7020322	3129	5447	2046 19
43	5459	2405	6741	2307	2289	2214	2450	2127	7538	2045 17
44	7863	2404	4434 6741 9046 9:6821349	2305	4501	2213	4575	2126	9581	2043 2042 16
45	9.6680265	2400	9.6821349	2302	6712	2210	6699	2123	9.7211623	2041 15
46 47	E064	2399	5952	2301	9-6961130	2208	9.7090943	2121	5004 5704	2040 13
48	7461	2397	8250	2298	3336	2206	3063	2120	7742	2038 12
49	9856	2394	9:6830548 2843	2295	5541	2204	5394 7531 9667 9·7071801 3933 6064 8194 9·7080323 2450 4575 6699 8822 9·7090943 3063 5182 7299 9415 9·7101529 3642 5753 7863 9972	2117	9779	203711
50	9.6692250	2392	2843	2204	7745	2202	7299	2116	9.7221814	2034
51	4642	2390	5137	2293	9947	2201	9415	2114	3848	2033
52	9420	2388	5137 7430 9720 9-6842010 4297	2290	9 0972148 4347	2199	3649	2113	7012	2034 2033 2032 2030
54	9.6701907	2387	9.6842010	2290	6545	2198	5753	2111	9943	2030 2029
55	4192	2394	4297	2286	R741	2195	7863	2100	9.7231972	2029
56	6576	2382	6583	2285	9:6980936	2193	9972	2108	4000 6026	2026
58	9.6711338	2390	9.6851151	2283	5321	2192	4186	2106	8051	2026 2026 2025 2024
59	3716	2378	3432	12281	7511	2190	7863 9972 9·7112080 4186 6290 8393	2104	9026 8051 9 7240075	2024
60	6093	2:0	5712	2200	9700	diff.	8393	2103	2097	
ľ	62°	diff.	610	diff	1 600	diff.	59°	diff.	58 °	diff.
					LOG. COS	INE.				

	Table II.												
1	270	diff.	280	diff.	290	diff	300	\diff.	310	diff.	1		
6	9.7071659	3122	9'7256744	3047	9.7437520	2979	9.7614394	2917	9.7787737	2862	60		
	7000	3121	9791	3046	9 7440499	2977	0-7590902	2916	9.7790599	2860	59		
2	9-7081022	3120	6891	3044	6453	2977	3149	2915	6319	2859	57		
l d	4141	3119	8925	3044	9428	2975	6056	2914	9177	2859	56		
5	7258	3116	9.7271967	2042	9.7452403	29/0	8969	2913	9.7802034	2357	55		
6	9.7090374	3114	6008	3040	5376	2973	9-7631891	2911	4891	2856	54		
7	3488	3113	8048	3039	8349	2971	4792	2910	7747	2855	53		
0	9713	3112	9.7281097	3037	19 7461320	2970	0-7640619	2910	3.4810005	2854	51		
10	0.7102024	3111	71.49	3037	4490	2969	2500	2908	2436	2853	01		
110	5 /102824 5922	3109	0.7900106	3035	9-7470997	2968	5820 6497	2907	0149	2853	40		
12	9041	3108	3230	3034	3194	2967	9334	2907	9-7822013	2851	48		
13	9-7112148	3107	6263	3033	6160	2906	9.7652239	2905	4864	2861	47		
14	5254	3104	9295	3033	9125	2064	5143	2904	7713	2040	46		
15	8358	3103	9.7302325	3029	9.7482089	2963	8047	2902	9.7830562	284R	45		
16	9.7121461	3101	5364	3029	5052	2961	9.7660949	2902	3410	2948	44		
19	7669	3100	0-7311410	3027	0.7400074	2961	6751	2900	6258	2846	43		
19	9.7130761	3099	4436	3026	3934	2960	9651	29(10)	9.7841949	2845	41		
30	2050	3098	7400	3024	5000	2958	0.7679550	2899	4204	2845	40		
21	6956	3097	9-7320494	3024	0980	2958	544R	3898	7639	2844	30		
22	9.7140051	3095	3506	3022	9.7502806	2956	8344	2896	9.7850481	2843	38		
23	3145	3000	6527	3030	5762	2064	9.7681240	2690	3323	2642	37		
24	6237	3092	9547	3010	8716	2952	4135	2894	6164	2940	36		
25	9329	3090	9.7332566	3018	9.7511669	2953	7029	2893	9004	2840	35		
20	97152419	3089	5584	3017	4622	2961	9922	2892	9'7861844	2835	34		
199	9506	3087	9-7241616	3015	0.7590592	2950	5705	2891	7820	2838	35		
29	9.7161682	3087	4631	3015	3472	2949	8596	2891	9.7870357	2837	31		
30	4767	3085	7064	3013	E490	4948	0.7701405	2889	2105	2836	20		
31	7851	3084	9:7350656	3012	9368	2948	4373	2888	5193) 6098	2839	29		
32	9.7170933	3082	3667	3011	9.7532314	2946	7261	2000	8863	2835	28		
33	4014	3081	6677	3000	5259	2945	9.7710147	2006	9-7581696	2533	27		
34	7094	3079	9695	3008	8203	2943	3033	2884	4529	2832	26		
35	97160173	3078	9'7362693	3006	9.7541146	2942	5917	2384	7361	2831	25		
37	6327	3076	9705	3006	7020	2941	0-7791694	2883	9.4890192	2831	24		
38	9402	3075	9.7371709	3004	9960	2940	4566	2882	8852	2929	22		
39	9-7192476	3074	4712	3003	9.7552908	2020	7447	2681	8681	2929	21		
40	5549	3013	7714	3002	5946	4938	9.7730327	2000	9.7901500	4821	20		
41	8620	3071	9.7380715	3001	8783	2937	3206	2879	4335	2827	19		
42	9.7201690	3070	3714	2999	9.7561718	4935 2025	6084	25/6	7461	2826	18		
43	4759	3068	6713	2997	4653	2934	8961	2877	9987	2824	17		
44	7827	3066	9710	2997	7587	2033	9.7741838	2875	9-7912811	2824	16		
46	3080	3065	91/392707	2995	97570520	2932	4713	2875	5635	2823	15		
47	7022	3064	9698	2994	6282	2931	9.7750469	2874	0.7021220	2822	13		
18	9.7220085	3063	9.7401689	2993	9313	2930	3334	2872	4101	2621	12		
49	3147	3062	4681	2992	9.7582242	2020	6206	2872	6921	2820	iil		
50	6207	2000	7672	4991	5170	2000	9077	4011	9741	2820	10		
51	9266	3059	9.7410662	2990	8096	20146	9.7761947	2870	9.7932560	2819	9		
52	97232324	3057	3650	2000	9-7591022	2026	4816	2860	5378	2017	8		
53	5391	3055	6639	2986	3947	2924	7685	2867	8195	2816	7		
54	8436	3054	9624	2985	6971	2923	9.7770552	2866	9.7941011	2616	6		
50	4540	3053	97/432009	2985	9794	2922	3418	2866	3827	2814	5		
57	7505	3052	0577	2983	ガ / DUZ/ Ib 数約2つ	2921	0140	2865	0455	2814	3		
158	9.7250646	3051	9.7431559	2982	8567	2920	9.7782012	2863	9.795226B	2813	2		
59	3695	3049	4540	2981	9-7611476	2010	4875	2863	5081	2813	i		
60	6744	3049	7520,	C200	4394	-310	7737	COD2	7892	2011	0		
1	620	diff.	610	diff.	600	diff.	1 590	diff	580	diff.	1		
1					LOG. CO	TAN.							

N

10)6				LOG. SI	NE.			[76] 36° 9.7692187 3925 5662 7398 9134 9.7700868 4702 9.7711249 4702 6426 8150 9872 9.7721593 3314 5033 6751 1900 3614 5327 7039 2168 3876 5583 7288 8993 17501 7501 9.7750697 2399 4101 7501 9199 9-7760897 2399 4101 7501 9199 9-7760897 2399 4101 7501 9199 9-7770897 2399 4101 7501 9199 9-7780897 2399 4101 7501 9199 9-7780897 2399 4101 7501 9199 9-7780897 2399 4101 7501 9199 9-7780897 2399 4101 7501 9199 9-7780897 2399 4101 7501 9199 9-7780897 2399 4101 7501 9199 9-7780897 2399 4101 7501 9896 997771060 977815697 9869 9-7771060	ble 11.
7	32	diff.	330	diff.	34	diff.	350	diff.	360	diff.
0	3.7242097	2021	9:7361088	1044	9.7475617	1972	9.7585913	1804	9.7692187	1739 60
1	4118	2020	3032	1944	7489	1871	7717	1802	3925	1737 59
2	0156	2013	4970 6010	1942	9,500 0:7.101:290	1870	9519	1802	7999	1736 55
4	9.7250174	2018	8959	1941	3099	1869	3121	1800	9134	1736 56
5	2189	2015	9.7370799	1940	4967	1868	4920	1799	9.7700868	1734 58
6	4204	2012	2737	1838	6833	1865	6718	1797	2601	1731 54
7	6217	2012	4675	1936	8698	1864	R515	1796	4332	1731 53
20	0.7960940	2011	6546	1935	2490562	1863	2106	1795	7793	1730 50
10	0040	\$000	0.7300420	1933	4000	1862	2000	1793	0500	1729
III	A257	5008	2412	1933	6149	1861	5899 5899	1793	9:7711249	1727 40
12	6264	2007	4343	1931	8007	1959	7493	1791	2976	1727 49
13	8269	2005	6273	1930	9866	1857	9274	1789	4702	1794 47
14	9-7270273	2003	8201	1928	9.7501723	1856	9.7611063	1788	6426	1794 46
1.5	2276	2002	9.7390129	1926	3579	1855	2851	1787	8150	1722 45
17	6979	3000	3080	1925	7997	1853	6424	1796	9-7721593	1721 43
18	8277	1999	5904	1924	9140	1853	8208	1784	3314	1721 42
19	0.7280275	1996	7827	1021	9.7510991	1851	9992	1783	5033	1719 41
20	2271	1000	9748	1000	2842	1040	9.7621775	1791	6751	1717 40
21	4267	1993	9.7401668	1940	4691	1847	3556	1781	8468	1717 35
27	6260	1993	3587	1918	6538	1847	5337	1779	9.7730185	1715 35
24	0-7900944	1991	7421	1916	0-7290921	1946	7110	1778	1900	1714 31
25	2234	1990	9337	1916	2075	1844	9-7630671	1777	5327	1713 35
26	4223	1989	9.7411251	1914	3919	1844	2447	1776	7039	1712 34
27	6211	1086	3164	1913	.5761	1941	4222	1774	8749	1710 33
28	6197	1985	5075	1911	7602	1840	5996	1773	9-7740459	1709 32
39	97300182	1983	6960	1909	9442	1838	7769	1771	2168	1709 31
30	2165	1983	8895	1908	9.7531280	1838	9540	1771	3876	1707 30
35	6198	1981	9710	1907	4954	1836	3080	1769	7988	1705 29
33	8100	1980	4616	1906	6790	1836	4849	1769	8993	1705
34	9.7310097	1978	6520	1304	8624	1539	6616	1766	9.7750697	1704 26
35	2064	1976	8423	1902	9.7540457	1931	8362	1765	2399	1702 25
30	4040	1975	91430325	1901	2286	1531	9*7669147	1764	4101	1700 29
39	7999	1974	4126	1900	5949	1830	3674	1763	7501	1700 22
39	9961	1972	6024	1998	7777	1828	5436	1762	9199	1698 21
40	9.7321932	19/1	7921	1004	9604	1000	7197	1401	9-7760897	1098
41	3902	1970	9817	1996	9.7551431	1827	8957	1760	2593	1606 19
42	5870	1967	9.7441712	1894	3256	1924	9.7660715	1758	4289	1694 18
43	7837	1966	3606	1892	5080	1822	2473	1756	5963	1693
45	9-7331769	1965	7390	1992	8724	1822	5995	1756	9360	1693 16
46	3731	1963	9230	1990	9.7560544	1920	7739	1754	9.7771060	1691 14
47	5693	1964	9.7451169	1887	2364	1819	9492	1759	2750	1680 13
48	7654	1960	3056	1887	4182	1817	9.7671244	1752	4439	1689 12
143	9614	1958	1943	1885	5999	1616	2996	1750	6128	1687
50	97341572	1957	6828	1884	7315	1915	4746	1748	7815	1686 2
59	5029	1956	9-7460505	1883	9.7571444	1814	PGP49	1748	9:7781196	1685
53	7440	1955	2477	1892	3256	1812	9989	1747	2870	1684 7
54	9393	1953	4359	1870	5068	1812	9.7681735	1746	4553	1683 6
55	9.7351345	1951	6237	1878	6878	1909	3480	1743	6235	1681 5
57	3296	1980	8115	1977	0.7500.405	1908	5223	1743	7916	1680 4
58	7195	1949	9-7471868	1876	2302	1807	8707	1441	9.7791275	1679 3
59	9142	1947	3743	1978	4108	1806	9.7690448	1741	2953	1679 1
50	9.7361088	1946	5617	1014	5913	1605	2197	7128	4630	16/7 0
1	570	diff.	560	diff.	550	diff.	542	diff	530	diff.
_					LOG. COS	SINE.)c .		

7	320 9.7957892 9.7957892 9.7957892 9.7957892 9.7957892 9.79571938 4745 9.7951569 4370 7176 9.7991569 4370 7176 9.8002769 9.80111611 3957 8365 9.8012340 9.802340 9.802340 9.802340 9.802340 9.802340 9.802340 9.802340 9.802340 9.8030716 6296 9.8030716 3506 6296 9.8041873 4651 7447 9.8050233 3506 6296 9.801133 9.8052 9.8061370 4152 9.80629 9.8066 9.8072494 9.807249 9.807249 9.807249 9.807249 9.807249 9.807249 9.807249 9.807249 9.807249 9.807249 9.807249 9.8				LOG.	TAN				1	07
1	320	diff.	330	diff.	340	diff.	35°	diff.	360	diff.	1
0	9.7957892	2811	9.8125174	2765	9.9289874	2726	9.8452268	2688	9-8612610	2667	60
1	9.7960703	2810	7939	2765	9 8292599	2724	4956	2688	5267	2656	59
2	6333	2809	3469	2764	9047	2724	0.0460399	2689	0.0000570	2655	57
3	9130	2808	6231	2763	9.8300769	2722	3018	26B6	3033	2655	56
6	9-7971938	2808	8993	2762	3492	2723	5705	2687	5887	2654	55
Б	4745	2001 9006	9.8141755	2702	6213	2721	8390	2000	8541	2054	54
7	7551	2805	4516	2761	8934	2726	9-8471075	2696	9.8631195	2653	53
6	9.7980356	2804	7277	2759	9 831 1654	2720	3760	2684	3848	2652	52
13	3160	2804	9.9190030	2759	4374	2719	6444	2683	6500	2052	al
Jio	5964	2803	2795	2759	7093	2716	9127	2683	9152	2651	50
11	B/0/	2802	0559	2757	0.0200500	2718	9.8481510	2682	9'8041603	2651	49
15	4370	2801	9-9161069	2757	6946 6946	2717	7174	2682	7105	2651	47
14	7176	2800	3824	2756	7963	2717	9852	2681	9755	2650	146
15	9970	2500	6580	2756	9.8330679	2716	1.6492530	2651	9.8652404	2041	45
16	9.8002769	2700	9335	2755	3394	9715	5210	2080	5053	2045	44
17	6567	2798	9.8172089	2753	610.	2714	789t	2679	7702	2648	43
18	8365	2796	4842	2753	F825	2713	9.8500575	2679	9.8660350	2647	42
19	a.portitor	2796	7595	2752	9.8341536	2713	3253	2678	2997	2647	41
20	3957	2795	9.8180347	2751	4249	2712	5931	2677	5644	2647	40
21	6762	2794	3098	2751	6961	2712	86.06	2677	H291	2646	39
37	0-202240	2794	8549	2750	0.0050000	2711	9.00 (1260	2676	9,9010931	2646	27
24	5133	2793	9-8191349	2749	10025500 E	2710	6637	2676	699 _e	2645	.6
25	7925	2792	4096	2748	7804	271	9312	2675	887:	2645	35
26	9.8030716	2791	6944	2748	9-8360513	2700	9.8521987	2670	9.8681517	2044	34
27	3506	2700	9592	2746	3221	2702	4661	2074 9674	4160	2042	33
28	6296	2789	9.8202338	2748	5929	2707	7335	2673	6804	2642	32
29	9085	2788	5084	2745	8636	2707)-853000€	2672	9446	2643	31
30	9.8041873	2790	7829	9745	9-8371343	2706	2680	2672	9.8692089	9649	30
31	4661	2786	9.8210574	2743	4049	2706	5351	2671	4731	2641	29
32	7447	2786	3317	2743	6755	2705	BUZ3	2671	7372	2641	28
24	2016	2786	0003	2743	3-0207164	2704	1,5940,034	2671	9.8100013	2640	26
35	5903	2784	9.8221545	2742	4867	2703	6034	5668	5293	2640	25
36	8587	2784)	4286	2741	7571	2704	8704	2670	7933	2640	24
37	9.8061370	2783	7026	2740	9.8390273	2702	3.8551372	2008	9.8710572	26.35	23
38	4152	2791	9766	9730	2975	2701	4041	2667	3210	2638	22
39	6933	2781	9.8232505	2739	5676	2701	6708	266B	6848	2638	21
40	9714	2790	5244	2777	8377	2700	9376	2686	8486	1622	20
41	9.8072494	2779	7981	273B	9 8401077	2699	9.8562042	2666	9.8721123	2637	19
12	6273	2779	9'8240719	2736	377(2699	4708	2666	3760	3631	18
44	8-2020200	2777	6101	2736	0475	2699	7.9570020	2665	00396	2630	16
45	3606	2777	8926	2735	9.8411871	2697	2704	2665	9-8731666	363€	15
46	6383	2777	9.8251660	2734	4569	2698	5368	2664	4302	2634	14
47	9158	2775	4394	9799	7265	2090	8031	2003	6937	2624	13
48	9.8091933	2774	7127	2722	9961	2696	9.8580694	2663	9571	5555	12
43	4707	2773	9860	2732	9.8422657	2694	3357	2662	9.6742204	2634	11
50	7480	2772	9.8262592	2721	5351	2/105	6019	2661	4838	5635	10
51	9.8100253	2772	5323	2730	8046	2693	8680	2661	7470	2632	9
152	. 3025	2771	8053	2730	9'8430739	2693	9'8591341	2661	919750102	2632	ä
5.4	5796 9566	2770	9.8270763	2730	6195	2693	4002 ecc1	2659	2734	2631	A
55	9-8111336	2770	5013 6941	2728	9R17	2692	9321	2660	7906	2631	5
66	4105	2769	8969	2728	9.844150R	2691	9.8601980	2659	9.8760627	2631	4
57	6873	2768	9.8281696	2727	4199	2691	4638	2058	3257	2630	3
58	9641	9767	4423	2796	6889	2600	7296	2659	5886	2620	2
59	9-8122408	2766	7149	2725	9579	2689	9954	2656	851F	2629	1
OU	5174	3.5	9874	1:0	9 3452268	25 15	9'8612610	2:0	9'8771144	2:0	U
	2.10	arg.	1 260	ary.	550	ary.	1 540	arg.	220	diff.	-
_					LOG. CO	CAN.					

108					LOG. SI	NE.			-	ible 1
1	370	diff.	380	diff.	390	diff.	40°	diff.	410	diff:
	7794630	1676	9·7893420	1616	9·7988718 9·7990278	1560	9-8080676	1 che	9.8169429	1453
1	6306 7981	1675	0000	11616	a spenaro					1452
2	9665	1674	6652 8266	1614	1836 3394	1558	3004	1504	2334	1451
3 4 9		1673	8266	1614				1502		1450
5 9	7801328	1672	9880 9:7901493 3104	1613	4951	1556	0090	1502	0430	1450
	3000 4671	1671	97901493	1611	6507	1555	8192	1500	5555	1448
6	6341	1670	3104			1554	9692	1500	8133	1448
B	8010	1669	4715 6325	1610	9616 9-8001169 9721	1553	9.8091192	1499	9581 9:8181028 2474	1447
9	9677	1667	7933	1608	9 5001109	1552	6031	1498	9.9191078	1446
1	2011	1671 1670 1669 1667 1667	1933			1561		1457		1445
			9541	1607	4272 5823 7372 8921	1551	9000	1496	3919	1445
1	3010	1665	9.7911148	1606	5823	1551 1549	7192	1496	5364	1443
2	4019	1664	2754	1605	7372	1549	8678	1494	6807	1443
3	0.337	1663	4359	1604	5823 7372 8921 9-9010468 2015	1547	9-8100172	1494	8250	1442
4						1547	divers	1493	9692	1441
5	9664	1660	7566	1602	2015 3561 5106 6649 6192	1546 1545 1543	3159	1491	9692 98191133 2573	1440
	7821324	1660	9105	1601	3501	1545	4650	1491	2573 4012 5450 6988	1439
7	2984 4643	1659	9.1920169	1600	5106	1543	6141	1490	4012	1438
B	6301	1668	2309	1599	0049	1543	7631	1490	5450	1438
9		1657	3968	1598	6192	1543	9121	1488		1437
100	7958	1656	5566	1507	9735	1541	9'8110609	1487	8325	1436
21	9614	1654		1597	0 0041410	1540	2096	1427	9761	1435
3 9.	7831268	1654	8760	1595	46,10	1520	9009	1486	9.8201196	1434
131	2922	1.0000	9.7930355	1004	4355	1520	BNOS	1485	2030	1433
14			1949	1504	5894	1527	6554	1494	4063	1433
16	6227	1652 1651 1650 1649	3543	1502	7431	1527	8038	1484 1483 1482	5496	1.491
6	7878	1650	5135	1600	8968	1596	9521	1499	6927	1431
7	9528	1649	6727	1500	9.8030504	1524	9.8121003	1481	00000	1430
	7841177	1647	8317	1500	2038	1504	2484	1491	9786	1429
29	2824	1647	8317 9907	1520	7431 8968 9·8030504 2038 3572	1522	6554 8038 9521 9-8121003 2484 3965	1470	9788 9-8211217	1429
10	4471	LOW	9·7941496 3083 4670	1000	5105	1000				
31	6117	1646	3083	1587	6637	1532	6923	1479	9·8221198 2621 4042 5463 6883	1427
12	7762	1645	4670	1587	8168	1531	9401	1478	6600	1427
33	7762 9406	1644	6256	1586	9699	1531	9878	1477	6926	1426
49	7851049	1043	7841	15%	9699 9-8041228 2757 4264 5811 7336	1529	9.8131354	1470	8351	1425
35	2691	1042	9425	L51:4	2757	1529	2829	1476	9775	1424
G.	4332	1041	9.7951008	1583	4284	1527	4303	14/4	9.8221198	1423
17	5972	1640	2590	1582	5811	1527	5777	14/4	2621	1423
B	7611	16398	4171	1981	7336	1525	7250	1473	4042	1421
9	9249	E CO CONTR	5751	F datises.	8861	1525	8721	1971	5463	1421
09	7860886	1637	9000	1579	A AA-DUA-	TO 24.3	0.0140100	Take	6000	1420
	OFFICE	1636	8909	1579	9·8050386 1906 3430 4961 6472 7991	1523				
1		1635	9.7960486	1577	2420	1522	2121	1469	B302	1419
3	5791	1634	2 1200450	1576	4051	1521	4600	1469	0-0991190	1417
4	7424	1633	9·7960486 2062 3638 5212	1576	647 1	1521	6062	1467	9555	1417
5	9066	1632	5212	1574	7001	1519	7524	1467	2300	1416
			6796	1574	7991 9510	1519	0000	1465	29/1	1415
7	2317	1631 1630 1629	0360	1573	9510 9:8061027 2544 4060 5575 7089 8602 9:8070114 1626 3136	1517	9-9150464	1465	8302 9721 9-8231138 2555 3971 6386 6800 8213 9626	1414
R	3946	1629	0020	1571	2544	1517	1099	1464	9919	1413
19	5574	1628	9.7971501	1571	4060	1516	3391	1463	9696	1413
-	6000	1628	2 13/1001	1570	4000	1515	4074	1463	30.40	1411
0	7202	1626 1625 1624	3071 4640	1569	5575	1514	4854	1461	9·6241037 2448 3658 5267	14(1)
1	5828	1625	4640	1568	7089	1513	6315	1461	2448	1410
	788(453	1624	6208	1567	8602	1512	7776	1459	3858	1409
3	2011	1624	7775	1566	9.8070114	1512	9235	1459	5267	1409
4	3701	1699	9341	1565	1626	1510	9.8160694	1458	6676	1407
5	5323	1621	9:7980906 2470 4034	1564	3136	1510	2152	1457	8083	1407
6	6944	1621	2470	1564	4646	1508	3609	1457	9490	1406
7					6154	1508	5066	1455	9.8250896	1405
8 3.	7890184	1618	5596	LECT	7662	1507	6521	1454	2301	1404
9	1802	1618 1618	7158	1560	9169	1506	7975	1454	3658 5267 6676 8083 9490 9-8250896 2301 3705 5109	1404
U	19:3100			diff.	9 8080675	1.00	9429 49°	1.30	6109	44.5
		diff.	510	A 18	500	diff.	4000		489	diff.

T	able 11.]		\$8° 9-8926098 9-8930702 3306 5909 8511 9-8941114 3715 6317 8918 9-89515199 9-8961918 4517 7116 9-8961918 4517 7507 9-8960104 2700 5296 5296 67667 9-9000665 3459 9-9011237 3830 6422 9-9903487 36766 9-9011237 3830 6422 9-9031966 41945 6766 9-9031966 4555 7144 9733 9-9021604 41945 6766 9-9031966 4555 6766 9-9031966 4555 6766 9-9031966		LOG. TA	N.				10	9
1	370	diff.	380	diff.	39º	diff.	400	diff.	410	diff.	1
0	9.8 71144	1362F	9-8926098	2604	9.9083693	2583	9.9238135	2566	9-9391631	2551	60
1	3772	3628	9-8930702	2604	6275	2583	9.9240701	2565	4182	2551	55
2	6400	2627	3306	2603	8858	2582	3266	2565	6733	2551	55
3	9027	2627	9909	3602	9-9091440	2582	5831	2565	9284	2551	5
4	3,9191994	2627	0.0041114	3603	4022	2591	6390	2564	9.9401839	2550	50
5	4281	2626	9'8941114	2601	6003	2582	9-9250960	2564	4355	2551	512
0	0907	2626	3/15	2602	0.0101700	2581	5524	2564	6936	2550	54
l l	0.0700150	2625	0317	2601	9.9101766	2581	0088	2564	0-0410096	2550	93
0	9.012219H	2624	0.0051510	2601	4347	2580	0002	2563	9.9412030	2549	61
3	4102	2625	a.0591013	2600	0947	2580	9 9201215	2563	4000	2650	DI
10	7407	2624	4119	2600	9507	2580	3778	2563	7135	2649	50
111	8.8800031	2623	6719	2600	9.9112087	2579	6341	2563	9684	2549	45
12	2654	2623	9319	2699	4666	2579	8904	2562	9.9422233	2549	46
13	5277	2623	0.8961918	2599	7245	2579	9 927 1466	2562	4782	2549	47
14	7900	2622	4517	2599	9824	2579	4028	2562	7331	254B	46
15	9.8810522	2622	7116	2598	9.9122403	2578	6590	2562	9879	2549	4
10	3144	2621	9714	2598	4981	2578	9152	2561	9 94 32428	2548	44
17	5/05	2621	9.8972312	2598	7559	2579	9-9281713	2561	4976	2548	4
18	8386	2621	4910	2597	9.9130137	2577	4274	2561	7524	2546	4
19	9.9231007	2620	7507	2597	2714	2577	6835	2561.	9 9440072	2547	4
20	3627	9610	9.8980104	JEGE	5291	9877	9396	0240	2619	9842	40
21	6246	9690	2700	2800	7868	9576	9-9291956	9560	5166	4047	39
22	8866	9610	5296	2506	9-9140444	9576	4516	2000 5560	7714	98.47	31
23	9-8831484	2610	7892	SORE	3020	2010	7076	2560	9.9450261	9546	3
24	4103	2618	9-8990487	2505	5596	9575	9636	2550	2807	9547	30
25	6721	2617	3082	2505	8171	2576	9.9302195	2560	5354	2546	31
26	9338	2618	5677	2504	9.9150747	2575	4755	2550	7900	9547	3
27	9 8841956	2616	8271	2504	3322	2574	7314	2558	9-9460447	2546	3
28	4572	2617	9.9000665	2594	5896	2575	9872	2559	2993	2546	3:
23	7139	2616	3459	2593	8471	2574	9.9312431	2558	5539	2545	3.
30	9805	OCIE	6052	aron	9.9161045	0044	4989	OFFE	8094	-U-10	30
33	9.8852420	2615	8645	2593	3618	2673	7547	2558	9.9470630	2546	20
32	5035	2015	9.9011237	2592	6192	2574	9.9320105	2558	3175	2546	28
33	7650	2010	3830	2593	8765	25/3	2662	2557	5720	254h	2
34	9.8360264	2014	6422	2592	9.9171338	2073	5220	2555	8265	2545	26
35	2878	2014	9013	2091	3911	4013	7777	2557	9-9480810	2546	2
36	5492	4014	9.9021604	9501	6483	2012	9.9330334	4001	3355	2040	24
37	8105	9619	4195	9501	9055	9570	2890	2000	5899	0844	2
38	9 8870718	9619	6786	2001	9.9181627	2574	5446	2000	8443	2544	25
39	3330	9619	9376	2050	4198	9571	8003	2001	9.9490987	4044	2
40	5942	4014	9-9031966	~DUU	6760	4011	9-9340559	4000	3531	-1794	101
41	8554	2612	4555	2589	9340	2571	2114	2558	6075	2544	1
42	9-8881165	2611	7144	2589	9-9191911	2571	5670	2556	8619	2544	1
43	3775	2610	9733	2589	4481	2570	8225	2655	9.9501162	2543	1
44	6386	2611	9.9042321	2588	7051	2570	9.9350780	2556	3706	2543	i
45	8996	2610	4910	2589	9621	2570	3335	2556	6248	2543	i
46	9.8891605	2609	7497	2557	9-9202191	2570	5889	2554	8791	2543	1
47	4214	2009	9.9050085	2585	4760	2569	8444	4555	9.9511334	2543	i
48	6823	ZUU!	2672	2587	7329	2569	9.9360998	2554	3976	2542	
49	9432	2009	5259	2007	9898	2569	3552	2554	6419	4543	i
50	0.2002040	200H	7045	4686	0-0919466	2008	6105	2553	0001	2542	1
51	4647	2607	0.0060423	2596	2 3212400	2568	9650	2554	0.021030-0	2542	E
59	7954	2607	2012	2586	7600	2568	0-0271919	2553	4045	2542	
52	0001	2607	5609	2586	0.0220170	2568	9764	2553	6592	2542	
15.4	0.2019469	2607	01003	2585	9797	2567	0100	2553	0120	2541	1
EE	5074	2606	0.0070772	25R5	5204	2567	9971	2553	0.0521670	2542	
56	7670	2605	2957	2564	> 7971	2567	0-0301403	2552	4911	2541	
57	0-9000000	2606	5041	2584	0.0030437	2566	2075	2552	6759	2541	
50	200000	260%	11966	2584	3004	2567	6527	2552	0702	2541	1
60	5404	2604	9:0091100	2584	5570	2566	D070	2552	0.05/1109/	2541	
100	5494	2604	2603	2583	8125	2565	0.0301631	2552	4374	2540	1
60											
60	500	diff	510	diff	500	11:0	490	dia	480	13:11	1

11	0				Log. St	NE.			[7	able 11.
1	420	diff.	430	diff.	440	diff.	450	diff.	460	diff.
0	9-8255109	1403	9.8337833	1355	9-6417713	1308	0.48404850	1263	9-8569341 9-8570561	1220 60
1 2	6512 7913	1401	9188 9-8340541	1353	V-0100000	1307			1779	1410 50
3	9314		1894			13070	0657	1262	9000	1219 57
4	9.9260715	CAUL		1350	2939	1.300	none:	1400		
6	2114	1399 1398	4024	1221	9.699	1304	9:8501157	1260	5432	1216 00
6	3612	1338	0340	1349	0049	1303	2447	1258	8040	1915 99
7	45.10	1397	7297 8646	1349	6851 8154	1303		1258	1003	46 6 90
8	6307 7703	1396	0004	1348	0.456	1302	6166	1257	0.0000000	1214 51
100		1395		1347		1301	2440		1505	1214 51 1213 50
10	9098 9-8270493	1395	9.8351341 2689	1347	9·8430757 2057	1300	0709	1256	9719	1213 60
12	1887	1394	Ango	1345	9954	1299	0062	1256	2020	1211 49
13	3279	1392	5228	1345	4000	$\frac{1299}{1298}$	0.3811911	1254 1254	6141	
14	1 4671	1392 1392	01.62	1344 1344	5953	1298	2405	1252	0351	1210 30
15	6063	1390	8000	1342	7.590	1297	5/1/	1252	7561	1203 at
16	7453			1342	6547	1295	4909	1251		
17	8843. 9:8280231		9-8360750 2091	1341	9842 98441137	1295	2421	1251	0.0001106	12119 40
19	1619	1388	3431	1340	2432	1295	0701			1204 41
20		1387	4771	1340	3725	1293	0.000	1249	20000	1400
21		1397	6100	1338	0105	1293	0-0501919	1248	4004	1205 39
22		1399		1338		1292	0.486	1248 1247	coon	ZHANNE
23		1386	8784	1337	7601	1291		1246	7213	
24		1293	9-8370121	1337	8891	1290	4980	1945	19410	1203
15		1392	1456	1335	9-8450181 1470	1289	6204	1246	9619 9-8600821	COLUMN TO STATE OF THE PARTY OF
25		1392	The state of the	1 2224	4 4 4 4	1288	7449	1244	9.8600921	1201 33
27 28	2694 4075	1381	4125 5468		2758 4045	1287		1243	2000	12011
29		1915				1287	9.8531179	1243	4499	120031
30	6933	1379	O DO		2010				× ann	1199 30
31	8212	1679	8122 9463	1331		1285	2000	1241	. 6091	1199 29
32	9589	1377	o.ongonenn	1330	0100	1285	4000	1240 1240	0010	1197 28
33		1377 1376	2112	1339	9.8460471	$\frac{1283}{1283}$		1299	9215	1197 27 1197 26
34	2342	1375	2441	1290	1109	1292	1381	1239	9:8610412	1449 415
35	3717	1374		1327	3036	1929	8019	1237	1009	1195 24
36		1373	6096	1326	4318	1281	9856 9856 9·8541093 2329	1237	2903 3997	1194 23
37	6464 7837	1373		1325	5599 6879	1280	2329	1236	5190	1193 22
39		1372	9.5390072	1328	0150	1279	2564	1230	6969	1193 21
40		1911		1324	0.400	1278	4700	1499	SERVICE AND ADDRESS OF	1193 20
41	1950	1370	9210	1323	O.O. ITOTE &	1278	6033	1234	07.07	1191 19
42	3320	1370	20.41	1364	1001	1277	7966			1191 18
43	4688	$\frac{1363}{1368}$	5363	1322	3267	1276 1276	8499	1233	9.8621148	1190 17
44	6056	1367	0009	1320	41748.7	1274	9730	1231	CHARGE	118911
45	7423	1366	GUIGH	1319	6917	1274	3.0000001	1231	3540	1100114
46	9:8320165	1366	9323 9400642	1319		1274	2194	1229		1188112
48		1364	1959	1317	O.C.O.E.	1272	4040	1229	7000	1186 12
49	2883	1364	3276	1317	0.0400000	$\frac{1272}{1271}$	E070	1228 1228	0074	
50	4246	1303	8500		9190		7106	1460	9460	1100 10
51	5609	1363	5908	1315	9.(50)	$\frac{1270}{1270}$	0999	1226 1226		1184 9
52	6970	1361 1361	7223	$\frac{1315}{1314}$	4720	1270	0.000	1226	1828	1183 7
63	8331	1360	8637	1313	5989	1266	9558	1224	3011	1162
84	9691	1250	9850	1312	7757	1267	2008	1224		1182 5
55 56	9.8331050 2408	1358	9°8411162 2474	1312		1267	3232	1223	6557	1181 4
57	3766	TIBBLE	2706	1311	9-8491057	1266	EC70	1223	7737	1180 3
58	5122	1356	5005			1265	GOOD	1222	8917	1180 2
59		1350	CADA	1309	3680	1264	9191	$\frac{1221}{1220}$	9-8640096	1179
60		1355	1713	1309	4850	1264	11/3/9.1	A . 100	1275	1179 0
1	470	diff.	460	diff.		diff.	440	diff.	430	diff.
		5			LOG. COS	INE.				

7	Table 11.											
	420	diff.	430	diff.	440	diff.	450	diff.	46□	diff.	1	
0	9-9544374	2541	9 9696559	2532	9.9348372	2528	10-00000000	2527	10 015 1628	2528	60	
1	0915	2540	9091	2533	979850900	2528	2527	2526	4156	2529	59	
3	0.0551995	2540	4157	2533	5956	2528	7580	2527	9213	2528	57	
4	4535	2540	6689	2532	8484	2528	10.0010107	2527	10 0161741	2528	56	
6	7075	2540	9221	4534	9.9861012	2525	2633	2525	4270	2529	55	
6	9615	2539	9-9711754	2632	3540	2528	5160	2526	6798	25.00	54	
7	9.9562154	2540	4286	2532	6068	2528	7686	2527	9327	2529	53	
8	7032	2539	0218	2532	0.0071199	2527	9740	2527	10.017 [899	2529	54	
10	0720	2539	0.0501000	2532	2 2011179	2528	2130	2526	7010	2529	21	
110	0.0579311	2539	9.31.21888	2531	6179	2528	7703	2527	0441	2528	40	
12	4850	2539	6945	2532	8706	2527	10-0030320	2527	10:0181970	2529	48	
13	7389	2539	9477	2532	9-9881234	2528	2846	2525	4499	2529	47	
14	9927	2539	9.9732008	2531	3761	2527	5373	2027	7028	2529	46	
15	9.9582465	2539	4539	2532	6289	2527	7900	2527	9557	2529	45	
16	2547	2538	7071	2531	8516	2528	10-0040427	2526	10.0192086	2529	44	
18	0.0500080-0	2538	9.0742133	2531	2871	2527	5490 5490	2527	7144	2529	40	
19	2618	2538	4664	2531	6399	2528	8007	2527	9674	2530	41	
20	5166	4531	7105	2531	8026	2527	10-0050634	2527	10-0005903	2529	40	
21	7693	2538	9726	2531	9.9901453	2527	3060	2526	4732	2529	39	
22	9-9600230	9597	9.9752257	2531	3981	2528	5587	2527	7262	2530	38	
23	2767	2538	4787	2531	6508	2527	8114	9597	9791	25/20	37	
24	5305	2537	7318	2531	9035	2527	10 0060641	2527	10-0212321	2530	36	
25	7842	2536	9849	2530	9.9911562	2627	3168	2527	4851	2529	35	
20	9010378	2537	3.3105313	2530	6616	2527	2030	2527	9910	2530	39	
98	5452	2537	7440	2531	9143	2527	10:0070749	2527	10-0222440	2530	30	
29	7988	0507	9970	2530	9.9921670	4027	3276	2021	4970	2530	31	
30	9-9620525	OFFICE	9.9772500	2000	4197	40.47	5803	4021	7500	4030	30	
31	3061	9596	5030	2230	6724	2527	8330	2527	10-0230030	2530	29	
32	5597	2536	7560	2530	9251	2527	10 0080857	2527	2560	2530	28	
33	8133	2536	9.9780090	2530	9-9931778	2527	3384	2527	5091	2530	27	
34	9.9030009	2535	2020 5140	2529	4309	2527	5911	2527	7621	2530	26	
136	5740	2536	7679	2530	9359	2527	10-0090966	2527	2689	2531	94	
37	8275	2535	9.9790209	2530	9-9941886	2527	3492	2527	5213	2531	23	
38	9-9640811	2535	2738	2530	4413	2527	6019	2527	7743	2530	22	
39	3346	2535	5268	2629	6940	2526	8547	2527	10-0250274	2531	21	
:40	5881	2525	7797	2520	9466	2527	10/0101074	9597	2605	9591	20	
41	8416	2535	9.9800326	2530	9.9951993	2527	3601	2529	5336	2531	19	
42	9-9650951	2535	2956	2529	4520	2527	6129	2527	7867	2531	18	
43	6020	2534	7914	2529	0572	2626	10-0111194	2628	10:026U398	2531	17	
45	8555	2535	9-9810443	2529	9.9962100	2527	3711	2527	5461	2632	15	
46	9.9661089	2534	2972	2529	4627	2527	6239	2528	7992	2531	14	
47	3623	2534	5501	2529	7154	2526	8766	2527	10-0270523	2531	13	
48	6157	2535	8030	2529	9680	2527	10.0121294	2527	3065	2532	12	
49	8692	2533	9,0620259	2528	9'9972207	2527	3521	2528	5567	2531	11	
50	9-9671225	2534	3087	2529	4734	2526	6349	2528	8118	2532	10	
51	6909	2534	2016	2529	7260	2527	8877	2527	2100	2532	9	
53	8827	2534	9-9830673	2528	9-9982314	2527	3035	2528	5714	2532	7	
54	9-9681300	2533	3202	2529	4840	2526	6460	2529	8246	2532	6	
55	3993	2533	5730	2528	7367	2527	8988	2528	10-0290779	2533	5	
56	6427	2533	8259	2529	9893	2527	10 0141516	2520	3311	2532	4	
57	8960	2533	9.9840787	2528	9-9992420	2527	4044	2528	5843	2533	3	
198 60	7-9091493	2533	3315	2529	7472	2526	0572	2528	0.000,0000	2533	2	
60	6559	2533	8372	2528	10.000,0000	2527	10-0151628	2528	3441	2532	0	
1	470	diff.	460	diff.	450	diff.	440	diff.	430	diff.	1	
		-			LOG. COT	CAN.		30	-		1	
-				-							_	

1	12				LOG. 81	NE.			[Te	ble s	a.
7	470	diff.	48º	diff.	490	diff.	500	diff.	510	diff.	1
	9.8641275	1177	9-8710735	1137	9-8777799	1097	9-8842540	1059	9.8905026	1023	60
1 2	2452° 3629	1177	1872 3008	1136	8896 9994	1098		1060	6049 7071	1022	59 68
3	4806	1177	4144	4 5 000	10-127230001	1096	5717	1058	8092	1021	57
4	5981	1175 1175	5279		-0106	$\frac{1096}{1095}$	6775	1058 1057	9113		56
5	7156	1175	6414	1124	3281	1095	7832	1057	9.8910133	1020	55
67	8331 9504	1173	7549 8691	1133		1094	8989 9945	1056	1153 2172	1010	179
8	9-8650677	1173	9813	1132	45000	1093	0-2051000	1055	3191	thia	53
9	1849	1172	9.8720945	1132	7656	1032	2055	TOPP	4208	1017	51
110	3021	1172	2076	1191	B74S	1092	2100	1054	5226	1018	50
11	4192	1171	3207	1131	9840	1092 1090	4162	$\frac{1053}{1053}$	6242	PERMISE	49
12	5362	1169	4331	1129	a.R1anaan	1091	5215	1052	7259	1016	48
13	6531 7700	1169		1120	2021	1089	5207	1052	8274 9289	11015	47
16	8868	1108	77:00	1126	1300	1089	P976	1051	9:8920303	1014	45
16	9.9660036	$\frac{1168}{1167}$	B849	$\frac{1127}{1127}$	E130/2	1088	0490	1050	1316	1013	44
17	1203	1166	9976	1126	6375	1087	9.8800470	1049	2329	1013	43
18	2369 3534	1165	9-9731102	1125	7462	1086	1519	1040	3342 4354	1012	42
		1165	2227	1125	8548	1086	2568	1048		I I I I I I I	
20 21	4699 5863	1164	3352 4476	1124	9634 9·8800719	1085		1047	5365 6375	1010	39
22	7026	1163	0.032	1123	1009	1084	5710	1047	7385	1010	35
23	9189	$\frac{1163}{1162}$	6722		2887	1084	6756	1046	8395	1010	37
24	9351	1161	7899	1123	3970	1082	1901	1045	9404	1/1/10	36,
25	9-9670512 1673	1161	8965 9-8740085	1120		1082	9840	1044	9·8930412 1419	1007	35
27	2833	1160	1908	1120	7.016	1081	9.6870934	1044	2426	1007	33
28	3992	1159	9295		0,000	1080	1977	$\frac{1043}{1042}$	3433	1007 1006	32
29	5151	1159 1158		1110	9310	1079		1042	4439	1005	31
30	6309	1157	4561	1119	9.9910455	1079	4061	1041	5444	1004	30
31	7466	1157	5679	1116	1994	1078	6102	1040	6446	345034	29
32	8623 9779	1166	6795 7912	1117	2612 3689	1077		1040		1004	27/
34	9-8680934	1100	0897	1115	4.70%	1077	0991	1039	0.460	1003	26
35	2089	1154	9.8750142	1115	5842	1076	0010	1039	9.8940461		25,
36	3242	1154	1256	1117		1074	9260	1037	1402	1001	24 23
37 38	4396 5548	1152	2369 3482	1113	7992 9067	1075		1037	2463 3464	1001	44
39	6700	1152	4504	1112	0.0000140	1073	2400	1030	4462	999	21
40	7851	1151	5706	1112	1010	1073	4444	1036	5463	1000	20
41	9002	1151	5103	1110	9905	1016	E470	1035	6461	998	19
42	9.8690152	1150 1149	7927	1111	3357		6513	1034 1034	7459		18
43	1301	1149	9030	1109	4439	1071		1022	9457 9453	006	16:
44	2449 3597	1148		1106		1008	9619	1054	9453	997	15
46	4744	1147	2361	1105	77/2000	1010	9-22006A4	IVak	1445	995	14
47	5891	1147	3468	1107	61,00	1068	1675	1031	2440	995, 995	13
48	7037	1145	4514	1106	9779	1067	2700	1030	3435	994	12
49	8182	1144	5080	1105	8.8930841	1067	3130	1029	4429	993	11
50 51	9326 9.8700470	1144		1104	1908 2974	17700		1049	5422 6414	992	9
52	1613	1143	500,5	1104	40.50	1065	6222	1028	7.406	992	8
53	2756	$\frac{1143}{1142}$	0.8770096	1103	5104		7850	1025	8398	992 991	7
54	3898	1141	1138	1100	0108	1064	9877	1026	9389	990	6
55	5039	1140	2300 3401	1101	1232	1062	חלינונות חבו- חד		9-8960379 1369	990	5
56	6179 7319	1140	4501	THU	0257	1003	1054	1020	2358	990	3
58	8458	1139 1139	1000	FINA	9.8840418	1061	2979	1020	3346	988 988	2
59	9597	1139	0.700		1479	1061	4003	1029	4334	985	1
60	9·8710735		1199	1	4990		0040	1	5321 38°	100	0
1	420	diff.	410	diff.	1 40°	diff.		diff.	1 200	diff.	1
1_					LOG. COS	TINE .					-

Table 11.												
1	470	diff.	480	diff.	490	diff.	50°	diff.	51°	diff.	1	
0	10-0303441	2533	10-0456626	2540	10-0608369	2552	10-0761865	2565	10-0916308	2583	60	
1	5974	2533	8166	2541	10 0610921	2552	4430	2566	8891	2584	59	
2	8507	2533	10-0400707	2541.	3473	2552	6996	2567	10-0021478	2584	58	
3	2672	2533	3248	2541	0025	2552	9503	2566	4059	2584	56	
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57	9614 9:967 0125	$\frac{511}{512}$	9.970 0061	496	8477	461 461	5394	436	0830		3
58 59	0637	511	0547 1032	485	9398 9398	460	5830 6265	435	1241	419	2
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1 2 3	28509	3518	43183	3643	65783	3782	97206	3938	39498	4112	
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12	63773	3537	79710	3665	10.4203714	3807	36708	3965	79750	4143	
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14	70950	3541	87042	3669	11331	3611	44641	3971	89039		
15	74391	3543	90711	3672	15142	3815	43612	3973	92187	4159	
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25	09917	3564	27530	3694	53399	3840	88475	4002	33950	4184	1
26	13481	3566	31224	3697	67239	3842	92477	4004	3B034	4167	В
27	17047	3568	34921	3699	61081	3845	96481	4008	42221	4190	æ
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49	96027	3613	16837	3749	46267	3900	85322	4069	35162	4259	
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25 26	2198 2599	401		5494 5870	376		7348 7701	353		7777 8106	329		7099	305	34
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53	3250 3639	389	1	5871 6236	365		7059 740 0	341	. *	8827 7144	317		5188 5482	294	9 8 7 6
54 55	3039 4027	388		6600	364	1	7740	340		7461	317		5776	294 294	5
56	4415	388 388		6964	364 364		8081	341 339		7778	317 316		6070	294 293	4
57 58	4903 5190	387		7328 7691	363		8420 8760	340		8094 8410	316		6363 6655	292	5 4 3 2 1
59	5577	387		8054	202		9099	339		8726	316		6947	292 292	ĩ
60	5963	386		8416	362	,	9438	339		9041	315	10	7239		0
1	170	dif.	16	0	dif.	15		dif.	14		dif.	13	,	dif.	
						LOG.	COSI	NE.							

T	able II.]			-	LOG. T	AN.		-	-	12	23
17	720	diff.	730	diff.	740	diff.	750	diff.	760	diff.	10
0	104882240			-	10-5425036		10:5210478	1	10(60(0)00.50)		60
				4520		4770		5056	22624	5385	59
1	96540 90844	4304	51130 55654	4524	34590	4774	29592	5061	43065	5391	58
3	95151		60182	4528	29806 34580 39359 44143	4779	34658	50G6	7-1-1	THE SHALL	100
4	99461	4310			44143	4784	39729	5071	48462 53864	5402	561
	10-4903776	4315	69250 73790	4536	48931			5077			
5	08093	4317	73790	4540	53724	4793	49887	5081		5414	54
6	12414	4321			58521	4797	54974	5087	70107	5420	53
7 8	16739	4325	78334 82982	4546	63322	4P01	60065	5091			
9	21067	4328	87434	4552	68128	4806	65162	5097	90966	5432	51
		4331		4555	72939	4811		5103	DUGUE	5439	128
10	25398	4335	91989	4560		4815	70265	5107	BUAUS	5444	120
11	29733	4339	90549	1564	77754	4819	75372	5113	91949	5451	49
12	34072	4342	ro 9504 [17-2]	4568	82573	4825	80485	5117	97300	5456	48
13	39414	4346	03031	4571	87398	4828	85602	5123	10-6102756	5463	
14	42760	4240	10252	4576	9222(4834	90725	5129	0.057 [3]	KARO	40
15	47109	4959	14828	4560	97061	4838	95854	5133			
16	51462	4356	19408	4583	10-5501806	4842	10-5500997	5139		5481	44
17	55919	4300	23991	4588	06740	4847	06126	5145	24044	5487	43
18	60178	4363	26679	4592	11587	4952	11271	5149	20121	5493	42
19	64541	4367	33171	4596	16439	4857	16420	5155	33944	5500	
20	68908		ウワフとフ	4600	21296	4861	21575	5160	41124	EEOC	40
21	73279	4371	42367		26157	4865	26735	5166	46630	5510	39
22	73279 77653	43/4		4604	31022	1021	31901				38
23	92031			4608	35893	4075	37072	5171 5176		0010	37
24	96412	4381	EGIOS	4613	35893 40768	1000	42248	5182	03159	5531	30
25	00707	4385	COBOC	4616 4620	45648	4884	47430	5187	00119	5537	
26	95186	4389	CF 400	4625	50532	4889	62617	5192	74252	5543	34
27	99578	4392		4629	55421	4894	57809	5198		5560	
28	10-5003974	4390		4633	60315	4899	63007	5204	55345	5555	
29	08374	4400		4637	65214	4903	68211	5208	90900	5563	
30	12777	4403	09869	7.	70117		73419		96463		1201
31	17104	4407	DEEUD.	4641	75025	4908	78634	5215	10-6009031	5568	20
32	21594	4410	03430	4645	79938	4913	83854	5220	nzene	5575	
33	and Colors	4415	07000	4650	84855	4917	00070	5225	19107	5581	
34	20426	4417	0.5202541	4653	89776	4923	94310	0.401	10775	5586 5594	
35	34848	4422	07100	465R	94705	4927	99546	5236		5601	40
36	-	4475	11061	4662	99637	4932 4937	10-5904788	5242 5247		5607	491
37				4666	10.5604574	4941	10035	5253		5613	40
38	48135		91100	4671	09515	1947	15288	5259	41150	5620	64
39		4436		4675 4679	14462	1951	20547	5264		5627	
40	57012	4441	20552		19413		25811			-	I DOM
41	61455	4443	"(פרספר	4683	24369	4956	31081	5270	59070	3033	19
42	65903	4448	20022	4687	29330	4961	36356	3410	63709	0039	18
43		4451	446142	4692	34296	4966	41637	6281		5040	
144	51010	44.513	40210	4696	39267	4971	46924	5287			
45			# 40 LO	4700	44243	4976	52216	5292	80667	5659	15
46	93731	4462	60715	4705	49224	4MDT	57514	5298		0000	w (a)
147	88108	4457	69494	4709	54209	1960	69010	0304			1.5
48	92668		20197	4713	59200	4991	68127	Datus		5679 5686	12
49	97142	44/4	79255	4718	64195	4995	73442	0315	18-6203371	5692	
150	10-5101620	4478	77577	4722	69196	5001	78763	INCOM A	Annan		1400
51	06102	4482	cocco.	4726	74201	5005	84090	5327	14769	5699	
152		4495	07022	4730	79211	5010	89422	5332	90460	91100	
53	10587 15076	4489	01769	4735	84227	5016	0.4260	10332	96101	2113	71
54	10570	4494	06800	4740	89247	5020	LO-RODGLOA	5344	21000	5719	6
56	19570 19570 24067	4497		4743	94273	5026				0140	5
156	03867	4500	nenna!	4748	99303	2020	20000	5356	emore o	0199	4
87 67				4753	10-5704339	30.50		5361	49099	DIAN	20
56	37591	4509	15500	4757	09379	DU49	91537	0201	54945	2140	2
69	37581 42093	4512	20270	4761	14425	อบสถ	26911	5374	60400	5104	1
60		4517	25036	4766	19475	5050	32289	5378	66359	5760	0
00		diff.		diff.	150 "	diff.		diff.		diff.	1
		meg.	20		Log. co	TAN		1			
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12	24						LOC	3. 8	NE.					[Ta	ble	Π.
	770	220	diff.	780	044	dif.	790	400	diff.	800	E1E	dif.	810	100	diff.	Ľ
ĭ	9-9001	531	292	3.3304	312	268	a.aa1a	711	245	9.9933	515 737	222	OFCE C	399	200	2
2		822	291		580	268		956	245		959	222		599	200	58
3	9.8669	113	290	9-990K	115	267	9-9920	201 445	244	9.9934	181	$\tilde{2}\tilde{2}\tilde{2}$		798	199	57
5		693	290	0000	382	267		689	244		624	221	9-9947	195	198	55
6	0.0000	982	289		648	266	0.0001	932	243		844	221		393	198	54
Ŕ	9.9009	560	289	9-9906	180	266	9.9921	418	243	9.9930	295	220		788	197	53
ğ		849	289		445	265		660	242		504	219		985	197	51
10	9-9890	137	287		710	264		902	242		723	219	9-9948	181	196	50
112		424 711	287	9-9907	974	265	9.9922	395	241	0.0036	942	218		377 573	196	49
13		998	287	3301	502	263		626	241	3330	378	218		769	196	47
14	9-9891	285	286	0.0000	766	263	0.0000	866	240		596	217	0-0040	964	194	46
16		856	285	a 2208	291	262	9 9923	346	240	9-9937	030	217	9 3349	352	194	44
17	9.9892	142	286 286		553	262 262		585	239		247	216		546	194	43
18		711	284	9-9909	815	262	0.0024	824	239	ì	463 670	216		740	193	42
120		QQE	284	0 0000	335	261	2 22%	301	238		204	215	9-9950	126	193	an an
$\tilde{21}$	9-9893	279	284		598	260		539	238	9.9938	109	215	3 3350	318	192	39
22		562	283	0.0010	859	260	0.000=	776	237		324	214		510	192	38
24	9-9894	128	283	9.9910	378	259	9.9925	250	237		752	214	ł	893	191	36
25		410	282		637	259		486	236	l	965	213	9-9951	084	191	35
20 27		692	281	0.0011	896	258		722	235	9.9939	178	213		274 484	190	134
28	9-9895	254	281	3 3311	412	258	9.9926	192	235		603	212		654	190	32
29		53 5	280		670	257		427	234	1	815	212		844	189	31
30 31	0.0006	815	280	0.0012	927	257		661	234	9.9940	027	211	9-9952	033	188	30
32	3 3030	374	279	9 9912	440	256	9.9927	129	234		449	211		409	188	28
33		654	278		696	256		362	233	1	659	211	1	597	188	27
35	9-9897	$\frac{932}{211}$	279	9-9913	952 207	255		595	232	0.0041	870 079	209		972	187	25
36	0 000.	489	278	3 3310	462	255	9.9928	059	232	1 3321	289	209	9-9953	159	187	24
37 38	0.0000	766	277		717	254		291	231		498	208	1	345	186	23
39	3 3030	320	277	9.9914	225	254		753	231		914	208	1	717	186	21
40		597	270		478	252		984	220	9.9942	122	200		902	105	20
41 49	0.0000	873	275	1	731	253	9.9929	214	230		330	207	9.9954	087	184	19
43	9.9633	148 423	275	9.9915	984 236	252		673	229		743	206		455	184	17
44		698	275		488	251		902	229		950	206		639	183	16
46	0.0000	973	274		739	251	la·aa30	131	228	9.9943	156	205	0.00EE	822	183	15
47	5 5500	521	274	9-9916	241	251 251		587	228		566	205	J J300	188	183	13
48 40	0.0001	794	273		492	249	0.000	814	227		771	204		370	182	12
50	9.9301	100	272		741	250	9.9931	041	227	0.0044	100	205		724	182	10
51		612	273	9-9917	240	249		208 494	226	9944	383	203		915	181	9
52		883	272	""	499	249		720	226		587	202	9.9956	095	181	8
54	9.9902	155	271		737	249	0.0020	946	225		789	203		276	180	6
55		697	271	9.9918	233	247	9 9932	396	225	9.9945	194	202		635	179	5
56 57	0.0000	967	270		480	247		621	224		396	201		815	178	4
£ 8	9.9903	237 506	269		127 974	247	0-0033	645 069	223		798	201	9.9957	993 179	179	2
59		775	269 260	9 ·9919	220	246 246	0 0000	292	224		999	201		350	178	Įį
οV	9.9904	044	J: 4	110	466	2.0	100	615	2:4	9.9946	199	1:4	90	528	2:0	0
Ι'	125		ay.	110		aiff.	100	COS	aif.	90		щŢ.	- 50		æIJ.	1
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7	able II.]				LOG. TA	N.				12	25
1	770	diff.		diff.	790	diff.	800	diff.	810	diff.	
0	10-6366359	5767	10 67 25 255	6216	10-7113477	6750	10.7536812	7394	10-8002875	8184	60
2	72126 77900	5774	31471 37695	6224	20227 26986	6759	44206 51611	7405	11059 19257	8198	59 59
3	83681	2181	43927	6232	33755	6769	51611 59028	7417	27470	8213 8226	57
4	89469	5788 5795	50168	6241 6248	40534	6779 6789	00457	7440	35698	8243	56
5	95264	5801	20410	6257	9/343	6799	73897	7453	43941	8257	55
6 7	10:6401065 06974	5809	62673 68939	0500		6808	81350 88815	1405	52198 60471	3273	54 53
8	12690	5816	75212	6273	67740	6919	96292	7477	68759	8288 8302	52
9	18513	5823 5829	81494	6292 6290		6626 6638	10-7603782	7490 7501	77061	8318	51
10	24342	5937	87784	6299	81415	6849	11283	7514	85379	5334	50
11	30179	5844	94082	6307	60%04	6858	18797	7525	93713	8348	49 46
12 13	36023 41874	5851	10:6800389 06705	6316		6869	26322 33861	7539	10·8102061 10425	8364	47
14	47733	9699	19029	6323	08860	6878	41411	7550	18904	8379	46
115	53598	5866 5872	19360	6332 6341	10199	6889 6899	48974	7563 7575	27198	8394 8410	45
116	59470	5880	25701	6349	22657	6909	56549	7588	35608	2100	44
117	65350 71237	5887	32050 38408	6358	29566 36486	6920	64137 71738	7601	44034 52475	9441	
19	77131	5894	44774	6366	43416	6930	79350	7612	60932	8457	41
20	83032	5901	51149	6375	50356	6940	86976	7626	69405	8473	40
21	88941	5909	57532	6383	67206	6950 6961	94614	7638 7651	77894	8489 9504	39
22	94857	5916 6923	63924	6392; 6401	64267	6971	10-7702265	7664	86398	8520	38
23	10-6500780	5930	70325	6409	71238 78220	6982	09929	7676	94918 10:6203454	8636	37 36
24 25	06710 12646	5936	76734 83152	6418	85212	6992	17605 25294	7689	12007	8553	35
26	18593	5945	89579	6427	92214	7002	32996	7702. 7715	20575	8568	34
27	24546	5953 5960	96015	6436 6444	99228	7014 7023	40711	7729	29160	8586 8601	33
29	30506	5967	10-6902459	6453	10:7306251	7035	48439	7742	37761	9617	32 31
29	36473	5975	08912	6462	13286	7046	56181	7754	46378	8634	30
30 31	42448 48430	5982	15374 21845	6471	20331 27367	7056	63935 71702	7767	55012 63662	8650	29
32	54420	5990	20325	6480	34453	7066	79482	7780	70000	8666	20
33	60417	5997 6005	34813	648F 6498	41530	$7077 \\ 7098$	87276	7794 7807	81011	9683 5700	27
34	66422	6012	41311	6506	49618	7099	95093	7820	89711	8717	26 25
35	72434 78464	6020	47817 54333	6516	55717 62827	7110	10:7802903 10736	7833	98428 10:8807161	8733	24
36 37	84491	6027	COCE?	6524	69947	7120	18583	7947 7861	15011	9750	23
38	90516	6035	67391	6534 6543	77079	$\frac{7132}{7142}$	26444	7673	24678	9767 9794	22
39	96559	6050	73934	6552	84221	7154	34317	7886	33462	8801	21
40	10-6602609	6059	80486	6560	91375	7164	42205	7901	42263	8818	20
41	08667 14733	6066	87046	6571	98539 10 7405715	7176	50106 58020	7914	51081 59917	8836	19 18
42	20806	6073	93617 :0:7000196	6579	12901	7186	65949	7929	68769	9852	17
44	98007	6081 6089	OCADA	6588	20099	$\frac{7198}{7209}$	73891	7942 7956	77639	8870 8888	16
45	32976	6007	13362	6607	27308	2990	81847	7969	86527	8904	15
46	39073 45177	6104	19989	6616	34528 41760	7232	99816 97800	7984	95431 10·8404354		14
46	51299	6112	33231	6626	49003	1243	10 7905797	7997			12
49	57409	$6120 \\ 6128$	39866	Theresay	56257	7254 7266	13909	9014 8026	22252	9975	11
50	63537	6136	46511	6645 6653	63523	7277	21835	8039	31227	8993	10
51	69673	6144	53164	6664	70800	7999	29874	9054	40220	9011	9
52	75817	6152	59828 66500		79088 85388	7300	37928 45996	8068	49231 56261	9030	8
53	81969 86128	6159	73183	6683	92699	7311	54078	8082	67308	9047	6
55	94296	OTOD	79874	6691 6702	10:2500022	7323 7335	62175	8097 6111	76373	9065 9084	Б
56	19 6700472	6176 6193	86576	6711	07357	7246	70200	8126	65457	9102	4
57	06655	6192	93287 10:7100007	6720		7358	78412 86551	8139	94559 10-8503679	9120	3
158 59	12847 19047	6200	06727	6730	90421	7370	94706	8155	19919	9139	1
60	25255	6208	13477	6740	36812	7381	10-8002875	0109	21975		Ô
'	120	diff.	110	diff.		diff.	90	diff.	80	diff.	1
					LOG. COT						

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1:	26						LOG.	BIN	E.					L	ble 1	n.
"	82		diff.	83		diff.	849		diff.			diff.	86	0	diff.	شا
0	9.9957	528 705	177	9.9967	507 662	155	9-9976	143 276	133	3.9983	442 553	111	9.9989	408 496	1 88	60 59
1 2		882	177		817	155		408	132	1	663	110	1	584	1 88	58
$\tilde{3}$	9-9958	059	177 176		971	154 154		540	132 132		772	109 109	i	671	87 87	57
4		235	176	9.9968		153		672 803	131		881 990	109		758 845	87	56 55
5 6		411 586	175		278 431	153		933	130	9.9984		109		931	96 96 86	54
7		761	175 175		584	153 152	9.9977	064	131 130	0001	207	108 108	9.9990	017	86	53
8		936	175		736	152		194	129	1	315	107		103	85	52
9	9.9959		173		888	152	ı	323	130		422	107		188	85	51
10 11		284 458	174	9-9969	191	151	ł	453 582	129	i	529 636	107		273 357	84	50 49
12		631	173		342	151		710	128	1	742	106		441	84	48
13	Ĭ	804	173 173	ĺ	492	150 150		838	128 128		846	106 105		525	84 93	47
14	9.9960	977	172		642 792	150	9-9978	966		9.9985	953	105		608 691	83 83 83	46
15 16	9 9900	321	172		941	149	9 9910	220		9 9900	163	105		774	83	44
17		492	171 171	9.9970	090	149 149			127	l	268	105 104		856	82 82 82	43
18		663	171		239	148		473	126		372	103	0.000*	938	82	42
19	0.000	834	170	l	387	148		599 725	126		475	104	9-9991	020	BI	41
$\frac{20}{21}$	9.9961	174	170		535 682	147		950	125		579 682	103		101 182	81	40 39
21 22 23 24		343	169		829	147		975	125		784	102		262	80	38
$\tilde{23}$		512	169 169		976	147 146	9.9979	UJJ	124 124		886	102 102		342	80 80	37
24		681	168	9-9971		146		223 347	124	0.0000	988	102		422	79	36
25 26	9.9962	849	168		268 414	146				9.9986	090 191	101		501 580	79	35 34
26 27	5 5502	195	168		559	145		EQ31	143		292	101		659	79	33
28		352	167 167		704	145 145		71C	140		392	100 100		737	78 78	32
29		519	167		849	144		838	122 122		492	99		815	77	31
30		696	166	9.9972	993	144	9-9980	960	121	1	591	100		892 969	77	30
31 32	9.9963	852 018	166	9 9912	280	143	9 9900	202	121	i	691 790	99	9.9992		77	29 28
33	0000	183	165 165	1	423	143 143		323	121 120		988	98 98	0002	122	76 76	27
34		348	165	1	566	142	1	443 563	120	0000	986	98		198	76	26
35			164		708 850	142		683	120	9.9987	084 181	97		274 349	75	25 24
36 37		841	164		991	141	l	802	119.		278	97		424	75	23
38	9.9964	004	163 163	9-9973	132	141		921	119		375	97 96		498	74	22
39		167	163		273	141	9 -9981		118		471	96	1	572	74	21,
40		330	163	1	414	140		158	117		567	96		646	74	20
41 42		493 655	162		554 693	139		275 393	118		663 758	95	ŀ	720 793	73	19 18
43		816	161 161		833	140 138		510	117		853	95 94		865	72	17
44	 a.aaa=	977	161	0.000	971	139		626	116 117	0.000-	947	94		938	73	16
	9.9965	138 299	161	9-9974	110 248	138		743 859	116	9-9988	041 135	94	9.9993	009	72	15
46 47		459	160		386	138		974	115		228	93		081 152	71	14
48		619	160 159		523	137	9.9982	089	115 115		321	93 93		223	1 / 1	12
49		7 78	159		660	137		204	114		414	92	1	293	70 71	11
50	0.000	937	159		797	136		318	115		506	92		364	69	10
51 52	9.9966	096 254	158	9.9975	933	136		433 546	113		598 689	91		433	70	9
53		412	158	סופק כן	205	136		660	114		780	91		503 572	69	8
54		570	158 157		340	135 135		772	112 113		871	91 91	1	640	pa	6
55		727	157		475	134		885		0000	962			708		5
56 57	9.9967	884 040	156	1	609 743	134	9.9983	997	112	9-9989	1/1	89	i	776	68	432
5 8		196	156		877	134	. 5503	220	111		230	89		844 911	67	2
59		352	156 155	9.9976	011	134 132		332	112		O L .	89		978	66	1;
60	P70	507		Ca	143			442			408		9 9994	044	00	0
	, 70	- 1	diff.	60		diff.		000	diff	40	'	diff	I 3º		diff	1'
L							LOG.	CO3	INE.							į

Ta	ble 11.]			LOG.	TAN	-			127
7	820	diff.	83°	diff.	840	diff.	850	1:4°	7
0	10.85 21975	9176	10.91 08562	10457	10.97 83798	12169	11-05 00400	diff.	60
1.	31151	9194	19019	10480	95967	12202	95056	14574 14623	59
2	40345 49558	9213	29499 40004	10505	10-98 08169 20406	12237	11.06 09679 24350	14671	58 57
4	58790	9232 9251	50534	10530 10555	32675	12269 12304	39071	14721 14769	56
5	68041	9270	61089	10580	44979	12339	53840	14820	55
6	77311 86600	9289	71669 82274	10605	57318 69690	12372	68660 83 52 9	14869	54 53
8	95908	9308 9328	92904	10630 10655	82097	12407	00440	14919 14971	52
9	10.86 05236	9347	10.92 03559	10681	94539	12442 12477	11.07 13419	15021	51
10	14583	9366	14240	10707	10.99 07016	12513	28440	15073	50
11 12	23949 33335	9386	24947 35679	10732	19529 32076	12547	43513 58637	15124	49 48
13	42740	9405 9425	46437	10758 10784	44660	12584 12619	73814	15177 15229	47
14	52165	9444	57221 68031	10810	57279 69934	12655	89043 11:08 04325	15282	46
15	61609 71074	9465	78867	10836	82625	12691	19660	15335	45 44
17	80558	9484 9505	89730	10863 10889	95353	12728 12764	35048	15388 15443	43
18	90063	9524	10.93 00619	10916	11.00 00111	12802	60491	15497	42
19	99587 10·87 09132	9545	11535 22478	10943	20919 33757	12838	01540	15552	41
20 21	18697	9565	33447	10969	46633	12876		15607	39
22	28282	9585 9606	44444	10997 11023	59506	12913 12951	11.09 12810	15663 15718	38
23	37888 47514	9626	55467 66518	11051	72497 85486	12989	28528	15775	37 36
24 25	57161	9647	77597	111013	00513	13021		19091	35
26	66829	9668 9689	88703	11106 11133	11.01 11579	13066 13104	76023	15889 15947	34
27	76518 86227	9709	99836 10 ·94 10998	11162	24683 37827		1 91970	16004	33 32
28 29	96967	9730	22187	11189 11218	51009	13182 13222	11·10 07974 24037	16063	31
30	10.88 05709	9752	33405	11246	64231	13262	40150	16121	30
31	15482	9773 9794	44651	11275	77493	13301	56340		29
32 33	25276 35091	9815	55926 67229	11303		13341	72580	16301	28 27
34	44928	9837 9859	78561	11332 11361	17517	13382 13423	11.11 05040	16362 16423	26
35	54787	9880	89922	11389	30940 44403	13463	21666	16484	25 24
36 37	64667 74569	9902	10·95 01311 12730	11419	57908	13505		16547	23
38	84492	9923 9946	24179	114 4 9 11478	71453	13545 13588	71306	16609 16672	22
39	94438	9968	35657	11507	85041	13629	8/9/8	16736	21
40	10.89 04406	9990	47164	11537	98670 11 ·03 12342	13672	11.12 04714	16799	20 19
41 42	14396 24409	10013	58701 70269	11568	26056	13714		16864	18
43	34443	10034 10057	81866	11597 11628	39812	13756 13800	55306	16929 16995	17
44	44500 54580	10080	93494 10·96 05152	11658	53612 67455	13843	72301	17061	16 15
46	64683	10103 10125	16841	11689 11720	81341	13886 13931	11.12 06400	17127	14
47	74808	10148	28561	11751	95272	13974	23683	17194 17262	13
48 49	84956 95128	10172	40312 52094	11782	11·04 09246 23265	14019		17330	12 11
50	10.90 05322	10194	63907	11813	37328	14063	75672	17398	10
51	15540	10218 10241	75751	11844 11876	51436	14108	00141	17468 17538	9
52	25781	10264	87627 99536	11909	65590	1415 4 14199	11·14 10679 28287	17608	8
53 54	36045 46333	10288	99536 10-97 11476	11940	79789 94033	14244	28287 45966	17679	9 8 7 6 5 4 3 2 1
55	56645	10312 10335	23448	11972 12004	11.05 08324	14291 14338	63717	17751 17822	5
56	00900	10360	35452 47490	12039	22662 37046	14384	00134	17895	4 2
57 58	77340 87723	10383	59559	12003	51477	14470	11-15 17403	17969	2
- 59	98131	10408 10431	71662	12103 12136	65956	14479 14526	35446	18043 18117	1
60	10·91 08562	diff.	83798 6°	diff.	80482 5°	diff.	53563 40	diff.	0
'	, , ,	~•IJ· •			OTAN.	~ JJ.	-	~·JJ · ·	

128	LOG. SIN	E.				LOG. TAN. [7	able 1	II.
′		diff.	1.	- 1	′.	96° diff. 87° d	liff.	7
0 1 2 3 4 5 6 7 8 9	9·9994 044 110	66	60 59	Norn. The trigonometrical lines near the extremities of the quadrant are give the trigonometrical line belonging to any arc below 2 defrees or above 89 degrees.	0	11.15 53563 18192 11.28 06042 24 71755 18269 30281 24	1407 ,	60 59
2	176	66	58	North te trigg	3	90023 10244 54655	23/2] ,	58
3	241	65 65	57	8	3	11.16 08367 10422 79166	TOTAL P	57
4	306 370	65 64	56 55		5	20/09 10400 11 29 03815 0	790	56 55
6	435	65	54	7.7	6	63866 10070 53535127	1930	54
7	498	63 64	53	5 %	6	82522 10727 78610	5075 5218	54 53
8	562 625	63	52 51	li son	8	20076 18817 11 30 03828 25	5366	52 51
10	688	63	50	2 2	10	1 10030	DD 14	50
11	750	62	49	long	ii	E70E4 1890U 00071 4	2003	อบ 49
12	812	62 62	48	3. 15	12	77016 10146 111-31 06187 3	2000	48
13 14	874 935	62 61 61	47 46	9 6	13 14	11.10 15303 19230 50001 26	2195 9	47 46
15	996	61	45	az	15		0202 J	40 45
16	9.9995 056	60	44	7 2	16	541061:040-111:32 11004	2441	44
17 18	116 176	60 60 60	43 42	2 8	17	13093 10g79 3/60/100	27621 9	43
19	236	60	41	belc	18 19	11:10 19999 19662 01303 26	3931	42 41
20	295	59	40	8 3	20	32579 19/50 11:22 12402	1099	40
21 22	353	58 58	39	de	21	E0417 19839 AFCCO 21	7267 7440	39 38
22	411	58	38 37	*	22	1201100001 131090	7612	38
23 24	469 527	58	36	2.0	23 24	11.20 12401 20113 11 34 00721 27	7789	37 36
25	584	57 57	35	3 9		32687 40400 56470 4	900 3	35
26 27	641	56	34	boa	25 26 27	52986 20394 11.25 12056 28	3147	34 33
28	697 753	56	33 32	7e 8	27	03070 20490 11 30 12950 28	טוטוסכ	33 32
28 29	809	56 56	31	2 2	28 29	70175	3703 3	31
30	865	54	30	The irigonometrical lines near the extremities of the quadrant are given ometrical line belonging to any are below 2 degrees or above 83 degrees.	30	35139 99069 99069	3	30
31 32	919	55	29 28 27	rive ces.	31	55921 20880 11 30 28155 29	282	29 28
33	974 9·9996 028	54	28	2 2	32 33	07722 20981 00017 29		28 27
34	082	54 54	26	62	34	11.22 18864 21062 11.37 16598 29	2001	26
35 36	136 189	53	25 24	3	35		00016	25 24
37	242	53	23	800	36 37	82726 2100 111 32 06273 00	J3UU 9	23
38	294	52 52	22	ion.	38	11.23 04223 21497 37384 30	2227 2	22
39	346	52	21	a a	39	25025 21710 68111 30	946	21
40 41	398 449	51	20 19	120	40 41	47535 21818 99057 31	166 2	20
42	500	51	18	be	42	01991 21928 11 39 30223 31	391	19 18
43	550	50 51	17	2.2	43		050 1	17
44 45	601 650	49	16 15	n.in	44 45	39409 99969 11 40 20083 99	mori 1	16
46	700	50	14	0,0	46	57731 22377 57168 32 80108 22402 89491 32	2323	15 14
47	749	49 49	13	9 11	47	11.25 02600 22492 11.41 22055 32	504	13
48 49	798 846	48	12 11	e z	48 49	40400 9979E 04804 99	norol L	12
50	894	48	10	able	50	47933 22845 87923 33	311	11
51	942	48	9	8	50 51	03742 22904 54902 33		10
52	989	47 47	8	ter	52	111.26 16828 23000 88632 33	829 1093	9 8
53 54	9.9997 036	46	7	8	53 54	62260[23333] 11 12 22720[34	2093	7
55	128	46	5	#	55	86826 23457 91724 34	636	6 5
56	174	46 46	4	181	56	11.27 10411 23585 11.44 26638 34	914	4
57 58	220 265	45	3 2 1	sea	57 58	5706 23842 01834 35	493	3
59	309	44	1	rie!	59	9/31/35	774	3 2 1
60	354	45	0	to every second at the beginning of the table, where we must search for	60	[11.28 06042 24105 69162 30	071	Ô
′′		diff.	1	, ,	1	3° diff. 2° d	iff.	′
ــــــــــــــــــــــــــــــــــــــ	LOG. COSI	NE.				LOG. COTAN.		

19,000,000

130)			LOG. SI	NE 88°.			[Table	11.
"	0′	1'	2'	3′	4'	5'	6'	7'	"
	9· 99 97354	9997398	9997441	9997484	9997527	•9997570	-9997612	7′ 9·9997653 54	60
1 2 3	54	თ 98	7.	on 85	න <u>28</u>		12 13	-	459
2	5 5	99	43	86	29	71	13	55	58
3	5 6	9997400	43	86 86	29	72	14	55	57
4	57	00	44	87	30	72	14	56	56
5	57	01	45	88	31	73	15	57	55
6	58	02	45	89	31	74	16	58	54
7	59	03	46	89	31 32 33	74	17	58 59	53
8	59 9 ·999736 0	9997404	·9997448	90	.00007774	75	9997618	9·9997660	52
- 1				9997491	9997534	9997576			51
10	61	05	48	91	34	77	19	60	50
11	62	06	. 49	92	35	77	19	61	49
12	62	06	49	93	36	78	20 21	62	48
13	63 64	07 08	50 51	94 94	36 37	79 79	21	62	47 46
14 15	65	08	52	95	38		22	63. 64	45
16	65	09	53	96	30	80 81	23	64	44
.17	66	10	53	96 96	38 39	82	24	65	43
18	67	ii	54	97	40	82	24	66	42
19	9.9997368	9997411	9997455	9997498	9997541	9997583	9997625	9.9997667	41
20	68	12			41		26	67	40
21	69	13	*56 56	99 99	42	84 84	26 26	68	39
22	70	13	57	9997500	43	84 85	27	69	38
23	70	14	50	01	43	86	28	69	37
24	71	15	58 58	01	44	86	28	70	36
25	72	15 16	59	02	45	87	29	69 70 71	35
25 26	73	16	60	03	46	88	30	71	34
27	73	17	61	04	46	89	30	72	33
28	72 73 73 74	18	61	04	47	89	31	72 73	32
29	9.9997375	9997419	9997462	9997505	9997548	9997590	-9997632	9-9997673	31
30	76	19	63	06	48	91	33	74	30
31	76	20	63	06	49	91	33	75	29
32	77	21	64	07	50	92	34	75	28
33	78	22	65	08	51	93	35	75 76	29 28 27 26
34	79 79 80	22 22 23 24	66	09	51	93	35	77	26
35	79	23	66 67	09	52	94	36	78	25
36	80	24	67	10	53	95	37	78	24
37	81	24	68	11	53	96	37	79	23
38	81	25	68	11	54	96	38	80	22
39	9·99973 82	9997426	9997469	9997512	9997555	9997597	·9 99763 9	9.9997680	21
40	83	27	70	13	55	98	40	81	20
41	84 84	27 27	71	14	56	198	40	82	19
42	84	28 29 30 30	71	14	57	99	41	82	18
43	85	29	72	15	58		42	83	17
44	86	30	73	16	58	00	42	84	16
45	87	30	74	16	59		43	84	15
46	87	31 32	74	17	60 60	02	44	9 5	14 13
48	88 89	32	75 76	18 19	61	03 03		87	12
49	9.9997389	9997433	9997476			9997604			ii
				1					
50	90	34	77	20	63		46	89	
51 52	91 92	35	78	, 21	63	05		89	
53	92	35	79		64				2
54	93		79 80						6
55	94	37	81		65	08			
56	95							92	1
57	95								3
58	96								2
59	9-9997397								1
60	98							95	0
"	59′	1 58	57	56	55'	54'	53′	52	111
l			•		SINE 1º		_		1
11						<u> </u>			

11 14669 162 46065534 4652 31 4679203 4716510 4751 479209 11 4830390 6752 11 4570369 6752 3441 4680441 7759 5400 3363 1031 8 1577 7970 4669 1680 9049 6660 4640 2955 8 3944 468041 47792 9049 6660 4640 2955 8 3944 468041 47792 9049 6660 4640 2955 8 3944 468041 47792 9049 6660 4640 2955 8 3944 461047 7127 4159 1509 9162 7184 5521 5276 3586 6512 3539 0834 8551 6548 4879 5 8 3944 4610407 7127 4159 1509 9162 7184 5521 5276 3586 6339 46004 7705 9729 9049 4660 2365 8971 6013 3385 1074 9095 7447 4 4 7622 4065 6366 6339 4010 7705 9729 9089 4 4 7622 4065 6016 7879 5261 2967 1031 4 7622 4065 6016 7879 5261 2967 1639 1530 1032 2276 4 4 4 7622 4 4 4 4 4 4 4 5 4 4										
0 11-4669162 4605534 4642213 4679203 4716510 4754 440 4799096 11-4830390 4 1672 11-4570369 16752 3441 4680441 77759 5400 3369 1672 1672 1672 1672 1672 1672 1672 1672	Ta	ble 11.]			LOG. T	an. 88°	•			131
1 14570369										1"
2 11-4570369 6752 3441 466044 7759 5400 3369 6728 6737 7361 4665 1660 9009 6660 4640 2955 8 6737 6861 1680 9009 6660 4640 2955 8 6738 6			4605534	4042213 - 2827						
4 1677 7970 4669 1680 9099 6660 4640 2955 5	2	11-4570369	二 6752	二 3441	4680441	二 7759	二 5400	二 3369	1672	58
66 2786 9188 5989 2919 4720259 7921 5912 4238 5 7 7 3390 9797 6512 3539 0884 8551 6548 4879 6 8 3394 4610407 7127 4159 1609 9182 7184 5521 5 10 5203 1626 8356 5399 2759 4760443 8457 6605 5 11 5607 2235 8971 6019 3385 1074 9093 7447 4 12 6412 22945 9586 6639 4010 7705 9729 9089 13 7017 3455 4656 2010 7759 4636 2336 40036 3734 4417 14 7622 4665 0816 7879 5261 2967 1003 9373 4 15 8227 4676 1431 8500 5867 3599 1639	3									
7 3390 4977 6512 3539 0884 8551 6548 4879 5 9 4558 1016 7741 4779 2134 9813 7820 5163 5 10 5203 1626 8356 5399 2759 4760443 8457 6605 5 11 5807 2235 8971 6019 3385 1074 9037 7447 4 12 6412 2945 9586 6639 4010 7705 9729 9089 4 13 7017 3455 4650201 7259 4636 2336 4003366 8731 4 14 7622 4065 0816 7879 5261 2967 1003 9373 4 15 8227 4675 1431 8500 5837 3599 1639 11 4840016 4 16 8832 5285 2046 9120 6513 4230 2276 0658 4 17 114580042 6605 3277 4690362 7765 5493 3350 1391 484016 4 18 114580042 6605 3277 4690362 7765 5493 3350 1391 49407 499 40647 7116 3892 0982 8391 6124 4187 2556 4912 2188 8336 5124 2224 9644 7388 5562 3329 4515 3222 4263 9947 5739 2945 4730270 8020 6099 4515 323 4230 2276 4230 9558 6355 3466 0897 8651 6737 5158 3 24 3674 4620168 6971 4088 1523 9283 7374 5601 322 466068 2377 4709 2150 9916 8012 6445 327 4230 4	5	2181	8579	5283	2300	9634	7291	5276	3596	55
8 39944610407 7127 4159 1509 9182 7184 5521 5 8	6		9188							
9									5521	52
111 5807 2235 8971 6019 3385 1074 9093 7447 4 12 6412 2945 9586 6639 4010 7705 9729 8089 4 14 7622 4675 1431 8500 5887 3599 1639 11*4840016 4 16 8832 5285 2046 9120 6513 4230 2276 6068 4 17 9437 5895 2661 9741 7139 4861 2913 1301 4 18 11*4580042 6505 3277 4690362 7765 45493 3550 1943 19 1252 7726 4508 1603 9017 6756 4925 3229 4 20 1252 7726 4508 1603 9017 6756 4925 3229 4 21 1858 8336 5124 2224 47389 5652										
12 6412 2845 9586 6639 4010 7705 9729 8089 4 13 7017 3485 4650201 77259 4636 2336 4800366 8731 4 14 7622 4065 0816 7879 5261 2967 1003 9373 345 15 8227 4675 1431 8500 5887 3599 1639 11*4840016 4 16 8832 5285 2061 9741 7139 4861 2913 1301 4 18 11*4890042 6505 3277 4690362 7765 5493 3550 1943 4 20 1252 7726 4508 1603 9017 6756 4925 3372 329 21 1858 8336 5124 2224 9644 7389 5462 3272 32 466420168 6971 4088 1523 9283 7377 5168 </th <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>50</th>										50
13	12									49
15 8227 4675 1431 8500 5887 3599 1639 11-4840016 4 16 8832 5285 2046 9120 6513 4230 2276 6658 417 7947 5895 2661 9741 7139 4861 2913 1301 4 18 11-4580042 6505 3277 4690362 7765 5493 3550 1943 4 20 1252 7726 4508 1603 9017 6756 4925 3372 3229 4 21 1858 8336 5124 2224 9644 7389 5462 3372 3 22 2463 8947 5739 2945 4730270 8020 6099 4515 3 24 3674 4620168 6971 4083 1523 9283 7374 55801 3 25 4280 0779 75877 4709 2150	13	7017	3455	4650201	7259	4636	2336	4800366	8731	47
16 8332 5295 2046 9120 6513 4230 2276 0658 4 17 9437 5895 2661 9741 7139 4861 2913 1301 4 19 0647 7116 3892 0982 8391 6124 4187 2596 4 20 1252 7726 4508 1603 9017 6766 4925 3229 4 21 1858 8336 5124 2224 9644 7389 5462 3372 3 22 2463 8947 5739 2346 0897 8651 6737 5158 3 24 3674 4620168 6971 4089 1523 9283 7374 5801 3 25 4280 0779 7587 4709 2150 9916 8012 6445 3 26 4886 1390 8203 5330 2777 4770548										46 45
18 11-4580042 6505 3277 4690362 7765 6493 3550 1943 4 19 0647 7116 3892 0982 8391 6124 4187 2566 4 20 1252 7726 4508 1603 9017 6756 4825 3229 4 21 1858 8336 5124 2224 9644 7388 5462 3872 3 22 2463 8947 5739 2845 4730270 8020 6099 4515 3 24 3674 4620168 6971 4083 1523 9283 7374 5801 3 25 4290 0779 7587 4709 2150 9916 8012 6445 3 26 4886 1390 823 5330 2777 4770548 8650 7088 3 28 6098 2612 9436 6673 4030 1813	16	8832	5285	2046	9120	6513	4230	2276	0658	44
19										43
20							6124			41
23	20					9017				40
23	21									39 38
25 4200 0779 7587 4709 2150 9916 8012 6445 320 2777 470548 8650 7088 3-27 5492 2001 8819 5952 3403 1180 9283 7732 3:2 366062 219436 6673 4030 1813 9926 8375 3:2 96704 3223 4660052 7195 4657 2445 4810564 9019 3:3 30 7310 3835 0669 7817 5284 3078 1202 9663 31 7916 4446 1285 8438 5912 3710 1840 11*4850307 2 9663 3443 2478 0951 32 8523 5058 1902 9060 6539 4343 2478 0951 2 34 11*4850307 2 362 11*569 2239 223 352 1902 9060 6539 4343 2478 0951 234 3443 2478 0951 <td< th=""><th>23</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>37</th></td<>	23									37
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1066	32	9766						5130224		28
36										27
37 3017 2211 1761 1675 1957 2616 8659 6092 239 39 4317 3623 3086 3011 3306 3978 5634 6480 2 40 4968 4180 3748 3680 3981 4659 5721 7174 2 41 5619 4836 4411 4348 4666 5340 6409 7869 1 42 6269 5493 5073 5017 5331 6022 7097 85631 4 43 6920 6150 5736 5686 6006 6703 7774 9257 1 44 7571 6807 6399 6355 6681 7385 8472 9952 1 46 8273 8121 7725 7693 8032 8749 9449 1341 1 47 9525 8778 8388 8362 8707 9430	34									26
37 3017 2211 1761 1675 1957 2616 8659 6092 239 39 4317 3623 3086 3011 3306 3978 5634 6480 2 40 4968 4180 3748 3680 3981 4659 5721 7174 2 41 5619 4836 4411 4348 4666 5340 6409 7869 1 42 6269 5493 5073 5017 5331 6022 7097 85631 4 43 6920 6150 5736 5686 6006 6703 7774 9257 1 44 7571 6807 6399 6355 6681 7385 8472 9952 1 46 8273 8121 7725 7693 8032 8749 9449 1341 1 47 9525 8778 8388 8362 8707 9430	36									24
38 3667 2867 2424 2343 2232 3297 4346 5786 22 40 4988 4180 3748 3680 3981 4659 5721 7174 2 41 5619 4836 4411 4348 4656 5340 6409 7869 1 42 6269 5493 5073 5017 5331 6022 7097 85631 1 43 6920 6150 5736 5686 6006 6703 7784 9257 1 44 7571 6807 6399 6355 6681 7385 8472 9952 1 45 8222 7464 7062 7024 7367 8066 9161 11*5180647 1 47 9825 8778 8388 8362 8707 9430 5140637 22431 1 225 2731 1 48 11*490176 9435 9051 <th>37</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>23</th>	37									23
39	38									22
41	39	4317	3523	3086	3011	3306	3978	5034	6480	21
42	40	4968	4180	3748	3680	3981	4659	5721	7174	20
43 6920 6150 5736 5686 6006 6703 7784 9257 1 44 76571 6807 6399 6355 6681 7385 8472 9952 1 45 8222 7464 7062 7024 7357 8066 9161 11:5180647 1 46 8873 8121 7725 7693 8032 8749 9849 1341 1 47 9525 8778 8388 8362 8707 9430 5140537 2036 1 48 11-490176 9435 9051 9032 9383 5100112 1225 2731 1 49 0750 498092 9715 9701 5060059 0794 1914 3426 1 50 1479 0750 4980378 5020371 0734 1476 2603 4122 1 51 2130 1407 1042 1041 1410 2158 3291 4817 1 52 2782 2065 1705 1710 2086 2241 3980 5513 1 53 3434 2723 2369 2380 2763 3523 4669 6208 5473 4038 3697 3720 4115 4888 6047 7600 56 5390 4696 4361 4390 4792 5571 6737 8296 567 6042 5354 5025 5061 5468 6254 7426 8992 568 6695 6013 5689 5731 6145 6937 8116 9688 569 7347 6671 6354 6402 6821 7620 8805 11:519088 60 7999 7329 7018 7072 7498 8304 495 1080 447 1080 1080 1080 1080 1080 1080 1080 108	41									19
Text			5493					7097	8563	18
46										17
46										16
47 9525 8778 8388 8362 8707 9430 5140537 2036 1 48 11·4900176 9435 9051 9032 9383 5100112 1225 2731 49 0627 4940092 9715 9701 5060059 0794 1914 3426 1 50 1479 0750 4980378 5020371 0734 1476 2603 4122 1 51 2130 1407 1042 1041 1410 2158 3291 4817 52 2782 2065 1705 1710 2086 2841 3990 5513 53 3434 2723 2369 2380 2763 3523 4669 6208 54 4086 3380 3033 3050 3439 4206 5358 6904 55 4738 4038 3697 3720 4115 4888 6047 7600 56 5390 4566 4361 4390 4792 5571							6066			15 14
48 11-4900176 9435 9051 9032 9383 5100112 1225 2731 1 50 1479 0750 4980378 5020371 0734 1476 2603 4122 51 2130 1407 1042 1041 1410 2158 3291 4617 52 2762 2065 1705 1710 2086 2841 3960 5513 53 3434 2723 2369 2380 2763 3523 4669 6208 54 4086 3380 3033 3050 3439 4206 5358 6904 55 4738 4038 3697 3720 4115 4888 6047 7600 56 5390 4696 4361 4390 4792 5571 6737 8296 57 6042 5354 5025 5061 5468 6254 7426 3992 58 6695 6013 5689 5731 6145 6937 8116 9688 59 7347 6671 6354 6402 6621 7620 8805 11*5190384 60 7999 7329 7018 <t< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th>0/20</th><th></th><th></th><th>13</th></t<>							0/20			13
49 0827 4940092 9715 9701 5060059 0794 1914 3426 1 50 1479 0750 4980378 5020371 0734 1476 2603 4122 1 51 2130 1407 1042 1041 1410 2158 3291 4617 52 2762 2065 1705 1710 2086 2841 3990 5513 53 3434 2723 2369 2380 2763 3523 4669 608 54 4066 3380 3033 3050 3439 4206 5358 6904 55 4738 4038 3697 3720 4115 4888 6047 7600 56 5390 4696 4361 4390 4792 5571 6737 8296 57 6042 5354 5025 5061 5468 6254 7426 8992 58 6695 <										12
50 1479 0750 4980378 5020371 0734 1476 2603 4122 1 51 2130 1407 1042 1041 1410 2158 3291 4817 52 2782 2065 1705 1710 2096 2841 3990 5513 53 3434 2723 2369 2380 2763 3523 4669 6208 54 4086 3380 3033 3050 3439 4206 5358 6904 55 4738 4038 3697 3720 4115 4888 6047 7600 56 5390 4696 4361 4390 4792 5571 6737 8296 57 6042 5354 5025 5061 5468 6254 7426 8992 58 6696 6013 5689 5731 6145 6937 8116 9688 59 7347 6671 <td< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>11</th></td<>										11
51 2130 1407 1042 1041 1410 2158 3291 4817 52 2782 2065 1705 1710 2086 2841 3990 5513 53 3434 2723 2369 2380 2763 3523 4669 6208 54 4086 3380 3033 3050 3439 4206 5358 6904 55 4738 4038 3697 3720 4115 4888 6047 7600 56 5390 4696 4361 4390 4792 5571 6737 8296 57 6042 5354 5025 5061 5468 6254 7426 8992 58 6695 6013 5689 5731 6145 6937 8116 9688 59 7347 6671 6354 6402 6821 7620 8805 11·5190384 60 7999 7329 7018	50	1470		4980378	5020371	0734				10
52 2782 2065 1706 1710 2086 2841 3990 5513 53 3434 2723 2369 2380 2763 3523 4669 6208 54 4086 3380 3033 3050 3439 4206 5358 6904 55 4738 4038 3697 3720 4115 4898 6047 7600 56 5390 4696 4361 4390 4792 5571 6737 8296 57 6042 5354 5025 5061 5468 6254 7426 3992 58 6695 6013 5689 5731 6145 6937 8116 9688 59 7347 6671 6354 6402 6621 7620 8805 11*519384 60 7999 7329 7018 7072 7498 8304 9495 1080 " 51' 50' 49' 4	51					1410				9
54 4096 3380 3033 3050 3439 4206 5358 6904 55 4738 4038 3697 3720 4115 4888 6047 7600 56 5390 4696 4361 4390 4792 5571 6737 8296 57 6042 5354 5025 5061 5468 6254 7426 8992 58 6695 6013 5689 5731 6145 6937 8116 9688 59 7347 6671 6354 6402 6821 7620 8805 11:5190384 60 7999 7329 7018 7072 7498 8304 9495 1080 4'' 51' 50' 49' 48' 47' 46' 45' 44'	52	2782	2065	1705	1710	2086	2841	3980		8
55 4738 4038 3697 3720 4115 4888 6047 7600 56 5390 4696 4361 4390 4792 5571 6737 8296 57 6042 5354 5025 5061 5468 6254 7426 8992 58 6695 6013 5689 5731 6145 6937 8116 9688 59 7347 6671 6354 6402 6821 7620 8805 11*5190384 60 7999 7329 7018 7072 7498 8304 9495 1080 " 51' 50' 49' 48' 47' 46' 45' 44'										7
56 5390 4696 4361 4390 4792 5571 6737 8296 57 6042 5354 5025 5061 5468 6254 7426 8992 58 6695 6013 5689 5731 6145 6937 8116 9688 59 7347 6671 6354 6402 6821 7620 8805 11*5190384 60 7999 7329 7018 7072 7498 8304 9495 1080 " 51' 50' 49' 48' 47' 46' 45' 44'										6
67 6042 5354 5025 5061 5468 6254 7426 8992 58 6695 6013 5689 5731 6145 6937 8116 9688 59 7347 6671 6354 6402 6821 7620 8805 11·5190384 60 7999 7329 7018 7072 7498 8304 9495 1080 " 51' 50' 49' 48' 47' 46' 45' 44'	P.C									5
58 6695 6013 5689 5731 6145 6937 8116 9688 59 7347 6671 6354 6402 6821 7620 8805 11·5190384 60 7999 7329 7018 7072 7498 8304 9495 1080 " 51' 50' 49' 48' 47' 46' 45' 44'	50 57									3
59 7347 6671 6354 6402 6821 7620 8805 11·5190384 60 7999 7329 7018 7072 7498 8304 9495 1080 " 51' 50' 49' 48' 47' 46' 45' 44'										2
60 7999 7329 7018 7072 7498 8304 9495 1080 7072 48′ 47′ 46′ 45′ 44′										ĩ
" 51' 50' 49' 48' 47' 46' 45' 44' '				7018	7072	7498	8304	9495	1080	0
	"	51'	50′	49'	48'			45'	44'	"
LOG. COTAN. 1°.				1	LOG. CO	TAN. 1	۰.			

13	134 LOG. SINE 88°.								н.
11	16'	17'	18'	19'	20'	21'	22'	23′	"
0	9-9998012	9998050	.8808666	9998125	9998162	9998199	9998235	9-9998271	60
1	13	2 51	图 89	26	<u>∞</u> 63	₾ 99	œ 36	72	59
2	14	52	89	27	64	9998200	36	72	58
3	14 15	52 53	90 91	27 26	64 65	01 01	37 38	73	67
5	16	54	91	28	65	02	38	73 74	56 55
6	16	54	92	29	66	03	39	75	54
7	17	55	92	30	67	03	39	75	53
8	17	55	93	30	67	04	40	76	52
9	9-9998018	9999056	9998094	9998131	19998168	9998204	9998241	9.9998276	51
10	19	57	94	32	68	05	41	77	50
11	19	57	95	32	69	06	42	77	49
12	20	58	96	33	70	06	42	78	48
13	21 21	59 59	96 97	33 34	70 71	07 07	43	79	47
14	22	60	97	35	72	08	44	79 90	46
15	23	60	98	35	72	09	45	80	44
17	23	61	99	36	73	09	45	61	43
18	2	62	99	37	73	10	46	82	42
19	9-9998024	9998062	9998100	9998137	9998174	9998210	9998246	9-9998282	41
20	25	63	01	38	75	11	47	93	40
21	26	64	01	38	75	12	48	83	39
22	26	64	02	39	76	12	48	84	38
23	27	65	02	40	76	13	49	85	37
24	28	66	03	40	77	13	49	85	36
25	28 29	66	04	41	78	14	50	86	35
26 27	30	67 67	05	42	78 79	15 15	51 51	86 87	33
28	30	69	06	43	79	16	52	88	32
29	9-9998031	-9998069	9998106	9998143	9998180	9998216	9998252	9-9998288	31
30	31	69	07	44	81	17	53	89	30
31	32	70	07	45	81	18	54	89	29
32	33	71	08	45	82	18	54	90	28
33	33	71	09	46	82	19	55	91	27
34	34	72	09	46	83	19	55	91	26
35	35	72	10	47	84	20	56	92	25 24
36	35	73	11 11	48	84	21 21	57 57	92	23
37	36 36	74 74	12	49	85 86	21	58	93 93	22
39	9-9998037	9998075	9998112	9998149	·9998136	9998222	9998258	9-9998294	21
40	38	76	13	50	87	23	59	95	20
41	38	76	14	16	87	24	60	95	19
42	39	77	14	Ďi.	88	24	60	96	18
43	40	77	15	52	89	25	61	96	17
44	40	78	15	53	89	25	61	97	16
45	41	79	16	53	90	26	62	98	15
46	42	79	17	54	90	27	63	98	14
47	42	80	17	54	91 92	27 28	63	99	13 12
48	9-9998043	9998081	·9998119	9998156	-9998192	9998229	9998264	9-9998300	11
50	44	9990001	19	56	93	29	65	01	10
51	45	82	20	57	93	30	66	oil	9
52	45	83	20	57	94	30	66	02	8
53	46	84	21	58	95	31	67	02	7
54	47	84	22	59	95	32	67	03	7 6 5
55	47	85	22	59	96	32	68	03	6
56	48	86	23	- 60	96	33	69	04	4
57	49	86	24	60	97	33	69	05	3
58	0.000000	-nnnooo-	24	.0000169	-0000100	-0000000	10000070	05000000	3 2 1
59 60	9-9998050 50	·9998087	·9998125 25	-9998162 62	-9998198 99	-9998235 35	·9998270 71	9-9998306	0
00	43'	42	41	40	39,99	38'	37'	36'	"
,	10 1	12.0	71		RINE ID.	00	01	00	

Ta	ble n.]	-		LOG. TA	N. 88°.				135
"	16'	17'	18'	19'	20'	21'	22'	23'	11
0	11.5191080			5318275	6361514	5405186	5449301	11:5493869	60
1	1777	→ 3770	→ 6173	₩ 8992			5450040	4615	59
3	2473	4473	6883	9710		6649	-0780	6362	58
	3170	5177		5320427	3687	7381	1519	6109	57
4	3867	5880	8304	1145		8113	2258	6856	56
- 6	4564	6584	9014	1862	5136	8845	2998	7603	55
6	5261	7289	9725	2580	5B61	9578	3736	8351	64
7	5958	7992		3298		5410310	4477	9098	53
8	6655	8696	1147	4016		1042	5217	9846	62
9	7352	9400	1858	4734	8037	1775	5957	11.920028	51
10		5240104	2569	5452		2508	6698	1341	50
11	8748	0908	3280			3240	7438	2089	49
12	9445	1513	3991		5370213	3973	8178	2837	48
13	11-5200143	2217	4703	7607	0939	4707	8919	3586	47
14	0941	2922	5414	8326		5440	9660	4334	46
15	1539	3627	6126	9045			5460401	5082	45
16	2237	4332	6835	9764	3117	6906	1141	5931	44
17	2935 3634	5037 5742		5330483		7640	1883	6590	43
19	4332	6447	8262 8974	1202 1921	4569 5296	9374 9108	2624 3365	7329 9077	41
		-							
20	5031	7153	9687	2640		9842	4107	9927	40
21	5729	7858	5290399	3360		5420576	4948	9576	39
22	6428	8564	1112	4079	7476	1310		11.5510325	39
23	7127	9270	1824	4799	8203	2044	6332	1075	37
25	7826	9975 5250681	2537	6519	8930	2779	7074	1924 2574	36
26	9225	1388	3250	6239	9657 5380385	3513 4248	7816 8558	3324	34
27	9924	2094	3963 4676	6959 7679	1112	4983	9300	4074	33
28	11.5210624	2800	5389	9400	1840	5718		4824	32
29	1323	3506	6103	9120	2567	6453	0785	5574	31
30	2023	100							
31	2023	4213	6816	9841	3295	7188	1528	6325	30 29
32	3423	4920 5626		5340561	4023	7923	2271	7075 7826	29
33	4123	6333	8244 8957	1282 2003	4751 5479	9659 9394	3014 3757	8577	27
34	4823	7040	9671	2724		5430130	4500	9328	26
35	5523	7747	5300385	3445	6936	0866	5243	11.5520079	25
36	6224	8455	1100	4167	7664	1602	5987	0830	24
37	6924	9162	1814	4888	8393	2338	6731	1581	23
38	7625	9969	2528	5610	9122	3074	7474	2333	22
39	8325	5260577	3243	6331	9851	3810	8218	3084)	21
40	9026	1285	3957		5390590	4547	5962	3836	20
41	9727	1992	4672	7775	1309	5283	9706	4588	19
42	11.5220428	2700	5387	8497	2039		5480451	5340	18
43	1129	3408	6102	9219	2769	6757	1195	6092	17
44	1831	4116	6817	9941	3497	7494	1939	6844	16
45	2532	4825	7532	5350664	4227	8231	2684	7596	15
46	3234	5533	8248	1386	4957	8968	3429	6349	14
47	3935	6242	8963	2109	5696	9705	4174	9102	13
48	4637	6950	9679	2832	6416	5440442	4919	9854	12
49	5339	7659	5310395	3554	7147	1180	5664	11.5530607	11
50	6041	8368	1110	4277	7877	1918	6409	1360	10
51	6743	9077	1826	5000		2656	7154	2113	9
52	7445	9786	2542	5724	9338	3393	7900		8
53	8147		3259	6447		4132	8646		7
54	8850		3975	7170		4870	9391	4373	6
55	9552		4691	7894			5490137	5127	5
66	11.5230255			8618		6346	0883		4
57	0959			9341	2992		1629		3
58 59	1661	4043		5360065			2376		3 2
60	2364 3067	4752 5462				8562	3122		0
11	43	42	8275		5196 39'	9301	3B69 37'	8897 36'	0
	1 30	10		40'	-		01'	20.	
				LDG, CO	TAN. 1º				

13	6			Log.	SINE 88	3.		[Table	n.
"	24'	25	26'	27'	28'	29'	30'	31'	"
0	9-9998306	9998342	9998376	9998411	9998445	9998478	9999512		60
1	07	O 42	3 77	a 11	co 45	₱ 79	D 12		59
2	08	43	77	12	46	79	13		58
3	0B	43 44	78	12 13	46	80	13	46	57
4	09 09	44	79 79	13	47	81	14 14	47	56 55
6	10	45	80	14	48	82	15	48	54
7	ii	46	80	15	49	82	15	48	53
8	îi	46	81	15	49	83	16	49	52
9	12	47	81	16	50	83	16	49	51
10	9 9998312	9998347	9996382	9998416	-9998450	9998484	9998517	9-9998550	50
11	13	48	83	17	51	84	18	50	49
12	13	49	83	17	51	85	18	51	48
13	14	49	94	18	52	85	19	52	47
14	15	60	84	19	53	86	19	52	46
15	15	50	85	19	53	87	20	53	45
16	16	51	85	20	54	87	20	53	44
17	16	51	86	20	54	88	21	54	43
18	17	52	87	21	55	88	21	54	42
19	18	53	87	21	55	89	22	55	41
20	9-9998318	9998353	9998388	9998422	9998456	9998489	9998523		40
21	19	54	88	23	56	90	23	56	39
22	19	54	89	23	57	91	24	56	38
23	20 21	55 55	89	24	58	91	24 25	57	37 36
24	21	56	90 91	24 25	58 59	92 92	25	57	35
25 26	22	57	91	25	59	93	26	58 59	34
27	22	57	92	26	60	93	26	59	33
28	23	58	92	27	60	94	27	60	32
29	23	58	93	27	61	941	- 27	60	31
30	9-9998324	9998359	9998393	9998428	9998461	9998495		9-9998561	30
31	25	60	94	28	62	95	29	61	29
32	25	60	95	29	63	96	29	62	28
33	26	61	95	29	63	97	30	62	27
34	26	61	96	30	64	97	30	63	26
35	27	62	96	31	64	98	31	63	25
36	28	62	97	31	65	98	31	64	24
37	28	63	97	32	65	99	32	65	23
38	29	64	98	32	66	99	32	65	22 21
39	29	64	99	33	67	9998500	33	66	
40		9998365	9998399	9998433	9998467	9998500	9998533	9-9993566	20
41	30	65	9999400	34	68	01	34	67	19
42	31	66	00	34	68	02	35	- 67	18
43	32 32	66 67	01 01	35 36	69 69	02 03	35 36	68 68	17 16
45	33	69	02	36	70	03	36	69	15
46	33	68	03	37	70	04	37	69	14
47	34	69	03	37	71	04	37	70	13
48	35	69	04	39	72	05	38	70	12
49	35	70	04	38	72	05	38	71	ii
50	9-9996336	9998370	9998405	9998439	9998473	9998506	9998539		10
51	36	71	05	40	73	07	40	72	
52	37	72	06	40	74	07	40	73	9 8 7
53	37	72	07	41	74	08	41	73	7
54	38	73	07	41	75	08	41	74	6
55	39	73	08	42	75	09	42	74	5
56	39	74	08	42	76	D9	42	75	4
57	40	75	09	43		10	43		3
58	40	75	09	44		10			2
	41	76	10	44	78	11	44	76	1
69		-							
69 60	42	76 34'	33'	32,45	31,78	30,12	29/	28' 77	0

Ta	ble 11.]			1	LOG. TA	n. 88°.				37
7,	24	1	25'	26'	27'	28'	29'	30′	31'	"
0	11.5538				5676850	5723824	5771310	5819321	11.5867868	60
1		652	<u>-</u> 5159	<u>-</u> 1148	≟ 7628	≟ 4611		5820126	8682	59
2	11.5540		5922	1919	9407	5398	2902	⇒ 0931	9496	58
3		161	6685	2690	9186	6186	3698	2541	11.5870310	57 56
4		1916	7447	3460 4232	9966	6973	4495 5291	3346	1124 1938	55
5 6		2671 3426	8210 8973	5003	5680745 1524	7761 8549	6088	4152	2753	54
7		1181	• 9737	5774	2304	9337	6884	4957	3568	53
8	1 2	937	5590500	6545	3084	5730125	7681	5763	4382	52
9		692	1263	7317	3864	0914	8478	6569	5197	51
10	1	3448	2027	8089	4644	1702	9275	7375	6012	50
ii		7203	2791	8861	5424	2491	5780073	8181	6828	49
12		7959	3554	9633	6204	3280	0870	8988	7643	48
13		3715		5640405	6984	4068	1668	9794	9459	47
14		471	5082	1177	7765	4859		5830601	9274	46
15	11.5550	228	5847	1949	8546	5647	3264		11.5880090	45
16		0984	6611	2722	9327	6436	4062	2214	0906	44
17		1741	7376	3494	5690108	7226	4860	3021	1722	43
18		2497	8140	4267	0889	8015	5658	3829	2539	42
19		3254	8905	5040	1670	8805	6457	4636	3355	41
20		1011	9670	5813	2451	9595	7255	5444	4172	40
21			5600435	6587		5740385	8054	6251	4989	39
22		5525	1200	7360	4015	1175	8853	7059	5806	38
23		6283	1966	8133	4796	1966	9652	7867	6623	37
24		7040	2731	8907	5578	2756	5790451	8675	7440	36
25		7798	3497	9681	6361	3547	1251	9483	8257	35
26		3556		5 650455	7143	4338		5840292	9075	34
27 28		9313	5028	1229	7925 8708	5128 5920	2850 3650	1100	9893	32
29	11.556	0829	5794 6560	2003 2777	9490	6711	4450	2718	11·5890710 1528	31
30		1588	7327	3552	5700273	7502	5250	3527	2347	30
31 32		2346	8093 8860	4326 5101	1056 1839	8294 9085	6050 6850	4336	3165 3983	29
33		3105 3863	9626	5876	2623	9877	7651	5146 5955	4802	27
34			5610393	6651	3406		8451	6765	5621	26
35		5381	1160	7426	4189	1461	9252	7575	6440	25
36		6140	1927	8201	4973		5800053	8384	7259	24
37		6899	2694	8977	5757	3046		9195	9078	23
38	l '	7659	3462	9752	6541	3838	1656	5850005	8897	22
39	1 1	8418	4229	5660528	7325	4631	2457	0815	9717	21
40	1	9178	4997	1304	8109	5424	3259	1626	11.5900537	20
41		9937	5765		8894	6217		2436	1357	19
42	11.557	0697	6532	2956	9678	7010	4962	3247	2177	18
43		1457	7300	3632	5710463	7803	5664	4058		17
44		2217	8069		1248			4869		16
45		2977	8837	5185					4638	15
46		3739	9605	5962		5760184		6492		14
47 48		4498		6739			8874			13
49		5259 6020	1143	7516 8293			9677	8115	7100 792 1	12 11
	1		1911							
50		6781	2680							10
51 52		7542 83 03	3450	9847 5670625						9
53		83 03 9064	4219						11. 5 910385 1207	8 7 6
54		9004 9826	5758							6
55	11.558		6527							5
56		1349								4
57		2111	8067				6908			3
58	1	2873	8837				7712	6241		2
59	1	3635	9607	6071	3037	5770515	8517	7055	6141	3 2 1 0
60		4397	5630378						6963	
"	35	1	34'	33′	32′	31'	30′	29′	28′	"
1					LOG. CO	TAN. 1	٠.			

13	8			LOG. SI	NE 88º.			[Table	n.
77	32'	33'	34'	35'	36'	37'	38'	39'	10
0	9.9998577	9998609	9998641	9998672 73	9998703	9998734	9998764	9-9998794	60
1 2	77	n 10	9 41 42	73	04 04	35 35	65 65	95 95	59
3	79	11	42	74	05	36	66	96	57
4	79	11	43	74	05	36	66	96	56
5	80	12	44	75	06	37	67	97	55
6	80 91	12 13	44	75 76	07 07	37 38	67 68	97 98	54
7	. 81	13	45	76	08	38	68	98	52
9	9-9998582	9998614	9998646	-9998677	9998708	9998739	9998769	9.9998799	51
10	62	14	46	78	09	39	69	99	50
11	93 83	15	47	78 79	09 10	40 40	70 70	9-9998800	49
12 13	84	16 16	47	79	10	41	71	01	47
14	84	17	48	90	11	41	71	01	46
15	85	17	49	80	11	42	72	02	45
16	86	18	49	81	12	42	72	02	44
17	86	18	50	81	12	43	73	03	43
18	0-0000507	-0000010	9998651	9998682	13	·9998744	9996774	9·9998804	42
19 20	9-9998587	-9998619 20		9998082	-9998713 14	9998744	'9996774 74	9-9998604	41
21	88	20	51 52	83	14	45	75	05	39
22	89	21	52	64	15	45	75	06	38
23	89	21 22	53	84	15	46	76	06	37
24	90	22	54	85	16	46	76	06	36
25	90	22	54	85	16	47	77	07	35
26	91	23 23	55	86	17	47.	77	07 08	34 33
27 28	910	24	55 56	96 87	17 18	49	78 78	08	32
29	9-9998593	9999625	9998656	-9998687	9998718	9998749	-9998779	9.9998809	31
30	93	25	57	88	19	49	79	09	30
31	94	26	57	88	19	50	80	10	29
32	94	26	58	89	20	50	80	10	28
33	95 95	27 27	58	89 90	20 21	51 51	81 81	11	27 26
34 35	96	28	59 59	90	21	52	82	12	25
36	96	28	60	91	22	52	82	12	24
37	97	29	60	92	22	53	83	13	23
38	97	29	61	92	23	53	83	13	22
39	9-9998598	9998630	9998661	9998693	9998723	9998754	-9998784	9-9998814	21
40	98	30	62	93	24	54	84	14	20
41	99 9-9998600	31 31	62 63	94 94	24 25	55 55	85 85	15 15	19
43	9 9996600	32	63	95	25	56	86	16	17
44	01	32	64	95	26	56	86	16	16
45	10	33	65	96	26	57	87	17	15
46	02	34	65	96	27	57	87	17	14
47	02 03	34. 35	66	97	27	58	88	18	13 12
49	9-9998603	9998635	-9998667	97 •9998698	28 9998728	·9998759	·9998789	18 9·9998819	11
50	04	36					9990103	19	10
51	04	36	67 68	98 99	29 30	59 60	90	20	9
52	05	37	68	99	30	60	90	20	8
53	05	37	69	9998700	31	61	91	21	7
54	06	38	69	00	31	61	91	21	6
55	06	38	70	01	32	62.	92	21	5
56	07	39	70	01	32	62	92	22 22	3
57 58	09 08	39 40	71 71	.02	33	63 63	93 93	23	2
59	9-9998669	9998640	9998672	9996703	9998734	9998764		9-9998823	î
60	09	41	72	03	34	64	94	24	0
79	27'	26'	25'	24'	23'	22'	21'	20'	"
				LOG. COS	SINE 10.				

1	Cal	le	n.]		1	LOG. TA	N. 88°.				135
	13		32'	33'	34'	35/	36'	37'	38/	39'	11
П	0	11	5916963	5966619		6067664		6171114	6223777	11.6277085	60
	I	B	7786			⇒ 8516	9944	≟ 1986	± 4660	7979	59
ш	2 3		8609				6120906		5543	8973	58
ш		и.	9433	9117		6070221		3732	6426	9768	57
	4 5	11	5920256		6020218	1073		4605	7310	11 6280662	56
	5		1080		1060	1926		5478	8194	1557	55
ш	6	13,	1903	1616		2779		6352	9078	2452	54
	7		2727	2449	2746	3632		7225	9962	3347	53
	9		3551	3283		4495	5983		6230847	4242	52
ш			4376	4116	4433	5338	6847	8973		5139	51
	10	1	5200	4950				9847	2616	6033	50
	11		6025	5784	6120	7045		6180721	3501	6929	49
Ш	2		6849	6619	6964	7899		1596	4386	7825	48
	13		7674	7453	7806		6130302	2470	5271	8722	47
	4	1	8499	8287	8652	9607	1167	3345	6157	9618 11:6290515	46
	6	21.	9324 5930150	9122		6080462		4220		1411	45
	7	TI		5980792	6030341 1186	1316 2171	2896 3761	5095 5970	7928 8814	2308	43
	18		1801	1627	2031	3026		6846	9701	3206	42
	9		2626	2462	2876	3981	5491		6240567	4103	41
			3452	3299						5001	40
	00					4736		8597	1473		
1 3	1 2		4278 5105	4133 4969	4566 5412	5591 6447	7222 8088	9473 6190350	2360 3247	5898 6796	39
	3		5931	5805	6258	7303		1226	4134	7694	37
	14		6758	6641	7103	8158		2102	5021	8593	36
	5	р.	7584	7477	7950		6140686	2979	5909	9491	35
	26		8411	B314	8796	9871	1552	3856		11.6300390	34
	7		9238	9150		6090727	2419	4733	7684	1289	33
	18	11	5940065		6040489	1583		5610	8572	2188	32
1 2	9		0693	5990824	1335	2440		6488	9461	3087	31 .
	10		1720	1661	2192	3297	5020	7366	6250349	3986	30
	ĩ		2548	2498		4154		8243	1238	4886	29
	2		3376	3336		5011		9121	2126	5785	28
	3		4204	4173	4724	5869		9999	3016	6685	27
	4		5032	5011	5571	6726			3904	7586	26
	5		5860	5849	6419	7584	9358	1756	4794	8486	25
	6	н	6689	6697.	7267	8442	6150226	2635	5683	9386	24
	7		7517	7525	8115	9300		3514	6573	11.6310287	23
	8	-	8346	8363				4393	7462	1188	22
3	9	1	9175	9202	9811	1016	2832	5272	8353	2089	21
	0	11	5950004			1875	3701	6151	9243	2990	20
	1		0833	0879		2734	4570		6260133	3892	19
	2	4	1663	1718		3592		7911	1024	4793	18
	3 .	+	2492	2558		4452		8791	1914	5695	17
	4	4	3322	3397	4055	5311	7178	9671	2806	6597	16
	5		4152	4236	4905	6170		6210551	3696	7499	15
	6		4982	5076	5754	7030		1431	4589	8402	14
	7		5812 6642	5916 6756	6604 7454	7989	9787 6160658	2312 3193	6371	9304 11:6320207	12
	9	1	7473	7596	B304	9609	1528	4074	7263	1110	
	- 1	1					-				
	0		8304	8436		6110470	2399	4955	8155	2013	10
	I		9134		6060004	1330		5836 6718	9047 9939	2917 3520	9
	2	11.	5960797	6010117 0958	0955 1705	2191 3051	4140 5011	7600	6270832	4724	7
	4	TT.	1628	1799		3912	5883	B481	1725	5628	6
	5		2459	2640	3407	4773	6754	9364	2617	6532	5
	6		3291	3481	4259	5635		6220246	3511	7436	4
	7		4123	4323	5109	6496	8497	1128	4404	B340	3
	8		4955	5165	5961	7358	9369	2011	5297	9245	2
	9		5787	6006	6913		6170242	2894		11.6330150	1
	0		6619	6849	7664	9082	1114	3777	7085	1055	0
11	4		27'	26'	25'	24'	23'	22'	21'	20'	1,
					1	og. co:	TAN. 10				ě

14	[Table	n.							
"	40′	41'	42′	43′	44'	45'	46′	47'	"
0	9·9998824 24	9998853 54	-9998882 ග 83	9998911	-9998939	9998966 9 67	-9998994 ന 94	9 -999902 1 21	60
1 2	25	54	83	ი 11 11	40	67	95	22	58
3	25 25 26 26	55	83 83	12	40	68	96	22	57
4	26	55	84	12 13	40	68	96	23	56
5	26	56 56	84 85	13 13	41 41	69 69	96	23 23	55
6	27 27	57	85	13	42	70	96 97	24	54 53
8	28	57	86	14	42	70	97	24	52
9	9-9996828	9998858	9998886	9999915	9998943	9998971	9998998	9-9999025	51
10	29	58	87	15	43	71	98	25	50
11	29 29 30 30	58 59	87	16	44	71	99	26	49
12	30	59	88 88	16	44	72	99	26	48
13 14	30 31	59	89	17 17	45 45	72 73	9999000	27 27	47 46
15	31	60 60	. 89	18	46	73	01	27	45
16	32	61 61 62	90 90 90	18	46	74	01	28	44
17	32	61	~ 90	19	47	74	01	28	43
18	9-9998833	9998862	91 • 9998 991	19	47 •9998947	75 -99 98 975	02 -9999002	27 28 28 29 9-9999029	42
19				·9998919		***************************************		9-9999029	41
20 21	34 34	63 63	92 92	20 20	48 48	76 76	03	30	40
22	35	64	93	20	49	76	04	30 31	39 36 37 36 35
23	35	64	93	21 21 22 22 23 23	49	77	04	31	37
24	36	65	93	22	50.	77	05	31 31 32 32	36
25	36	65	94	22	50	78	05	32	35
26	36 37 37	65 65 66 66 67	94 95	23	51 51	78	06 06	32	34 33 32
27 28	38	67	95 95	23	52	79 79	06	33 33	33
29	9.9998838	9998867	·9998896	9998924	-9998952	9998980	9999007	9-9999034	31
30	39	68	96	25	53	80	07	34	30
31	39	68 68	97	25	2.3	81	08	35	29
32	40	69	97	25 26 26	53	81	08	35 35 35	29 28 27 26 25 24
33	40	69	98	26	54	81	09	35	27
34 35	41 41	70 70	98 99	26 27	54 55	82 82	09 10	36 36	26
36	42	71	99	27 27	55	83	iŏ	37	20
37	42	71	9998900	28 28	56	83	10	37	23
38	42	71	00	28	56	84	11	38	23 22
39	9.9999843	9998872	9998901	-9998929	•9998957	9998984	9999011	9-9999038	21
40	43	72	01	29	57	85	12	39	20
41 42	44 44	73 73	02 02	30 30	58	85 86	12 13	39	19
43	44	74	02	31	58 59	86	13	39 40	18 17
44	45	74	03	31	59	86	14	40	16
45	46	75	03	32 32	59	87	14	41	15
46	46	75	04	32	60	87	14	41	14
47 48	47	76 76	04	33	60 61	88	15 15		13
48	9-9998848	-9998877	9998905	-9998933	-9998961	-9998989	9999016		12 11
50	48	77	06	34	62	89	16	10 00000	10
51	49		06	34	62				9
52	49	78	07	35	63	90	17	44	8
53	50		07	35			18	44	7
54 55	50	79 80			64 64	91 91	18		6
56	51 51				65				5
57	52		09		65	92	19		3
58	52	81	10	38	65	93	20	47	2
59	9.9998853		9998910					10 00000-	1
60	19, 53	18,82	17'	16,39	15' 66		13′		0,
	13	. 19.	17	16'		14'	1 13'	12′	۱"
L				LOG. CO	SINE 1º	•			

Tak	ble n.]			LOG.	TAN. 8	80.			141
11	40'	417	42'	43'	44'	45'	46'	47'	11
0	11.6331055							11:6728857	60
1	1960						6670729	9849	59
3	2865	7537	2904	8986		3368			68
3	3771	8454	3933	9927	6754	4334	2687	1834	57
4	4677	9371		6500968	7708	5300		2827	56
6	6583		5691	1909		6267	4646	3819	55
7	6489	1206	6621	2751	9615	7233	5625	4812	54
8	7395 8302	2124 3042	7550		6560569	6200	6605	5806	53
9	9208	3960	8480 9410	4635		9167	7585	6799	52
				5577		6620134	6566	7793	51
10	11-6340115		6450340	6619		1102	9546	8767	50
11	1022	5797	1271	7461	4388		6680527	9781	49
12	1930	6716	2201	8404	5343	3037		11-6740776	48
13	2837	7635	3132		6299	4006	2489	1770	47
14	3745	8554		6510290		4974	3471	2765	46
15	4653	9473	4994	1233	8209		4452	3760	45
16	5561		5926	2177	9165	6911	5434	4756	44
17	6469		6857		6570122	7890	6416	5751	43
18	7377	2233	7789	4064	1078	8849		6747	42
19	8286		8721	5009		9819	E381	7743	41
20	9195	4073	9653	5953	2991	6630788	9364	8740	40
21	11.6350104		6460586	6897	3948	1758	6690347	9736	39
22	1013	5914	1518					11.6750733	38
23	1922	6835	2451	8787		369B	2313	1730	37
24	2832		3384	9732		4669	3297	2727	36
25	3742	8678	4317			5639	4281	3724	36
26	4652	9599	5250	1623		6610	5265	4722	34
27		6410521	6184	2569		7581	6249	5720	33
28	6472	1443	7118			8553	7234	6718	32
29	7393	2365	8052	4461	1612	9524	8219	7716	31
30	8293	3287	8986	5408	2571	6640496	9204	8715	30
31	9204	4210	9920	6354			6700189	9714	29
32	111.6360115	5132	6470955	7301	4489	2440	1174		28
33	1026	6055	1790	8248	5449	3413	2160	1712	27
34	1938	6978	2725	9195		4385	3146	2711	26
35	2850	7902	3660	6530143		5358	4132	3711	25
36	3761	9825	4595	1090		6331	5118	4711	24
37	4673	9749	5531	2038		7305	6105	5711	23
38		6420673	6467	2986		8278	7092	6712	22
39	6498	1597	7403	3934	1211	9252	8079	7712	21
40	7411	2521	8339	4883	2172	6650226	9066	9713	20
41	8324	3445	9275		3133		6710053	9714	19
42	9237		6480212	6780	4094	2174	1041		18
43	11.6370150	5295	1149	7729	5056	3149	2029	1717	17
44	1063	6220	2086	8679			3017	2719	16
45	1977	7145	3023	9628	6980		4005	3721	15
46	9000	8071	3960			6074	4994	4723	14
	2890		1200	1528	8905	7050	5983	5726	13
47	3804	8996	4898			# 1/CD/			
47 48	3804 4719	9922	5836	2478	9868	8025	6972	6728	12
47	3804 4719				9868			6728 7731	12
47 48	3804 4719	9922 6430848	5836 6774	2478 3428	9868 6600831	9025 9001	6972 7961	7731	12
47 48 49	3804 4719 5633	9922	5836 6774 7712	2478 3428 4379	9868 6600831 1794	9025 9001 9977	6972 7961 9950	7731 8734	12 11 10
47 48 49 50	3804 4719 5633 6547	9922 6430848 1774	5836 6774 7712 8650	2478 3428 4379 5329	9868 6600831 1794 2757	9025 9001 9977 6660954	6972 7961 9950 9940	7731 8734 9739	12 11 10
47 48 49 50 51	3804 4719 5633 6547 7462	9922 6430848 1774 2701 3627	5836 6774 7712 8650 9589	2478 3428 4379	9868 6600831 1794 2757	9025 9001 9977 6660954	6972 7961 9950	7731 8734 9739 11:6780741	12 11 10 9
47 48 49 50 51 52	3804 4719 5633 6547 7462 8377	9922 6430848 1774 2701 3627	5836 6774 7712 8650	2478 3428 4379 5329 6280 7231	9868 6600831 1794 2757 3721 4684	8025 9001 9977 6660954 1930 2907	6972 7961 9950 9940 6720930 1920	7731 8734 9739 11-6780741 1745	12 11 10 9
47 48 49 50 51 52 53 54 55	3804 4719 5633 6547 7462 8377, 9292	9922 6430848 1774 2701 3627 4554	5836 6774 7712 8650 9589 6490528 1467	2478 3428 4379 5329 6280 7231 8183	9868 6600831 1794 2757 3721 4684 5649	8025 9001 9977 6660954 1930 2907 3984	6972 7961 9950 9940 6720930 1920 2910	7731 8734 9739 11-6780741 1745 2749	12 11 10 9 8 7
47 48 49 50 51 52 53 54	3804 4719 5633 6547 7462 8377 9292 11-6380207	9922 6430848 1774 2701 3627 4554 5481 6408	5836 6774 7712 8650 9589 6490528 1467 2406	2478 3428 4379 5329 6280 7231 8183 9134	9868 6600831 1794 2757 3721 4684 5649 6613	8025 9001 9977 6660954 1930 2907 3984 4861	6972 7961 9950 9940 6720930 1920 2910 3901	7731 8734 9739 11*6780741 1745 2749 3754	12 13 10 9 6 7
47 48 49 50 51 52 53 54 55 56 57	3804 4719 5633 6547 7462 8377 9292 11-6380207 1123	9922 6430848 1774 2701 3627 4554 5481	5836 6774 7712 8650 9589 6490528 1467 2406	2478 3428 4379 5329 6280 7231 8183	9868 6600831 1794 2757 3721 4684 5649 6613	8025 9001 9977 6660954 1930 2907 3984 4861 5839	6972 7961 9950 9940 6720930 1920 2910 3901 4892	7731 8734 9739 11*6780741 1745 2749 3754 4756	12 11 10 9 6 7 6
47 48 49 50 51 52 53 54 55 56 57 58	3804 4719 5633 6547 7462 8377. 11-6380207 11-23 2039	9922 6430848 1774 2701 3627 4554 5481 6408 7336	5836 6774 7712 8650 9589 6490538 1467 2406 3345	2478 3428 4379 5329 6280 7231 8183 9134 6550086	9868 6600831 1794 2757 3721 4684 5649 6613	8025 9001 9977 6660954 1930 2907 3984 4861 5839	6972 7961 9950 9940 6720930 1920 2910 3901	7731 8734 9739 11*6780741 1745 2749 3754	12 11 10 9 6 7 6 8 4
47 48 49 50 51 52 53 54 55 56 57 58 59	3804 4719 5633 6547 7462 8377 9292 11*6380207 1123 2039 2955 3871	9922 6430848 1774 2701 3627 4554 5481 6408 7336 8263	5836 6774 7712 8650 9589 6490528 1467 2406 3345 4285	2478 3428 4379 5329 6280 7231 8183 9134 6550086 1038 1990	9868 6600831 1794 2757 3721 4684 5649 6613 7577 8542	8025 9001 9977 6660954 1930 2907 3984 4961 5839 6816 7794	6972 7961 9950 9940 6720930 1920 2910 3901 4892 5883	7731 8734 9739 11*6780741 1745 2749 3754 4758 5763 6768	12 11 10 9 6 7 6 4
47 48 49 50 51 52 53 54 55 56 57 58 59 60	3804 4719 6633 6647 7462 8377 11-6380207 1123 2039 2955 3871 4787 5703	9922 6430848 1774 2701 3627 4554 5481 6408 7336 8263 9191	5836 6774 7712 8650 9589 6490529 1467 2406 3345 4265 5225	2478 3428 4379 5329 6280 7231 8183 9134 6550086 1038 1990	9868 6600831 1794 2757 3721 4684 5649 6613 7577 8542 9507	8025 9001 9977 6660954 1930 2907 3984 4861 5839 6816 7794 8772	6972 7961 9950 9940 6720930 1920 2910 3901 4892 5883 6874	7731 8734 9739 11*6780741 1745 2749 3754 4756 5763	12 11 10 9 6 7 6 8 4
47 48 49 50 51 52 53 54 55 56 57 58	3804 4719 5633 6547 7462 8377 9292 11-6380207 1123 2039 2955 3871 4787	9922 6430848 1774 2701 3627 4554 5481 6408 7336 8263 9191 6440119	5836 6774 7712 8650 9589 6490528 1467 2406 3345 4285 5225 6165	2478 3428 4379 5329 6280 7231 8183 9134 6550086 1038 1990 2943	9868 6600831 1794 2757 3721 4684 5649 6613 7577 8542 9507 6610472	8025 9001 9977 6660954 1930 2907 3984 4961 5839 6816 7794	6972 7961 8950 9940 6720930 1920 2910 3901 4892 5883 6874 7866	7731 8734 9739 11-6780741 1745 2749 3754 4756 5763 6768 7773	12 10 10 10 10 10 10 10 10 10 10 10 10 10

142	2			LOG. SI	NE 88°.			[Table	11.
"	48'	49'	50′	51'	52	53′	54'	55′	"
	9-9999047	9999074	-9999100 5. 00	9999125	9999150	-9999175	9999200	9-9999224	60
1 2 3	48	D 74		a 26	o 51	a 76		24	59
2	49	75	00 01	26 26	51	76 76	00 01	24 25	58 57
3	49 49	75 75	01 01	20	52 52	77	01	25 25	56
4	50	76	02	27	52	77	02	26	55
5 6 7 8 9	50	76	02	.28	53	77	02	26 26 26	54
7	51	77	03	28 28 29 9999129	53	78	02	26	53
Ŕ	51	77	03	29	54	78	03	27	52
9	9.9999051	9999078	9999103	9999129	·9999154	9999179	·9999203	9.9999227	51
10	52	78	04	29	54	79	04	28	50
ii.	52	76	04	30	55	80	04	28	49
12	53	79	05	30 30	55	90 90 90 81	04	28 28	48
13	53	79	05	31	56	80	05	29 29 30 30 30 31	47
14	54	80	06	31 31 31 32 32	56	81	05	29	46
15	54	80	06	31	57	81	06 06 06 07	30	45
16	54	81	06 07	32	57	82 82 83	06	30	44
17	55	81	07	32	57	82	06	30	43
18	55	82	07	33	58	83		31	42
19	9.9999056	9999082	9999108	·9999133	9999158	9999183	9999207	9·9999231	41
20 21 22	56	82	08 09	34	59	83	08	32 32 33 33 34 34	40
21	57	83	09	34	59	84	08	32	39
22	57	83	09	34	59	84	08 09	32	38
23	58	84	09	35 35	60 60	85	09	33	3/
24	5 8	84	10	35	60	85	10	33	30
20	58	85	10 11	36	61 61	84 85 85 85 86 86	10	34	30
97	59 59	85 85	ii	36 37	62	96	10	34	33
20	60	86	12	37	62	87	ii	35 35	39 37 36 35 34 33 32
23 24 25 26 27 28 29	9.9999060	-9999086	9999112	·9999137	9999162	9999187	9999211	9-9999235	31
30	61	87	12		63	87	12		30
31	61	87	13	38 38 39	63	87	12	36 36 36 37 37	20
32	61	88	13	30	64	88 88 89	12 12 13 13	36	29 28 27 26 25 24
33	-62	88	14	39	64	89	13	37	27
34	62	88	14	39	64	89	13	37	26
35	63	89	15	40	65	89 89	14	38 38	25
36 37	63	89	15	40	65	90	14	38	24
37	64	90	15	41	66	90	14	38	23 22
3 8	64	90	16	41	66	91	15	39	22
39	9-9999065	9999091	·99 99 116	9999142	9999166	9999191	.9999215	9-9999 239	21
40	65	91	17	42	67	91	16	39 40	20
41	65	91	17	42	67	92	16	40	19
42	66	92	18	43	68	92	16	40	18
43	66	92	18	43	68	93	17	41	17
44	67	93	18	44	69	93	17	41	16
45 46	67 68	93 94	19 19	44	69 69	93	18 18	41 42	15 14
47	68	94 94	20	44 45	70	94 94	18	42	13
48	68	94	20 20	45 45	70	94 95	19	43	12
49	9-9999069	9999095	9999120	9999146	·9999171	-9999195	9999219	9.9999243	iĩ
50	69	95	21	46	71	96	20	43	10
51	70	96	91	47	71	90	20	43	9
52	70	96	99	47	72	96	20	44	ค
53	71	97	22 22 23	47	72	96 96 97	20 20 21	45	7
54	71	97	23	48	73	97	21	45	6
55	72	97	23 23	48	73	98	22	45	5
56	72	98	23	49	73	98	22	46	4
57	72	98	24	49	74	98	22	46	3
58	73	99	24	49	74	99	23	47	8 7 6 5 4 3 2
59	9.9999073		9999125	9999150	9999175	9999199		9-9999247	1
60	74		25	50	75	9999200	24	47	0
	11'	10'	9'	8'	7'	6′	5′	1 A/	, ,,
ı			-	LOG. CO	SINE 1º.	, ,			•

Ta	ble 11.]			LOG. T	м. 88°.				143
"	48'	49′	50′	51'	52'	53′	54'	55'	1 "
0	11-6788779				7037083		7166766		60
1		6 850 55 8	= 2193		= 8148			4202	59
2	11.6790790	= 1578	3227	5764	9213	3603	8960	5316	58
3	1797	2598	4262	6814	7040279	4684	7170058	6430	57
4	2803	3619	5297	7864	1344	5765	1156	7545	56
5	3810	4640	6333	8914	2410	6847	2254 3353	8660	55
6	4817 5824	5661 6682	7369	9965 69 81016	3476 4543	7929 9012	4451	9776 11 ·7240 892	54
8	6831	7704	9441	2067	5609		5550	2008	52
9	7839		6920477	3119	6676	1177	6650	3124	51
-		4							1
10	9846	9747	1514	4170	7744	2260	7749	4240	50
11 12	9855	6860770 1792	2551 3588	5222 6275	9811 9879	3344 4428	8849 9949	5357 6474	49
13	11.6800863 1871	2815	4625		7050947		7181050	7592	47
14	2880	3838	5663	8380	2015	6596	2151	8709	46
15	3889	4861	6701	9433	3084	7680	3252	9827	4
16	4898	5885		6990486	4152	8765		11.7250946	44
17	5908	6908	8777	1540	5221	9850	5455	2064	43
is	6917	7932	9816	2593	6291	7120935	6556	3183	42
19	7927	8957	6930855	3647	7360	2021	7658	4302	41
20	8938	9981	1894	4702	8430	3107	8761	5422	40
21		6871006	2933	5756	9500	4193	9864	6542	35
22	11.6910959	2031	3973	6811	7060571	5280	7190966	7662	38
23	1969	3056	5013		1641	6366	2070	8782	37
24	2981	4081	6053	8921	2712	7453	3173	9902	36
24 25 26	3992	5107	7093		3783	8540		11.7261023	35
26	5003	6133		7001033	4855	9628	5381	2144	34
27 28	6015	7159	9175	2089	5926	7130716	6485	3266	33
28	7027	8185	6940216	3145	6998	1804	7590	4388	32
29	8040	9212	1257	4201	8070	2892	8695	5510	31
30	9052	6880239	2299	5258	9143	3981	9800	6632	30
31	11.6820065	1266	3341	6315		5069	7200906	7755	29
32	1078	2293	4383	7373		6159	2012	8878	2
33	2091	3321	5425	8430	2362	7248	3118	11.7270001	27
33 34	3105	4349	6468			8338	4224	1124	26
35	4118	5377	7511			9428	5330	2248	25
36	5132	6405	8554		5583		6437	3372	24
37	6146	7434	9597	2663	6658	1608	7545	4496	2:
38	7161		6950641	3722		2699	8652	5621	22
39	8175				8807	3790	9760	6746	21
40	9190		2729		9882		7210868	7871	20
41	11.6830205	1550	3774			5973	1976	8997	19
42	1221	2580				7065	3085	11.7280123	18
43	2236	3610	5863	9020	3109	8157	4194	1249	17
44	3252	4640		7020081	4185	9250	5303	2375	16
45	4268	5671 6702	7954	1142 2203		7150342 1435	6412	3502	18
46 47	5285 6301		8999 6960045	3264	6339 7416	2529	7522 8632	4629 5756	13
48	7318	8764	1091	4325	8493	3622	9742	6884	12
49	8335	9795	2138	5387	9570	4716	7220853	8011	lii
	1								
50	9352		3184	6449 7511	7090648	5810	1964 3075	9140 11: 729 0268	10
51	11.6940370 1387	1859 2891	4231 5278	8574	1726 2805	6904 7999	4186	1397	
52 53	2405	3924	6326	9637	3883	9094	5298	2526	7
54	3424	4957	7373		4962		6410	3655	ė
55	4442	5990	8421	1763	6041	1284	7522	4785	Ě
56	5461	7023	9469	2826	7121	2380	8635	5915	4
57	6480		6970518	3890	8200	3476	9747	7045	3
58	7499	9090	1567	4954	9280	4572	7230861	8175	2
59		6910124	2615	6019	7100360	5669	1974	9306	î
60	9538	1158	3665	7083	1441	6766	3088	11.7300437	Ö
	11'	10	44	8′	7'	6'	5'	4'	

14-	1	LOG. S	NE 880.		L	OG. SINE	89°.	[Table	11
11	56'	57'	58'	59'	0'	1'	2'	3'	. "
0	9.9999247	9999271	9999294	9999316	9999338	9999360	9999382		
1	48 48	4.4	39	D 17	39	D 61			
2	49	71 72	94	17	39	61	83		
4	49	72	95 95	17 17 18	40 40	61 62	63 83		
5	49	73	96	18	40	62		05	5
6	50	73	96	19	41	63	84	05	5
7	50	73	96	19	41	63	84	05	5
8	50	74	97	19	41	63	85		5
9	9.9999251	9999274	9999297	9999320	9999342	9999364	-9999335	9-9999406	5
10	51	75	97	20	42	64	85	06	5
11	52	75	98	20	43	64	86	07	4
[2]	52	75	98	21	43	65	86	07	4
13	52 53	76	99	21	43	65	86	08	4
14	53	76	99	21 21 22	44	65	67	09	4
15	53 54	76 77	9999300	22	44	66	87 88	08	4
17	54	77	00	23	45	66 66	88	09	4
18	54	78	00	23	45	67	88	09	4
19	9-9999255	9999279	9999301	-9999323	9999345	9999367	-9999399		4
20	55	78	01	24	46	68	89	10	4
21	56 56	79	02	24	46	68		10	3
22	56	79	02	24	47	68		11	3
23	56	80	02	25	47	69			3
24	57	80	03	25	47	69	90	11	3
24	57	80	03	26	48	69	91	12	3
26	58	81	04	26	48	70	91	12	3
27	58	81	04	26	48	70	91	12	3
28	58 9-9999259	·9999292	04	27	49	70	92 9999392		3
29			9999305	9999327	9999349	9999371			3
30	59	82	05	27	49	71	92	13	3
31	59	83	05	28	50	72	93 93	14	2
32	60 60	83	06 06	28 29	50 51	72 72	94	14 14	2 2
34	61	84	07	29	61	73	94	15	2
35	61	84	07	29	51	73	94	15	2
36	61	85	07	30	52	73	95	16	2
37	62	85	08	30	52	74	95	16	2
38	62	85	08	30	52	74	95	16	2
39	9-9999263	9999286	'999930B	.8099331	9999353	9999374	9999396	9.9999417	2
10	63	86	09	31	53	75	96	17	2
11	63	Bti	09	31	53	75	96	17	1
12	64	87	10	32	54	75 75	97	16	1
13	64	87	10	32	54	76	97	19	1
4	65	88	10	33	55	76	97	18	1
15	65 65	89 88	11	33	55 55	77 77	98 98	19 19	1
16	66	99	11 11	34	56	77	98	19	i
18	66	89	12	34	56	79	99	20	i
19	9.9999266	9999289	9999312	-9999334	9999356	9999379		9.9999420	î
50	67	90	13	35.	57	78	9999400	20	ı
51	67	90	13	35	57	79	00	21	1
52	68	91	13	36	57	79	00	21	1
13	68	91	14	36	58	79	01	21	
54	68	91	14	36	58	80	01	22	
55	69	92	14	37	59	80	01.	22	
56	69	92	15 15	37	59	80	02	22	
57	70	93	15	37 38	59	81	02	23 23	
8	70 9·9999270	93	16 9999316		60	18	.0000402	9-9999423	1
59 30	919999270	·9999293 94	3333210	9999338	9999360 60	·9999382 82	03	24	,
//	3′ ′1	2' 94	1' 16	0′ 38	59	58	57	56'	1
	· ·	4	E 1º.	U	00		COSINE 0		

Ī	Ta	ble 11.]	LOG. T	an. 88°		I	OG. TA	v. 89°.		145
I	"	56'	57'	58′	59'	O'	1'	2'	3'	"
Ħ	0	11.7300437		7438351			7653792		11.7803592	60
H	1	1569	9996	9519	7510172	± 1992	= 5020	9295	4863	59
ľ	2		7371146		1359	3199	6247	7730544	6133	58
ı	3	3832	= 2296	1856	2547	4407	7475	1793	7404	57
ı	4 5	4965 6097	3446 4597	3024 4194	3735 4923	5614 6823	8703 9932	3043 4292	8676 9947	56 55
B	6	7230	5748	5363	6112	8031			11.7811220	54
ı	7	8363	6899	6533	7301	9240	2390	6793	2492	53
Ħ	8	9497	8050	7703		7590449	3620		3765	52
ı	9	11.7310630	9202	8873	9679	1658	4850		5038	51
H	10	1764		7450044		2868		7740547	6312	50
E	iĭ	2899	1507	1215	2060	4078	7311	1799	7586	49
H	12	4033	2659	2386	3250	5289	8542		8860	49
H	13	5168	3812	3558	4441	6500	9773	4304	11.7820135	47
ı	14	6304	4966	4730	5632		7671005		1410	46
ı	15	7439	6119	5902	6824	8922	2237	6810	2686	45
ı	16	8575	7273	7075		7600134	3470		3962	44
ı	17	9711	8427	8248			4703		5238	43
ı	18	11.7320847	9582		7530401	2559		7750573	6514	42
I	19		7390737		1593		7169		7791	41
ı	20	3121	1892	1768	2787	4985	8403		9069	40
H	21	4258	3047	2942		6198			11.7830347	39
ı	22	5396	4203		5174	7412			1625	38
I	23	6534	5359	5292		8627	2107	6851	2903	37
ı	24 25	7672 8811	6515 7672	6467 7642	7563	9941 7611056	3342 4578		4182 5461	36 35
I	26	9949	8829	8818	9953	2271		7760622	6741	34
1	27	11.7331089	9986		7541148	3487	7050		8021	33
ı	28	2228			2344	4703	8287	3138	9301	32
ı	29	3368	2302	2347	3540	5919	9524		11.7840582	31
B	30	4508	3460	3524	4737	7135	7690761	5655	1863	30
٠	31	5648	4619	4702	5934	8352	1999		3145	29
ı	32	6788	5777	5879	7131	9570	3237	8174	1427	28
۱	33	7929	6937	7057		7620787	4475		5709	27
I	34	9071	8096	8236		2005		7770695	6992	26
H	35	11.7340212	9256	9414	7550724	3224	6953		8275	25
I	36	1354	7410416		1923	4442	8193		9558	24
ı	37	2496	1576	1773	3121	5661	9432		11.7850842	23
1	38 39	3638	2737 3898	2952		6880			2126 3411	22 21
I		4781	1			1	1913			
	40	5924	5059	5312		9320	3154	8264	4696	20
	41	7067	6221	6493		7630540	4395		5981	19
H	42 43	9355 9355	7393 8545		9120 7 56 0321	1761 2982	5637 6879		7267 8553	13
	44	11.7350499	9708	7490036		4204	8121		9839	17
ij	45		7420871	1218		5425	9364		11.7861126	15
ı	46	2788	2034	2400		6647		5847	2413	14
ı	47	3933	3197	3583			1850		3701	13
li	48	5079	4361	4766		9092	3094		4939	12
	49	6224	5525	5949	7533	7640316	4338	9644	6277	11
ı	50	7370	6690	7132	8736	1539	5583	7790910	7566	10.
ı	51	8517	7854	8316	9939	2763	6827	2176	8855	9
li	52	9663	9019		7571143	3987	8073		11.7870145	8
	53	11.7360810	7430185		2347	5211	9318		1434	7
U	54	1957	1350	1869	3552		7720564		2725	6
	55	3105	2516	3054	4756	7661	1810		4015	5
	56	4253	3683	4240	5962	8887	3057	8515	5306	4
	57	5401	4849 6016	5426 6612	7167	7650113 1339	4304 5551	9784 7801053	6598 7890	3 2
	5 8	6549 7698	7183	7798	8373 9579	2565	6799		7890 9182	1
	60	8847	8351	8985	7580785	3792	8047	3592	11.7880474	ô
ı	"	3/	2	1'	0,00	59'	58'	57	56'	"
Ŀ	•	, J	OG. COT.					OTAN.		i i
T.		L	Ja. CUI.	wite T.			Mou.		·	

13

14	6			L06. 81	NE 890.			[Table	п.
11	4'	5'	6'	7'	8'	9' 1	10'	11' 1	71
0	9.9999424	9999444	9999464	9999484	9999503		9999541	9-9999559	60
1	24	0 44	on 65	on 84	a 03	r 22	S 41	59	59
2	24	45	65	84	04	23	41	59	58
	25 25	46	65 66	85 85	04	23 23	42	~ 60	57
4	25	46 46	66	85	04 05	24	42	60 60	56
5	26	46	66	. 86	05	24	42	61	54
6	26	47	67	86	05	24	43	61	53
9	27	47	67	86	06	25	43	61	52
9	9.9999427	9999447	9999467	9999487	9999506	9999525	9999543	9-9999562	51
10	27	48	67	87	06	25	44	62	60
11	28	48	69	97	07	26	44	62	49
12	28 28	48 49	69 68	88 88	07 07	26 26	44	62	48
13	25	49	69	88	08	26	45 45	63	47
14	29	49	69	89	08	27	45	63 63	46
15	29	50	69	89	08	27	46	64	44
16	30	50	70	89	09	27	46	64	43
18	30	50	70	90	09	28	46	64	42
19	9-9999430	9999451	9999470	9999490	9999509	9999528	9999546	9-9999565	41
20	31	51	71	90	09	28	47	65	40
21	31	51	71	91	10	29	47	65	39
22	31	52	71	91	10	29	47	65	38
23	32	52	72	91	10	29	48	66	37
24	32	52	72	92 92	11	30	49	66	36
25 26	32	53 53	72 73	92	11	30	48 49	66	35
27	33	53	73	93	12	30	49	67	33
28	33	54	73	93	12	31	49	67 67	32
29	9-9999434	9999454	9999474	-9999493	9999512		9999549	9-9999567	31
30	34	54	74	94	13	31	50	68	30
31	34	55	74	94	13	32	50	68	29
32	35	55	75	94	13	32	50	68	28
33	35	55	7.5	95	14	32	51	69	27
34	35	56	75	95	14	33	51	69	26
35	36	56	76	95	14	33	51	69	25 24
36	36	56	76 76	95 96	15	33	52 52		23
37	36	57 57	77	96	15 15	34 34	52		22
39	37 9:9999437	9999457	9999477	9999496	9999515	9999534	9999552		21
40	37	58	77	97	16	34	53	to monage	20
41	38	58	78	97	16		53		19
44	38	58	78	97	16		53		18
43	39	59	78	98	17	35	54	72	17
44	39	59	79	98	17	36	54	72	16
45	39	59	79	98	17	36	54	72	15
46	39	60	79	99	19		55	73	14
47	40	60	80	99	18	37	65	73	13
48	40	60	80	99	18	37	55		12
49	9-9999440	9999461	9999490	9999500	9999519		9999556	0 2000010	11
50	41	61	81	00	19	38	56	74	10
51	41	61	81	00	19		56	74	9 8 7
52	41	62	81	01	20		56	74	9
53 54	42	62 62	82 82	01	· 20	38 39	57	75 75	6
55	42	63	82	02	21	39	57 57	75	6 5
56	43	63	83	02	21	39	58	75	4
57	43	63	83	02	21	40	58	76	3
58	43	64	83	03	21	40	58	76	3 2 1
59	9-9999444	9999464	-9999484	9999503	9999522		9999559	9-9999576	
60	44	64	94	03	22	41	59	77	0
17	55'	54'	53′	52'	51'	50′	49'	48'	11
				LOG. CO	SINE 00.				

ble	п.]			LOG. TA					4
1	4'	5'	6'	7'	8'	9'	10'	11'	1
11	7880474	7958741		8119636		8286718			1
	1767	7960058		8121001		- 8138	→ 4181	1962	
1	3061	-1375		- 2369	5159	9558	6629	3440	ı
1	4354	2692	-2468	3736	6553	8290979	7078	4918	ı
	5649	4010	3810	5103	7946	2400	8528	6397	
	6943	5328	5152	6471	9341	3922	9978	7877	
1	8238	6646	6495	7939	8210735	5244	8381428	9357	1
1	9533	7965	7839	9208	2130	6666	2879	11:8470838	
111	7890829	9284	9182		3526	8089	4331	2319	
1	2125			1947	4922		5783	3901	
1						1		5283	
1	3421	1924	1871	3317		8300936	7235		
1	4718	3244	3216		7715	2361	8688	6766	
1	6015	4565	4561	6058	9113		8390142	8249	
1	7313	5887	5907	7429			1596	9733	
1	8611	7208	7254	8801	1909			11.8481217	1
	9909			8140173		8063	4605	2701	1
111	790120B			1546	4706	9490	5960	4187	
	2507	7981176	8061295	2919	6106	8310917	7416	5672	
	3907	2499	2643	4292	7506	2344	8872	3159	1
	5107	3823	3991	5666	8906	3772	8400329	8645	ı
	6407	5147	5340			5201	1787	11.8490133	ı
			6639		1709		3244	1620	
	7708								
	9009		8039		3111	8060		3109	
111	7910310			8151166				4598	ı
		7990447				8320920		6087	ŀ
	2914	1773	2090		7319	2351	9080		I
1	4217	3100		5296			8410541	9067	1
1	5520	4427	4793		8240127	5214		11.8500558	
	6824	5754	6145		1531	6647	3463	2049	ı
	6127	7082	7497	9429	2936	8079	4924	3541	L
	9432	9410	8850	8160809	4342	9513	6387	5033	
112	7920736		8050204	2187		8330946	7849	6526	
1.2	2041	8001067	1558		7154	2381	9313	8020	
					8561		8420776	9513	
	3347	2397	2912					11-8511008	1
	4652	3727	4266		9968	5251 6686		2503	
1	5959	5057	5621	7709			3705	3998	
1	7265	6397	6977	9090	2784	9122	5170		1
	8572	7718		8170471	4193		6636	5494	
	9880	9050	9689			8340996	8102	6991	l
11	7931187	8010381	8091046	3236	7011	2434	9569	8488	١
1	2495	1714	2403	4619	8421	3872	8431036	9985	ı
1	3904	3046	- 3761	6003	9832	5310	2504		
	5113				8261243	6749	3972		
1	6422	5713		9771	2654	8188	5441	4481	1
	7732	7047	7836		4066		6910	5980	1
					5478		8379	7480	
12	9042	8381	9195	1541	6891	2510	9849	8981	1
111	7940353	9716		2927					1
		8021051	1915	4313	8304		8441320		1
	2976	2386	3276	5700	9718	5393	2791	1984	1
	4286	3722	4637	7087	8271132	6835	4263	3486	۱
	5599	5058	5998	8475	2547	8278	5735	4989	1
1	6911	6395	7360		3962		7208	6492	1
	8224	7732	6722		5377		8681	7996	1
	9537	9070	8110085	2640	6793			9500	i
119	7950851	8050408			8210		1629		1
144	2165	1746	2912		9627	5499	3103	2510	
1							4578	4016	1
1	3479	3095	4176			6946		5522	1
	4794	4424	5540		2462		6054		1
1	6110	5764	6905	9591	3880	9838	7530	7029	1
	7425	7104	8270			8371285	9007	8536	1
	8741	8444	9636		6718		3460484	11 8550044	1
	55/	54'	53'	59'	51'	50"	49'	48'	1

14	18			Log. St	NE 89°.		-	[Table	
77	19'	13'	14'	15'	16'	17'	18'	19	77
0	9-9999577	9999591		9999628				9-9999691	60
1	77	5 94	on 11	P 28	\$ 45	D 61	O 76	91	59
2	77	95	12	28	45	61	76	92	
3	78	95	12	29	45		77	92	57
4	75	95	12	29	45		77	92	
5	78	96	13	29	46			92	
6	78	96	13	30	46	62	77	93	
7	79	96	13	30	46		78		53
8	79	96	13	30	46		78		52
9	9.9999579	9999597	9999614	9999630	9999647	19999663	-9999678	9-9999693	51
10	80	97	14	31	47	63	79	94	50
ii	80	97	14	31	47 47	63	79	94	49
12	80	98	16	31		63	79		48
13	80	98	15	31	48		79	94	47
14	81	99	15	32	48	64	79		46
15	81	98	15	32	48		80	95	45
16	81	99	16	32	49		80		43
17	82	99	16	33	49	65	80 80		42
18	82	99	16	9999633	-0000040	65 -9999665		96 9-9999696	41
19	9.9999562	9999600	9999617	200000	9999649				100
20	83	00	17	33	50	66	81	96	40
21	83	00	17	34	50		81	96	39
22	83	00	17	34	80		82	97	3S 37
23	83	01	18	34	50		82	97	36
24	84	01	18		61	67	82 82	97	35
25	84	10	18	35	51:	67	83		34
26	84	02	19	35	51	67	83	98 98	33
27	85	02	19	35 36	52 52		83	98	32
28	85	02	19	9999636	9999652		9999683		31
29	9-9999585	9999602	9999619						1000
30	85	03	20	36	52	68	84	99	30 29
31	86	03	20	36	53		84	99	28
32	86	03	20	37	53		84 84	99 99	27
33	86	04	20	37	63		85		26
34	87	04	21	37 27	53	69 69	85	9.88888460	35
35	87	04	21 21	38	54 54	70	85	00	24
36	87	04	21	39	54	70	85	00	23
37	87	05	22	38	54	70	86	01	22
38	89	05	9999622		9999655	-9999670	9999686	9-9999701	21
39	9-9999588	9999605				80000	86		20
40	58	06	22	39	55	71	86	61	19
41	89	06	23	39	55		87	01	18
42	894	06-	23	39 40	55 56		87	02	
43	89	06	23		56		87	02	16
44	89	07	23 24	40	56		87	02	lâ.
45	90	07	24	40	57	72	88	03	14
46	90	07 08	24	41	57	73	88	03	13
47	90	08	25	41	57	73	89	03	12
48	0.0000501	9999608	9999625	9999641	-9999657	-9999673	9999688	9-9999703	11
49 50	9-9999591			42	58	73	89	04	10
50	91	08	25 25	42	58	74	89	04	9
51	92	09	25 26	42	58	74	89	04	8
52	92	09 09	26	42	58	74	89	04	8
53	92	09	26 26	43	59	74	90	65	6
54 55	92 93	10	27	43	59	75	90	05	5
56	93	10	27	43	59	75	90	05	
57	93	10	27	44	59.		90	05	3
58	94	11	27	44	60	75	91	06	1
59	9.9999594	9999611	9999626		-9999660		9999691	9-9999706	
60	94			44'	43′	76	91	06	0
11	47'	AG!	45'	44'	43'	42'	41'	40'	11
	47	200	3.0		SINE Oo.				

	ble n.]		1	LOG. TA	N. 89°.				14
,	19'	13'	14'	15'	16'	17'	18'	19'	-
0	11.8550044	8641490	8734901	8630366	8927975	9027828	9130030	11 9234694	6
1	1553	= 3030	\pm 6475	- 1975	9620	9512	= 1754	6460	6
2	3004	41751.1	OUNT	200000	SOCIAL PROPERTY.	9931190	399 (D)	0.641	5
3	4571 6081	6113			= 2913	2881	5204		5
4 5 6			8741201			4567		11-9241762	
5	7592	9198		8416 8840028			91403B4		5
b	11.3560614	8650741 2285				9629			
7	9196	2000			8941157		3840		
9	2620	5374		4868		3000		11-9250614	
	3639 5152 6666 8190	2014							
0	6182	0919	9750667 2247	6492 8097			0021	2386 4159 50 21	
1	0100	8465 8660012	3827	9713			9150762	5933	
2	9695	20000774		8851329			310010-	4734	-
	11.8571210			2046	9910	0051461	4997	9493 11-9261259	4
5	2726	4655		4567	8951069 2724 4379	2154	5061	11-0261250	4
6	4242	6204	8760154	6181	4370	4947	7695 9430	3035	4
7	5759			7800	6034	6542	9430	4814	
á	7276			9419			9161165	6592	
9		8670853		8861039		9932			
)	11 8580313				8961005			11-9270150	
J	1832			4900	9,462	3326	6276	1031	27 274
2	3351	5509	00000	5902	4.0000	5023	Q115	1931 3712 5494 7277 9060	5
3	4871	7060	8771248	7594	5981	6722	9854	5494	4 67
1	6392	8614	2936	0147	7641	8421	9171594	7977	200
5	7913	8680167	4423	7524 9147 9870770	9302	9070120	3334	9060	5
Š	9434		6012	2394	8970063	1920	5075	11.9260644	47
7	11.8590957	3277	7601	4019	2625	3521		2629	
3	2479		7601 9190	5644		5999	(AMAG)	4414	2
9	4003		9780781	7270		6925	9180303	6201	5
)	5596	7044				8628	2047		
i	7051	9502		8990523		9080332			6
2	8575	8691059	5554	9151	8980944	2036		11-9291564	6 6 4
3	11-8600101		2 4 4 7	9840	2610	3741	7283	3353	3
4	1627	4176		5408	4276	5447		5143	
5	3153	5735	6790334	7038		7153	9190777	6934	
6	4680	7295		8668		8860	2525	8725	
7	6208		3523	8390298		9090568	4274	11.9300517	2
9	7736	8700417	5118	1930	B990948	2276	6024		2
ğ	9264	1978			2618	3985	7774	4104	2
0	11:8610793					5695	9525		5
ĺ	2323						9201277	7694	i
2	3853		9801505				3029	9489	
3	5394	8230	3104	8900096	9302	9100828	4782	11:9311286	1
4	6915		4703	1731	9000975	2540	6536	3083	j
5		8711359			2649	4253		4892	1
6	9980						9210046		
7	11.8621512	4491	9503	6639	5997	7681	1802	8480	1
ŝ	3046	605B	8811104	8277	7673	9396	3559	11-9320220	1
9	4530				9349	9111112	5316	2081	1
0	6114	9193	4309	8911554	9011025		7074 8833	3993	1
ĭ		8720761	5912				8833	5686	ľ
2	9185		7515				9220593	7489	
3	11:8630721	3899							
4	2258	5469	8820724					11-9331098	
5	3795	7040	2330	9757	9418	9121421	5875	2904	
6	5333		3936	8921399	9021099	3141	7636	4710	
7	6971	8730183	5549	2042	2780	4862	9401	6517	
В	8410	1755	7149	4686		6584	9231165	8325	
9	9950		8757	53.30	6145		2929	11.9340134	
0	11 8641490		8830366	7975 44'	7828	9130030	4694	1943 40'	
	47'	46'	45'	4.4/	43'	42'	41'	407	1 1

150)			LOG.	SINE 89	· .		[Table	II.
"	20′	21'	22′	23′	24'	25′	26′	27'	"
0	9-9999706	9999721	·9999735	·9999748	9999762 9 62	·9999775 • 75	9999788	9· 9999800 . 00	60 59
1 2	06	21	35	49	62	75	88	00	58
3	06 06 07 07	21 21 21 21 21	35 35 36	49	63	76	88	01	57
5	07	21 22	36 36	49 50	63 63 63	76 76	-9999786 6 88 88 88 88 88	01 01	56 55
6	07	22	36	50	63	76		01	54
7	08 08	22 22 22	36 37	50 • 5 0	63 64	76 77	89 89	01 02	53 52
8 9	08	23	37	50	04 04	77	89	. 02	51
10	9.9999708	9999723	-9999737	9999751	9999764	-9999777	-9999790	9-9999302	50
11	09 09	23 23	37	51	64	77	90	02 02	49 48
12 13	09	24	37 38	51 51	65 65	77 78 78	90 90 90	02	47
14	09	24	38 38	52	65	78	90	03	46
15	10 10	24 24	38 38	52 52	65 65	78 78	. 91 . 91	03	45 44
16 17	10	25	39	52	66	79	91	03	43
18	10	25 25	39	53	66	79	91 92	04	42
19	11 9 ·99997 11	9999725	39 ·9999739	53 -9 9997 53	66 -9999766	79 -9999779	9999792	04 9-9999804	41 40
20 21	11		9899139	53	66		92	04	
22	11	26	40	53	67	79 80 80 80 80	92	04	38
23 24	12 12	26 26	40 40	54 54	67 67	80	92 93	05 05	36
25	12	26 26 26 26 26 27	40	54	67	80	93	06 06 05	39 38 37 36 35 34 33 32 31
26	12 13	27	41 41	54 55	68 68	80 81	93	05 05	34
27 28	13	27 27 27	41	55	68	81	93 93	06	32
29	13		41	55	68	81	94	06	
30	9.9999713	9999728	9999742 42	9999755	9999768	9999781	-9999794	9.9999806	30 29 28 27 26 25 24 23
31 32	14 14	28 28	42	55 56	· 69	82 82	94 94	06 06	28
33	14	28	42	56	69	82	94	07	27
34 35	14 15	28 29 29 29 29	43 43	56 56	69 70	82 82	95 95	07 07	26 25
36	15	29	43	57	70	83	95	07	24
37	15	29 30	43 43	57	70	83	95	07 08	23 22
38 39	15 15	30	43	57 57	70 70	83 83	95 96	08	21
40	9.9999716	9999730	9999744	9999757	9999771	9999783	9999796	9-9999808	20
41	16	30	44	58	71 71	84	96 96	08	19
42	16 16	30 31	44 45	5 8 5 9	71	84 84	96 96	08 08	18 17
44	17	31	45	58	71	84	96 97	09	16
45 46	17 17	31 31	45 45	59 59	72 72	84 85	97 97	09 09	15 14
47	17	32	45	59	72	85	97	09	13
48	19 18	32 32	46 46	59	72 73	85	97	09	12
49 50	9· 99997 18	·9999732	·9999746	59 • 999976 0	·9999773	9999786	98 9 9997 98	10 9 -999 9	11 10
51	18	33	46	60	73	86	98 98	10	
52	19	33	47	60	73	86	98 98	10	8
53 54	19 19	33	47 47	60 61	73 74	86 86	98	10 11	7
55	19	34	47	61	74	87	99 99 99	11	5
56	20 20	34 34	48 48	61 61	74 74	97 87	99 99	11	3
57 58	20	34	48	61	74	87	99	11 11	2
59	20	34	18	62	75	87	9999800	12	ı
60	39′ 21	35 38′	37 ′ ⁴⁸	62 36 ′	75 35′	34′	33′	32 12	0,
'			-,		SINE 0°.				•

	able II.]			LOG.	TAN. 8			15	
"	20'	21'	22'	23'	24'	25'	26'	41	"
	11-9341943	9451906	9564726	9690554	9799555	11.9921908	12:0047808	12-0177466	60
1 2 3	3753	≟ 3763	6631	= 2511	9801566	3977	9938	9660 12·0181555 4052 6219 8448 12·0190647	53
2	5564	5620	8533	4469	= 3578	6047	12.0052068	12.0181865	58
3	7375		9570445	6427	5592	8117	4200	4052	57
4	9188	9337		8387	7606	11-9930189	6333	6219	5ti
	11.9351001			9690347	9621	2262	8466	8448	55
6	2815	3057		2308	9811636	4335 6410 8486 11*9940562	13.0000001	12.0190647	54
7	4629	4919		4271 6234	3653	0410	2737	2848	oa.
	6445	6781			00/1	11-0040560	48/4	5050 7253	
9	8261		9581904	8198					
	11:9360078		3817	9700162	9709	2640	9151	9457	50
11	1396	2372		2128	9821730	4718	12.0071591	12.0201662	49
12	3714	4237		4095	3752	6768	3432	3869	48
13	5533	6103		6062	5774	8879	5574	6076	47
14	7353		9591478	8031	7797	1119950960	7717	8285	40
15	9174	9838	3395	9710000	9822	3043	9862	12.0210494	45
	11-9370995	9481706	5313	1970	9831847	5126	12.0082007	2705	44
17	2818	3576		3941	3573	7211	4153	4917	43
18	4641	5446		5913	5901	9297	6301	7130	4.5
19			9601072	7886	7929	11.5561383	8449	9457 12·0201662 38:09 6076 82:55 12·0210494 27:05 49:17 71:30 9345	41
20	8289	9188	2993	9860	9958	3471	12:0090599	12:0221560 3776 6994 8213 12:0230433 2654 4376 7099	40
	11.9380114		4915	9721834	9841988	5559	2749	3776	39
22	1940	2934	6838	3910	4019	7649	4901	5994	38
23	3767	4808	8762	5787	6051	9740	7054	8213	37
24	5595		9610687	7764	8084	11.5611831	9208	12.0230433	36
25	7423	9559	2613	9742	9850117	3924	12:0101363	2054	35
26		9500436	4539	9731721	2152	6017	3519	4876	34
27	11-9391082	2313	6467		4188	8112	5676	7099	33
28	2913	4191				11.9980208	7834	9324	
29	4746		9620324		8262			12-0241549	
30	6577	7950			9860301	4402	12:0112153	3776	30
31	8410	9831	4185	9741631	2340	6501	4315	6004 9233 12:0250463 2694	29
	11-9400244				4381	8600	6477	8233	28
33	2078				6422	11.9990701	8641	12.0250463	27
34	3913	5477			8465	2803	12:0120805	2694	26
35	5750		9631916		9870508	4906	2971	4927	145
36	7586	9246		9751563		7009	2971 5138 7305	7160	24
37		9521131		3552	4598	9114	7305	9395 12-0261631 3868	23
	11-9411263	3018			6644	12-0001220	9474	12.0261631	22
39	3102	4905	-		8692	3327	12.0131644		21
40	4942	6793	9641600	9525	9880740	5435	3815	6106	20
41	6783	8682		9761517	2789	7544	5987	8345 12-0270586	119
42		9530571	5480	3511	4839	5435 7544 9654	8161	12-0270586	18
	11.9420466	2462	7421	5506	6890	12'0011764	12 0140335	2827	17
44	2310	4353	9363	7501	8942	3876	2510	5070	
45	4154	6245	9651306	9498	9890995	9654 12'0011764 3876 5989 8103	4687	7314	
46	5998	8138		9771495	3049	8103	6865	9559	14
17		9540032			5104	14/0020218	9043	112 0281806	
48	9690	1926			7160	2334	15.0191553	4053	
	11-9431537	3822	1		9217	9452	2404	6302	11
50			9661033		9901275	6570	5586		10
51	5233	7615		9781496	2224	8680	7769	12:0290802	
52	7083	9513	4931	3499	5394	12.0030809		3055	87
53		9551412		5502	7455	2930	12/0/62138	3055 5308 7562 9818 12-0302075 4333 6592	7
	11-9440784			7507	9517	5053	4325	7562	6
55	2636		9670783	9513	9911580	7176	6512	9818	5
56	4488	7113		9791519	3643	9300	8701	12.0302075	4
57	6342	9015	4669	3527	5708	12.0041426	12.0170890	4333	3
58		9560918	6643	5535	7774	3552	3081	6592	2
	11.9450051		8598	7545	9841	6680	5273	8852	1
60	1906	4726	9680554	9555	9921908	7808	7466	12-0311114	0
"	39'	38'	37	36'	35'	34'	33′	4333 6592 8852 12-0311114 32	"
				1.06	. COTAP	v. 00.			1

13	52			L00, 8	INE 89°.			[Table	: п.
11	1 28'	29'	30"	31'	32'	33'	34	35	777
0	9-9999812	-9999823	9999835	9999945	9999856	-9999866	-9999876	9-9999986	60
1	12	co 24	a 35	on 46	on 56	on 66	o 76	85	59
3	12	24	35	46	56	66	. 76		58
	12	24	35	46	56	67	76	86	57
4	13	24	35	46	57	67	76	86	56
5	13	24 25	36 36	46 47	57 57	67 67	77	86	55
6 7	13	25	36	47	57	67	77	86 86	54 53
9	13	25	36	47	57	67	77	96	52
9	9.9999814	9999825	9999836	9999847	9999857	9999968	9999877	9-9999837	Si
10	14	25	36	47	58	68	77	87	50
11	14	26	37	47	58	68	78	87	49
12	14	26	37	49	58	68	78	87	48
13	14 15	26 26	37 37	48	58 58	68 68	78	87	47
14	15	26	37	48	59	69	78 78	87 87	46
15 16	15	26	38	48	59	69	78	98	44
17	15	27	38	48	59	69	78	89	43
is	15	27	38	49	59	69	79	88	42
19	9.9999816	9999827	-9999838	9999849	9999859	9999869	9999879	9-9999588	11
20	16	27	38	49	59	69	79	68	40
21	16	27	38	49	60	70	79	88	39
22	16	28	39	49	60	70	79	89	38
23	16	28	39	50	60	70	79	89	37
24	17 17	28 28	39 39	50 50	60 60	70 70	80	89	36
25 26	17	28	39	50	60	70	80	89 89	34
27	17	29	40	50	61	70	80	89	33
28	17	29	40	50	61	71	80	89	32
29	9-9099817	9999829	99999840	9999851	-9999861	9999871	9999980	9-9999890	31
30	18	29	40	51	61	71	81	90	30
31	18	29	40	51	61	71	81	90	29
32	18	29	40	51	61	71	18	90	28
33	18	30	41	51 51	62	71	81	90	27
34	19 19	30	41 41	52	62 62	72 72	81 81	90	26 25
36	19	30	41	52	62	72	81	90 91	24
37	19	30	41	52	62	72	82	91	23
38	19	31	42	52	62	72	82	91	22
39	9-9999919	9999931	9999842	9999852	9999863	9999872	9999882	9.9999891	21
40	20	31	42	52	63	73	83	91	20
41	20	31	42	53	63	73	83	91	19
42	20	31	42	53	63	73	82	92	19
43	20 20	31	42 43	53° 53	63	73	83	92	17
45	20	32 32	43	53	63 64	73 73	83	92 92	16
46	21	32	43	54	64	74	83	92	15 14
47	21	32	43	54	64	74	83	92	13
48	21	32	43	54	64	74	83	92	12
49	9-9999821	.9999833	2999844	9999854	9999864	9999874	9999883	9-9999893	11
50	22	33	44	54	64	74	84	93	10
51	22	33	44	54	65	74	84	93	9
52	22	33	44	55	65	75	84	93	8
53 54	22 22	33	44	55	65	75	84	93	8 7 6
55	22	34 34	44 45	55 55	65 66	75 75	84 84	93	5
56	23	34	45	55	65	75	85	93 94	4
57	23	34	45	55	66	75	85	94	3
58	23	34	45	56	66	75	85	94	3 2
59	9 9999823	9999934	9999845	9999856	9999866	9999876	9999885	9-9999894	1
60	23	35	45	56	66	76	85	94	0
"	31'	30′	29'	28'	27'	26'	25'	24'	"
				LOG. CC	SINE Oo.				

Ta	ble 11.]		1	LOG. TA	n. 89°.			1	53
11	28'	29'	30'	31'	32	33'	34'	35'	"
0	12.0311114		0591416	0738656	0891062	1049012	1212923	12-1383262	60
1		0451340	3830	0741153		≥ 51694		86159	59
2	5640		6244		96236		19494	89057	58
3 4	7905		8661	6150		57062		91957	57
4	12:0320171	0460695	0601078 3497		0901416 04009	59749 62437	24073 26865	94859 97763	56
5	4707	3037	5917	3658	06601	65127	29659		55
7	6977	5380	8339	6164	09197	67819	32455	03577	53
8	9248		0610762	8670	11793	70513	35252	06487	52
9	12:0331520	0470071	3186	0761179	14392	73208	38051	09399	51
10	3794	2418	5612	3688	16992	75904	40953	12313	50
ii	6068	4766	8039	6200	19593	79603	43656	15229	49
12	8344	7115	0620467	8712	22196	81303	46460	18147	48
13	12:0340621	9466		0771226	24801	84005	49267	21066	47
14		0481818	5329		27407	86708	52075	23988	46
15	5178		7761	6259	30015	89413		26912	45
16	7459 9740		0630195	8778	32624	92120	57697	29837	44
17	12.0352023			0781298	35235	94829	60511	32765	43
18.	4307	3598	5066 7504	3819 6342	37847	97539 1100251	63327 66144	35695 38626	41
20	6592		9943	-	43077	02964	68963	41560	40
21	8879		0642384		45694	02964	71785	44495	39
22	12-0361167		4826	3919	48313	08397	74607	47433	38
23	3456		7270	6448	50933	11115	77432	50372	37
24	5746		9714	8978		13936	80259	53314	36
25	8037		0652161		56178	16558	83087	56257	35
26	12.0370330		4609	4043	58803	19282	85918	59203	34
27	2623		7057	6578		22007	88750	62150	33
28	4918		9507	9114	64059	24734	91584	65100	32
29	7214		0661959		66688	27463	94420	1	31
30	9512		4412	4191	69319	30194	97257	71004	30
31	12.0391810		6867	6731	71952	32926		73960	29
32	4110 6411	4376	9322 0671780	9273	74587 77223	35661 38396	02938 06782	76917 79877	28
33	8713		423B	4362	79861	41134	08627	82839	26
35	12-0391917		6698	6909	B2500	43873	11474	85802	25
36	3322	3890	9160	9457	85141	46614	14323	88768	24
37	5627		0681622	0832006	87784	49357	17173	91735	23
38	7935	8655	4087	4557	90429	52101	20026	94705	22
39	12.0400243		6552	7110	93074	54848	22880	97677	21
40	2553	3425	9019		95721	57596	25737	12*1500650	20
41	4863		0691488		98370	60345	28595	03626	19
42	7175		3957	4776		63097	31455	06604	18
43	12:0411803	0550590 2981	6429 8901	7335 9895	03673 06327	65850 68605		09584 12565	17 16
45	4119		0701375		08983	71361	37181 40047	15549	15
46	6436	7767	3851	5020	11640	74120	42915	18535	14
47		0560161	6328	7594	14299	76880	45784	21523	13
48	12:0421074	2558	8806	0860150	16959	79642	48656	24513	12
49	3394	4955	0711286	2718	19621	82406	51529	27506	11
50	5716	7354	3767	5287	22295	85171	54404	30500	10
51	8039	9754	6249	7858	24950	87938	57281	33496	9
52	12-0430364			0870430	27617	90707	60161	36494	8 7 6
53	2690	THE P	0721218	3004	30286	93478	63042	39495	7
54	5016 7345	6963	3705	5579	32956	96260	65924	42497	6
55 56		9368 0581775		9156 0880734	35629	99025 1201901	68809 71696	45502 45508	5
57	12-0442005		0731174	3314	40977	04578	74585	51517	3
58	4337	6593	3667	5895	43653	07358	77475	54528	2
59	6670		6160	8478	46332	10139	80368	57541	i
60		0591416	8656	0891062	49012	12923	83262	60556	ô
21	31'	30'	29'	28'	27'	26'	25'	24'	"
				LOG, CO	TAN. DO				

154	1	to the second		LOG. SI	NE 89°.			[Table	n,
"	36'	37"	38'	39'	40'	41'	42'	43"	17
0	9-9999894	9999903	9999911	-9999949	9999927	9999934		9.9999947	60
1	94	D 03	D 11	D 19	D 27	on 34	Ø 41	47	59
2	94	03	11	19	27	34	41	47	581
3	95	03	11	19	27	34	41	47	57
4	95	03	12	19	27	34	41	47	56
5	95	04	12	20	27	34	41	47	55
6	95	04	12	20	27	34	41	48	54
7	95	04	12	20	27	34	41	48	53
8	95	04	12	20	27	35	41	48	52
9	0.9999995	99999904	9999912	99999920	9999928	9999935	-9999941	9-9999948	51
10	96	04	12	20	23	35	42	48	50
11	96	04	13	20	28	35	42	48	49
12	96	04	13	21	28	35	42	48	48
13	96	0.5	13	21	28	35	42	48	47
14	96	05	13	21	28	35	42	48	46
15	96	05	13	21	28	35	42	48	45
16	97	05	13	21	28	36	42	49	44
17	97	05	13	21	29	36	42	49	43
18	97	0.5	13	21	29	36	43	. 49	42
19	9-9999897	9999905	9999914	-99999921	99999999	.9999936	9999943	9-9999949	11
20	97	06	14	22	29	36	43	49	40
21	97	06	14	22	29	36	43	49	39
22	97	06	14	22	29	36	43	49	39
23	98	06	14	22	29	36	43	49	37
24	99	06	14	22	29	36	43	49	36
25	98	06	14	22	30	37	43	49	35
26	98	06	15	22	30	37	43	50	34
27	98	07	15	22	30	37	43	50	33
28	98	07	15:	23	30	37	44	' 50	32
29	9-9999898	9999907	9999915		9999930	9999937	9999944	9-9999950	31
30	99	07	15	23	30	37	44	50	30
31	99	07	15	23	30	37	44	50	29
32	99	07	15	23	30	37	44	80	28
33	99	07	15	23	30	37	44	50	27
34	99	08	16	23	31	38	44	50	26
35	99	08	16	23	31	38	44	50	25
36	99	08	16	24	31	38		51	24
37	9-9999900	08	16	24	31	38	44	61	23
38	9 9999900	08	16	24	31	38	45	51	22
39	9-99999900	-9999998	9999916	-9999924	9999931	-9999938	9999945	9.99999951	21
									20
40	00	08	16	24	31	38	45	51	
41	00	08	17	24	31.	39	45	51	19
42	00	09	17	24	32	39	45	51	18
43	00	09	17	24	32	39	45	51	17
44	01	09	17	25	32	39	45	51	16
45	01	09	17	25	32	39	45	51	15
46	01	09	17	26	32	39	45	52	14
47	01	09	17	25	32	39	46	52	13
48	01	09	17	25	32	39	46	52	12
49	9-9999901	.9999910	9999918	99999925	-9999932	9999939	9999946	9.9999952	11
50	01	10	18	25	33	39	46	52	10
51	02	10	18	25	33	39	46	52	9
52	02	10	18	26	33	40	46	52	8
53	02	10	18	26	33	40	46	52	7
54	02	10	18	26	33	40	46	52	7
55	02	10	is	26	33	40	46	52	
56	02	11	18		33		46	63	5
57	02	11	19	26	33	40	47	53	31
58	03	ii	19		33	40	47	53	2
59	9.9999903	9999911	9999919		9999934	-9999940	9999947		1
60	03	11	19		34	40	47	63.	0.
11	23'	22	21'	20'	19'	18'	17'	16'	"
				LOG, CO	SINE OF			_	

"al	ble 11.]			LOG.	TAN. 8	9°.		1	55
"	36′	37'	38′	39′	40′	41'	42'	43'	"
0	12-1560556			2140492		2575159		12.3058214	60
1		₹ 48544	41744	ذ، 43940	å 56011	₹ 78970		62474	59
1 2 3 4	66592	~ 51695	45038	47391	59634	82785	18024	66738	58
3	69613	54847	49335	50845	63261	86603	22055	71007	57
4	72637	58003	51634	54301	66891	90424	26089	75279	56
b	75662 78690	61160 64320	54935 58239	57760 61222	70524 74160	94249 98077	30127 34169	79556 83837	55 54
5 6 7	81720	67482	61545	64687	77708	2601909	38215	88122	53
8	84751	70646	64854	68155	81440	05743	42264	92411	52
9	87785	73813	68166	71625	85085	09582	46318	96705	51
10	90821	76982	71480	75098	89734	13423	50375	12.3101003	50
iĭ	93860	80153	74797	78574	92385	17269	54435	05305	49
12	96900	83327	78116	82052	96039	21117	58500	09611	48
13	99942	86503	81437	85534	99696	24969	62568	13922	47
14	12.1602987	89681	84762		2403357	28824	66641	18237	46
15	06034	92861	88088	92505	07020	32683	70717	22556	45
16 17	09082 12133	96044 99230	91418 94749	95995 99487	10687 14356	36545 40411	74797 78880	26980 31208	44 43
18	15187	1802417	98084	2202983	18029	44280	82968	35540	42
19	18242		2001421	06481	21705	48152	87059	39876	41
20	21299	06799	04760	09982	25384	52028	91154	44217	40
21	24359	11994	08102	13486	29066	55908	95254	48562	39
22	27421	15191	11447	16993	32751	59791	99357	52912	38
23	30485	18390	14794	20502	36440	63677	2903463	57266	37
24	33551	21592	18144	24015	40131	67567	07574	61624	36
25	36619	24796	21497	27530	43926	71460	11689	65987	35
26 27	39689	28002	24852		47523	75357	15807	70354	34
28	42762 45837	31211 34422	28209 31569	34569 38093	51224 54928	79258 83161	19930 24056	74725 79101	33 32
29	48913		34932		58636		28187	83481	31
30	51993		38298		62346	90980	32321	97866	30
31	55074	44070	41666		66060	94894	36459	92255	29
32	58157	47291	45036		69776		40601	96649	28
33	61243		48410	55754		2702733		12.3201047	27
34	64331	53739	51785	59295	77220	06658	48897	05449	26
35	67421	56967	55164	62839	80946		53051	09856	25
36 37	70513	60197	58545	66386	84675	14519	57209	14267 18683	24 23
38	73609 76704	63430 66665	61929 65315	69936 73489	98409 92144	18455 22394	61371 65537	23104	22
39	79803	69902		77044	95883		69707	27529	21
10	82904	73142		80602	99626	30283	73881	31958	20
11	86008		75490			34233	78059	36392	19
12	89113			87728	07120	38187	82241	40830	18
43	92221	82876		91295	10872	42144	86427	45273	17
44	95331	86126	85689	94865	14628	46105	90617	49721	16
45	98443	89378	89094	98438	18386	50069	94811	54173	15
46 47	12·1701557 04674	92632	92502		22148	54037	99010	58629 63091	14 13
48	07793	95889 99149	95912 99325	05593 09175	25913 29681	58009 61984	3003212 07418	67557	12
49	10914			12760	33453		11629	72027	iĩ
50	14038	05675	06159	16348	37228		15843	76502	10
51	17163	08941	09580	19939	41006			80982	19
52	20291	12211	13004	23532	44788	77922	24284	85466	8
53	23421	15482	16431	27129	48572	81916	28511	89955	7
54	26554	18756	19860	30729	52360		32742	94448	6
55	29688	22033	23292	34331	56152		36977	98947	5 4
56 57	32825 35964	25312 28593	26726 30164	37937	59947 63745	93919 97927	41216 45459	12·3303449 07957	2
58	39106	31877	33604	41546 45157		2801939	49707	12469	3 2
59	42250	35164	37046	48772	71351	05955	53958	16986	1
50	45396	38453	40492	52390	75159	09974	58214	21508	0
"	23′	22′	21'	20′	19'	18′	17'	16'	"
v=-			1	LOG. CO	ran. 0°				

15	В	· · · · · · · ·		LOG. SI	NE 89°.			[Table	n.
"	44'	45'	46′	47'	48'	49'	50′	51'	"
0	9.9999953	9999959	-9999964	9999969	9999974	9999978		9-9999985	60
1	53	ග 59	o 64	œ 69	o 74	o. 78	o 82	85	59
2 3	53 53	59	64 64	69 69	74 74	78 78	82 82	85 85	58 57
4	53 53	59 59	64	69	74	78	82	85	56
5	5 3	59	64	69	74	78	82	85	55
6	54	59	64	69	74	78	82	85 86 86	54
7	54	59	65	70	74	78	82	· 86	53
8	54	59	65	70	74	78	82	86	52
9	9.9999954	9999959	9999965	999997 0	9999974	9999978	9999982	9-9999986	51
10	54	60	65	70	74	78	82	86	50
11	54 54	60 60 60	65 65	70 70	74 74	79 79	82 82	86 86	49 48
13	54	60	65	70	74	79	82	86	47
14	54	60	65	70	75	79	82	96 96 96 96 96	46
15	54	60	65	70	75	79	83	86	45
16	55	60 60	65	70 70	75	79	83 83	86	44
17	55	60	65	70	75	79	83	86	43 42
18 19	55 9 -9999 955	-9999960	·9999966	70 •9999970	75 -9999975	79 •9999979	-9999983	9-9999986	41
20 21	55 55	60 61	66 66	71 71	75 75	79 79	83	96 96	40 39
22	55	61	66	71	75	79	83 83	96 96 96 96 97 97	38
23	55	6î	66	71	75	79	83	96	37
24	55	61	66 66	71	75	79	83	86	36
25	55	61	66	71	75	79	83	86	35
26	55	61	66 66	71	75	79	83	87	34 33
21 22 23 24 25 26 27 28	56	61 61	66	71 71	75 76	90 90	83 83 83	87	33
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31	56 56	61 61	67 67	71	76 76	80 80	83 83	87	20
32	56	62	67	71	76	80	84	87 87	29 28
33	56	62	67	72	76	80	84	87	27
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35	56	62	67	72	76	80	84	87	25
36 37	56 57	62 92	67 67	72 72	76 76	80 80	84 84	87 87	24 23
38	57	62	67	72	76	80	84	87	22
39	9.9999957	9999962	9999967	9999972	9999976	.9999980	9999984	9 9999987	21
40	57	62	67	72	76	80	84	87	20
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42 43	57	62	67	72 72	77	81	84	87	18 17
44	57 57	63 63	68 68	72	77 77	81 81	84 84	87 87	16
45	57	63	68	72	77	81	84	87	15
46	57	63	68	73	77	81	84	88	14
47	57	63	68	73	77	61	84	88	13
48	58	63	68	73	77	81	84	88	12
49 50	9-9999958	·9999963	9999968	9999973	9999977	·9999981	9999985	9 ·999 9988	11
51	58 58	63 63	68 68	73 73	77 77	81 81	85 85	88	10
52	58	63	68	73	77	81	85	88 88	8
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55	58	64	69	73	77	81	85	98 99 98 98	5
56 57	58	64	69	73 73	77	81	85 85	98 88	4
58	58 58	64 64	69 69	73 73	78 78	81 82	85 85	88 88	2
59	9.9999959	·9999964	·9999969	-9999973	·9999978	9999982	9999985	9.9999988	ĩ
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2	30565	11461	11787					28354 36419	59 58
ã	35101	16300	16973					44499	57
4	39641	21144						52594	56
5	44187	25994	27363		4601174			60704	55
6	48787 53291	30849 35710	32567 37778	56821 62436	07252 13339		5406375 13692	68829 76970	54
8	57851	40576	42995	68058			21022	85125	53 52
ğ	62415	45447	48218	73687	25538		28365	93297	51
10	66985	50324	53447	79324	31651	15103	35719	12-5901483	50
11	71559	55207	58683	84968	37772	21790	43087	09685	49
12	76137	60095	63925	90619	43902		50466	17903	48
13 14	80721	64388	69173	96278		35194	57859	26136	47
15	85310 89903	69887 74792	79689	4301944 07617	56187 62343	41912 48640	65263 72681	34384 42649	46 45
16	94501	79702	84956	13298	68508	55379	80111	50929	44
17	99104	84618	90230	18986	74681	62128	87554	59225	43
18	12:3403712	89539	95510	24682	80863	68887	95010	67537	42
19	08325	94466	4000797	30385	87054	75657	5502479	75865	41
20	12943	99398	06090	36096	93254	82438	09960	84209	40
21 22		3704336	11389	41814	99463	89229	17454	92569	39
23	22193 26826	09280 14229	16696 22008	47540 53273	4705681 11907	96031 5102843	32482	12·6000945 09337	38
24	31463	19184	27327	59014	18142	09666	40015	17745	36 I
25	36105	24145	32653	64762	24387	16500	47562	26170	35
26	40753	29111	37985	70519	30640	23345	55121	34611	34
27	45405	34083	43323	76282	36903	30201	62694	43069	33
28 29	50063	39061	48669	82054	43174	37067	70290	51543	32
30	54725	44044	54020	87833	49455	43944	77879	60033	31
31	59392 64065	49033 54028	59379 64744	93620 99414	55744 62043	50832 57731	95492 93118	68541 77065	30 29
32	68742	59028	70116	4405216	68351		5600757	85605	28
33	73425	64035	75494	11026	74668	71563	08410	94163	27
34	78112	69047	80879	16844	80994	78495		12.6102737	26
35 36	82805	74065	86270	22670	87330	85438	23756	. 11329	25
37	87503 92205	79039 84118	91669 97074	29503	93674 4800028	92392 99358	31449 39157	19937 28563	24 23
38	96913		4102486	40194			46877	37206	22
39	12.3501626	94195	07904	46051	12764	13322	54612	45866	21
40	06344	99242	13330	51916	19146	20321	62360	54543	20
41		3804295	18762	57788	2553 8	27332	70123	63237	19
42 43	15796	09353	24201	63669	31939	34354	77899	71949	18
44	20529 25268	14418 19489	29647 35099	69558	38349 44769	41387 49431	85699 93493	80679 89426	17 16
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46	34761	29648	46025	87272	57637	62555		12-6206974	14
47	39515	34736	51498	93193	64085	69634	16990	15774	13
48	44275	39831	56978	99122	70543	76724	24850	24592	12
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50 51	53809	50037	67959	11005	83488	90940	40614	42282	10
52	58584 63365	55150 60268	73460 78968	16958 22920	89975 96472	98066 5305203	48519 56436	51155 60045	9
63	68150	65393	84483		4902978	12352	64368	68954	7
54	72941	70523	90005	34867	09494	19513	72315	77881	6 5
55	77738	75660	95534	40853	16020	26685	80276	86826	5
56 57	82539		4201070	46848	22556	33870	88252	95790	4
56	87346 92158	85951 91106	06613 12163	52851 58862	29101 35657	41066 48274	5804248	12·6304772 13773	3 2
5 9	96976	96267	17720	64881	42222	55494	12269	22793	ĩ
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11	52"	53'	54'	55'	56'	57'	58'	59'	1
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B	. 89	91	94	96	97	98	99	00	
	99999989	-9999991	9999994	-9999996	9999997	-99999999	9-9999999		
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il	89	91	94	96	97	99	99	00	
2	89	92	94	96	97	99	99	00	
3	89	92	94	96	97	99	99		
4	89	92	94	96	97	99	99	00	
5	99	92	94	96	97	99	99	00	a
6	99	92	94	96	97	99	99		4
7	89	92	94	96	97	99	99	00	1
8	89	92	94	96	97	99	99		3
	9999989	-9999992	9999994	-9999996	9999999		9-9999999		
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2	89	92	94	96	98		10-00000000	00	4
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7	90	92	94	96	99				
8	90	92	94	96	98	0.0	00		
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NATURAL SIGNS AND TANGENTS

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5	001	4544		9066	000	3530				2073		6046		9748	120	312~	55
6		7453	019			6437	054	0798		4974		8943	106	2641		6015	54
7	002	0362		4883		9344		3693			089	1840		5533		8901	53
8		3271		7791	037	2251		6597	072	0777		4738		8425	124	1788	52
9		6180	020	0699		5158		9502		3678		7635	107	1318		4674	51
10		9089		3608		8065	055	2406		6580	090	0532		4210		7560	50
11	003	1998		6516	038			5311		9481		3429			125	0446	49
12		4907		9424		3878				2382		6326		9994		3332	48
13			021	2332	l		066	1119		5283		9223	108			6218	47
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24		9913		4322		8757		3064		7190	094	1083		4689		7956	36
25	007	2721			042	1663		5 967	077			3979			129	0841	35
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47	ĺ	6713	031			5592		9836		3 880		7669	118			4274	13
48		9622		4108		8498	066			6778	101			4040		7156	12
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27		8541	الكان	3127		7866	060			8237	090		113	0517		7648	33
28	008	1450		6038	043		-	5787	078			7019	***		131	0607	32
29		4360		8948		3695		8706		4090		9955		6410		3566	31
30		7269	026				061	1626		7017	096	2990		9356		6525	30
31 32	009	0178 3087		4770 7681	044	9524 2438		4546 7466	070	9944 2871		5826 8763	114	2303 5250	120	9484 2444	29 28
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34		8905		3503		8268	-	3306		8726		4635	115	1144		8364	26
	010	1814			045	1183			080	1653		7572		4092	133	1324	25
36 37		4724 7633	ດາວ	9325		4097	روي	9147 2067		4581 7509	098	0509 3446		7039		4285	24 23
	011	0542	V.20	5148		9927	003	4988	081	0437			116	9987 2936	134	7246	22
39		3451			046	2842		7908		3365		9320	***	5884		3168	21
40		6361	029	0970		5757	064	0829		6293	099	2257		8832		6129	20
41		9270		3882		8673		3750		9221		5194	117	1781		9091	19
42 43	012	2179		6793 9705	047	1588				2150	100	8133		4730			18
44		5088 7998	030	2616		4503 7419	065	9592 2513		8007	100	1071	110	7679 0628		5015 7978	17 16
45	013	0907		5528	048	0334	200	5435	083	0936		6947	1	3578			15
46		3917	00.	8439		3250		8356		3865		9886		6529		3903	14
47 48		6726	031	1351 4263		6166	V66					2824		9478		6866	13
49	014	9635 2545		7174	049	9082 1997		4199 7121		9723 2653		5763 8702		2428 5378		9830 2793	12 11
50			032	0086	1 23		067	0043	1		1	1641		8329	1	5757	10
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53 54		4183	022	8822		3662	000	8809		4372	103	0460		7192		4650	7
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58		8731		3383		8244		3422		9025				1941		9476	2
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25 26		708 585		6129 8999	101	8052	100	9425 2276	215	0194 3035	232	0309 3138	240	9716 2533	266	8366 1170	35 34
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29 30	_	217	165	7607 0476			199	0829 3679	216	1550 4396	233		250)	0984 3800	267	9581 2384	31
31	148 0		100	3345	182	2355 5215		6530		7236		4454 7282		6616	201	5197	29
32		848		6214		8075		9380	217	0076	234	0110		9432		7989	28
33 34		724 601	166	$9082 \\ 1951$	183	0935 3795	200	2230 5080		2915 5754		2938 5766	251	2248 5063	268	0792 3594	27 26
35	149 2	477	100	4819		6654		7930		8593		8594		7879		6396	25
36 37		353	167	7687 0556	104	9514 2373		0779 3629	218		235	1421 4248	252	0694 3508	269	9198 2000	24 23
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50		5607		7828										0082		8400	10
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55 56	155 2	9978 2851	172	2156 5022		3811 6667		4898 7734		5337 8172		5104 7927		4139 6950		2390 5187	5
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3 4	140	7276 0243	159	2791 5774	177	5270		5881		4688 7730 0772	232	7876 0941 4007	250	2551 5642 8734	269	6847 1967 5087	57 F6
6 7	142	3211 6179	160	8757 1740 4724	178	8270 1271 4273		1922 4943		3814	İ		251	1826 4919	270	8207	54 53
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10 11		5084 8053		3677 6662		3279 6281		4008 7031	1	5988 9032		9342 2410		4200 7294	271		F0 49
12 13	144	1022 3991	162	9647 2632	160	9284		0053 3076	216			5479 8548	253	0389	272	6940 0064	48 47
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20 21 22	147	4784 7756 0727		3537 6525		3319 6324		4248 7274		6448 9496	237	3116	050	5165 8264	274	5072	40 39
23 24	121	3699 6672	165	9513 2501 5489	183	9330 2337 5343	201	0300 3327 6354	219	5593 8643	920	6189 9262	200		275	8201 1330 4459	38 37 36
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27 28		5590 8563		4456 7446		4365 7373		5437 8465	221	7793 0844	239	1560 4635		6868 9970		3850 6981	33 32
29 30	149	1536 4510	167	0436 3426	185	0382 3390	203	1494 4523		3895 6947	240		258	3073 6176	277	0113 3245	31 30
31 32	150	7484 0458		6417 9407		6399 9409	204	7552 0582	222	9999 3051		3864 6942	259	9280 2384		6378 9512	29 28
33 34 35		3433 6408 9383	168	2398 5390	186	5428		3612 6643 9674	ດດາ	6104 9157	241	3097	000	5488 8593	278	5780	27 26 25
36 37	151	2358 5333	169	9381 1373 4366	187	8439 1449 4460	205	2705 5737	223	5265 8319	242	6176 9255 9334	200	4805 7911	279	8915 2050 5186	24 23
38 39	152	8309 1285	170	7358	188	7471 0483	206	8769	224	1374 4429	~1~	5414 8494	261	1018 4126	280	8322	22 21
40 41		4262 7238		3344 6338		3495 6507		4834 7867	225	7485 0541	243	1575 4656	262	7234 0342		4597 7735	20 19
42 43	153	0215 3192	171	9331 2325	189	9520 2533	207	0900 3934		3597 6654	244	7737 0819		3451 6560	281	0873 4012	18 17
44 45 46	154	6170 9147		5320 8314		5546 8559	208		226	9711 2769			263	9670 2780	282		16 15
47 48	104	2125 5103 8082	172	1309 4304 7300	190	1573 4587 7602		3038 6073	227	8885 1944		0068 3151 6236	264	5891 9002 2114		3432 6573 9715	14 13 12
49	155	1061	173		191		209		~~.	5003		9320 2405	201		283	2857 5999	iî 10
51 52		7019 9998		6288 9285		6648	210		228	1123 4184		5491 8577	265	1452 4566	284	9143 2286	9
53 54	156	2978 5958	174	2282 5279	192			4293			247	1663	266	7680 0794		5430 8575	7
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57 58 59	150	4900 7881 0863	170	4273 7272	104	4748 7766		6446 9486	230	9492 2555 5618		4013 7102		3257			3 2 1
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7		5941		3183		9529		49:8			360	2682 5395		4938		6047	53
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20 21	281	2251 5042	298	9303 2079		5448 8209	331	3379		4812 7540	364	7932 0641	380	9944 2634	396	3468	40 39
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31 32		2942	201	9832 2606		5805 8563	334	0810 3552		4798	367	7719 0425	353	9522 2209	399	0158 2825	29 28
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39			303	2016			336	2735	1	6584			385	1008	401	- 1	21
40 41	287	8032 0819		4788 7559	320	0619 3374		5475 8214		9306 2027	369	2061 4765		3693 6377		4150 6814	20 19
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43 44		6391 9177			321	6885 1640		3691 6429	354	7469 0190	3/0	2872	360	1744 4427	402	4804	16
45 46	288	1963	31) =	8643 1413		4395	330	9167 1905		2910 5630		5574 8276		7110 9792	402	7467 0129	15 14
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57 58		5371 8153	308	1869 4636	325	7429 0180	341	2000 4734		5531 8248	374	7973 0671	390	9277 195 5	406	9393 2051	3 2
59	292	0935		7403		2931	240	7468	358	0964		3369		4633		4709	ī
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34		4796		5785		8396	1	4286	375	2115	395	2552	710	5774	433	1966	26
35 36	200	7962 1129	317	8986 2187	336	2134 5372	256	7562 0840		5433 8753		5916 9280	410	9186		5429	25 24
37	200	4297	.,,,	5389		8610	350		376	2073	396		410	2598 6012	437	8893 2357	23
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50		8609		9661		8681		5630	705	0469		3161		3668		1953	10
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9		8941		4246		7246		7909		6198		2083		5530		6509	51
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23	25635	23979	38679	71030	22465	94571		1:4308039	
4	32146	30754	45736	78393		1-3002624	97551	16906	
6	39662	37532	52799	95762	37860	10684		25781	
5	45182	44316	69866	93136	45566	18750	14458	34664	
7	51706	51104		1-2400515	53277	26822	22922	43554	
8	58235		74015	07900	60995	34900	31392		
9	64768	64693	81097	15290		42984			
- 1					69718		39869		
0	71305	71495	68184	22685	76447	51075	48353		
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2	84391	85112	1-2002373	37492	91922	67276	65342	68114	
3	90941	91927	09475	44903	99669	75386	73947	97049	
4	97495	98747	16591	52320	1/2907421	83502	82358	1-4405991	
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6	10616	12400	30810	67169	22943	99753		23897	
7	17183	19234	37932	74602	30713		13907934	32862	
8	23754	26073	45058	82040	38488	16029	16473		
9				89484				A G TOTAL A	ч
	30329	32916	52190		46270	24177	25019	00014	н
20	36909	39763	59327	96933	54057	32331	33571	59301	
1	43493	46615	66468	1:2504389	61850	40492	42131	68796	
22	50081	53472	73615	11848	69649	48658	50698	77798	
23	56674	60334	90767	19313	77454	56832	59272	86808	
24	63271	67200	87924	26784	85265	65011	67852		
25	69872	74071	95085	34260	93081	73199	76440		
6	76478	80947		41742		81390	85034	13863	
27		87827	09424	49229	09733	89589			
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	89702	94712	16601	56721	16567	97794		31971	
29	96321	t·1701601	23783	64219	24407	1-3506006	10860	41027	
nois	1-1302944	08496	30970	71723	32254	14224	19483	50000	ıls
31	09571	15395	38162	79232	40106	22449	28113	69161	E
32	16203	22298	45359	86747	47964	30680	36749	68240	
33	22839	29207	52562	94267	55828	38918	45393	77326	
14	29479	36120	59769		63699	47162	54044	86420	
15	36124	43038	66982	09323	71575	55413	62702	95522	
36	42773	49960	74199	16860	79457	63670		1 4604600	
							71367	14604632	1
37	49427	56888	81422	24402	87345	71934	80039	13749	1
18	56085	63820	88650	31950	95239	80204	98718	22974	1
19	62747	70756	95883	39503	1.3103140	88481	97406	32007	1
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11	76086	84644	10364	54626		1.3605054	14799	50296	
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4	96126	1-1805512	32125	77353	42731	29963	40943	77788	
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6		19447	46658	92532		46602			
7	09508	26422			58610		58409	96155	
	16206			1-2700130	66559	54931		14705350	
8	22908	33402	61211	07733	74513	63267	75904	14553	
9	29615	40387	69496	15342	82474	71610	84662	23764	[]
(6)	36326	47376	75796	22957	90441	79959	93427	32983	1
1	43041	54370	83081	30578	98414	88315		42210	
2	49762	61369	90381	38204		96678	10979	51445	
3	56486	68373	97697	45835	14379	1.3705047	19766	60688	
4	63215	75382	1-2304997	53473	22370	13423	29561	69938	
		82395				21906			
5	69949		12313	61116	30368		37362	79197	
56	76687	89414	19634	68765	35371	30195	46171	88463	
57	83429	F6437	26961	76419	46381	38591	54998	97738	-
18		1 1203465	34292	94079	54397	46994		1 4907021	1
	96928	10498	41629	91745	62420	55403	72642	16311	
				00440	80440	Charle	D1.400		1
9	1603684	17536	48972	99416	70446	63919	81480	25610	
	1503684 41°	17536 40°	48972 39°	380	370	360	350	340	

176		/u/ +:	-			-	NAT	. 81	NE.	-				۲,	Table	777
-,-	1 56 °	57	10 I	5	80		90		00	1 6	10	6	20	L	30	
o	829 0376					857			0254		6197				0065	60
1	2002		3290		2022		3171		1708			883	0841		1385	59
2	3628 5252		3873		3562 5102		4668 6164		3161 4614	07E	9016 0425		2206 3569		2705 4024	58 57
4	6877		1455 3037		6641		7660		6066	010	1832		4933		5342	56
5	8500	4	1618		8179		9155		7517		3239		6295		6659	55
6	830 0123		6199		9717	858	0649	000	8967		4645		7656		7975	54
8	1745 3366		7778 9357	849	1254 2790		2143 3635	867	0417 1866		6051 7455	884	9017 0377	892	9291 0606	53 52
9	4987	840 0			4325		5127		3314		8859		1736		1920	51
10	6607	2	2513	1	5860		6619		4762	976	0263		3095		3234	50
11	8226		1090		7394		8109		6209		1665		4453		4546	49
12	9845 831 1463		5666 7241	OEA	8927	orn	9599 1088		7655 9100		3067		5810		5858	48
13 14	831 1463 3080		3816	000	0459 1991	009		868	0544		4468 5868		7166 8522		7169 8480	46
15	4696	841 (0390		3522		4064		1988		7268		9876		9789	45
16	6312		1963		5053		5551		3431	~~	8666	385	1230	893		44
17 18	7927 9541		3536 5108		6582 8111		7037 8523		4874 6315	877	0064 1462		2584 3936		2406 3714	43
19	832 1155		6679		9639	860			7756		2858		5288		5021	41
20	2768	1		851	1167		1491		9196		4254		6639		6326	40
21	4380	9	9819		2693		2975	869	0636		5649		7989		7632	39
22 23	5991 7602		1388 2956		4219 5745		4457 5939		2074 3512		7043 8437	000	9339 0688	004	8936 0240	38
24	9212		1524		7269		7420		4949		9830	000	2036		1542	36
25	833 0822		091		8793		8901		6386	878	1222		3383		2844	35
26 27	2430			852		861	0380		7821		2613		4730		4146	34
27	4038 5646	843 0	222		1839 3360		1859 3337	870	9256 0691		4004 5394		6075 7420		5446 6746	33 32
29	7252		2351		4881	,	4815	010	2124		6783		8765		8045	31
30	8858	1	3914		6402		6292		3557		8171	887	0108		9344	30
31	8 34 0463	5	5477		7921		7768		4989		9559		1451	895	0641	29
32	2068 3672		039	053	9440 0958	060	9243		6420	879	0946 2332		2793 4134		1938	28 27
34		844 0			2475	002	2191		7851 9281		3717		5475		3234 4529	26
35	6877	1	720		3992		3 664	871	0710		5102		6815		5824	25
36	8479		3279		5508		5137		2138		6486		8154		7118	24
37 38	835 0080 1680		1838 395		7023 8539		6608 8079		3566 4993		7869 9251	222	9492 0830		8411 9703	$\frac{23}{22}$
39	327 9			854	0051		9549		6419	880	0633	300		896	0994	21
40	4878		9508		1564	863	1019		7844		2014		3503		2285	20
41	6476	845 1	1064		3077		2488		9269		3394		4838		3575	19
42	8074		2618		4588 6099		3956	872			4774		6172		4864	18
44	9670 93 6 1 266		1172 5726		7609		5423 6889		2116 3538		6152 7530		7506 8839		6153 7440	17 16
45	2 862	7	7278		9119		8355		4960		8907	889	0171		8727	15
46	4456				0627	00.4	9820		6391	881			1503	897	0014	14
47	6050 7643	946 0)381 1932		2135 3643	604	1284 2748		7801 9221		1660 3035		2834 4164		1299 2584	13 12
49	9236		3481		5149		4211	873	0640		4409		5493		3868	11
50	337 0827		5030		6655		5673		2058		5782		6822		5151	10
51	2419	6	5579		8160		7134		3475		7155		8149		6433	9
52 53	4009		3126 3673	856	9664 1168	ocr	8595		4891 6307		9527 9898	000	9476 0803		7715	8
54	5598 7187		1219	900	2671	900	1514		7722	882		090		898	8996 0276	6
55	8775	2	2765		4173		2973		9137	302	2638		3453		1555	5
56	839 0363	4	4309		5674			874	0550		4007		4777		2834	4
57 58	1950 3536		5853 7397		7175 8675		5887 7344		1963 3375		5376 6743		6100 7423		4112 5389	3 2
59	5121			857	0174		8799		4786		8110		8744		6665	î
60	6706	848 (0481		1673		0254		6197		9476		0065		7940	Ô
'	33°	32	30	3	10		0°		90	2	80	2	70	2	60	,
·						N.	AT. C	OSI	NE.				-		~	

	able in.]			NA	T. TAN.			17
1	560	570	580	590	60°	61°	620	630
0	1.4825610	1-5398650		1.6642795				1.9626108
1 2		1-5406460	13709	53766	32149	52860	20470	
	44231	18280	24082	64748		65256	33690	
3	53554	28108 37946	34465	75741 86744	55468 67144	77664	46924 60172	
5	62884 72223	47792	44858 55260	97758		1.6102521	73436	
6	81570	57647	65672	1.6708782		14969		1-9711077
7	90925	67510	76094		1.7402245		1-8900006	25296
B	1-4900288	77383	86525	30864	13969	39904	13313	39531
9	09659	87264	96966	41921	25705	52391	26635	
10	19039		1 6107417	52988		64892	30971	68050
11			17878	64067	49213	77405	53322	
12	28426 37822	16963	28349	75156	60984	89932	666S8	82334 96635
13	47225	26880	38829	86256		1-8202473		1-9810952
14	56637	36806	49320	97367	84564	15026	93464	25286
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16	75486	56685	70330		1:7508191	40173	20299	54003
17	84923	66639	80850	30765	20023	52767	33739	68387
S	94367	76601	91380	41919		65374	47193	82787
19	1:5003P21		1-6201920	53085	43722	77994	60663	
20	13282	96552	12469	64261	55590	90628		1-9911637
21		1 5606542	23029	75449		1.8303275	87647	26087
22	32229	16540	3359	86647	79362		1-9101162	40554
23	41716	26548	44178	97856	91267	29610	14691	55038
24	51210	36564			1.7603183	41297	28236	69539
25	60713	46590	65368	20308	15112	53999	41795	84056
265	70224	56625	75977	31550	27053	66713	55370	98590
27	79743	66669	86597	42804	39007	79442		2-0013142
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29	98807		1.6307967	65344		t-8404940		42296
20	1.5108352	96856	18517	76631	74940		1 9209921	56897
31		1-5706936	29177	87929	86943	30492	23472	71516
32	27466	17020	39847	99238	98958	43289	37138	66153
33	37036	27126	50528			56099	60919	
34	46614	37234	61218	21890	23024	68923		
35	56201	47352	71919	33233	35076		78228	30164
36	65796	57479	82630	44587	47141	94613		44869
37	75400	67615	93351	55953	59216	1 8507479	1.9705699	59592
39	85012	77760	1 5404082	67329	71307	20358	19457	74331
39	94632	87915	14824	78717	83409	33252	33231	89088
40	1.6204261	98079	25576	90116	95524	46159	47020	2-0203862
41	13899	1.5808253	36338	1.7101627	1 7807651	59080	60925	
42	23545	18430	47111	12949		72015	74645	
43	33200	, 28628	57893	24382		84965	88481	48289
44	42863	38830	68687	35827	44107		1-9402333	63133
45	52535	49041	79490	47263		1.8610905	16200	77994
46	62215	59261	90304	58751	68475	23596	30083	92873
47	71904		1.6501128	70230		36902		2.0 07765
48	81602	79731	11963	81720		49921	57896	22693
49	91308	39971	22808	93222	1.7905121	62955	71826	37615
50	1.5701023			1:7204736	17362	76003	85772	52565
60 A	10746	10505	44529	16261	29616			67532
	20479	20763	55405	27797		1-8702141		82517
52		31070	66292	39346	54162	15231	27704	97519
52 53	30219			50905	66454	28336		20112540
52 53 54	39969	41366	77189		1 700 m/d	41455	55739	27578
52 53 54 55	39969 49727	41366 51672	98097	62477	78759			
52 53 54 55 56	39969 49727 59494	41366 51672 61987	99016	62477 74060	91077	54588	69780	42634
51 52 53 54 55 56 57	39969 49727 59494 69270	41366 51672 61987 72312	99016 1-6609945	62477 74060 65654	91077; 1/8003408	54588 67736	69780 83837	42634 57706
52 53 54 55 56 57 58	39969 49727 59494 69270 79054	41366 51672 61987 72312 92647	99016 99016 1-6609945 20884	62477 74060 65654 97260	91077 1-8003408 15751	54588 67736 80898	69780 83937 97910	42634 57706 72800
52 53 54 55 56 57 58	39969 49727 59494 69270 79054 89848	41366 51672 61987 72312 82647 92991	99016 99016 1-6609945 20884 31934	62477 74060 65654 97260 1-7308878	91077 1-8003408 15751 28108	54588 67736 80898 94074	69780 83937 97910 1-9612000	42634 57706 72800 87910
52 53 54 55 56 57 58	39969 49727 59494 69270 79054 89848	41366 51672 61987 72312 92647	99016 99016 1-6609945 20884	62477 74060 65654 97260	91077 1-8003408 15751 28108	54588 67736 80898	69780 83937 97910 1-9612000	42634 57706 72800

W

178				NAT.	SINE.			[Table	
,	640	65°	66°	670	680	690	70°	710	
0		906 3078					939 6926 7921	945 5186	
1	9215 899 0489	4307 5535	6637 7819	6185 7320	2928 4016	6846 7888	8914	6132 7078	
3	1763	6762	9001	8455	5104	8928	9907	8023	
4	3035		914 0181	9589	6191		940 0999	8968	
5	4307	9215		921 0722		934 1007	1891	9911	5
6	5578 6848	907 0440 1665	2540 3718		9363 9447	2045 3082	2881 3871	946 0654 1795	
8	8117	2888	4895		928 0531	4119	4860	2736	
9	9386	4111	6072		1614	5154	5848	3677	E
10	900 0654	5333	7247	6375	2696	6199	6835	4616	4
11 12	1921 3189	6554 7775	8422 9597	7504 8632	3778 4858	7223 8257	7822 8808	5555 6493	
13	4453		915 0770		5938	9289	9793	7430	4
14		908 0214	1943	922 0884	7017	935 0321	941 0777	8366	4
15	6982		3115	2010	8096	1352	1760	9301	4
16 17	9246 9508	2649 3866	4286 5456	3134	9173 929 0250	2392 3412	2743 3724	947 0236 1170	3
18	901 0770	5082	6626	5381	1326	4440	4705		
19	2031	6297	7795	6503	2401	5468	5686		
20	3292	7511	8963		3475	6495	6665	3966	1
21 22	4551	8725 9938	916 0130 1297	9745 9865	4549 5622	7521 8547	7644 8621	4897 5827	
23	5810 7068	909 1150		923 0984	6694	9671	9598	6756	1
24	8325	2361	3627	2102		936 0595		7684	1
25	9582	3572	4791	3220	8835	1618	1550	8612	
26 27	902 0838	4781 5990	5955	4336	9905 930 0974	2641 3662	2525	9539 948 0464	
28	2092 3347	7199	7118 8279	6567	2042	3002 4683	3498 4471	1385	
29	4600	8406	9440	7682	3109	5703	5444	2313	
30	5853	9613	917 0601	8795	4176	6722	6415	3237	
31		910 0819 2024	1760	9908 9 24 1020	5241 6306	7740 8758	7386 8355	4159 5081	
32 33	8356 9606	3228	4077	2131	7370	9774	9324	6002	1
34	903 0856	4432	5234	3242		937 0790		6922	1
35	2105	5635	6391	4351	9496	1806	1260	7842	
36 37	3353 4600	6837 8038	7546 8701	6568	931 0558 1619	2S20 3S33	2227 3192	8766 9678	
38	5847	9238	9855	7676	2679	4846	4157	949 0595	
39		911 0438			3739	5858	5122	1511	:
40	8338	1637	2161	9888	4797	6869	6085	2426	9
41	9582	2835		925 0993	5855	7880	7049	3341 4255]
42 43	904 0825 2068	4033 5229	4464 5614	2097 3201	6912 7969	8889 9 898	8010 8971	5168	
44	3310	6425	6763			938 0906	9931	6080	
45	4551	7620	7912		932 0079		944 0890	6991	
46 47	5792	\$815 912 (1008	9066	6506 7606	1133 2186	2920 3925	1849 2807	7902 8612	
48	8271	1201	1353		3238	4930	3764	9721	1
49	9509	2393	2499		4290	5934		950 0629	
50	905 0746			926 0902	5340	6938	5675	1536	:
51	1983	4775	4788	2000	6390 7439	7940	6630 7594	2443	
52 53	3219 4454	5965 7154	5931 7073	3096 4192	8488	8942 9943	7584 8537	3348 4253	
54	5688		8215	5286	9535	939 0943	9489	5157	
55	6922		9356		933 0582		945 0441	6061	
56	9386 9386	913 0716 1902	9 20 04 96 1635		1628 2673	2940 3938	1391 2341	6963 7865	
57 58	906 0618		2774	9658	3718	4935	3290	2766	
59	1848	4271	3912	927 0748	4761	5931	4238	9666	
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60	250	240	230	220	210	20°	19°	180	1

T_i	able III.]			NAT	TAN.			17	9
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3	48531	94021	2-2513221	23615801	24813190	2-6113995	49554	2-9124649	
4	63732	2-1510378	30885	34946	34023	41766	74561	52286	56
5	78950	26757	48572	64118	54887	64571	99608	79909	55
6	94187	43156	66283	73316	75781		2.7624695	249207610	
7	2'0609442	59575	84016	92540		2.6210296	49822	35358	
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9	40008	92476	19554	31068	38645		27700199	90995	
10	55710	2-1608958		50372	59661	79121		2-9315885	100
11	70646	25460	55184	69703		2 6302136	50738		
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	2 0701359	58527		2.3803444	2.5001784			74807	193
14	16743	75091		27855	22891	71392	26853	2-9402840	
15	32146	91677			44029			30921	
			26729		65198	94549	52307	59050	
16		2-1708283	44674			2:6417741	77802	87227	
17	63007	24911	62643		2 5107629			2-9515453	
18	78465	41559		2-3905769	MODI-O	64232	29917	43727	
19	93942	58229	99653		1	87531	64537	72050	
	2-0609438		2-2916693		71507	2.6510867	80198	2.9600422	46
21	24953	91631	3475B			34238	28005901	28842	35
22		2.1808364	52846	84118	2-5214249	57645	31646		
23	56039	25119	70959	2-4003774		81089	57433	85831	
24	71610	41894	89096			2:6604569	83263	2 9714399	
25	87200	58691	2-2907257	43168		28085	28109164	43016	
26	2 0902809	75510			2.5000111	5163B	35048	71/83	
27	18437	92349				75227		29800400	
28		2-1909210		24102465		98853	87003	29167	
29	49751	26093	80143			2-8722516		57983	
30	65436	42997	98425		0.4.2.00	46215	39129	86850	
31	81140		2:3016732			69951			
32	96864	76871	35064		2·5408151 29855	93725	91426	2-9915766	
	≥1012607	93840				2-6817535		44734	
34		2.2010831	die and	24201851				73751	
35			71801			41383		3-0002820	
36	44150	27843	2:3108637			65267 89190	70196	31939	
37	59951	61934			2-5516992		96539	61109	
38	75771				38858		2-0122926	90330	
	91611	79012		2-4301938		37147		3.0119603	
	2-1107470	96112	64076	22041	82686	61191	76831	48926	2]
40		2 2113234	82606		2:5604649		2.8502349		
41	39246	30379	2:3201160	62331	26645	2.7009364	28911	3 0207728	
42	55164	47545			48674	33513	55517	37207	
43	71101	64733	38345	2.4402736	70735	57699	82168	66737	
44	87057	81944	56975			81923	9-9608863	96320	
	2-1203034	99177	75630		2.5714957	2-7106186		3 0325954	
46		2-2216432		63559	37118	30487	62386	55641	
47	35046		2-3313017	93891	59312	54826	89215	85381	
48	51082	51009		2.4504252				3-0415173	
49	67137	68331	50505		2-5603900		43007	45018	
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		2-2003043	88095		48421	52569		3.0504966	
	2-1315423	20433			70782		2-8824033	34870	
53	31559	37845	25787		93177	27301674	61132	64929	
54	47714	55280	44672		2-5915606	26284	78277	95038	
55	63890	72738	63582		38068	50934	2.8905467	3 0625203	
56	80085	90218			60564	75623	32704	55421	
67	96301		2:3501491	88616		2.7400352	59986	85694	
	2.1412537	25247			2-6005659	25120	87314	3.0716020	1
59	28793	42796			28258		2-9014699	46400	
60	45069	60368	58624	60869	50891	74774	42109	76835	1
		100.4			A PAN -	I mon	300		4 .
1	250	240	230	220	210	200	190	180	Ľ

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180				NAT.	SINE.			[Table	ш.
1	72°	73°	740	75°	760	770	78°	.79°	·
Ŷ	951 0565 1464	956 3048 3898	961 2617 3418	965 9258 966 0011	970 2957 3661	974 3701 4355	978 1476 2080	981 6272 6826	60 59
1 2 3	2361	4747	4219	0762	4363	5008	2684	7380	59
3	3258	5595	5019	1513	5065	5660	3287	7933	57
5	4154 5050	6443 7290	5818 6616	2263 3012	5766 6466	6311 6962	3889 4490	8485 9037	56 55
6	5944	8136	7413	3761	7165	7612	5090	9587	54
7	6838	8981	8210	4508	7863	8261		982 0137	53 52
8	7731 8623	9825 957 0669	9005 9800	5255 6001	8561 9258	8909 9556	6288 6886	0686 1234	51
10	9514	1512		6746	9953	975 0203	7483	1781	50
11	952 0404	2354	1387		971 0649	0849	8079	2327	49
12 13	· 1294 2183	3195 4035	2180 2972	8234 8977	1343 2036	1494 2138	9674 9268	2873 3417	48 47
14	3071	4875	3762	9719	2030 2729	2781	9862	3961	46
15	3958	5714	4552	967 0459	3421		979 0455	4504	45
16 17	4844 5730	6552 7389	5342 6130	1200 1939	4112 4802	4065 4706	1047 1638	504 6 55 87	44
18	6615	8225	6917	2678	5491	5345	2228	6128	42
19	7499	9060	7704	3415	6180	5985	2918	6668	41
20	8382	9895	8490	4152	6867	6623	3406	7206	40
21 22	9264 953 0146		9275 963 0060	4888 5624	7554 8240	7260 7897	3994 4581	7744 8282	39 38
23	1027	2394	0843	6358	8926	8533	5167	8818	37
24	1907	3226	1626	7092		9168			36 35
25 26	2786 3664	4056 4886	2408 3189	8557	972 0294 0976			9888 983 0422	34
27	4542	5715	3969	9288	1658	1068	7504	0955	33
28 29	5418			968 0018	2339	1699 2330	8086		32 31
30	6294 7170	7371 8197	5527 6305	0748 1476	3020 3699		1	2019 2549	30
31	8044	9023		2204	4378			3079	29
32	8917	9848		2931	5056		980 0405		28
33 34	9790 9 54 0662	959 0672 1496		3658 4383	5733 6409				27 26
35	1533	2318	964 0181	5108		6098			25
36	2403			5932		6723	2712		24
37 38	3273 4141	3961 4781		6555 7277	8432 9105				23 22
39	5009								21
40	5876				973 0449				20
41	6743		4806	9439 969 0157					19
43	7608 8473					977 0456 1078			
44	9336	9684	7108	1593	3125	1693	7285	9889	16
45 46	955 0199 1062								15
47	1923								13
48	2784	293	965 0168	4453	5789	4159	9552	1956	
49	3643		1				981 0116		
50 51	4509 5361								
52	6218	617	7 320	7301	8439	661	1 1805	4010	8
53	7074	698	3968	8011	9100	722	2366	4521	7
54 55	7930 878!				9760 8 974 04 19				
56	9639	940	624	970 0136	107	905	0 404	6050	4
57 58		961 020							
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60	304	3 261	7 925	2957	370	1 147	6 627	2 8071	
'	170	160	150	140	13°	120	110	100	1'
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,	730	730	740	750	7.14	770	780	- 20
0					1-0107809			60
1 2 3	3:0807325		3.4912470	63980	57570		4 7113686	3:1
2	27869	76715	50874		4 0207446		81256	
3		3.2810907	89356		57440		4:7249012 4:7316954	57 56
4	99122 3·0929831	79487	3·5027916 66555	94963 3-7538813		4 3604003		55
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9	53223	3.3017438	3.5221902	3.7715185	59877	4:3838654	4.7659410	51
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11	3:1115254	86811		3-7903951		4.3955 77	97837	49
12		3.3121598	39251	49481			4.7867300	48
13	77509	56452	78528	93109	63892		4-7936957	47
14	3-1208722				4.0815199			46
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17	3:1302701	3.3331736	3.5526449		4-1021649	73500		42
18	65639		3.2612300			4:4433762		91
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21	3-1428607 60478	37724 73191			4-1230079			39
22 23		3-3508728		3.8344861	82499		4.8644359	37
24	3.1523994		3.5815975		4-1335046			36
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35 36	77540 3·1910039	40631	3.6304771	3-8900449 47429	75606	82608		24
37		3.4013612	46064		4.2029835			23
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42	3.2106304	97333	53844	3-9231563		64141	5.0045111	18
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48		3.4420226	3.6806115 48475	3·9519615 68011		4 6317056	5·0503690 80907	12
49	38078	57635						
50	71438	95120		3.9616518			5.0658352	10
51		3 4532679 70315		3.9713868	4.2903199	4.6513788		8
52	38346 71996	3.4608026			4-2915885	79721	92061	7
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55	39184		3.7104558	60739		4.6712124	5.1049024	5
56		3.4721616	47561	3.9909924	85974	78595	5-1127855	4
57	3.2606728	59632	90658		4.3142955	4:6845248	5-1206921	3
58	40596	97726			4.3200079			2
59		3.4835996	77131	58165	57347		5.1365763	0
60	3 2708526				4·3314759 13°	4°7046301 12°		U
1	170	160	150	140	-	140	110	
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Ī	182	5				-		N	AT.	SINE	<u> </u>	-			•	[7	able	m.
I	,	1 80	0	81	0	82	0	83	0	1 84	0	85	0	86	0	1 87	10	1
ı	0			9976	883							9961	947	9975	641	9986		66
ı	1			9877		9903			816			9962			843		447	59
H	2	9849		9878	792		489 891	9926	169	9946	825		452 704	9976	045 245		598 748	58 57
ı	4	9850		3010		9904		1	973	9940	428		954		445		898	56
ſ	5	1		9879				9327	224		729	9963	204			9987		55
H	6	9851				9905			573	9947	028	9963	453		843		194	54
I	7	2050		9880			494		922	1	321		701	9977			340	53
H	8	9852	590		497	9906		9928			625	9964	948		237		486	52
ı	-						-	ı	618						433		631	51
Ħ	10 11	9653	583	9881			687	9929		9948	513		440 685		627 821		775 919	50 49
H	12	9854		9882			478	3323	655		907		020	0072	015	9988		49
ł	13		574		728		873		999	9949	101	9965	172	3310	207	2000	203	47
H	14	9855		9883		9908		9930	342		393		414		399		344	46
ı	15	00=0	561		615	0000	659		080		085		055		589		484	45
H	16 17	9850	544	9684	498	9909	051 442	9931	267	0050	976	9966	895		779 968		623 761	44 43
ı	18	9857			939		832		706		556			9979			899	42
ı	19		524	9885				9932			844		612	3313		9989		41
Ħ	20	9858	013		817		610			9951		1	849		530		171	40
ı	21		501	9886	255		997	1	721		419	9967	085		716		306	39
I	22		988			9911		9933			705		321		900		440	38
l	23 24	9859	475 960	9887		0010	770		393		990		555	9980	084		573	37
Ħ	25	9860			998	9912		9934		9952	274	nnco	789		267 450		706 837	36 35
H	26	3000		9888			923	3332	395		840	9968	254		631		968	34
ı	27	9861		0000		9913			727	9953	122		485		811	9990		33
l	28			9889				9935	058	9953	403		715		991		227	32
H	29	9362			-	9914					683		945	9981			355	31
ı	30	0000	856	9890			449		719		962	9969			348		482	30
H	31 32	9863		0001	588	9915	828			9954			401		525		609	29 28
I	33	9864	293	3691	445	9919	584		375 703		518 795		628 854		701 877		734 859	28
ı	34		770		872		961	9937	029	9955	070	9970	080	9982	052		983	26
ı	35	9865		9892		9916	337		355		345		304		225	9991		25
ŧ	36	2000	722		723	~~~	712		679		620		528		398		228	24
ı	37 38	9860	670	9893	148 572		459	9938		9956	893		750		570		350	23 22
1	39	9867			994		832		649			9971	972		742 912		470 590	21
H	40			0204		9918			969		709			9983			709	20
	41	9868			838			9939			979		622		250		709 827	19
	42		557	9895	258		944		610	9957	247		851		418		944	18
	43	9869	027		677	9919	314		928		515	9972	069		585	9992	060	17
	44 45		496 964	9896		9920		9940	246	noro	783	9972	286		751		176	16
	46	9870		1	931		416		203	9959	312		717	0004	917		290 404	15 14
	47	33.0		9897				9941	195		580		931	3304	245		517	13
	48	9871	363		762	9921	147		510		844	9973	145		408	1	629	12
	49		827	9898			511			9959	107		357		570		740	11
H	50	9872			590		874	9942			370		5 69		731		851	10
	51	0070		9899		9922			448		631		780		891		960	9
	52 53	9873	678		415 826		599		760		892	9974	990	9985		9993		8
	54	9874		9900		9923	319	3343	379		411		199 408		209 367		177 284	6
I	55		598		646		679	ŀ	688		669		615		524		390	5
I	56		057	9901	055	9924	037		996		926		822		680		495	4
H	57		514		462		394	9944	303	9961	183	9975	028	l	835		600	3
ı	58 59	9878	972	9900	869 275	0005	107		009		438		233	0000	989		704	2
	60		883			3340	462	9945	210		947		641	9986	143 295		906 908	1
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	790	800	81°	820	83°	840	85°	
0		5.6712818						60
1	525557	809446	256601	304190	639786	410613	468474	59
2	605813	906394	376126	455308	837041	679068	507154	58
3	767051	5·7003663 101256	496092 616502	759437	8.2035239	949022 9·6220486	546093 585294	57
5	848035	199173	737359	912456	434485	493475	624761	56 55
6	929264	297416	859665	7.2066116	635547	768000	664495	54
7	5.2010738	395988	980422	220422		9.7044075	704500	53
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9	174428	594122	225301	530987	244577	600927	785333	51
10	256647	693688	348428	687255	449558	881732	826167	50
11	3391 16	793588	472017	844184		9.8164140	867282	49
12	421836	893825		7.3001780	862519	448166	908682	48
13	504809	994400	720591 845581	318989	8.4070515	733823 9·9021125	950370 992349	47
14 15	671517	5·8095315 196572	971043	478610	279531 489573	310088		46 45
16	755255		6.5096981	638916	700651	600724	077192	44
17	839251	400117	223396	799909	912772	893050	120062	43
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19	5·3008 018	605051	477672	7.4123978	340172	048283	206716	41
20	092793		605538	297064	555468	078031	250505	40
21	177830		733892		771838	107954	294609	39
22	263131	915084	862739		999290	138054	339028	38
23 24	434527	5.9019138	992080 6·6121919		8-6207833 427475	168332 198789	383768 428831	37 36
25	520626	228322	252259	7.5113178	648223	229428	474221	35
26	606993		383100	280571	870088	260249	519942	34
27	693630	438952	514449	448699	8.7093077	291255	565997	33
28	780538		646307	617567	317198	322447	612390	32
29	867718		778677	787179	542461	353827	659125	31
30	955172		911562	957541	768974	385397	706205	30
31	5.4042901		6.7044966		996446	417158	753634	29
32 33	130906	971957 6·0079676	178891 313341	473174	8·8225186 455103	449112 481261	801417 849557	28 27
34	307750		448318		686206	513607	898058	26
35	396592	296247	583826	820769		546151	946924	25
36	485715	405103	719867	995735	8.9152009	578895	996160	24
37	575121	514343	856446		386726	611841	13.045769	23
38	664812	623967	993565	348028	622668	644992	095757	22
39	754788		6.8131227	525366	859843	678348	1	21
40	935604	844381	269437 408196		9.0098261	711913	196883	20
41 42		955174 6·1066360	547508	882453 7 8062212	337933 578867	745687 779673	248031 299574	19 18
43	117579	177943	687378	242790	821074	813872	351518	
44	209005	#89923	827907		9.1064564	848288		16
45	300724	402303	968799	606423	309348	882921	456625	15
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47 48	485052 577663	628272 741865	252489 395192	973396	902838 9-2051564	952850 988150		13
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	2 34421	548588 665515	410482	475647	830663	241712		5
55	200474		557905		9.4090384	278985	065459	4
56	329474			QG(V)4*3				
56 57	424838	782868	705934	860042 8-1053599	351531 614116	316304 353970	123536 182092	2
56 57 58	424838 520516	782868 900651	705934 854573	8.1053599	614116	353970	182092	3 2 1
56 57	424838 520516 616509 712818	782868 900651 6·3018866 137515	705934 854573 7·1003826 153697	8·1 053 599 248 071		353970 391885 430052	182092 241134	2 1 0
56 57 58 59	424838 520516 616509	782968 900651 6:3018966	705934 854573 7·100 3 826	8·1 053 599 248 071	614116 878149	353970 391885	182092 241134	1

18	4 N.	AT. SINE.			NAT. T.	AN.	[Table	m.
0	88° 9993 908	9999 477 60	1 %	860	870	Não Portacero	890	1
1	9994 009	527 59	0	14·300666 360696	19:081137 187930		57·289962 58·261174	
2	110	577 59	2	421230		29 122005	59-265972	
3	209	625 57	3	482273	405133		60-305820	
4	308	673 56	- 4	543833	515584	624499	61:382905	56
5	405	720 55	5	605916	627296		62:499154	55
6	502	766,54	t)	668529	740291	30-144619	63:656741	54
7	598	812/53	7	731679	854591	411580	64.858008	53
9	693 788	856/52	8	795372	970219	683307	66:105473	52
-		900 61			20:087199	959928	67'401854	51
10	186	942 50	10	924417	205553		68.750087	50
11 12	974 9995 066	984 49	11	989784	325308	528392	70-153346	49
13	157	9999 025 46 065 47	12	15:055723 122242	446486 569115	820516 32-118099	71.615070	48
14	247	105 46	14	199349	693220	421295	73-138991 74-729165	46
15	336	143 45	15	257052	818828	730264	76:390009	45
16	424	181 44	16	325358		33 045173	78-126342	44
17	612	218 43	17	394276		366194	79-943430	43
18	599	264 42	18	463814	204949	693509	81.847041	42
19	684	289 41	19	533991	336851	34.027303	83:843507	41
20	770	323 40	20	604784	470401	367771	85:939791	40
21	854	357 39	21	676233	605630	715115	88-143572	39
22	937	389 39	22	748337		35 069546	90-463336	38
23 24	9996 020	421 37	23	821105	881251	431262	92-908487	37
25	101	452 36	24	894645		800553	95-489475	36
26	162 262	482 35 511 34	25 26	968667	163980 308097		98-217943	35
27	341	539 33	27	16'043482 118998	454096	562659 956001	101-10690	34
28	419	567 32	23	195225	602015	37-357892	104-17094 107-42648	32
29	497	593 31	29	272174	751892	768613	110-89205	31
30	573	619 30	30	349855	903766	39-188459	114 58865	30
31	649	644 29	31		23 057677	617738	118 54018	29
32	724	66S 28	32	507456	213666	39.056771	122.77396	28
33	798	602 27	33	597396	371777	505695	127-32134	27
34	971	714 26	34	668112	532052	965460	132:21851	26
35	943	736 25	35	749614	694537	40.435837	137:50745	25
36	9997 015	756 24	36	931915	859277	917412	143-23712	24
38	086 156	776 23 795/22	37	915025 998957		41.410598	149-46502	23
39	224	813 21	39	17:083724	195714 367509	915790 42-433464	156:25908	21
40	292						163-70019	
41	360	831 20 847 19	40	169337 255809	541758	964077 43:508122	171:89540	20 19
42	426	863 18	42	343155		44-066113	180·93220 190·98419	18
43	492	878 17	43	431385	25.079757	638596	202:21875	17
44	556	892 16	44	520516	264361	45-226141	214.85762	16
45	620	905 15	45	610559	451700	829351	229 18166	13
46	683	917 14	46	701529	641832		245.55198	14
47	745	928 13	47	793442	634823		264 44080	13
49	807 867	939 12 949 11	48		26:030736	739501	286-47773	12
-	-		49	980150	1	48.412064	312-52137	11
50	927	958 10	50	18.074977	431600	and managed of	343-77371	10
51 52	986 9998 044	966 9 973 8	51	170307	636690	815726	381.97099	9
53	101	979 7	52 53	267654	27:056557	50 548506	429-71757	8 7
54	157	985 6	54	464471		52.080673	491·10600 572·95721	6
55	213	989 5	55	564473	499853	882109	687:54687	5
56	267	993 4	56	665562		53.708597	859-43630	4
57	321	996 3	57	767754		54:561300	1145 9153	3
58	374	998 2	58	871068	28.166422	55'441517	1718-8732	2
59	426	1.0000000 1	59	975523	399397	56.350590		1
60	4771	000 0	60	19.081137		57.289962	Infinite.	0
,	10	00 //	2.4	30	20	10	00	1
	NAT.	COSINE.			NAT.	COTAN.		

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TRAVERSE TABLE

TO EVERY QUARTER POINT OF THE COMPASS.

186	Dif.	of hish i	ınd de	p. for \	Point.	Dif. 6	f lat. a	nd dep	for h	Point.	[T. w.
dist. 1 2 3 4 5 6 7	tat. 01·0 02·0 03·0 04·0 05·0 06·0 07·0 08·0 09·0	dep. 00·0 00·1 00·1 00·2 00·2 00·3 00·4 00·4	dist. 61 62 63 64 65 66 67 68	lal. 60°9 61°9 62°9 63°9 64°9 65°9 66°9 68°9	dep. 03°0 03°1 03°1 03°1 03°2 03°2 03°3 03°3	dist. 2 3 4 5 6 7 8 9	01:0 02:0 03:0 04:0 05:0 06:0 07:0 08:0	dep. 00·1 00·2 00·3 00·4 00·5 00·6 00·7 00·8	dist, 61 62 63 64 65 66 67 68	lat. 60·7 61·7 62·7 63·7 64·7 66·7 66·7 68·7	dep. 06:0 06:1 06:2 06:3 06:4 06:5 06:6 06:7
10 11 12 13 14 15 16 17 18 19 20	10·0 11·0 12·0 13·0 14·0 15·0 16·0 17·0 18·0 19·0 20·0	00·5 00·6 00·6 00·7 00·7 00·8 00·8 00·9 00·9	70 71 72 73 74 75 76 77 78 79 80	69.9 70.9 71.9 72.9 73.9 74.9 75.9 76.9 77.9 79.9	03·5 03·5 03·5 03·6 03·7 03·7 03·8 03·9 03·9	10 11 12 13 14 15 16 17 18 19 20	10.0 10.9 11.9 12.6 13.9 14.9 15.9 16.9 17.9 18.9	01·0 01·1 01·2 01·3 01·4 01·5 01·6 01·7 01·8 01·9	70 71 72 73 74 75 76 77 78 79 80	69·7 70·7 71·7 72·7 73·6 74·6 76·6 77·6 78·6 79·6	06·9 07·0 07·1 07·2 07·3 07·4 07·4 07·5 07·6 07·7
21 22 23 24 25 26 27 28 29 30	21·0 22·0 23·0 24·0 25·0 26·0 27·0 28·0 29·0 3 · (01·0 01·1 01·1 01·2 01·2 01·3 01·3 01·4 01·4	81 82 83 84 85 86 87 88 89	80°9 81°9 82°9 83°9 84°9 86°9 86°9 88°9 88°9	04·0 04·0 04·1 04·1 04·2 04·2 04·3 04·3 04·4	21 22 23 24 25 26 27 28 29 30	20·9 21·9 22·9 23·9 24·9 26·9 27·9 28·9 29·9	02·1 02·2 02·3 02·4 02·4 02·5 02·6 02·7 02·8 02·9	81 82 83 84 85 86 87 88 89	80.6 81.6 82.6 83.6 84.6 85.6 86.6 87.6 88.6	07-9 08-0 08-1 08-2 96-3 08-4 08-5 08-6 08-7
31 32 33 34 35 36 37 38 39 40	31.0 32.0 33.0 34.0 35.0 36.0 37.0 38.0 39.0 40.0	01.5 01.6 01.6 01.7 01.7 01.8 01.8 01.9 01.9	91 92 93 94 95 96 97 98 99 100	90-9 91-9 92-9 93-9 94-9 96-9 97-9 98-9	04·5 04·5 04·6 04·6 04·7 04·7 04·8 04·8 04·9	31 32 33 34 35 36 37 39 40	30·9 31·8 32·8 33·8 34·9 35·8 36·8 37·8 38·8 39·8	03·0 03·1 03·2 03·3 03·4 03·5 03·6 03·7 03·9	91 92 93 94 95 96 97 98 99 100	90·6 91·6 92·6 93·6 94·5 95·5 96·5 97·5 98·5	08·9 09·0 09·1 09·2 09·3 09·4 09·5 09·6 09·7
41 42 43 44 45 46 47 48 49 50	41.9 42.9 43.9 44.9 46.9 46.9 47.9 48.9	02·0 02·1 02·1 02·2 02·2 02·3 02·3 02·4 02·4 02·5	10L 102 103 104 105 106 107 108 109 110	100:9 101:9 102:9 103:9 104:9 105:9 106:9 107:9 108:9 109:9	05·0 05·0 05·1 05·1 05·2 05·2 05·3 05·3 05·4 05·4	41 42 43 44 45 46 47 48 49 50	40.8 41.8 42.8 43.8 44.8 45.8 46.8 47.8 48.8 49.6	04·0 04·1 04·2 04·3 04·4 04·5 04·6 04·7 04·8 04·9	101 102 103 104 105 106 107 108 109 110	100·5 101·5 102·5 103·5 104·5 105·5 106·5 107·5 108·5 109·5	09·9 10·0 10·1 10·2 10·3 10·4 10·5 10·6 10·7 10·8
51 52 53 54 55 56 57 58 59 60 dist,	50·9 51·9 52·9 53·9 54·9 56·9 57·9 58·9 dep.	02·5 02·6 02·6 02·7 02·7 02·8 02·9 02·9 02·9 02·9 lat.	111 112 113 114 115 116 117 118 119 120 dist.	110·9 111·9 112·9 113·9 114·9 115·9 116·9 117·9 118·9 119·9 dep.	05·5 05·5 05·5 05·6 05·6 05·7 05·7 05·8 05·9 lat.	51 52 53 54 55 56 57 58 59 60 dist.	50·8 51·7 62·7 53·7 54·7 55·7 56·7 57·7 58·7 59·7 dep.	05-0 05-1 05-2 05-3 05-4 05-5 05-6 05-7 05-8 05-9 lat.	111 112 113 114 115 116 117 118 119 120 dist.		10·9 11·0 11·1 11·2 11·3 11·4 11·5 11·6 11·7 11·8 Lat.

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T.17.] Dif	of tat	and d	ep. for	Point.	Dif.	of lat.		p. for	1 Point	
dist.	lat.	dep.	dist.	lat.	dep.	dist.	lat.	dep.	dist.	lat.	dep.
1 2	01-0 02-0	00.3	61 62	60·3	08 ⁻⁹	1 2	01·0 02·0	00·2 00·4	61 62	59·8 60·8	11·9 12·1
3	03.0	00.4	63	62.3	09.2	3	02.9	00.6	63	61.8	12.3
4	04.0	00.6	64	63.3	09.4	4	03.9	00.8	64	62.8	12.5
5 6	04·9 05·9	00.7	65 66	64·3	09·5 09·7	5	04·9 05·9	01·0 01·2	65 66	63·7 64·7	12·7 12·9
7	06.9	01.0	67	66.3	09.8	7	06.9	01.4	67	65.7	13.1
8	07.9	01.2	68	67.3	10.0	8	07-8	01.6	68	66.7	13.3
9 10	09·9	01.2	69 70	68·2 69·2	10·1 10·3	9 10	08.8	01·8 02·0	69 70	67·7 68·7	13·5 13·7
11 12	10·9 11·9	01.6 01.8	71 72	70·2 71·2	10·4 10·6	11 12	10·8	02·3 02·3	71 72	69·6 70·6	13·9 14·0
13	12.9	01.9	73	72.2	10.7	13	12.7	02.5	73	71.6	14.2
14	13.8	02.1	74	73.2	10.9	14	13.7	02.7	74	72.6	14.4
15 16	14·8 15·8	02.3	75 76	74·2 75·2	11·0 11·1	15 16	14·7 15·7	02·9	75 76	73·6 74·5	14·6 14·8
17	16-8	02.5	77	76.2	11.3	17	16.7	03.3	77	75.2	15.0
18	17.8	02.6	78	77.2	11.4	18	17.7	03.2	78	76.5	15.2
19 20	19·8	02·8 02·9	79 80	78·1	11·6 11·7	19 20	18·6 19·6	03·7 03·9	79 80	77·5 78·5	15·4 15·6
21 22	20.8	03·1 03·2	81 82	80.1	11.9	21 22	20.6	04.1	81	79.4	15.8
23	21.8	03.4	83	81·1 82·1	12·0 12·2	23	21·6 22·6	04·3 04·5	82 83	80·4 81·4	16·0 16·2
24	23.7	03.2	84	83.1	12.3	24	23.5	04.7	84	82.4	16.4
25 26	24·7 25·7	03.7	85 86	84·1 85·1	12·5 12·6	25	24.5	04.9	85 86	83.4	16.6
27	26.7	04.0	87	86.1	12.8	26 27	25·5 26·5	05·1	87	84·3 85·3	16·8 17·0
28 29	27.7	04.1	88	87.0	12.9	28	27.5	05.5	88	86.3	17.2
30 31	28·7 29·7	04·3 04·4	89 90	89·0	13·1 13·2	29 30	28·4 29·4	05.7	89 90	87·3	17·4 17·6
31 32	30.7	04·5 04·7	91 92	90.0	13.3	31	30.4	06.0	91	89.2	17.8
33	31·7 32·6	04.8	93	91·0 92·0	13·5 13·6	32 33	31·4 32·4	06·2 06·4	92 93	90·2 91·2	18·0 18·1
34	33.6	05:0	94	93;0	13.8	34	33.3	06.6	94	92.2	18.3
35 36	34·6 35·6	05·3	95 96	94·0 95·0	13·9 14·1	35 36	34.3	06.8	95 96	93.2	18.5
37	36.6	05.4	97	95.9	14.2	37	36.3	07·0 07·2	97	94·2 95·1	18·7 18·9
38 39	37.6	05.6	98	96.9	14.4	38	37.3	07.4	98	96.1	19-1
40	39·6	05·7 05·9	99 100	97·9 98·9	14·5 14·7	39 40	38·2 39·2	07·6 07·8	90 100	97·1 98·1	19·3 19·5
41	40.6	06.0	101	99.9	14.8	41	40.2	08.0	101	99.1	19.7
42 43	41.5	06.3	102 103	100·9 101·9	15·0 15·1	42 43	41·2 42·2	08·2 08·4	102 103	100·0 101·0	19·9 20·1
44	42·5 43·5	06.2	104	102.9	15.3	44	43.2	08.6	104	102.0	20.3
45	44.5	06.6	105	103.9	15.4	45	44.1	08.8	105	103.0	20.5
46 47	45·5 46·5	06·7 06·9	106 107	104·8 105·8	15·5 15·7	46 47	46.1	09·0 09·2	106 107	104·0 104·9	20·7 20·9
48	47.5	07.0	108	106.8	15.8	48	47.1	09.4	108	104.9	21.1
49 50	48·5 49·5	07·2 07·3	109 110	107·8 108·8	16·0 16·1	49 50	48·1 49·0	09.8	109 110	106·9 107·9	21·3 21·5
51	50.4	07.5	111	109-8	16.3	51	50.0	10.0	111	108-9	21.7
52 53	51·4 52·4	07.6	112	110.8	16.4	52	51.0	10.1	112	109.8	21.9
54	53.4	07·8 07·9	113 114	111·8 112·8	16·6 16·7	53 54	52·0 53·0	10· 5	113 114	110 · 8	22·0 22·2
55	54.4	08.1	115	113.7	16.9	55	53.9	10.7	115	112.8	22.4
56 57	55·4 56·4	08·2 08·4	116	114·7 115·7	17·0 17·2	56	54.9	10.9	116	113.8	22.6
58	57.4	08.2	117	116.7	17.3	57 58	56·9	11·1 11·3	117 118	114·7 115·7	22·8 23·0
59	58.4	08.7	119	117-4	17.5	59	57.9	11.2	119	116.7	23.2
dist.	59·3 dep.	08.8 lat.	120 dist.	118.7	17.6 lat.	60	58.8	11.7	120 dist.	117.7	23.4
4000.	wep.	For	71 Po	dep.	ut.	dist.	dep.	lat.	aist. Poit	l <i>dep.</i> its.	lat.
	-										

list.	lat.	dep. 1	dist.	lat. 1	dep.	dist.	lat.	dep.	dist.	lat.	dep.
1 2 3 4 5	01·0 01·9 02·9 03·9 04·9	00.2 00.5 00.7 01.0 01.2	61 62 63 64 65	59·2 60·1 61·1 62·1 63·1	14·8 15·1 15·3 15·6 15·8	1 2 3 4 5	01·0 C ₁ ·9 02·9 03·8 04·8	00°3 00°6 00°9 01°2 01°5	61 62 63 64 65	58:4 59:3 60:3 61:2 62:2	17.7 18.0 18.3 18.6 18.9
6 7 8 9 10	05·8 06·8 07·8 08·7 09·7	01.5 01.7 01.9 02.2 02.4	66 67 68 69 70	64·0 66·0 66·9 67·9	16·0 16·3 16·5 16·8 17·0	6 7 8 9	05·7 06·7 07·7 08·6 09·6	01.7 02.0 02.3 02.6 02.9	66 67 68 69 70	63·2 64·1 65·1 66·0 67·0	19-2 19-4 19-7 20-0 20-3
11 12 13 14 15 16 17 19 20	10·7 11·6 12·6 13·6 14·6 15·5 16·5 17·5 18·4 19·4	02·7 02·9 03·2 03·4 03·6 03·9 04·1 04·4 04·6 04·9	71 72 73 74 75 76 77 78 79 80	68·9 69·8 70·8 71·8 72·8 73·7 74·7 75·7 76·6 77·6	17.3 17.5 17.7 18.0 18.2 18.5 18.7 19.0 19.2	11 12 13 14 15 16 17 18 19	10.5 11.5 12.4 13.4 14.4 15.3 16.3 17.2 18.2 19.1	03·2 03·5 03·8 04·1 04·4 04·6 04·9 05·2 05·5 05·8	71 72 73 74 75 76 77 79 79	67·9 68·9 69·9 70·8 71·8 72·7 73·7 74·6 75·6 76·6	20·6 20·9 21·2 21·5 21·8 22·1 22·3 22·6 22·9 23·2
21 22 23 24 25 26 27 28 29 30	20·4 21·3 22·3 23·3 24·3 25·2 26·2 27·2 28·1 29·1	05·1 05·3 05·6 05·8 06·1 06·3 06·6 06·8 07·0 07·3	81 82 83 84 85 86 87 89 89	78.6 79.6 80.5 81.5 82.5 83.4 84.4 85.4 86.3 87.3	19·7 19·9 20·2 20·4 20·7 20·9 21·1 21·4 21·6 21·9	21 22 23 24 25 26 27 28 29 30	20·1 21·1 22·0 23·0 23·9 24·9 25·8 26·8 27·8 28·7	06·1 06·4 06·7 07·0 07·3 07·5 07·8 08·1 08·4 08·7	81 82 83 84 65 86 87 88 89 90	77.5 78.6 79.4 80.4 81.3 92.3 93.3 94.2 85.2 86.1	23·5 23·8 24·1 24·4 24·7 25·0 25·2 25·5 26·1
31 32 33 34 35 36 37 38 39	30·1 31·0 32·0 33·0 34·0 34·9 35·9 36·9 37·8 36·8	07.5 07.8 08.0 08.3 08.5 08.7 09.0 09.2 09.5 09.7	91 92 93 94 95 96 97 98 99 100	88°3 89°2 90°2 91°2 92°2 93°1 94°1 96°0 97°0	22·1 22·4 22·6 22·8 23·1 23·3 23·6 23·8 24·1 24·3	31 32 33 34 35 36 37 38 39 40	29.7 30.6 31.6 32.5 33.5 34.5 35.4 36.4 37.3 38.3	09·0 09·3 09·6 09·9 10·2 10·4 10·7 11·0 11·3 11·6	91 92 93 94 95 96 97 98 99 100	87·1 88·0 89·0 90·0 90·9 91·9 92·8 93·8 94·7 95·7	26:4 26:7 27:0 27:3 27:6 27:9 28:2 28:4 28:7 29:0
41 42 43 44 45 46 47 48 49 50	39·8 40·7 41·7 42·7 43·7 44·6 45·6 46·6 47·5 48·5	10·0 10·2 10·4 10·7 10·9 11·2 11·4 11·7 11·9 12·2	101 102 103 104 105 106 107 108 109 110	98.0 98.9 99.9 100.9 101.9 102.8 103.8 104.8 105.7 106.7	24·5 24·8 25·0 25·3 25·5 25·8 26·0 26·2 26·5 26·7	41 42 43 44 45 46 47 48 49 50	39·2 40·2 41·2 42·1 43·1 44·0 45·0 46·9 47·9	11.9 12.2 12.5 12.8 13.1 13.3 13.6 13.9 14.2 14.5	101 102 103 104 105 106 107 108 109 110	96·7 97·6 98·6 99·5 100·5 101·4 102·4 103·4 104·3 105·3	29·3 29·6 29·9 30·2 30·5 30·6 31·1 31·4 31·6 31·9
51 52 53 54 55 56 57 58 59 60 dist	49-5 50-4 51-4 52-4 53-4 54-3 55-3 56-3 57-2 58-2 dep.	12·4 12·6 12·9 13·1 13·4 13·6 13·9 14·1 14·3 14·6 lat.	111 112 113 114 115 116 117 118 119 120 dist.	107·7 108·6 109·6 110·6 111·6 112·5 113·5 114·5 115·4 116·4	27-0 27-2 27-5 27-7 27-9 28-2 28-4 28-7 28-9 29-2 lat.	51 52 53 54 55 56 57 58 59 60	48.8 49.8 50.7 51.7 52.6 53.6 54.5 55.5 56.5	14·8 15·1 15·4 15·7 16·0 16·3 16·5 16·8 17·1	111 112 113 114 115 116 117 118 119 120	106·2 107·2 108·1 109·1 110·1 111·0 112·0 112·9 113·9 114·8	32·2 32·5 32·8 33·1 33·4 33·7 34·0 34·2 34·5

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T. 17	.] Dij	f. of lat	. of de	o. for 14	Point.	Dif. o	f lat: 6	dep.	or 2 1	Point.	189
dist.	lat. 00·9 01·9	dep. 00.3 00.7	dist. 61 62	lat. 57·4 58·4	dep 20·5 20·9	dist.	lat. 00·9 01·8	dep. 00·4 00·8	dist. 61 62	lat. 56·4 57·3	dep. 23·3 23·7
345	02·8 03·8 04·7	01·0 01·3 01·7	63 64 65	59·3 60·3 61·2	21·2 21·6 21·9 22·2	3 4 5	02·8 03·7 04·6	01·1 01·5 01·9	63 64 65	58·2 59·1 60·1	24·1 24·5 24·9
6 7 8 9	05·6 06·6 07·5 08·5	02 0 02·4 02·7 03·0	66 67 68 69	62·1 63·1 64·0 65·0	22·6 22·9 23·2	6 7 8 9	05·5 06·5 07·4 08·3	02·3 02·7 03·1 03·4	66 67 68 69	61·0 61·9 62·8 63·8	25·3 25·6 26·0 26·4
10 11	09·4 10·4	03·4 03·7	70 71	66·8	23·6 23·9	10 11	09·2 10·2	03.8	70	64.7	26.8
12 13 14 15 16 17 18 19	11·3 12·2 13·2 14·1 15·1 16·0 17·0 17·9 18·8	03 7 04·0 04·4 04·7 05·1 05·4 05·7 06·1 06·4	72 73 74 75 76 77 78 79 80	67.8 68.7 69.7 70.6 71.6 72.5 73.4 74.4 75.3	24·3 24·6 24·9 25·3 25·6 25·9 26·3 26·6 26·9	12 13 14 15 16 17 18 19	10-2 11-1 12-0 12-9 13-9 14-8 15-7 16-6 17-6 18-5	04·2 04·6 05·0 05·4 05·7 06·1 06·5 06·9 07·3	71 72 73 74 75 76 77 78 79 80	65.6 66.5 67.4 68.4 69.3 70.2 71.1 72.1 73.0 73.9	27·2 27·6 27·9 28·3 28·7 29·1 25·5 29·9 30·2 30·6
21 22 23 24 25 26 27 28 29 30	19·8 20·7 21·7 22·6 23·5 24·5 25·4 26·4 27·3 28·2	07·1 07·4 07·7 08·1 08·8 09·1 09·4 09·8 10·1	81 82 83 84 85 86 87 88 89	76·3 77·2 78·1 79·1 80·0 81·0 81·9 82·9 83·8 84·7	27·3 27·6 28·0 28·3 28·6 29·0 29·3 29·6 30·0 30·3	21 22 23 24 25 26 27 28 29 30	19·4 20·3 21·3 22·2 23·1 24·0 24·9 25·9 26·8 27·7	08·0 08·4 09·8 09·2 09·6 10·0 10·3 10·7 11·1 11·5	81 82 83 84 85 86 97 88 89	74·8 75·8 76·7 77·6 78·5 79·5 80·4 81·3 82·2 83·2	31·0 31·4 31·8 32·1 32·5 32·9 33·3 33·7 34·1 34·4
31 32 33 34 35 36 37 38 39 40	29·2 30·1 31·1 32·0 33·0 33·9 34·8 35·8 36·7 37·7	10·4 10·8 11·1 11·5 11·8 12·1 12·5 12·8 13·1 13·5	91 92 93 94 95 96 97 98 99	85·7 86·6 87·6 88·5 89·4 90·4 91·3 92·3 93·2 94·2	30·7 31·0 31·3 31·7 32·0 32·3 32·7 33·0 33·3 33·7	31 32 33 34 35 36 37 38 39 40	26.6 29.8 30.5 31.4 32.3 33.3 34.2 35.1 36.0 37.0	11.9 12.2 12.6 13.0 13.4 13.3 14.2 14.5 14.9 15.3	91 92 93 94 95 96 97 98 99 100	84·1 85·0 85·9 86·8 87·8 88·7 89·6 90·5 91·5 92·4	34.8 35.2 35.6 36.0 36.4 36.7 37.1 37.5 37.9 38.3
41 42 43 44 45 46 47 48 49 50	38·6 39·5 40·5 41·4 42·4 43·3 44·3 45·2 46·1 47·1	13.8 14.1 14.5 14.8 15.2 15.5 16.2 16.5 16.8	101 102 103 104 105 106 107 108 109 110	95·1 96·0 97·0 97·9 98·9 99·8 100·7 101·7 102·6 103·6	34·0 34·4 34·7 35·0 35·4 35·7 36·0 36·4 36·7 37·1	41 42 43 44 45 46 47 48 49 50	37·9 38·8 39·7 40·6 41·6 42·5 43·4 44·4 45·3 46·2	15·7 16·1 16·5 16·8 17·2 17·6 19·0 18·4 18·8 19·1	101 102 103 104 105 106 107 108 109 110	93·3 94·2 95·2 96·1 97·0 97·9 98·9 99·8 100·7 101·6	38·7 39·0 39·4 39·8 40·2 40·6 41·0 41·3 41·7 42·1
51 52 53 54 55 56 57 58	48·0 49·0 49·9 50·8 51·8 52·7 53·7 54·6 55·5	17·2 17·5 17·9 18·2 18·5 19·2 19·5	111 112 113 114 115 116 117 118	104·5 105·4 106·4 107·3 109·3 109·2 110·2 111·1 112·0	37·4 37·7 38·1 38·4 38·7 39·1 39·4 40·1	51 52 53 54 55 56 57 58 59	47·1 48·0 49·0 49·9 50·8 51·7 52·7 53·6 54·5	19·5 19·9 20·3 20·7 21·0 21·4 21·8 22·2 22·6	111 112 113 114 115 116 117 118 119	102.6 103.5 104.4 105.3 106.3 107.2 108.1 109.0 109.9	42·5 42·9 43·2 43·6 44·0 44·4 44·8 45·2 45·5
dist.	56·5 dep.	20·2 lat. For 6	120 dist. Poi	113·0 dep. nts.	40·4 lat.	60 dist.	55·4 dep.	23·0 lat. For 6	dist. Poin		45·9 lat.

Dif	of lat.	d-des	for 21	Point.	Dif. o	flat.4	dep. j	or 21 I	Point.	[T. IV.
lat. 00-9 01-8 02-7 03-6 04-5 05-4 06-3 07-2 08-1 09-0	dep, 00-4 00-9 01-3 01-7 02-1 02-6 03-0 03-4 04-3	61 62 63 64 65 66 67 68 69 70	55.1 56.0 57.0 57.9 58.8 59.7 60.6 61.5 62.4 63.3	dep. 26·1 26·5 26·9 27·4 27·8 28·2 28·6 29·1 29·5 29·9	dist. 1 2 3 4 5 6 7 8 9	lat. 00°9 01°8 02°6 03°5 04°4 05°3 06°2 07°1 07°9 08°8	dep. 00·5 00·9 01·0 91·9 02·4 02·8 03·3 03·9 04·2 04·7	dist. 61 62 63 64 65 66 67 68 69 70	1at. 53·8 54·7 55·6 56·4 57·3 58·2 59·1 60·0 60·9 61·7	dep. 28-8 29-2 29-7 30-2 30-6 31-1 31-6 32-1 32-5 33-0
09·9 10·8 11·8 12·7 13·6 14·5 15·4 16·3 17·2 18·1	04·7 05·1 05·6 06·0 06·4 06·9 07·3 07·7 08·1 08·6	71 72 73 74 75 76 77 78 79 80	64·2 66·0 66·9 67·8 68·7 69·6 70·5 71·4 72·3	30·4 30·8 31·2 31·6 32·1 32·5 32·9 33·4 33·8 34·2	11 12 13 14 15 16 17 18 19	09·7 10·6 11·5 12·3 13·2 14·1 16·0 16·8 17·6	05·2 05·7 06·1 06·6 07·1 07·5 08·0 08·5 09·0	71 72 73 74 75 76 77 78 79 80	62·6 63·5 64·4 65·3 66·1 67·0 67·9 68·8 69·7 70·6	33·5 33·9 34·4 34·9 35·4 35·8 36·3 36·8 37·2 37·7
19-0 19-9 20-8 21-7 22-6 23-5 24-4 25-3 26-2 27-1	09-0 09-4 09-8 10-3 10-7 11-1 11-5 12-0 12-4 12-8	81 82 83 84 85 86 87 88 89 90	73°2 74°1 75°0 75°9 76°8 77°7 78°6 79°6 80°5 81°4	34.6 35.1 35.5 35.9 36.3 36.8 37.2 37.6 38.1 38.5	21 22 23 24 26 26 27 28 29 30	18·5 19·4 20·3 21·2 22·1 22·9 23·8 24·7 25·6 26·5	09-9 10-4 10-8 11-3 11-8 12-3 12-7 13-2 13-7 14-1	81 82 83 84 85 86 87 88 89	71·4 72·3 73·2 74·1 75·9 76·7 77·6 78·5 79·4	38·2 38·6 39·1 39·6 40·1 40·5 41·0 41·5 41·9 42·4
28.0 28.9 29.8 30.7 31.6 32.5 33.4 34.4 35.3 36.2	13.3 13.7 14.1 14.5 15.0 15.4 16.2 16.7 17.1	91 92 93 94 95 96 97 98 99 100	82·3 83·2 84·1 85·0 86·9 86·8 87·7 89·6 89·5 90·4	38·9 39·3 39·8 40·2 40·6 41·1 41·5 41·9 42·3 42·8	31 32 33 34 35 36 37 39 40	27-3 28-2 29-1 30-0 30-9 31-8 32-6 33-5 34-4 35-3	14.6 15.1 15.6 16.0 16.5 17.0 17.4 17.9 18.4 18.9	91 92 93 94 95 96 97 98 99 100	80°3 81°1 82°0 82°9 83°8 84°7 85°6 86°4 87°3 88°2	42.9 43.4 43.8 44.3 44.8 45.2 45.7 46.2 46.7 47.1
37·1 38·0 39·9 39·8 40·7 41·6 42·5 43·4 44·3 45·2	17-5 18-0 18-4 18-8 19-2 19-7 20-1 20-5 21-0 21-4	101 102 103 104 105 106 107 108 109 110	91·3 92·2 93·1 94·0 94·9 95·8 96·7 97·6 98·5 99·4	43.2 43.6 44.0 44.5 44.9 45.3 45.8 46.2 46.6 47.0	41 42 43 44 45 46 47 48 49 50	36·2 37·9 38·8 39·7 40·6 41·5 42·3 43·2 44·1	19·3 19·8 20·3 20·7 21·2 21·7 22·2 22·6 23·1 23·6	101 102 103 104 105 106 107 108 109 110	89-1 90-0 90-8 91-7 92-6 93-5 94-4 95-3 96-1 97-0	47.6 48.1 48.5 49.0 49.5 50.0 50.4 50.9 51.4 51.8
46·1 47·0 47·9 48·8 49·7 50·6 51·5 52·4 53·3 54·2 dep.	21.8 22.2 22.7 23.1 23.5 23.9 24.4 24.8 25.2 25.7 lat.	111 112 113 114 115 116 117 118 119 120 dist.	100°3 101°2 102°1 103°1 104°0 104°9 105°9 106°7 107°6 108°5 dep.	47.5 47.9 48.3 48.7 49.2 49.6 50.0 50.5 50.9 51.3 lat.	51 52 53 54 55 56 57 58 59 60 dist.	45·0 46·7 47·6 48·5 49·4 50·3 51·2 52·0 52·9 dep.	24·0 24·5 25·0 25·5 25·9 26·4 26·9 27·3 27·8 28·3 lat.			52·3 52·8 53·3 53·7 54·2 54·7 65·1 56·6 1at.
	lat. 0099 0188 0653 072 0366 0654 0663 072 0990 0099 1068 1164 1653 172 1366 1456 2652 265	lat. dep. 00.9 00.4 01.8 00.9 02.7 01.3 03.6 01.7 04.5 02.6 06.3 03.0 07.2 03.4 09.0 04.3 09.0 04.7 10.8 05.1 11.6 05.6 05.6 05.7 08.1 05.6 09.0 04.7 10.8 05.1 11.6 05.6 05.6 05.8 15.4 07.3 15.4 07.3 15.4 07.3 15.4 07.3 15.4 07.3 15.4 07.3 15.4 07.3 16.5 06.8 19.0 09.0 19.0 09.0 19.0 09.0 19.0 09.0 19.0 09.0 19.0 09.0 19.0 09.0 19.1 08.1 10.3 08.5 11.1 12.8 22.6 10.7 23.6 11.1 24.6 11.5 25.3 12.0 25.3 12.0 25.3 16.0 32.5 15.4 34.4 16.2 35.3 16.7 35.9 18.4 34.4 16.2 35.3 16.7 35.9 18.4 34.4 16.2 35.9 18.4 34.4 16.2 35.9 18.4 34.4 16.2 35.9 18.4 34.4 16.2 35.9 18.4 34.4 16.2 35.9 18.4 34.7 22.2 44.6 19.7 45.5 20.1 45.6 23.9 55.6 23.9	lat. dep. dist. 00.9 00.4 61 01.8 00.9 62 02.7 01.3 63 03.6 01.7 64 05.6 05.6 06.3 03.0 67 07.2 03.4 68 09.1 03.9 69 09.0 04.3 70 09.9 04.7 71 10.8 05.1 72 11.8 05.6 73 12.7 08.0 74 13.6 06.4 75 14.5 06.8 76 15.4 07.3 77 16.3 07.7 78 17.2 08.1 79 17.2 08.1 79 18.1 08.6 80 19.0 09.0 81 19.9 09.4 82 20.8 09.8 83 21.7 10.3 84 22.6 10.7 85 23.5 11.1 87 25.3 12.0 88 24.4 11.5 87 25.3 12.0 88 26.2 12.4 89 28.0 13.3 91 28.9 13.7 92 28.0 13.3 91 28.9 13.7 92 28.0 13.3 91 28.9 13.7 92 29.8 14.1 93 30.7 14.5 94 31.6 15.0 95 32.5 15.4 96 33.4 15.8 97 34.4 16.2 98 35.3 16.7 99 35.3 16.7 99 36.2 17.1 100 37.1 17.5 101 38.0 18.0 102 38.9 18.4 103 39.9 18.4 103 39.9 18.4 103 39.9 18.8 104 40.7 19.2 10.5 41.6 19.7 106 42.5 20.1 107 43.4 20.5 108 44.3 21.0 109 45.2 21.1 4 47.0 22.2 112 47.9 22.7 113 48.8 23.1 114 49.7 23.5 115 50.6 23.9 116 51.5 24.4 118 53.3 25.2 119 46.1 24.8 118 53.3 25.2 119 46.1 24.8 118 53.3 25.2 119 46.1 24.8 118 53.3 25.2 119 46.2 25.7 120 46.2 46.2 46.5 46.4 46.4 46.5 46.4 24.8 118 53.3 25.2 119 46.4 24.8 118 53.3 25.2 119 46.4 24.8 118 53.3 25.2 119 46.4 24.8 118 53.3 25.2 119 46.4 24.8 118 53.3 25.2 110 46.4 24.8 118 53.3 25.2 110 46.4 24.8 118 53.3 25.2 110 46.4 24.8 118 53.3 25.2 110 46.4 24.8 118 53.3 25.2 110 46.4 24.8 118 53.3 25.2 110 46.4 24.8 118	lat. dep. dist. lat. 00.9 00.4 61 55.1 01.8 00.9 62 56.0 02.7 01.3 63 57.0 03.6 01.7 64 57.9 04.5 02.6 66 59.7 06.3 03.0 67 60.6 07.2 03.4 68 61.5 09.1 03.8 69 62.4 09.0 04.3 70 63.3 09.9 04.7 71 64.2 11.8 05.6 73 66.0 11.8 05.6 73 66.0 11.8 05.6 73 66.0 11.8 05.6 73 66.0 11.8 05.6 73 66.0 11.7 08.0 74 66.9 13.6 06.8 76 68.7 15.4 07.3 77 69.6 15.4 07.3 77 69.6 15.4 07.3 77 69.6 15.4 07.3 77 69.6 15.4 07.3 77 69.6 15.4 07.3 77 69.6 15.4 07.3 77 69.6 17.2 08.1 79 71.4 18.1 08.6 80 72.3 19.0 09.0 81 73.2 19.0 09.0 81 73.2 19.0 09.0 81 73.2 19.0 09.0 84 75.9 22.6 10.7 85 76.8 23.6 11.1 86 77.7 24.4 11.5 87 78.6 25.3 12.0 88 79.6 26.2 12.4 89 80.5 27.1 12.8 90 81.4 28.0 13.3 91 82.3 28.9 13.7 92 83.2 29.8 14.1 93 84.1 30.7 14.5 94 85.0 31.6 15.0 95 85.9 32.5 18.4 96 85.9 33.4 16.2 98 89.6 35.3 16.7 99 89.5 35.3 16.7 99 89.5 35.3 16.7 99 89.5 35.3 16.7 99 89.5 35.3 16.7 99 89.5 35.3 16.7 99 89.5 35.3 16.7 99 99.5 44.3 20.5 108 97.6 44.3 21.0 107 96.7 43.4 20.5 108 97.6 44.3 21.0 107 96.7 43.4 20.5 108 97.6 44.3 21.1 100 46.1 21.8 111 100.3 47.9 22.7 113 102.1 48.8 23.1 114 103.1 49.7 23.5 115 104.0 50.6 23.9 116 104.9 50.7 23.5 116 104.9 50.8 23.7 114 103.1 49.7 23.5 115 104.0 50.6 23.9 116 104.9 50.7 23.6 116 104.9 50.8 23.1 114 103.1 49.7 23.5 115 104.0 50.8 23.1 114 103.1 49.7 23.5 115 104.0 50.8 23.1 114 103.1	lat. dep. dist. lat. dep.	lat. dep. dist. lat. dep. dist. 009 004 61 55:1 26:1 1 1 1018 009 62 63 57:0 26:5 2 2 20:5 63 57:0 26:9 3 30:6 01:7 64 57:9 27:4 4 4 4 4 4 4 2 5 5 6 6 26:5 2 2 3 36:6 01:7 64 57:9 27:4 4 4 4 4 4 2 5 5 6 6 59:7 28:2 6 6 65:4 29:5 6 6 65:4 29:5 6 6 65:4 29:5 6 6 65:4 29:5 6 6 65:4 29:5 6 6 65:4 29:5 6 6 6 6 6 6 6 6 6	lat. dep. dist. lat. dep. dist. lat. 00.9 00.4 61 55.1 26.5 2 01.8 01.8 00.9 62 56.0 26.5 2 01.8 01.7 63 57.0 26.9 3 02.6 03.6 01.7 64 57.9 27.4 4 03.5 03.6 01.7 64 57.9 27.4 4 03.5 06.3 03.0 67 60.6 28.6 7 06.2 07.2 03.4 68 61.5 29.1 8 07.1 08.1 03.9 69 62.4 29.5 9 07.9 09.0 04.3 70 63.3 29.9 10 08.8 09.9 04.7 71 64.2 29.5 9 07.9 09.0 04.3 70 63.3 29.9 10 08.8 09.9 04.7 71 64.2 30.4 11 09.7 10.8 05.1 72 65.1 30.8 12 10.6 11.8 05.6 73 66.0 31.2 13 11.5 12.7 08.0 74 66.9 31.6 14 12.3 13.6 06.4 75 67.8 32.9 17 15.0 15.4 07.3 77 69.6 32.9 17 15.0 15.4 07.3 77 69.6 32.9 17 15.0 15.3 17.2 08.1 79.7 71.4 33.8 19 16.8 15.9 17.2 08.1 79.7 71.4 33.8 19 16.8 18.5 19.9 09.4 82 74.1 35.1 22 19.4 20.8 09.8 83 75.0 35.5 23 20.3 21.7 10.3 84 75.9 35.9 24 21.2 22.6 10.7 85 76.8 36.3 25 22.1 22.5 31.1 58 77.7 36.8 26 22.9 22.5 22.1 22.5 31.1 58 77.7 36.8 26 22.9 22.5 22.1 22.5 31.1 30.7 41.5 87 73.6 37.2 27 23.8 23.3	lat. dep. dist. lat. dep. dist. lat. dep. 00°9 00°4 61 55°1 25°1 1 00°9 00°5 01°8 00°9 62 55°0 26°5 2 01°8 00°9 00°5 02°7 01°3 63 57°0 26°9 3 02°6 01°0 03°6 01°7 64 57°9 27°4 4 03°5 01°9 04°5 02°1 65 58°8 27°8 5 04°4 02°4 02°4 66 59°7 28°2 6 06°3 02°8 00°3 03°0 67 60°6 28°6 7 06°2 03°3 03°0 67 60°6 28°6 7 06°2 03°3 03°1 03°8 69 62°4 29°5 9 07°9 04°2 09°0 04°3 70 63°3 29°9 10 08°8 04°7 09°9 04°7 71 64°2 23°4 11 09°7 05°2 09°0 04°3 70 63°3 29°9 10 08°8 04°7 08°9 04°7 71 64°2 30°4 11 09°7 05°2 11°8 05°6 73 66°0 31°2 13 11°5 06°1 12°7 08°0 74 66°9 31°6 14 12°3 06°6 13°6 06°4 75 67°8 32°1 15 13°2 07°1 16°3 07°7 78 70°5 33°4 18 15°9 08°5 15°4 03°4 13°8 19°1 18°3 10°6 80°7 72°3 34°2 20°1 17°6 09°4 19°0 09°0 81 73°2 34°2 20°1 17°6 09°4 19°9 09°4 82 74°1 35°1 22 19°4 10°4 19°9 09°4 82 74°1 35°1 22 19°4 10°4 10°5 10°6 11°1 10°3 10°8 10°8 10°8 10°9 10°9 10°1 10°3 10°8 10°9 1	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	00+9 00+4 61 55-1 26-1 1 00-9 00-5 61 53-8 01-8 00-9 62 56-0 26-5 2 01-8 00-9 62 54-7 02-7 01-3 63 57-0 28-9 3 02-6 01-0 63 55-6 03-6 01-7 64 57-9 27-4 4 03-6 01-9 64 56-4 04-5 02-1 65 58-8 27-8 5 04-4 02-4 65 57-3 05-4 02-6 66 59-7 28-2 6 06-3 02-9 66 58-2 06-3 03-0 67 60-6 29-6 7 06-2 03-3 67 59-1 07-2 03-4 68 61-5 29-1 8 07-1 03-8 68 60-0 08-1 03-6 09 62-4 29-5 9 07-9 04-2 69 60-9 09-0 04-3 70 63-3 29-9 10 08-8 04-7 70 61-7 09-9 04-7 71 64-2 30-4 11 09-7 05-2 71 62-6 09-1 03-6 05-1 72 65-1 30-8 12 10-6 05-7 72 63-6 11-8 05-6 73 66-0 31-2 13 11-5 06-1 73 64-4 11-8 05-6 73 66-0 31-2 13 11-5 06-1 73 64-6 11-6 05-7 73 66-0 32-9 17 15-0 09-0 77 67-9 11-8 05-6 73 66-0 32-9 17 15-0 09-0 77 67-9 11-8 05-6 73 68-0 32-9 17 15-0 09-0 77 67-9 11-8 05-6 73 68-0 32-9 17 15-0 09-0 77 67-9 11-8 05-6 73 68-0 32-9 17 15-0 09-0 77 67-9 11-8 05-6 73 68-0 32-9 17 15-0 09-0 77 67-9 11-8 05-6 73 68-0 32-9 17 15-0 09-0 77 67-9 11-8 05-6 73 68-0 32-9 17 15-0 09-0 77 67-9 11-8 05-6 73 68-6 32-9 17 15-0 09-0 77 67-9 11-8 05-6 77 78 70-5 33-4 18 15-9 09-5 77 66-7 0 11-9 09-0 81 73-2 34-6 21 13-5 09-9 81 77-6 91-7 1 11-9 09-0 81 73-2 34-6 21 13-5 09-9 81 77-6 91-7 1 11-9 09-0 81 73-2 34-6 21 13-5 09-9 81 77-6 91-7 1 11-9 09-0 81 73-2 34-6 21 13-5 09-9 81 77-6 91-7 1 11-9 09-0 81 73-2 34-6 21 13-5 09-9 81 77-6 91-7 1 11-9 09-0 81 73-2 34-6 21 13-5 09-9 81 77-6 91-7 1 11-9 09-0 81 73-2 34-6 21 13-5 09-9 81 77-6 91-7 1 11-9 09-0 81 73-2 34-6 21 13-5 09-9 81 77-6 91-7 1 11-9 09-0 81 73-2 34-6 21 13-5 09-9 81 77-6 91-7 1 11-1 00-1 00-1 00-1 00-1 00-1 00-1

T' IV) Die	of lat	& den	for 21	Points	Dif.	of lat.	& den.	for 3 1	Points	191
dist. 1 2 3 4 5 6 7 8 9	lat. 00:0 01:7 02:6 03:4 04:3 05:1 06:0 07:7 08:6	dep. 00·5 01·0 01·5 02·1 02·6 03·1 03·6 04·1 04·6 05·1	dist. 61 62 63 64 65 66 67 68 69 70	lat. 52°3 53°2 54°0 54°9 55°8 56°6 57°5 58°3 59°2 60°0	dep. 31.4 31.9 32.4 32.9 33.4 33.9 34.4 35.0 35.5 36.0	dist. 1 2 3 4 5 6 7 8 9 10	lat. 00:8 01:7 02:5 03:3 04:2 05:0 05:8 06:7 07:5 08:3	dep. 00·6 00·1 01·7 02·2 02·8 03·3 03·9 04·4 05·0 05·6	dist. 61 62 63 64 65 66 67 68 69 70	tat. 50.7 51.5 52.4 53.2 54.0 54.9 55.7 56.6 57.4 58.2	dep. 33-9 34-4 35-0 35-6 36-1 36-7 37-2 37-8 33-3 38-9
11 12 13 14 15 16 17 18 19	09-4 10-3 11-2 12-0 12-9 13-7 14-6 15-4 16-3 17-2	05·7 06·2 06·7 07·2 07·7 08·2 08·7 09·3 09·8 10·3	71 72 73 74 75 76 77 78 79 80	60·9 61·8 62·6 63·5 64·3 65·2 66·9 67·8 68·6	36.6 37.0 37.5 38.0 38.6 39.1 39.6 40.1 40.6 41.1	11 12 13 14 15 16 17 18 19 20	09·1 10·0 10·8 11·6 12·5 13·3 14·1 15·0 15·8 16·6	06·1 06·7 07·2 07·8 08·3 08·9 09·4 10·0 10·6 11·1	71 72 73 74 75 76 77 78 79 80	59·0 59·9 60·7 61·5 62·4 63·2 64·0 64·9 65·7 66·5	39·4 40·0 40·6 41·1 41·7 42·2 42·8 43·3 43·9 44·4
21 22 23 24 25 26 27 28 29 30	18·9 19·7 20·6 21·4 22·3 23·2 24·0 24·9 25·7	10°8 11°3 11°8 12°3 12°9 13°4 13°9 14°4 14°9 15°4	81 82 83 84 85 86 87 89 90	69°5 70°3 71°2 72°0 72°9 73°8 74°6 75°5 76°3 77°2	41.6 42.2 42.7 43.2 43.7 44.2 44.7 45.2 45.7 46.3	21 22 23 24 25 26 27 28 29 30	17·5 18·3 19·1 20·0 20·8 21·6 22·4 23·3 24·1 24·9	11·7 12·2 12·8 13·3 13·9 14·4 15·0 15·6 16·1 16·7	81 82 83 84 85 86 87 88 89 90	67·3 68·2 69·0 69·8 70·7 71·5 72·3 73·2 74·0 74·8	45·0 45·6 46·1 46·7 47·2 47·8 48·3 48·9 49·4 50·0
31 32 33 34 35 36 37 38 39 40	26·6 27·4 28·3 29·2 30·0 30·9 31·7 32·6 33·5 34·3	15.9 16.4 17.0 17.5 18.0 13.5 19.0 19.5 20.0 20.6	91 92 93 94 95 96 97 93 99 100	78·1 78·9 79·8 80·6 81·5 82·3 83·2 84·1 84·9 85·8	46.9 47.3 47.8 48.3 48.9 49.3 49.9 50.4 50.9 51.5	31 32 33 34 35 36 37 38 39 40	25·8 26·6 27·4 28·3 29·1 29·9 30·8 31·6 32·4 33·3	17·2 17·8 18·3 18·9 19·4 20·0 20·6 21·1 21·7 22·2	91 92 93 94 95 96 97 98 99 100	75·7 76·5 77·3 78·2 79·0 79·9 80·6 81·5 82·3 83·1	50.6 61.1 51.7 52.2 52.8 63.3 63.9 54.4 55.0 55.6
41 42 43 44 45 46 47 48 49 50	35·2 36·0 36·9 37·7 38·6 39·5 40·3 41·2 42·0 42·9	21·1 21·6 22·1 22·6 23·1 23·6 24·2 24·7 25·2 25·7	101 102 103 104 105 106 107 108 109 110	86·6 87·5 88·3 89·2 90·1 90·9 91·8 92·6 93·5 94·3	51·9 52·4 52·9 53·5 54·0 54·6 55·0 56·5 56·0	41 42 43 44 45 46 47 48 49 50	34·1 34·9 35·9 36·6 37·4 39·2 39·1 39·9 40·7 41·6	22·8 23·3 23·9 24·4 25·0 25·6 26·1 26·7 27·2 27·8	101 102 103 104 105 106 107 108 109 110	84·0 84·8 86·5 86·5 87·3 88·1 69·0 89·8 90·6 91·5	56·1 56·7 57·2 57·8 58·3 58·9 59·4 60·0 60·6 61·1
51 52 53 54 55 56 57 58 59 60 dist	43·7 44·6 45·5 46·3 47·2 48·0 43·9 49·7 50·6 51·5 dep.	26·2 26·7 27·2 27·8 28·3 28·8 29·3 30·3 30·8 lat.	111 112 113 114 115 116 117 118 119 120 dist.	95·2 96·1 96·9 97·8 98·6 99·5 100·4 101·2 102·1 102·9 dep.	57·1 57·6 59·1 59·6 59·1 59·6 60·1 60·7 61·2 61·7 Lat.	51 52 53 54 55 56 57 58 59 60 dist	42·4 43·2 44·1 44·9 45·7 46·6 47·4 48·2 49·1 49·9 dep.	28·3 28·9 29·4 30·0 30·6 31·1 31·7 32·2 32·8 33·3 lat.	111 112 113 114 115 116 117 118 119 120 dist.	92·3 93·1 94·0 94·8 95·6 96·4 97·3 99·1 98·9 99·8 dep.	61·7 62·2 62·8 63·3 63·9 64·4 65·0 65·6 66·1 66·7 lat.

100	Diff.	Flat &	den	Com 21 i	Dainte	Diff.	£7.00 d	Jan de	- 21 /	Dalude.	177
192	lat.	dep.	dist.	lat.	dep.	dist.	lat.	dep. Je	dist.	lat.	[T.w.
1 2 3 4 5 6 7 8 9	00·8 01·6 02·4 03·2 04·0 04·8 05·6 06·4 07·2 08·0	00·6 01·2 01·8 02·4 03·0 03·6 04·2 04·8 05·4 06·0	61 62 63 64 65 66 67 68 69 70	49.0 49.8 50.6 51.4 52.2 53.0 53.8 54.6 55.4 56.2	36-3 36-9 37-5 38-1 38-7 39-3 40-5 41-1 41-7	2 3 4 5 6 7 8 9	00·8 01·5 02·3 03·1 03·9 64·6 05·4 06·2 07·0 07·7	00°6 01°3 01°9 02°5 03°2 03°8 04°4 05°1 05°7	61 62 63 64 65 66 67 68 69 70	47·1 47·9 48·7 49·5 50·2 51·0 51·8 52·6 53·3 54·1	dep. 38-7 39-3 40-0 40-6 41-2 41-9 42-5 43-1 43-8 44-4
11 12 13 14 15 16 17 18 19	09-8 09-6 10-4 11-2 12-0 12-8 13-7 14-5 15-3 16-1	06·6 07·1 07·7 08·3 08·9 09·5 10·1 10·7 11·3 11·9	71 72 73 74 75 76 77 78 79 80	57.0 57.8 68.6 59.4 60.2 61.0 61.8 62.6 63.4 64.3	42·3 42·9 43·5 44·1 44·7 45·3 45·9 46·5 47·1 47·7	11 12 13 14 15 16 17 18 19 20	08·5 09·3 10·1 10·8 11·6 12·4 13·1 13·9 14·7 15·5	07-0 07-6 08:2 08:9 09-5 10:1 10:8 11-4 12:0 12:7	71 72 73 74 75 76 77 78 79 80	54·9 55·7 56·4 57·2 58·0 58·7 59·5 60·3 61·1 61·8	45·0 45·7 46·3 46·9 47·6 48·2 48·8 49·5 50·1 50·7
21 22 23 24 25 26 27 28 29 30	16-9 17-7 18-5 19-3 20-1 20-9 21-7 22-5 23-3 24-1	12.5 13.1 13.7 14.3 14.9 15.5 16.1 16.7 17.3 17.9	81 82 83 84 85 86 87 88 89	65·1 65·9 66·7 67·5 68·3 69·1 69·9 70·7 71·5 72·3	48·3 48·9 49·4 50·0 50·6 51·2 51·8 52·4 53·0 53·6	21 22 23 24 25 26 27 28 29 30	16-2 17-0 17-8 18-5 19-3 20-1 20-9 21-6 22-4 23-2	13·3 14·0 14·6 15·2 16·5 17·1 17·8 18·4 19·0	81 82 83 84 85 86 87 88 89 90	62·6 63·4 64·2 64·9 66·7 66·5 67·2 68·0 68·8 69·6	51.4 52.0 52.7 53.3 53.9 54.6 55.2 55.8 56.5
31 32 33 34 35 36 37 39 40	24·9 25·7 26·5 27·3 28·1 28·9 20·7 30·5 31·3 32·1	18·5 19·1 19·7 20·3 20·9 21·4 22·6 23·2 23·8	91 92 93 94 95 96 97 98 99 100	73·1 73·9 74·7 75·5 76·3 77·1 77·9 78·7 79·5 80·3	54·2 54·8 55·4 56·0 56·6 57·2 57·8 58·4 59·0 59·6	31 32 33 34 35 36 37 38 39 40	24·0 24·7 25·5 26·3 27·1 27·8 28·6 29·4 30·1 30·9	19·7 20·3 20·9 21·6 22·2 24·8 23·6 24·1 24·7 25·4	91 92 93 94 95 96 97 98 99 100	70·3 71·1 71·9 72·7 73·4 74·2 75·0 75·7 76·5 77·3	57-7 59-4 59-6 60-3 60-9 61-5 62-2 62-8 63-4
41 42 43 44 45 46 47 48 49 50	32·9 33·7 34·5 35·3 36·1 36·9 37·7 38·6 39·4 40·2	24·4 25·0 25·6 26·2 26·8 27·4 28·0 28·6 29·2 29·8	101 102 103 104 105 106 107 108 109	91·1 81·9 82·7 83·5 84·3 85·1 85·9 86·7 87·5 88·4	60-2 60-8 61-4 62-0 62-6 63-1 63-7 64-3 64-9 65-5	41 42 43 44 45 46 47 48 49 50	31·7 32·5 33·2 34·0 34·8 35·6 36·3 37·1 37·9 38·6	26·0 26·6 27·3 27·9 28·5 29·8 30·4 31·1 31·7	101 102 103 104 105 106 107 108 109 110	78·1 78·8 79·6 80·4 81·2 81·9 82·7 83·5 84·3	64·1 64·7 65·3 66·0 66·6 67·2 67·9 68·5 69·1 69·8
51 52 53 54 55 56 57 58 69 60 dist.	41.0 41.8 42.6 43.4 44.2 45.0 45.8 46.6 47.4 48.2 dep.	30·4 31·6 32·2 32·8 33·4 34·6 35·1 35·7 lat.	111 112 113 114 115 116 117 118 119 120 dist.	89·2 90·0 90·8 91·6 92·4 93·2 94·0 94·8 95·6 96·4 dep.	66·1 66·7 67·3 67·9 68·5 69·1 69·7 70·3 70·9 71·5 lat.	51 52 53 54 55 56 67 58 69 60 dist.	39-4 40-2 41-0 41-7 42-5 43-3 44-1 44-8 45-6 46-4 dep.	32·3 33·6 34·3 34·9 35·5 36·2 36·8 37·4 38·1 lat.	111 112 113 114 115 116 117 118 119 120 dist.	85.8 86.6 87.3 88.1 88.9 89.7 90.4 91.2 92.0 92.8 dep.	70·4 71·0 71·7 72·3 73·0 73·6 74·2 74·9 76·5 76·1 lat.
_		For 4	Poin	ts.]	For 4	Poin	ts.	

T. 1V.	Dif.	of lat.	4 dep	. for 3	Points	Dif.	of lat.	4 dep.	for 4	Points	. 193
dist.	lat.	dep.	dist.		dep.	# dist.	lat.		dist.	lat.	
1	00.7	00.7	61	45.2	41.0	1	00.7	dep. 00.7	61	43.1	dep. 43·1
2	01.5	01.3	62	45.9	41.6	2	01.4	01.4	62	43.8	43.8
3	02.2	02.0	63	46.7	42.3	ã	02.1	02.1	63	44.5	44.5
4	03.0	02.7	64	47.4	43.0	4	02.8	02.8	64	45.3	45.3
5	03.7	03.4	65	48.2	43.6	5	03.5	03.5	65	46.0	46.0
6	04.4	04-0	66	48.9	44.3	6 7	04.2	04.2	66	46.7	46.7
7	05.2	04.7	67	49.6	45.0	7	04.9	04.9	67	47.4	47.4
8	05-9	05.4	68	50.4	45.7	8 9	05.7	05.7	68	48.1	48.1
, 9	06.7	06.0	69	51.1	46.3	9	06.4	06.4	69	48.8	48.8
10	07.4	06.7	70	51.9	47-0	10	07.1	07.1	70	49.5	49.5
. 11	08.2	07:4	71 72	52:6	47.7	-11	07.8	07:8	71	50.2	50.2
11 12	08-9	08.1	72	53.3	48.3	12	08.2	08-5	72	50-9	50.9
13	09.6	08.7	73	54.1	49.0	13	09.2	09.2	73	51.6	51.6
14	10.4	09.4	74	54.9	49.7	14	09.9	09.9	74	52.3	52.3
15	11.1	10.1	75	55.6	50.4	15	10.6	10.6	75	53.0	53.0
16	11.9	10.7	76	26.3	51.0	16	11.3	11.3	76	53.7	53.7
17	12·6 13·3	12.1	77 78	57.0	51·7 52·4	17	12.0	12.0	77	54.4	54.4
18 19	14.1	12.8	79	57·8 58·5	53.0	18	12.7	12·7 13·4	79	55.2	55.2
20	14.8	13.4	80	20.3	53.7	19 20	13·4 14·1	14.1	79 80	55·9 56·6	55.9
1											56.6
21 22	15.6	14·1 14·8	81	60.0	54.4	21	14.8	14'8	81	57.3	57.3
22	17.0	15.4	82	60.8	55.1	22	15.6	15.6	82 83 84	58.0	58.0
23 24	17.8	16.1	83 84	61.5	55·7 56·4	23 24	16·3 17·0	16.3	83	58.7	58.7
25	185	16.8	85	62·2	57.1		17.7	17·0 17·7	84	59·4 60·1	59.4
26	19.3	17.5	86	63.7	57.7	25 26	18.4	18.4	85 86	60.8	60·1
27	209	18.1	87	64.2	58.4	27	19.1	19.1	87	61.5	61.5
28	20.7	18.8	88	65.2	59.1	28	19.8	19.8	88	62.2	62.2
29	21.8	19.5	89	65.9	59.8	20	20.5	20.5	89	62.9	62.9
29 30	22.2	20.1	90	66.7	60.4	29 30	21.2	21.2	90	62·9 63·6	63.6
31	23.0	20.8	91	67.4	61.1	31	21.9	21.9	91	64.3	64.3
32	23.7	21.5	92	68.2	61.8	32	22.6	22.6	92	65.1	65.1
33	24.4	22.2	93	68.9	62.4	33	23.3	23.3	93	65-8	65.8
34	25.2	22.8	94	69.6	63.1	34	24.0	24.0	94	66.5	66.5
35	25.9	23.5	95	70.4	63.8	35	24.7	24.7	95	67.2	67.2
36 37	26.7	24.2	96	71.1	64.2	36	25.5	25.5	95 96 97	67.9	67.9
37	27.4	24.8	97	71.9	65.1	. 37	26.2	26.2	97	68.6	68.6
38	28.2	25.5	98 99	72.6	65.8	38	26.9	26.9	98	69.3	69.3
39	28.9	26.2	99	73.3	66.8	39	27.6	27.6	99	70.0	70.0
40	29.6	26.9	100	74.1	67.2	40	28.3	28.3	100	70.7	70.7
41	30.4	27-5	101	74.8	67.8	41	29.0	29.0	101	71.4	71.4
42	31.1	28.3	102	75.6	68.2	42	29.7	29.7	102	72.1	72.1
43	31.9	28.9	103	76.3	69.2	43	30.4	30.4	103	72.8	72.8
44	32.6	29.5	104	77.1	69.8	44	31.1	31.1	104	73.5	73.5
45	33.3	30.5	105	77.8	70.5	45	31.8	31.8	105	74.2	74.2
46 47	34.8	31.6	106 107	78.5	71·2 71·8	46 47	32.5	32.5	106	75.0	75.0
48	35.6	32.2	108	79·3 80·0	72.5	48	33·9	33.5	107 108	75·7 76·4	75·7 76·4
49	36.3	32.9	109	80.8	73.2	49	34.6	34.6	109	77.1	77.1
50	37.0	33.6	110	81.2	73.9	50	35.4	35.4	110	77.8	77.8
	37.8	34.2	111								
51	38.5	34.9	112	82.2	74·5 75·2	51 52	36.1	36·8	111	78.5	78.5
52 53	39.3	35.6	113	83·0 83·7	75.9	53	36·8 37·5	37.5	112 113	79·2 79·9	79·2 79·9
53 54	40.0	36.3	114	84.5	76.5	54	38.5	38.2	114	80.6	80.6
55	40.7	36.9	115	85.2	77.2	55	38.9	38.9	115	81.3	81.3
56	41.5	37.6	116	85.9	77-9	56	39.6	39.6	116	82.0	82.0
57	42.2	38.3	117	86.7	78.6	57	40.3	40.3	117	82.7	82.7
58	43.0	38.9	118	87.4	79.2	58	41.0	41.0	118	83.4	83.4
59	43.7	39.6	119	88.2	79-9	59	41.7	41.7	119	84.1	84.1
60	44.5	40.3	120	88.9	80.6	60	42.4	42.4	120	84.8	84.8
dist.		lat.	dist.	dep.	lat.	dist.	dep.	lat.	dist.		lat.
	1	For 44	Poin	ts.				For 4	Poin	ts.	
-											

TABLE V.

A TABLE OF RUMBS,

SHOWING

THE DEGREES, MINUTES, AND SECONDS, THAT EVERY POINT AND QUARTER-POINT OF THE COMPASS MAKES WITH THE MERIDIAN.

NO	RTE.	Pt	.qr.	, 0	,		P	.qr.	801	TH.
		0	1	2	48	45	0	1		
	1	0	1 2 3	5 8	37 26	30 15	0	3		
N. by E.	N. by W.	ĭ	ŏ	11	15	0		ő	S. by E.	S. by W.
N.N.E.	N.N.W.	1112	1 2 3 0	14 16 19 22	3 52 41 30	45 30 15 0	1 1 1 2	1 2 3 0	S.S.E.	s.s.w.
N.E. by N.	N.W.by N.	3		25 28 30 33	18 7 56 45	45 30 15 0	1	30	S. E. by S.	S. W . by S.
N.E.	N.W.	3 3 4	1 2 3 0	36 39 42 45	33 22 11 0	45 30 15 0	3 3 4	1 2 3 0	S.E.	s.w.
N.E. by E.	N.W.byW.	4 4 4 5		47 50 53 56	48 37 26 15	45 30 15 0	4 4 5	1 2 3 0	S.E. by E.	S.W.by W.
E.N.E.	W. N. W .	5 5 5 6	3	59 61 64 67	3 52 41 30	45 30 15 0	5 5 6	1 2 3 0	E.S.E.	w.s.w.
E by N.	W. by N.	6 6 7	1 2 3 0	70 73 75 78	18 7 56 45	0	6 6 7	1 2 3 0	E. by S	W. by S.
East.	West.	7 7 7 8	3	81 84 87 90	33 22 11 0	45 30 15 0	7 7 7 8	1 2 3 0	East	West.
		_						_		

WORKMAN'S TABLE,

FOR CORRECTING THE MIDDLE LATITUDE.

196			DIFF	[Ta	ble VI.				
Mid.	3°	40	50	60	70	80	90	10°	110
15 16 17 18 19 20 21 22 23 24	0 02 0 02 0 02 0 02 0 02 0 02 0 02 0 02	0 03 0 03 0 03 0 03 0 03 0 03 0 03 0 03	0 04 0 04 0 04 0 04 0 04 0 04 0 04 0 04	0 06 0 06 0 06 0 06 0 06 0 06 0 06 0 06	0 09 0 09 0 08 0 08 0 07 0 07 0 07 0 07 0 07	0 12 0 12 0 12 0 11 0 11 0 10 0 09 0 09 0 09 0 09	0 15 0 15 0 14 0 14 0 13 0 12 0 12 0 12 0 12 0 12	0 19 0 18 0 17 0 17 0 16 0 15 0 15 0 15 0 15	0 23 0 22 0 21 0 20 0 19 0 18 0 17 0 17 0 16
25 26 27 28 29 30 31 32 33 34	0 02 0 02 0 02 0 02 0 02 0 02 0 02 0 02	0 03 0 03 0 03 0 03 0 03 0 03 0 03 0 03	0 04 0 04 0 04 0 04 0 04 0 04 0 04 0 04	0 05 0 05 0 05 0 05 0 05 0 05 0 05 0 05	0 07 0 07 0 07 0 06 0 06 0 06 0 06 0 06	0 09 0 09 0 06 0 06 0 08 0 08 0 08 0 08 0 08	0 11 0 11 0 11 0 10 0 10 0 10 0 10 0 10	0 14 0 14 0 14 0 13 0 13 0 13 0 13 0 13 0 13 0 13	0 16 0 16 0 16 0 15 0 15 0 15 0 15 0 15 0 15
35 36 37 38 39 40 41 42 43 44	0 02 0 02 0 02 0 02 0 02 0 02 0 02 0 02	0 03 0 03 0 03 0 03 0 03 0 03 0 03 0 03	0 04 0 04 0 04 0 04 0 04 0 04 0 04 0 04	0 05 0 05 0 05 0 05 0 05 0 05 0 05 0 05	0 06 0 06 0 06 0 06 0 06 0 06 0 06 0 06	0 06 0 08 0 08 0 08 0 06 0 06 0 06 0 09 0 09	0 10 0 10 6 10 0 10 0 10 0 10 0 10 0 10	0 13 0 13 0 13 0 13 0 13 0 13 0 13 0 14 0 14	0 15 0 15 0 15 0 15 0 15 0 15 0 15 0 16 0 16
45 46 47 48 49 50 51 52 53 54	0 02 0 02 0 02 0 02 0 02 0 02 0 02 0 02	(03 0 03 0 03 0 03 0 03 0 03 0 03 0 03	0 04 0 04 0 04 0 04 0 04 0 04 0 04 0 04	0 05 0 05 0 05 0 05 0 05 0 05 0 05 0 05	0 07 0 07 0 07 0 07 0 07 0 07 0 07 0 07	0 09 0 09 0 09 0 09 0 09 0 09 0 09 0 09	0 11 0 11 0 11 0 11 0 11 0 11 0 11 0 12 0 12	0 14 0 14 0 14 0 14 0 14 0 14 0 14 0 15 0 15	0 16 0 16 0 16 0 16 0 17 0 17 0 17 0 18 0 18 0 19
55 56 57 58 59 60 61 62 63 64	0 02 0 02 0 02 0 02 0 02 0 02 0 02 0 02	0 03 0 03 0 03 0 03 0 03 0 03 0 03 0 03	0 04 0 04 0 04 0 04 0 04 0 05 0 05 0 05	0 06 0 06 0 06 0 06 0 06 0 06 0 07 0 07	0 08 0 08 0 08 0 09 0 09 0 09 0 09 0 09	0 10 0 10 0 11 0 11 0 12 0 12 0 12 0 12	0 13 0 13 0 14 0 14 0 15 0 15 0 16 0 16 0 17	0 16 0 16 0 17 0 17 0 18 0 19 0 19 0 20 0 20 0 21	0 19 0 20 0 20 0 21 0 22 0 23 0 23 0 24 0 25
65 66 67 68 69 70 71 72	0 02 0 02 0 02 0 02 0 02 0 02 0 03 0 04 0 04	0 04 0 04 0 04 0 04 0 05 0 05 0 06	0 06 0 06 0 06 0 06 0 06 0 06 0 07 0 08	0 08 0 08 0 08 0 08 0 09 0 09 0 09 0 10	0 10 0 10 0 11 0 11 0 12 0 13 0 13	0 13 0 14 0 15 0 15 0 16 0 17 0 18 0 19	0 17 0 18 0 18 0 19 0 20 0 21 0 22 0 23	0 21 0 22 0 23 0 24 0 25 0 26 0 27 0 29	0 25 0 26 0 27 0 28 0 30 0 31 0 33 0 35

Ťab	e v1.]		DIFI	ERENCE	OF LA	TITUDE		-	197
Mid. Lat.	120	130	140	150	160	170	180 .	190	20°
15 16 17 18 19 20 21 22 23 24	0 27 0 26 0 25 0 24 0 23 0 22 0 21 0 20 0 20 0 19	0 31 0 30 0 28 0 27 0 26 0 25 0 25 0 24 0 24 0 23	0 35 0 34 0 32 0 31 0 30 0 29 0 29 0 28 0 28 0 27	0 40 0 38 0 37 0 36 0 34 0 33 0 33 0 32 0 32 0 31	0 45 0 43 0 42 0 41 0 40 0 38 0 37 0 36 0 36	0 51 0 49 0 48 0 46 0 45 0 43 0 42 0 41 0 40	0 58 0 56 0 54 0 52 0 50 0 48 0 47 0 46 0 45 0 44	1 06 1 03 1 01 0 58 0 56 0 54 0 53 0 51 0 50 0 48	1 14 1 11 1 08 1 06 1 03 1 00 0 58 0 56 0 55 0 53
25 26 27 28 29 30 31 32 33 34	0 19 0 19 0 19 0 18 0 18 0 18 0 18 0 18 0 18	0 23 0 22 0 22 0 21 0 21 0 21 0 21 0 21 0 21	0 27 0 26 0 26 0 25 0 25 0 25 0 25 0 25 0 24 0 24	0 31 0 30 0 30 0 29 0 29 0 28 0 28 0 27 0 27	0 35 0 34 0 33 0 33 0 32 0 32 0 32 0 31 0 31	0 39 0 38 0 38 0 37 0 36 0 36 0 36 0 36 0 35 0 35	0 43 0 42 0 42 0 41 0 41 0 41 0 41 0 40 0 40	0 47 0 47 0 46 0 46 0 45 0 45 0 45 0 45 0 44 0 44	0 52 0 52 0 51 0 51 0 50 0 50 0 50 0 50 0 49 0 49
35 36 37 38 39 40 41 42 43 44	0 18 0 18 0 18 0 18 0 18 0 18 0 18 0 19 0 19	0 21 0 21 0 21 0 21 0 21 0 22 0 22 0 22	0 24 0 24 0 24 0 25 0 25 0 25 0 26 0 26 0 27	0 27 0 27 0 27 0 27 0 28 0 28 0 28 0 29 0 30 0 30	0 31 0 31 0 31 0 32 0 32 0 32 0 33 0 34 0 34	0 35 0 35 0 35 0 36 0 36 0 36 0 37 0 37 0 38 0 38	0 40 0 40 0 40 0 40 0 41 0 41 0 42 0 42 0 43	0 44 0 44 0 45 0 45 0 45 0 46 0 46 0 47	0 49 0 49 0 49 0 50 0 50 0 50 0 50 0 50 0 51 0 51
45 46 47 48 49 50 51 52 53 54	0 19 0 19 0 20 0 20 0 21 0 21 0 21 0 22 0 22 0 23	0 23 0 23 0 23 0 23 0 24 0 24 0 24 0 25 0 25	0 27 0 27 0 27 0 28 0 28 0 28 0 29 0 30	0 31 0 31 0 31 0 32 0 32 0 32 0 33 0 33 0 34	0 35 0 35 0 35 0 36 0 36 0 37 0 37 0 38 0 39	0 39 0 39 0 40 0 40 0 41 0 41 0 42 0 42 0 43 0 44	0 43 0 44 0 44 0 45 0 45 0 46 0 47 0 48 0 49 0 50	0 47 0 48 0 49 0 50 0 51 0 52 0 53 0 54 0 55	0 52 0 53 0 54 0 55 0 57 0 58 0 59 1 00 1 01 1 02
55 56 57 58 59 60 61 62 63 64	0 23 0 24 0 24 0 25 0 26 0 27 0 27 0 28 0 29 0 29	0 26 0 27 0 28 0 29 0 30 0 31 0 31 0 32 0 33	0 30 0 31 0 32 0 33 0 34 0 35 0 36 0 37 0 39 0 40	0 35 0 36 0 37 0 38 0 39 0 40 0 41 0 42 0 44 0 46	0 40 0 41 0 42 0 44 0 45 0 46 0 47 0 49 0 51 0 53	0 45 0 46 0 48 0 50 0 51 0 52 0 54 0 56 0 58 1 00	0 51 0 52 0 54 0 55 0 57 0 59 1 01 1 03 1 05 1 07	0 57 0 58 1 00 1 02 1 04 1 06 1 08 1 10 1 12 1 14	1 03 1 04 1 06 1 08 1 10 1 13 1 15 1 18 1 21 1 24
65 66 67 68 69 70 71 72	0 30 0 31 0 33 0 34 0 36 0 38 0 40 0 42	0 35 0 37 0 38 0 40 0 44 0 44 0 46 0 49	0 41 0 43 0 45 0 48 0 50 0 52 0 55 0 58	0 48 0 50 0 53 0 55 0 58 1 00 1 03 1 06	0 55 0 58 1 00 1 02 1 05 1 08 1 12 1 16	1 02 1 05 1 07 1 10 1 13 1 17 1 22 1 27	1 09 1 12 1 16 1 19 1 23 1 28 1 32 1 38	1 17 1 21 1 25 1 30 1 34 1 39 1 44 1 50	1 27 1 31 1 35 1 39 1 44 1 50 1 56 2 04

17*

A TABLE

ATMOSPHERICAL REFRACTIONS,

WITH CORRECTIONS FOR THE HEIGHT OF THE BAROMETER, AND THER-MOMETER, TAKEN FROM THE NAUTICAL ALMANACK.

TABLE VII.

·									
	Refr.	Diff.	Diff.	Diff.		Refr.	Diff.	Diff.	Diff.
App.	Br. 30.	for	for	for -10 Fak	App. Altitude.	Br. 30	for	for	for -1°Fak
Altitude.	Th. 500.	I Alt.	+1' B.	-10Fth.	Altitude.	Th. 500.	1 Alt.	+1 B.	-Iokar
	, ,,			<i>u</i>	0 1	111	"		"
åó	11 52	2.2	24-1	1.70	§ ó	5 54	· 6	11.9	.76
10	11 30	21	23.4	1.64	10	5 47	.6	11.7	.74
20	11 10	20	22.7	1.58	20	5 41	.6	11.5	.73
30	10 50	1.9	22-0	1.53	30	5 36	6	11.3	.71
40	10 32	1.8	21.3	1.48	40	5 30	.5	11.1	.71
50	10 15	1.7	20.7	1.43	50	5 25	•5	11.0	.70
	1		1			1	1 1		1
5 0	9 58	1.6	20.6	1.38	10 0	5 20	-5	10.8	-69
10	9 42	1.5	19.1	1.34	10 0	5 15	.5	10.6	.67
20	9 27	1.5	19.1	1.30	20	5 10	.5	10-4	.65
30	9 11	1.4	18.6	1.26	30	5 5	•5	10.3	·64
40	8 58	1.3	18.1	1.22	40	5 0	•5	10.1	·63
50	8 45	1.3	17.6	1.19	50	4 56	•4	9.9	·62
~ 1				7	, ~~ i		1		1
6 0	8 32	1.2	17.2	1.15	11 0	4 51	-4	9.8	-60
10		1.3			10		-4		-59
	8 20		16.8	1.11		4 47		9.6	
20	8 9	1.1	16.4	1.09	20	4 43	-4	9.5	.58
30	7 58	1.1	16.0	1.06	30	4 39	•4	9.4	.57
40	7 47	1.0	15.7	1.03	40	4 35	•4	9.2	.56
50	7 37	10	15.3	1.00	50	4 31	•4	9.1	-55
- ~	, ,,	1	100	- 00	~	1 - 3 -	•		١ "
7 0		1.0	12.0	.00	10 0	428.1	·38	0.00	-556
	7 27	1.0	15.0	.98	12 0			9.00	
10	7 17	.9	14.6	.95	10	4 24 4	.37	8.86	•548
20	78	.9	14.3	∙93	20	4 20 8	.36	8.74	·541
30	6 59	.8	14-1	·91	30	4 17.3	-35 ∣	8:63	.533
40	6 51	·š	13.8	-89	40	4 13-9	33	8:51	.524
50	6 43	8	13.5	.87	50	4 10.7	.32	8.41	-517
<i>3</i> 0	0.49		10.0	91	30 I	3 10.1	34	041	1 21,
1	1 200	_				ا ـ ـ ـ ا		000	
8 0	6 35	.7	13.3	.85	13 0	4 75	.31	8.30	-509
10	6 28	.7	13.1	.83	10	4 4.4	·31	8.20	.503
20	6 21	-7	12.8	-82	20	4 1.4	.30	8.10	496
30	6 14	.7	12-6	-80	30	358.4	·30	8.00	490
40	6 7	- 7	12.3	.79	40	355.5	.29	7.89	482
50		-6	12.1	10			29		
20	60	-6	12.1	77	50	3 52.6	29	7.79	476

TABLE VII.
TABLE OF REFRACTIONS.

!											
App.		Refr. Br. 30.	Diff.	Diff.	Diff. for -10 F	App	a.	Refr. Br. 30 Th. 500.	Diff.	Diff.	Diff. for -10 F.
Altitue	le.	Th.500.	li Alt.	+1'B.	-10 F.	A/titu	de.	Th. 500.	1 Alt.	+1 B.	-10 F.
14	4	3 49.9	28	L'ac	· 4 69	48	ń	52.3	·ő31	1.75	·104
	Ó		728	7.76			Ŏ				
	10	3 47-1	·28 ·27	7.61	464	49	0	50.5	.030	1.69	·101
	90	3 44.4		7.52	458	50	0	48.8	029	1.63	.097
	30	3 41.8	'26	7.43	453	51	Õ	47.1	028	1.58	.094
	10	3 39.2	.26	7.34	•448	62	0	45.4	.027	1.52	-090
1 8	50	3 36.7	.25	7.26	·444	53	0	43.8	.026	1.47	.088
					400		_	40.0			
15	0	3 34.3	-24	7.18	·439	54	0.	42.2	026	1.41	.085
	30	3 27.3	.22	6.95	424	55	Ŏ	40.8	025	1.36	082
16	0	3 20 6	.21	6.73	411	56	0	39.3	025	1.31	079
	30	3 14.4	.20	6.51	.399	57	Ŏ	37.8	025	1.26	076
17	0	3 85	.19	6.31	.386	58	0	36.4	024	1.22	073
1	30	3 2-9	.18	6.12	·374	5 9	0	35∙0	024	1.17	070
10	^	0.57.0	.17	E.00	-362	60	Λ	33.6	.000	1.10	.00#
18	Ŏ	257.6	17	5.98			Ŏ	32.3	.023	1.12	067
19 20	0	2 47.7	16	5.61	·340 ·322	61	0	31.0	022	1.08	065
	Ŏ	2 38.7	15	5.31		62	Ŏ		022	1.04	.062
21	0	2 30.5	.13	5.04	305	63	0	29.7	021	.39	050
22 23	0	2 23.2	.13	4.79	290	64	Ŏ	28.4	.021	.95	.057
23	0	2 16.5	.11	4.57	.376	65	0	27.2	.020	.91	·055
24	0	0 10.1	·10	4.35	.264	66	0	25.9	.020	.04	.050
		2 10 1			252					-87	052
25 26	õ	2 4.2	.09	4.16		67	0	24.7	.020	-83	060
27	õ	1 58.8	-09	3.97	241	68	0	23.5	.020	.79	.047
	0	1 53.8	.08	3.81	230	69	0	22.4	· 0 20	.75	045
28	0	1 49-1	.08	3.65	219	70	0	21.2	020	.71	·043
29	0	1 44.7	.07	3.20	.209	71	0	19-9	∙020	.67	·040
30	0	1 40-5	.07	3.36	·201	72	0	18-8	.010	.63	-038
31	Ö	1 36-6	06	3.23	193	73	ŏ	17.7	.019	.59	
32		1 33-0	.06	3.11	186	74	ŏ	16.6	.018	56	036
33	ŏ	1 29.5	-06	2.99	179	75	Ö	15.5	.018		.033
	0		.05	2.88	173		0	14.4	.018	.52	.031
34	Ŏ					76			018	.48	029
35	0	1 23.0	·05	2.73	·167	77	0	13.4	·017	·45	.027
36	0	1 200	.05	2.68	·161	78	0	12.3	-017	-41	.005
36		1 17.1	05	2.58	155	79	ŏ	11.2		·41 ·38	025
	0		-05	2.49	1100	80	0	10.3	017		.023
38	0	1 14·4 1 11·8	.04	2.40	144	81	ŏ	9-2	017	34	.021
39	0	1 9.3	04	2.32	139	82	Ö	8.2	017	-31	018
40	0		04	2.24	134	83	Ö	7.1	.017	-27	.016
41	0	1 6-9	04	2 24	104	ಿ	U	[[71]	017	-24	·014
42	٥	1 4.6	.038	2.16	·130	84	0	6.1	-017	-20	·012
43		1 24	.036	2.09	125	85	ŏ	5.1	017	17	010
	0	1 0.3	034	2.03	120	86	ŏ	4.1	017	-14	.008
44	0	58.1	034	1.94	117	87	Ö	3.1		10	.006
45	0		033	1.88	112	88	Ö	20	017	-07	
46	0	56.1	.032	1.81	108	89	Ö	1.0	017	-03	.004
47	0	54-2	UJE	101	100	00	v	1.0	-017	טעד	.003
									<u> </u>		

900 TABLE X.

	nt of Re-	
Alt.	Dim. of semidi.	
50	25"	
6	19	
6 7 8	14	
	11	l
9	9	
10	8 7	
11	7	
12	6 5	
13	5	
14	4	
15	4	
16 18	3 3	
20	2	
30	l î l	
45	l i l	
10		

TABLE XI.

A			
Augmentation of the)'s semidiam.			
Alt.	Aug.		
00	0'		
5	1 1		
10	3		
15	4		
20 25	6 7 8		
25	7		
30	8		
35	9		
40	10		
45	11		
50	19		
56	13		
60 70	14		
70	15		
80	15		
90	16		

TABLE XIL

Lat	Horizontal Parallax.					
	54'	56'	58′	60′	62	
ô	0.0	0.0	0.0	0.0	0.0	
8	0.2	0.2	0.2	0.2	0.2	
16	0.8	0.8	0.9	0.9	0.9	
20		1.3	1.4	1.4	1.5	
24	1.8	1.9	1.9	2.0	2.0	
28	2.4	2.5	2.6	2.6	2.7	
33	3.0	3.1	3.3	3.4	3.5	
36	3.7	3.9	4.0	4.1	4.3	
40	4.5	4.6	4.8	5.0	5.1	
44	5.2	5.4	5.6	5.8	6.0	
48	6.0	6.2	6.3	6.6	6.8	
52	6.7	7.0	7.2	7.4	7.6	
56	7.4	7.7	8.0	8.2	8.5	
60	8-1	8.4	8.7	9.0	9.3	
64	8.7	9.1	9.4	9.7	10.0	
68	9.3	9.6	10.0	10.3	10-6	
72	9.8	10.1	10-4	10.8	11.2	
	10.2	10.6	10.9	11.3	11.7	
	10.7	11.1	11.5	11.9	12.0	
100	108	11.5	11.6	12.0	12.4	

Sun's par. in Alt.		
Alt.	Par.	
, 00	9"	
10	9	
20 30	8	
30	9°9 88 76 54 43 22	
40	7	
50	6	
55	5	
60	4	
65	4	
70	3	
75	2	
80	2	
85 90	1	
י 90 ו	0	

TABLE IX.